

## REPORT

## SUPERCONDUCTIVITY

# Spatial control of heavy-fermion superconductivity in $\text{CeIrIn}_5$

Maja D. Bachmann<sup>1,2\*</sup>, G. M. Ferguson<sup>3\*</sup>, Florian Theuss<sup>3</sup>, Tobias Meng<sup>4</sup>, Carsten Putzke<sup>1,5</sup>, Toni Helm<sup>1</sup>, K. R. Shirer<sup>1</sup>, You-Sheng Li<sup>1,2</sup>, K. A. Modic<sup>1</sup>, Michael Nicklas<sup>1</sup>, Markus König<sup>1</sup>, D. Low<sup>3</sup>, Sayak Ghosh<sup>3</sup>, Andrew P. Mackenzie<sup>1,2</sup>, Frank Arnold<sup>1</sup>, Elena Hassinger<sup>1,6</sup>, Ross D. McDonald<sup>7</sup>, Laurel E. Winter<sup>7</sup>, Eric D. Bauer<sup>7</sup>, Filip Ronning<sup>7</sup>, B. J. Ramshaw<sup>3</sup>, Katja C. Nowack<sup>3,8†‡</sup>, Philip J. W. Moll<sup>1,5†‡</sup>

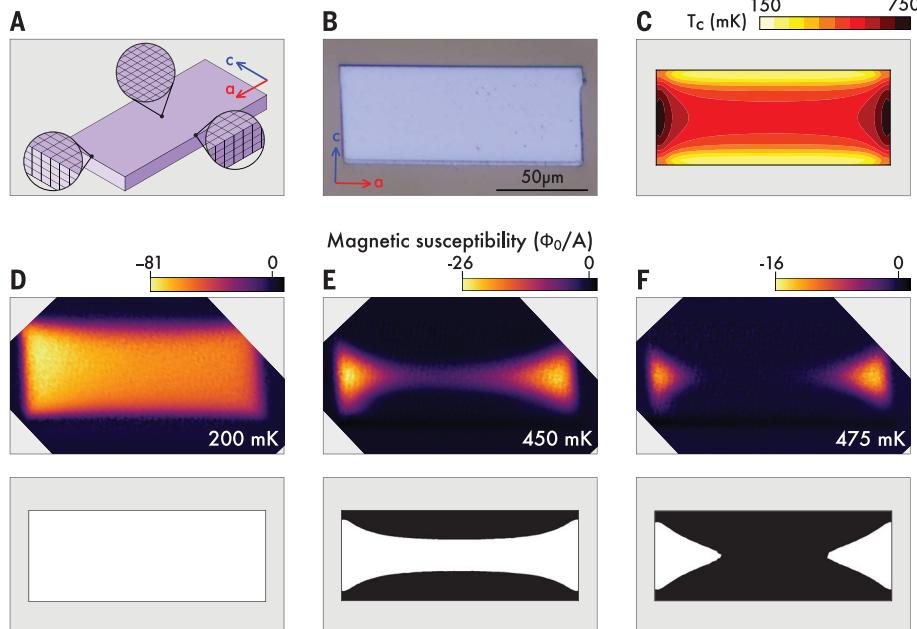
Although crystals of strongly correlated metals exhibit a diverse set of electronic ground states, few approaches exist for spatially modulating their properties. In this study, we demonstrate disorder-free control, on the micrometer scale, over the superconducting state in samples of the heavy-fermion superconductor  $\text{CeIrIn}_5$ . We pattern crystals by focused ion beam milling to tailor the boundary conditions for the elastic deformation upon thermal contraction during cooling. The resulting nonuniform strain fields induce complex patterns of superconductivity, owing to the strong dependence of the transition temperature on the strength and direction of strain. These results showcase a generic approach to manipulating electronic order on micrometer length scales in strongly correlated matter without compromising the cleanliness, stoichiometry, or mean free path.

The electronic ground state of heavy fermions sensitively depends on the coupling between a localized state and an itinerant electronic system. As the coupling strength is tuned, metallic, superconducting, or magnetically ordered phases are induced, yielding the rich phase diagrams typical for materials of this class. This tunability could be exploited for device-based applications if the electronic order can be locally controlled within a crystalline sample: Metallic, magnetic, or superconducting regions could be induced within a single crystal by precise spatial control over the tuning parameter. Strain is a particularly powerful way to achieve this goal: It introduces no disorder, and its independent components offer multiple degrees of freedom to couple to electronic order. Most commonly, uniform uniaxial strain (1) or biaxial strain (2) is applied. In this work, we demonstrate micrometer-scale control over the superconducting order in stoichiometric and ultraclean  $\text{CeIrIn}_5$  by inducing a nonuniform

tailored strain field in microstructured single-crystal devices. Our experimental approach exploits strain induced by differential thermal contraction between the sample and the substrate, as well as our submicrometer control over the shape of the sample. The tetragonal

heavy-fermion metal  $\text{CeIrIn}_5$  exhibits material parameters that are ideal for establishing spatial control of a correlated state [Sommerfeld coefficient  $\gamma \sim 720 \text{ mJ mol}^{-1} \text{ K}^{-2}$  (3), effective mass  $m^* \sim 30m_e$ , where  $m_e$  is the mass of an electron (4)]. The superconducting transition temperature,  $T_c$ , of this material is highly sensitive to strain, owing to the strong dependence of Ce 4f hybridization on the Ce-Ce interatomic distance. Straining the sample along the  $a$  direction increases the bulk superconducting transition temperature ( $T_c = 400 \text{ mK}$ ) by  $56 \text{ mK/kbar} \sim 14\% T_c/\text{kbar}$ , whereas compression along the  $c$  direction decreases it at the rate of  $-66 \text{ mK/kbar} \sim -16.5\% T_c/\text{kbar}$  (5, 6). Although uniaxial strain strongly alters  $T_c$ , the almost equal but opposite effects of  $a$ - and  $c$ -direction strain lead to an overall weak change of  $T_c$  under hydrostatic pressure ( $10 \text{ mK/kbar} \sim 2.5\% T_c/\text{kbar}$ ) (7). For a crystal subjected to a nonuniform strain field, complex patches of superconductivity are expected to appear within the heavy Fermi liquid.

Figure 1 illustrates nonuniform superconductivity for the simple case of a rectangular slab also referred to as a lamella. The lamella ( $150 \mu\text{m}$  by  $30 \mu\text{m}$  by  $2 \mu\text{m}$ ) was carved from a macroscopic crystal by using focused ion beam (FIB) machining [for fabrication details, see (8–10)] and was joined to the sapphire substrate with a thin layer of epoxy (approximately



**Fig. 1. The superconducting transition in a lamella under biaxial strain.** (A) Sketch of the distortion of a thin lamella of  $\text{CeIrIn}_5$  coupled to sapphire at low temperatures. (B) Optical image of a  $2\text{-}\mu\text{m}$ -thick lamella cut by FIB machining in the  $(a, c)$  plane. (C) Finite element simulation of the  $T_c$  map across the sample, arising from the strain profile and strain dependence of  $T_c$  (10). (D to F) (Top) Local susceptibility images at three representative temperatures. A negative diamagnetic susceptibility indicates superconducting regions of the sample. The susceptibility is measured in units of superconducting magnetic flux quanta ( $\Phi_0$ ) applied to the field coil. (Bottom) Superconducting regions (white) calculated from the strain profile in the device, corresponding to constant temperature contours of the  $T_c$  map in (C).

<sup>1</sup>Max Planck Institute for Chemical Physics of Solids, D-01187 Dresden, Germany. <sup>2</sup>School of Physics and Astronomy, University of St. Andrews, St. Andrews KY16 9SS, UK.

<sup>3</sup>Laboratory of Atomic and Solid State Physics, Cornell University, Ithaca, NY 14853, USA. <sup>4</sup>Institute for Theoretical Physics, Technical University Dresden, D-01062 Dresden, Germany. <sup>5</sup>Institute of Material Science and Engineering, École Polytechnique Fédérale de Lausanne (EPFL), 1015 Lausanne, Switzerland. <sup>6</sup>Physik-Department, Technische Universität München, Garching, D-85748 Germany. <sup>7</sup>Los Alamos National Laboratory, Los Alamos, NM 87545, USA. <sup>8</sup>Kavli Institute at Cornell for Nanoscale Science, Cornell University, Ithaca, NY 14853, USA.

\*These authors contributed equally to this work.

†These authors contributed equally to this work.

‡Corresponding author. Email: philip.moll@epfl.ch (P.J.W.M.); kcn34@cornell.edu (K.C.N.)

a few hundred nanometers thick). This epoxy is substantially softer than the crystalline substrate and the sample; finite element modeling corroborates the intuitive assumption that the differential thermal contraction transmitted through the epoxy is largely independent of the exact details of the glue layer, such as its thickness or elastic moduli [see (10) for details]. The crystallographic *c* direction is aligned with the short side of the lamella and the *a* direction with the long side. The use of sapphire cut along the (0001) surface ensures isotropic thermal contraction of the substrate. Whereas sapphire is known for its low thermal contraction, CeIrIn<sub>5</sub> contracts strongly upon cooling, as is typical of many Ce-based compounds (11). As a result, the sample is under tensile strain at low temperature.

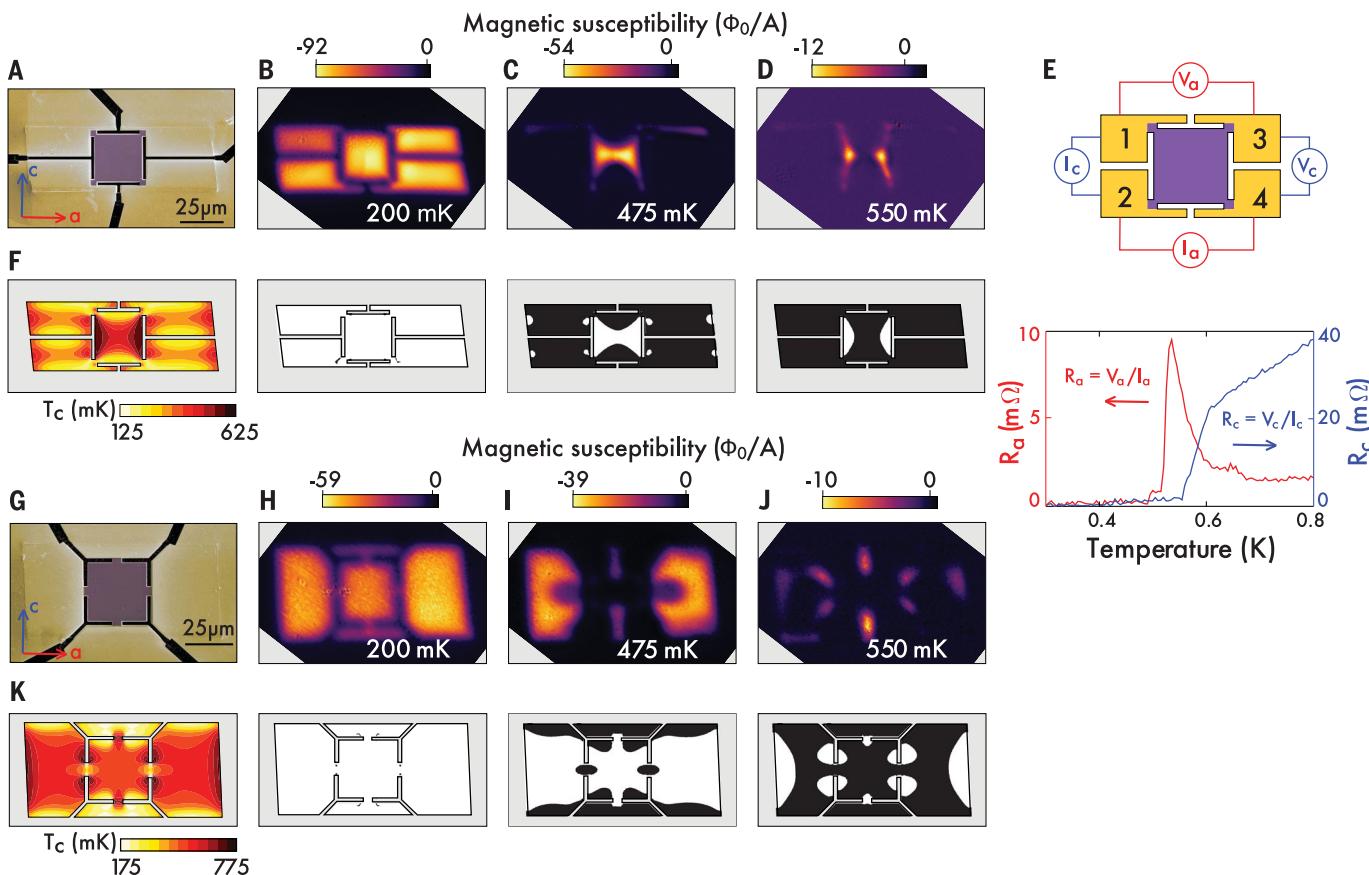
To study the superconducting transition in the lamella, we use scanning superconducting quantum interference device (SQUID) micro-

copy (SSM) to image the diamagnetic response of the sample with micrometer-scale resolution. To detect superconductivity, we apply a local magnetic field by sourcing a current through a ~6-μm field coil integrated on the SQUID chip. The ~1.5-μm SQUID pickup loop detects the local magnetic susceptibility measured in magnetic flux per unit current in the field coil [see (10) for details]. Superconducting regions of the sample exhibit a strong diamagnetic response, which enables us to distinguish them from metallic and insulating regions.

Susceptibility images as a function of temperature (top images in Fig. 1, D to F) reveal that superconductivity first emerges at the short edges while most of the lamella remains metallic. As the temperature is lowered, larger fractions of the lamella become superconducting, thus leading to the growth of triangular superconducting patches protruding into the

lamella, which eventually join in the center (Fig. 1E). At even lower temperatures, the order parameter remains suppressed on the long edge. The observation of superconductivity at the edge of the sample before the interior is unexpected. Usually, for a thin superconducting slab cooled in Earth's magnetic field, the demagnetization factor at the sample edges initially favors the appearance of superconductivity in the center of the sample (12).

Before analyzing the spatial pattern in the images, we estimate whether strain caused by differential thermal contraction combined with the strain sensitivity of  $T_c$  in CeIrIn<sub>5</sub> can cause the observed variations in  $T_c$  of several hundred millikelvin. When cooled to cryogenic temperatures, CeIrIn<sub>5</sub> and sapphire contract by ~0.3 and ~0.08%, respectively. Given this mismatch, we expect strain on the order of 0.1% to exist within the CeIrIn<sub>5</sub> crystal at low temperature. Using a typical elastic modulus



**Fig. 2. Spatial control over correlations.** (A) Scanning electron microscopy (SEM) image of device 1. The lamella is FIB-cut in the (*a*, *c*) plane and contacted by evaporated Au (yellow). The center square of the device is 25 μm by 25 μm by 3 μm, held by contacts in the corners. (B to D) (Top) Local susceptibility images at three representative temperatures illustrate the temperature evolution of the spatially modulated superconducting state. (Bottom) Calculated superconducting patterns (10). (E) Montgomery transport measurement upon cooling of device 1. As the first superconducting regions appear on the sides along the *c* direction (D), the *c*-direction resistance  $R_c = V_c/I_c$  vanishes and the *a*-direction

resistance  $R_a = V_a/I_a$  experiences a resistance spike, caused by a sudden current redistribution.  $I$ , current;  $V$ , voltage. At lower temperatures, these regions touch (C), leading to zero resistance across all contacts. (F)  $T_c$  map for device 1 from finite element calculations (10). (G) SEM image of device 2. The fabrication of device 2 was as similar as possible to that of device 1, but with the constrictions connecting at the middle of each side of the square, not the corners [compare with (A)]. (H to K) The same as in (B) to (D) and (F), but for device 2. A completely different superconducting pattern develops, as expected from the difference in position of the contacts.

of 150 GPa, this is equivalent to a uniaxial pressure of  $\sim 1.5$  kbar, which changes  $T_c$  by  $\sim 100$  mK (5). Hence, both the uniaxial pressure studies and the image series presented here are consistent with  $\sim 0.1\%$  strain generating  $\sim 100$  mK variation in  $T_c$ .

To understand the patterns of superconductivity, we perform finite element method simulations of the device's strain field, which is caused by the difference in the thermal contraction between CeIrIn<sub>5</sub> and sapphire (10). We then compute the local transition temper-

ature,  $T_c$ , from the strain field using

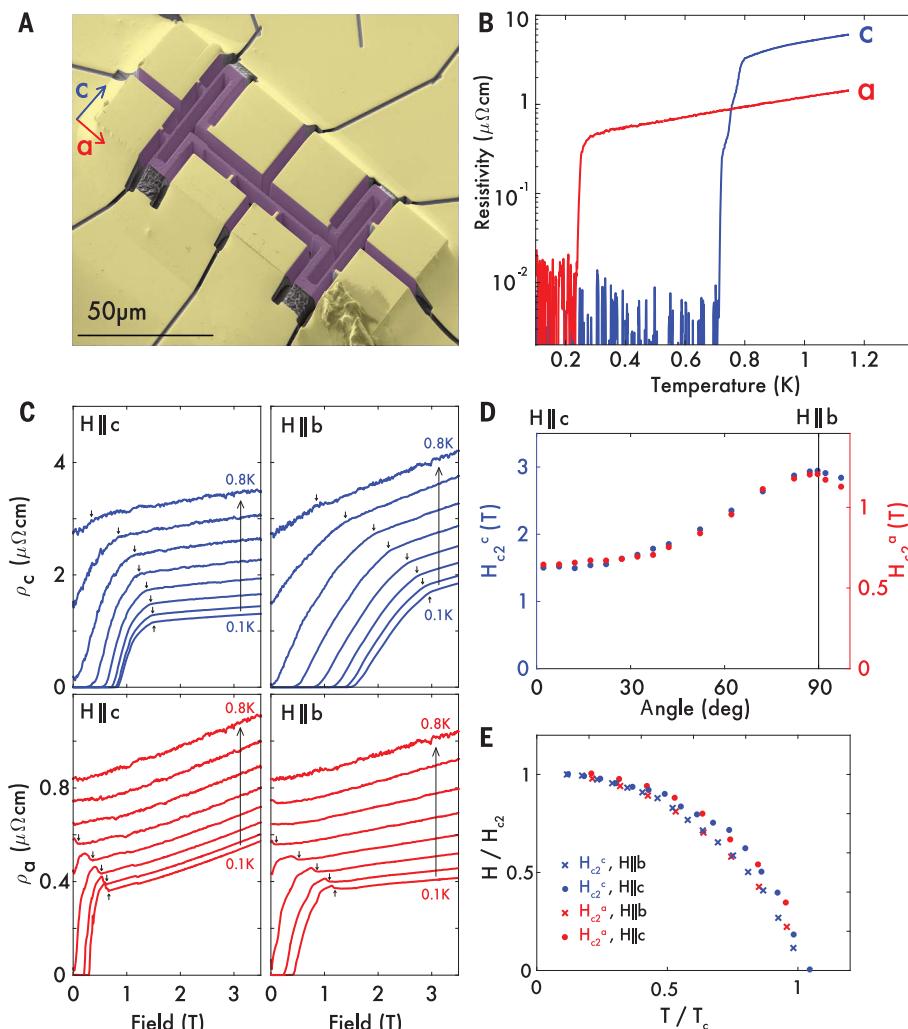
$$T_c = T_{c0} + \frac{\delta T_c}{\delta \varepsilon_a} (\varepsilon_a + \varepsilon_b) + \frac{\delta T_c}{\delta \varepsilon_c} \varepsilon_c$$

for each point on the grid, resulting in a spatial  $T_c$  map (Fig. 1C). Here,  $\varepsilon_i$  with  $i = a, b, c$  are the diagonal elements of the strain tensor along the corresponding crystallographic directions. We estimate  $\frac{\delta T_c}{\delta \varepsilon_a} = -57$  K and  $\frac{\delta T_c}{\delta \varepsilon_c} = 66$  K from reported bulk measurements of  $T_c$  as a function of uniaxial pressure, as well as our measured elastic moduli (5, 6, 10). We

generate binary images from this map, marking superconducting and metallic regions at each temperature that can be directly compared to our susceptibility images (Fig. 1, D to F). We find detailed agreement between the spatial patterns of superconducting regions observed in the SSM images at various temperatures and the pattern predicted by the simulations, which are free of fitting parameters. This agreement indicates that our modeling captures both the physical origin of the complex superconducting patches and the essence of the  $T_c$  modulation in the sample. Note that shear strains are not relevant to determine  $T_c$  for two reasons: (i) The shear strains are an order of magnitude smaller than the uniaxial strains in the lamella, and (ii) the symmetry of the superconducting order parameter in CeIrIn<sub>5</sub> requires that shear strain couples to  $T_c$  at higher order than the uniaxial strains [see (10) for details]. Comparison of the data and simulations shows that including these higher-order couplings is not required to model the experimental results.

Next, we show that the induced strain field and the shape of the superconducting regions can be tailored by using FIB micromachining. To define the strain field in the devices, additional trenches were cut through the lamella down to the substrate, changing the boundary conditions for the elastic equations. In both devices shown in Fig. 2, the trenches define a square in the  $(a, c)$  plane. In device 1, the square is anchored by four constrictions, one in each corner (Fig. 2A). In device 2, the constrictions connect to the center of each side of the square (Fig. 2G). Under biaxial tension, each of the contact pads is pulled outward, subjecting the square to nonuniform strain.

Device 1 is designed to measure anisotropic resistances in the plane by passing current through any pair of neighboring contacts while measuring voltage across the remaining pair (13, 14). In this device, the simulated  $T_c$  map predicts a pattern of superconductivity first developing on the edges aligned with the  $c$  direction as the device is cooled (Fig. 2F). These regions extend toward the center upon lowering the temperature, eventually connecting in the middle of the device. Such patterns are evident in the SSM images (Fig. 2, B to D) and lead to three distinct regimes for transport through device 1: (i) the normal state in which all contacts are separated by metallic regions, (ii) a state in which only the contact pairs along the  $c$  direction are connected by superconducting regions, and (iii) a state in which all contacts are connected by a single superconducting region. As a result, when current is sourced between contacts along the  $c$  direction (1 and 2), a transition to zero voltage, signaling superconductivity at a relatively high temperature  $T_c^*$ , is



**Fig. 3. Smaller structures.** (A) SEM image of device 3. The device consists of long bars with dimensions  $1.8 \mu\text{m} \times 8 \mu\text{m} \times 22 \mu\text{m}$ . Two bars are oriented along the  $c$  direction and one along the  $a$  direction. (B) Resistivity as a function of temperature for device 3. Strain suppresses  $T_c$  along the bar aligned with the crystallographic  $a$  axis and enhances  $T_c$  along bars aligned with the  $c$  axis. (C) Temperature-dependent magnetoresistance along the  $a$  and  $c$  directions in CeIrIn<sub>5</sub> for different field orientations. All measurements were taken in a full Lorentz force configuration except  $\rho_c$  for  $H \parallel c$ , which is naturally longitudinal ( $\rho$ , resistivity,  $H$ , magnetic field). (D) Angle dependence of the critical fields defined as the points where deviation from the normal magnetoresistance occurs [arrows in (C)], for both current configurations. The data collapse onto a single curve by scaling (compare the two vertical axes). (E) Temperature dependence of the critical fields for all four current and field configurations. The curves for each field configuration collapse when scaled by the respective values of  $H_{c2}(0 \text{ K})$  and  $T_c$ , using the experimental values for in-plane transport ( $T_c \sim 0.45 \text{ K}$ ,  $H_{c2}^a \parallel b(0 \text{ K}) \sim 1.2T$ ,  $H_{c2}^a \parallel c(0 \text{ K}) \sim 0.65T$ ) and along the  $c$  direction ( $T_c^* \sim 0.8 \text{ K}$ ,  $H_{c2}^{*,c} \parallel b(0 \text{ K}) \sim 2.95T$ ,  $H_{c2}^{*,c} \parallel c(0 \text{ K}) \sim 1.5T$ ).

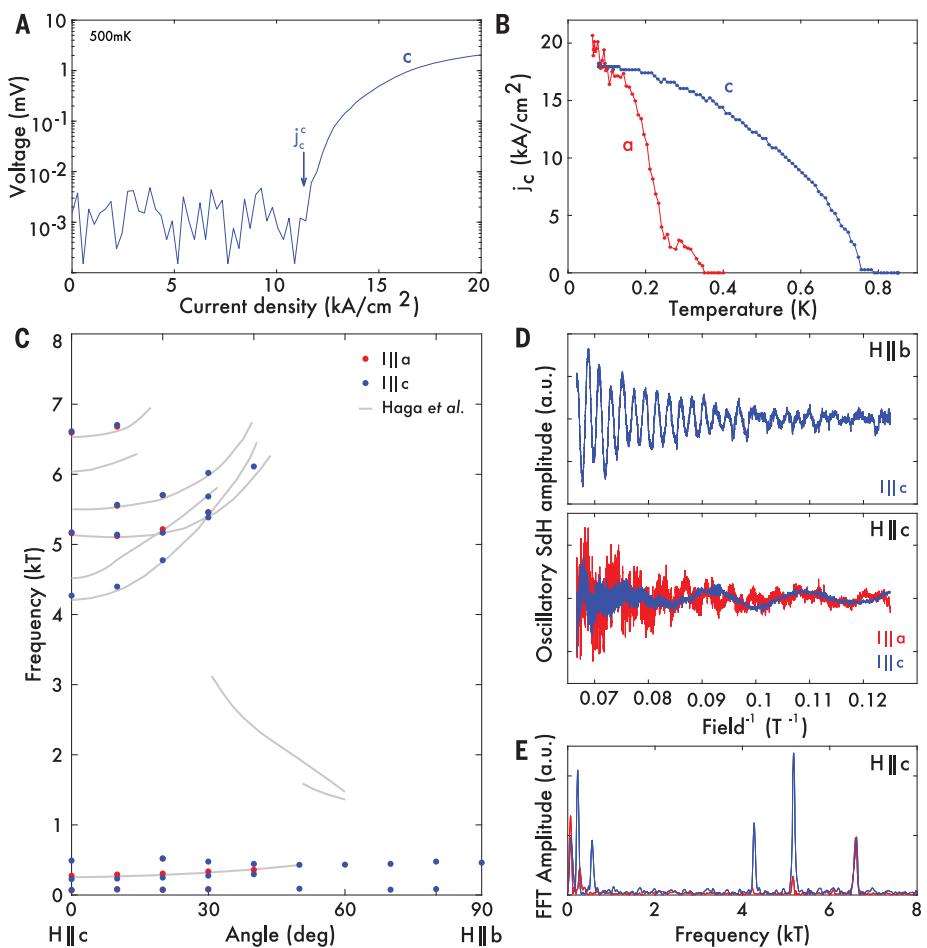
observed (Fig. 2E, blue trace). For currents sourced between contacts along the *a* direction (labeled 2 and 4), we observe a sharp upturn in resistance along *a*,  $R_a$ , as the *c*-direction resistance,  $R_c$ , goes to zero (Fig. 2E). The elongated superconducting regions identified in Fig. 2D cause the current from contacts 2 to 4 to distribute evenly over the width of the device, leading to a larger current to flow at the voltage probes (labeled 1 and 3). Eventually, a second transition to a zero-resistance state occurs when all contacts are connected by a single superconducting region. The electrical response and the direct imaging of this device consistently capture the key concepts of the microscopic control over correlations: Two directed superconducting paths form in a chemically homogeneous metal, arising from the imprinted strain profile.

In contrast to those of device 1, the edges in device 2 parallel to the *a* axis superconduct well before the central region of the device (Fig. 2, G to K). As with device 1, we find that simulations of the strain profile in the device reproduce the structure of the superconducting transition in detail. The contrast between the two image series indicates that the structure in the images is determined by the interplay between the intrinsic strain sensitivity of the material and the strain field imposed by the FIB-defined features.

In device 2, we observe a pronounced suppression and enhancement of  $T_c$  in the *a*- and *c*-aligned constrictions, respectively. The strain in the constrictions is enhanced because the contact pads on one side and the square on the other side exert forces on the constrictions that point outward. This observation suggests a strategy to design devices that exhibit a strong modulation of  $T_c$  and to generate confined regions of suppressed superconductivity.

Smaller devices exhibit an even more pronounced dependence of the transport  $T_c$  on their geometry than larger devices. Device 3 features three series-connected straight beams with dimensions 22  $\mu\text{m}$  by 1.8  $\mu\text{m}$  by 8  $\mu\text{m}$ , with two beams aligned with the *c* direction and one with the *a* direction (Fig. 3A). These fine structures cannot be resolved in detail with SSM. In transport, the transition temperature for the *c*-aligned beam  $T_c^c \sim 700$  mK is higher than the bulk  $T_c$ , whereas the transition temperatures for the *a*-aligned beams  $T_c^a \sim 200$  mK are considerably lower than the bulk  $T_c$ . Additional small structures show equally or even more pronounced variations of  $T_c$  (10). Therefore, a modulation of the transition temperature by more than a factor of 4 within a single crystal can be realized within our fabrication approach.

To exploit strain tuning of the superconducting order for future device-based experiments, the superconducting state must remain



**Fig. 4. Robust superconductivity coexists with quantum oscillations.** (A) Current–voltage characteristic along the *c* direction measured on device 3 (see Fig. 3A). The onset of measurable voltage above the experimental noise level (arrow) was used to define  $j_c^c$  and  $j_c^a$ . (B) Critical current along both directions. A robust, high- $j_c$  state is observed along the *c* direction, whereas the *a* direction is in a metallic state. (C) Angle dependence of Shubnikov–de Haas (SdH) oscillations at 80 mK measured in device 3 (points) overlaid on de Haas–van Alphen oscillations measured on bulk single crystals (gray lines) (4). (D) SdH oscillations in the microstructure for  $H||b$  (top) and  $H||c$  (bottom). a.u., arbitrary units. (E) Fast Fourier transform (FFT) spectrum for the oscillations in (D).

robust after device fabrication. To estimate the critical current of each beam, we apply high currents to device 3 (Fig. 4, A and B). The current is increased until an observable voltage signals the breakdown of the zero-resistance state. To minimize self-heating, 83- $\mu\text{s}$  rectangular current pulses are applied to the sample, with a cooldown time between pulses of 100 ms. Because the critical current decreases monotonically with increasing temperature, the obtained values represent a lower bound of their magnitude in the absence of heating. Figure 4A shows a typical current–voltage characteristic of the *c*-aligned beam at 500 mK, well above the bulk  $T_c$ . A robust zero-resistance state is detected up to a critical current density of  $\sim 12.5$   $\text{kA cm}^{-2}$ . Upon cooling, the critical current density increases to  $j_c^c(0 \text{ K}) \sim 18$   $\text{kA cm}^{-2}$  (Fig. 4B). This high critical current is typical for bulk heavy-fermion

superconductors [ $\sim 3.8$   $\text{kA cm}^{-2}$  for  $\text{UPt}_3$  (15),  $\sim 24$   $\text{kA cm}^{-2}$  for  $\text{URu}_2\text{Si}_2$  (15), and  $\sim 1$  to  $5$   $\text{kA cm}^{-2}$  for  $\text{CeCu}_2\text{Si}_2$  (16)], strongly supporting a scenario of robust, bulk-like superconductivity over the formation of sparse superconducting filaments under strain.

Incidentally, our observations answer an open question about the origin of the commonly observed discrepancy between thermodynamic and resistive measurements of  $T_c$  in  $\text{CeIrIn}_5$ . Bulk crystals display a transition to a zero-resistance state well above  $T_c$ , starting as high as  $T_c^* \sim 1.2\text{K}$  (17–19) and dependent on the details of the sample. Our results microscopically confirm proposals that strain fields around defects induce this 1 K phase (20–22). In particular, the upper critical fields  $H_{c2}$  of the strain-induced superconductivity in the microdevices can be directly scaled onto the bulk values (Fig. 3, C to E). This critical field

scaling was experimentally identified early in the study of macroscopic crystals as a hallmark signature of the 1 K phase (3). On the basis of these observations, we propose that the 1 K phase is a strain effect arising from crystal handling and wire sawing. To directly test this hypothesis, we prepared macroscopic samples by wire saw cutting. Although all samples initially had a  $T_c > 1$  K, the resistive signatures of this 1 K phase are completely removed by short surface etching in HCl, after which the resistive transition coincides with thermodynamic probes at  $T_c \sim 400$  mK (10). This result demonstrates the absence of defect-strained superconducting patches in single crystals of CeIrIn<sub>5</sub> and establishes the discrepancy between thermodynamic and resistive measurements of  $T_c$  in CeIrIn<sub>5</sub> as an effect of surface strain.

Here, we report a strategy to spatially modulate superconductivity within a clean electronic system that is induced by strong, nontrivial strain patterns. Spatial gradients of  $T_c$  have been generated by other methods—for example, by modulating the chemical potential across the sample by gradient doping with molecular-beam epitaxy techniques (23). In this method, variations in the local charge carrier density modify the local transition temperature. In the stoichiometric CeIrIn<sub>5</sub> microstructures that we studied, the charge carrier density is uniform, as evidenced by unperturbed quantum oscillations in device 3 (Fig. 4, C to E). These quantum oscillations quantitatively match the angle dependence of previously reported de Haas-van Alphen oscillations (4) measured on macroscopic crystals and indicate that the Fermi surface shape remains unchanged by the weak strain field. In particular, the large, heavy orbits and their fine structure are readily observed, which is usually very difficult in transport. This observation is incompatible with the presence of strong charge carrier density changes across the sample, which would lead to spatial variations in the Fermi surface cross sections and subsequently suppress quantum oscillations by phase smearing.

At the same time, the strain fields in device 3 are strong enough to modulate  $T_c$  by almost a factor of 4, from 200 to 780 mK. This finding suggests that the strain field spatially modulates the degree of 4f hybridization across the device and thereby also affects  $T_c$ . This mechanism, which is initially surprising, is compatible with experimental observations in the related compound CeRhIn<sub>5</sub> in which hydrostatic pressure suppresses antiferromagnetism and eventually induces superconduc-

tivity. Despite the clear changes in the 4f magnetism and the spin fluctuation spectrum, the quantum oscillation frequencies remain unchanged in the entire pressure range up to the quantum critical point (24). However, the 4f hybridization increases, as evidenced by a quasiparticle effective mass that grows in response to applied pressure. This result strongly suggests that the hybridization with the 4f electrons varies without changes in the overall volume of the Fermi surface. Here we propose that the same microscopic physics underlies the spatial modulation of  $T_c$  in CeIrIn<sub>5</sub> microstructures.

In general, strongly correlated materials exhibit a pronounced sensitivity to perturbations, owing to the small energy scales defining their physics. The strain accessible by our fabrication approach is sufficient to substantially alter the electronic properties of these materials without introducing chemical disorder. Unlike chemical approaches to tune correlations, the FIB provides micrometer-scale control over both the direction and magnitude of the induced strain field. We expect that the approach demonstrated here will enable spatial control of a wide range of broken symmetry states in strongly correlated systems. We envision clean interfaces between regions with different electronic order within a sample generated by a spatially modulated strain field—e.g., by generating superconducting regions in structures made from antiferromagnetic CeRhIn<sub>5</sub> (24). Further, this approach is immediately compatible with any material that can be patterned using a FIB. Notably, although we focus on devices aligned along specific crystal axes, devices can be oriented along any direction to generate strain patterns of any desired symmetry. Strain engineering may offer an alternative way to fabricate superconducting circuitry within a metallic layer without any physical junctions, providing a route to fabricating superconductor/normal metal/superconductor Josephson junctions within a single crystal.

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## SUPPLEMENTARY MATERIALS

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Materials and Methods  
Supplementary Text  
Figs. S1 to S13  
Tables S1 and S2  
References (26–37)

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