

## Corrections

### I. Calculation of the stress intensity factor in Griffith's and penny shape cracks

1. Using the principle of superposition of elastic solutions, the stress intensity factor of a through crack of length 2a (aka Griffith's crack) that undergoes a symmetric stress distribution  $\sigma(x)$  where x is the distance to the y axis is given by:

$$K = 2 \sqrt{\frac{a}{\pi}} \int_0^a \frac{\sigma(x)}{\sqrt{a^2 - x^2}} dx$$

With the help of this result, calculate the stress intensity factor of a through crack of length 2a in an infinite body under a remote stress  $\sigma$ .

$$\begin{aligned} K_I &= 2 \frac{\sqrt{a}}{\sqrt{\pi}} \int_0^a \frac{\sigma(x) dx}{\sqrt{a^2 - x^2}} = 2 \frac{\sigma \sqrt{a}}{\sqrt{\pi}} \int_0^a \frac{dx}{\sqrt{a^2 - x^2}} = 2 \frac{\sigma \sqrt{a}}{\sqrt{\pi}} \int_0^1 \frac{adu}{a\sqrt{1-u^2}} \text{ posing } u = x/a \\ K_I &= 2 \frac{\sigma \sqrt{a}}{\sqrt{\pi}} \int_0^1 \frac{du}{\sqrt{1-u^2}} = 2 \frac{\sigma \sqrt{a}}{\sqrt{\pi}} \int_0^{\pi/2} \frac{\cos \theta d\theta}{\sqrt{1-\cos^2 \theta}} = 2 \frac{\sigma \sqrt{a}}{\sqrt{\pi}} \int_0^{\pi/2} \frac{\cos \theta d\theta}{\sqrt{1-\sin^2 \theta}} = 2 \frac{\sigma \sqrt{a}}{\sqrt{\pi}} \int_0^{\pi/2} d\theta = 2 \frac{\sigma \sqrt{a}}{\sqrt{\pi}} \frac{\pi}{2} = \sigma \sqrt{\pi a} \\ \text{posing } u &= \sin \theta \end{aligned}$$

2. In axisymmetric conditions, cylindrical coordinates are used with r, the distance to the symmetry axis and the stress intensity factor becomes:

$$K = \frac{2}{\sqrt{\pi a}} \int_0^a \frac{r \sigma(r)}{\sqrt{a^2 - r^2}} dr$$

Show that the stress intensity factor of a penny shape crack of length 2a in an infinite body under a remote stress  $\sigma$  writes  $K_I = \frac{2\sigma}{\pi} \sqrt{\pi a}$ .

$$\begin{aligned} K_I &= \frac{2}{\sqrt{a\pi}} \int_0^a \frac{r \sigma(r) dr}{\sqrt{a^2 - r^2}} = \frac{\sigma}{\sqrt{a\pi}} \int_0^a \frac{2r dr}{\sqrt{a^2 - r^2}} = \frac{2\sigma}{\sqrt{a\pi}} \left[ -\sqrt{a^2 - r^2} \right]_0^a \\ K_I &= \frac{2\sigma}{\sqrt{a\pi}} (0 + a) = \frac{2\sigma a}{\sqrt{a\pi}} = \frac{2\sigma \sqrt{a}}{\sqrt{\pi}} = \frac{2\sigma \sqrt{\pi a}}{\pi} \end{aligned}$$

### 2. Fatigue lifetime predictions

1.- Derive an expression for the number of stress cycles required to grow a semi-circular surface crack in a semi-infinite plate from an initial radius  $a_0$  of 4 mm to a final size  $a_f$ , assuming the Paris equation describes the growth rate with an exponent equal to 4. Assume that the crack maintains its semi-circular shape, and that the stress amplitude  $\Delta\sigma$  is constant.

For an elliptical crack,  $K_I$  writes with  $C = 1.12$  for short cracks:

$$K_I = C \frac{\sigma \sqrt{\pi a}}{\frac{3}{8} \pi + \frac{a^2}{8c^2} \pi} \left( \sin^2 \varphi + \frac{a^2}{c^2} \cos^2 \varphi \right)^{1/4}$$

**Answer:**

$$\begin{aligned}
 K_I &= 2.24\sigma\sqrt{\frac{a}{\pi}} \\
 \Delta K &= 2.24\Delta\sigma\sqrt{\frac{a}{\pi}} \\
 \frac{da}{dN} &= C\Delta K^m = C\left(2.24\Delta\sigma\sqrt{\frac{a}{\pi}}\right)^m = C\left(\frac{2.24\Delta\sigma}{\sqrt{\pi}}\right)^m a^{m/2} \equiv ka^{m/2} \\
 a^{-m/2} da &= kdN \\
 \int_{a_0}^a \frac{a^{1-m/2}}{1-m/2} da &= kN \\
 N &= \frac{1}{C} \left( \frac{2.24\Delta\sigma}{\sqrt{\pi}} \right)^{-m} \frac{a^{1-m/2} - a_0^{1-m/2}}{1-m/2}
 \end{aligned}$$

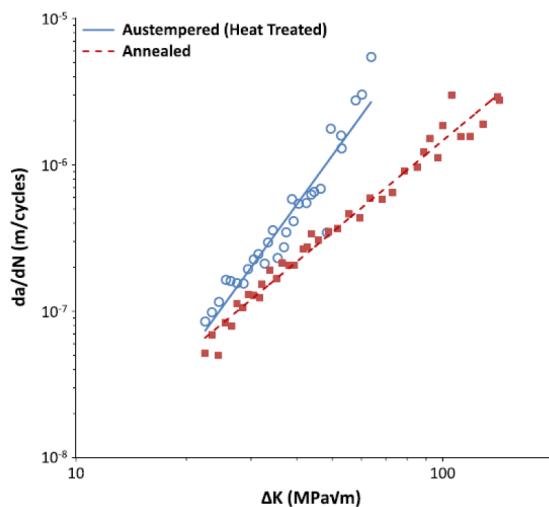
2.- If it takes 1000 cycles for the crack length to increase from 2 to 2.5 mm, how many cycles does it take for the crack to advance from 2 to 4 mm if the Paris exponent,  $m$ , is equal to 4?

*For a fixed stress amplitude,*

$$\begin{aligned}
 N &= A \left( a^{1-\frac{m}{2}} - a_0^{1-\frac{m}{2}} \right), \text{ where } A \text{ is a constant;} \\
 1000 &= A \left( \frac{1}{2.5} - \frac{1}{2} \right) = -0.1A \Rightarrow A = -10'000; \\
 N(4[\text{mm}]) &= -10'000 \times \left( \frac{1}{4} - \frac{1}{2} \right) = \frac{10'000}{4} = 2'500 \text{ cycles}
 \end{aligned}$$

### 3. Dynamic fatigue crack growth under load-control

The figure below shows fatigue data from (i) cold-rolled and annealed and (ii) austempered compact tension (CT) specimens of a high carbon steel with  $a/W = 0.3$ ,  $W = 50.8$  mm and  $B = 4$  mm, tested under load control, that is, with fixed values of the maximum and minimum load during each cycle.



*Comparison of the dynamic fatigue crack growth behaviour of annealed and austempered compact tension (CT) specimens of AISI 4140 steel tested at 5 Hz under load control, with  $R = 0.1$  and a 2 mm long starter crack (V. Ramasagara Nagarajan, S.K. Putatunda, International Journal of Fatigue 62 (2014) 236–248.)*

1.- Estimate the Paris law constants for the two data sets in the figure.

You can get the Paris law constants from the slope (m) and intercept of a linear fit to the data on this log-log plot with  $\Delta K = 1$  (i.e.  $\log \Delta K = 0$ ). The authors of the paper the data came from give the following values:

Material condition	C	m
Batch A - Cold rolled and annealed	$1 \times 10^{-10}$	2.08
Batch B - Heat treated (austempered)	$2 \times 10^{-12}$	3.45

2.- What are the initial values of  $K_{\max}$  and  $K_{\min}$  noticing that crack growth starts roughly at  $\Delta K = 20 \text{ MPa} \cdot \text{m}^{1/2}$ .

Answer:

$$\left. \begin{aligned} \frac{K_{\min}}{K_{\max}} &= 0.1 \\ K_{\max} - K_{\min} &= 20 \text{ MPa} \cdot \text{m}^{1/2} \\ 0.9K_{\max} &= 20 \text{ MPa} \cdot \text{m}^{1/2} \\ K_{\max} &= 22.2 \text{ MPa} \cdot \text{m}^{1/2} \\ K_{\min} &= 2.22 \text{ MPa} \cdot \text{m}^{1/2} \end{aligned} \right\}$$

3.- What is the maximum load during each loading cycle? The stress intensity factor  $K_{\max}$  of a CT specimen loaded under  $P_{\max}$  writes:

$$K_{\max} = \frac{P_{\max}}{BW^{1/2}} f\left(\frac{a}{W}\right)$$

$$f\left(\frac{a}{W}\right) = \frac{\left(2 + \frac{a}{W}\right)}{\left(1 - \frac{a}{W}\right)^{3/2}} \left[ 0.886 + 4.64\left(\frac{a}{W}\right) - 13.32\left(\frac{a}{W}\right)^2 + 14.72\left(\frac{a}{W}\right)^3 - 5.6\left(\frac{a}{W}\right)^4 \right]$$

Answer:

$$K_{\max} = \frac{P_{\max}}{BW^{1/2}} f\left(\frac{a}{W}\right)$$

$$f\left(\frac{a}{W}\right) = \frac{\left(2 + \frac{a}{W}\right)}{\left(1 - \frac{a}{W}\right)^{3/2}} \left[ 0.886 + 4.64\left(\frac{a}{W}\right) - 13.32\left(\frac{a}{W}\right)^2 + 14.72\left(\frac{a}{W}\right)^3 - 5.6\left(\frac{a}{W}\right)^4 \right]$$

$$f(0.3) = \frac{(2 + 0.3)}{(1 - 0.3)^{3/2}} \left[ 0.886 + 4.64(0.3) - 13.32(0.3)^2 + 14.72(0.3)^3 - 5.6(0.3)^4 \right] = 5.62$$

$$\frac{BW^{1/2} K_{\max}}{f\left(\frac{a}{W}\right)} = P_{\max} = \frac{4 \times 10^{-3} \times \sqrt{50.8 \times 10^{-3}} \times 22.2 \times 10^6}{5.62} = 3.56 \text{ kN}$$

3.- If both specimens have the same static  $K_c$ , which specimen is likely to fail first?

$K_{\max}$  depends on the crack length and the magnitude of the maximum stress. In this kind of experiment the stress amplitude is constant, so  $K_{\max}$  depends only on the crack length. The crack length increases more rapidly with the number of cycles for the austempered specimen (blue data points in the figure).  $K_{\max}$  will therefore reach  $K_c$  sooner, i.e. after fewer cycles, in the austempered specimen.