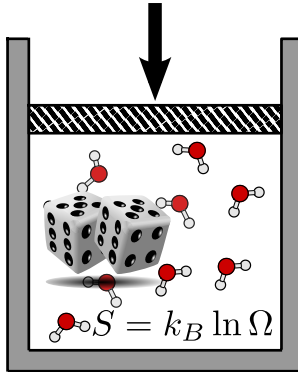
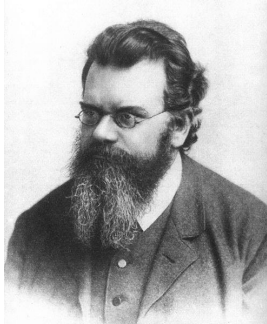


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# **Everything you Need to Know about Classical Thermodynamics**

MSE 421 - Ceriotti

# From classical mechanics to statistical mechanics

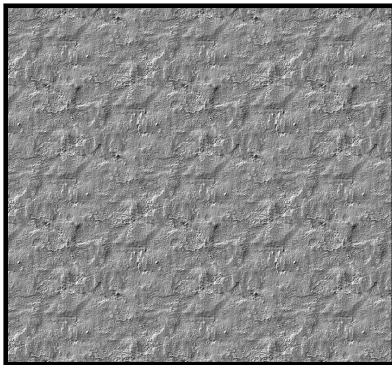


Ludwig Boltzmann (1844-1906): statistical mechanics: reconcile molecular picture and macroscopic thermodynamics

# Microstates and Macrostates

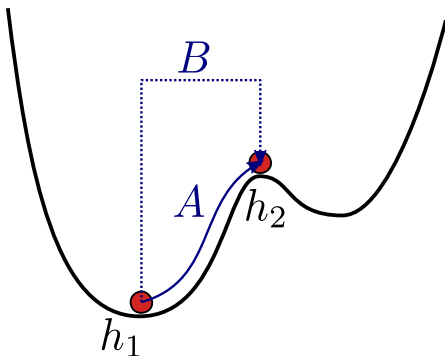
- The task of measuring position and velocities of a macroscopic amount of atoms or molecules is practically impossible
- We can characterize the macroscopic state of *equilibrium* systems by a small number of macroscopic observables, e.g. volume  $V$ , temperature  $T$ , pressure  $p$ , molar amounts of components  $n_i$

$p, V, T$



# Thermodynamic variables

- *State variables* are macroscopic quantities that only depend on the state of the system and not on how the system has been prepared (e.g.  $T$ ,  $p$ ,  $E$ ,  $V$ ,  $n$ , ...)
  - Infinitesimal changes in state variables are exact differentials (e.g.  $\int_{V_1}^{V_2} dV = V_2 - V_1$ , irrespective of the path)
  - *Extensive* variables ( $n$ ,  $V$ ) double when system size is doubled. *Intensive* variables (e.g.  $T$ ,  $p$ ) do not depend on system size



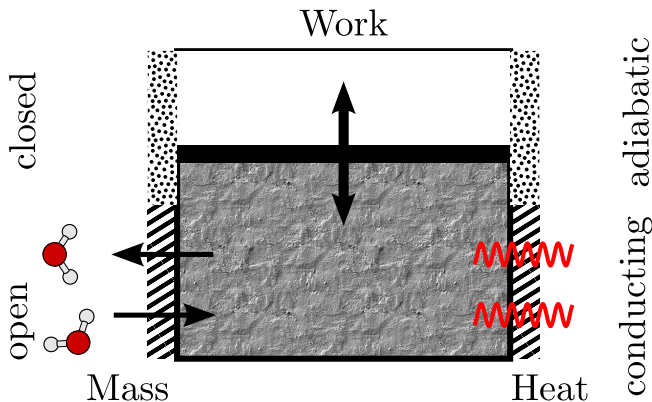
# Thermodynamic variables

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# Boundary Conditions

- The boundary of the system can be open or closed relative to the exchange of mass, and conducting or adiabatic relative to exchange of heat with its surroundings (closed+adiabatic≡isolated)
- The state of the system can also be changed by application of work



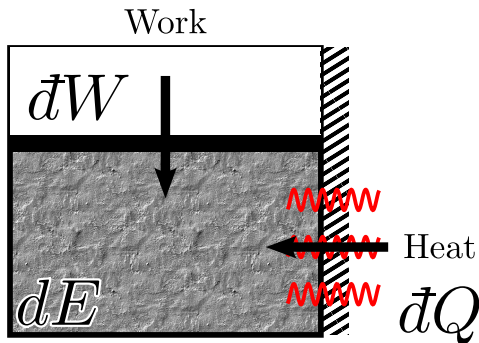
# The internal energy $E$

- The internal energy is a function of state that expresses the potential the system has to generate work. Can be defined by assuming it is

- 1 Extensive ( $E = E_1 + E_2$ )
- 2 Conserved. Can change by doing **work**, or by exchanging **heat**

$$dE = dW + dQ \quad \text{First Law}$$

- 3 Note the (arbitrary) convention for the sign of differentials.



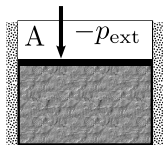
The internal energy is also indicated as  $U$  in many books.  $d$  indicates an exact differential,  $\delta$  indicates an inexact differential, and depends on the path followed during a transformation.

# Measuring the change in internal energy

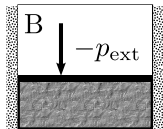
- Work is associated with change of one of the extensive mechanical variables  $X$  defining the state of the system
- For each variable there is a (generalized) force  $f$  that links it with the work done by changing it (e.g.  $dW = -p_{\text{ext}}dV$ )

$$dW = f dX,$$

- We can *measure*  $dE$  as the work spent doing an *adiabatic* transformation between two states  $A$  and  $B$



$$dW_{\text{ad}} = E_B - E_A$$

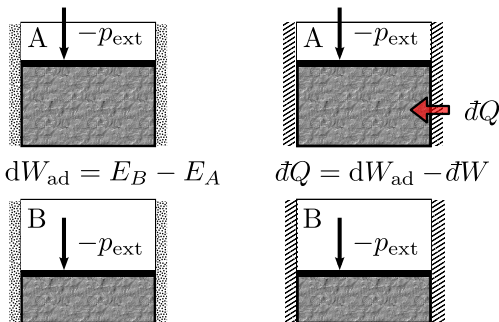




# The first law as the definition of heat

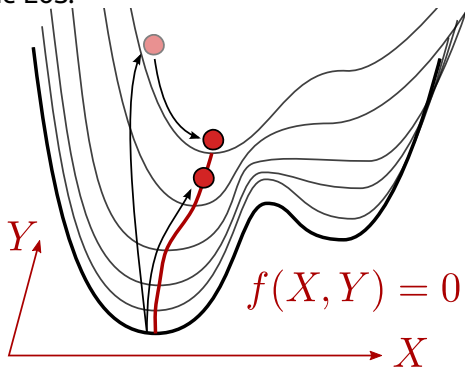
- We can consider the first law as the *definition* of heat
  - 1 Do an adiabatic transformation to measure the change in internal energy  $E_B - E_A$
  - 2 Repeat with open walls, measure the new work  $dW$  and obtain  $dQ$  as the difference

$$dQ = dW_{\text{ad}} - dW$$



# Equilibrium and transformations

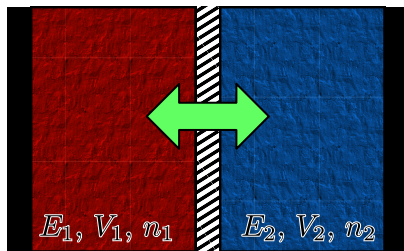
- *Equilibrium* states do not change unless perturbed. If the system returns to a state after a small perturbation, it is said to be *stable*.
- An *equation of state*  $f(\mathbf{X}) = f(E, V, n_i, \dots) = 0$ , determines which values of thermodynamic variables are compatible with equilibrium
- *Reversible* transformations proceed along a series of equilibrium states. *Irreversible* transformations traverse values of thermodynamic variables that violate the EoS.



E.g. for a perfect gas,  $pV - nRT = 0$

# The search for equilibrium states

- How do we determine if a system is in equilibrium?
- How do we determine *what* is the equilibrium state of a system?
- How do we determine the evolution of a system after we remove some *internal constraints*?
- We can try to define a single state function to answer all these questions: entropy!



# An axiomatic definition of entropy

- Define the entropy  $S(E, \mathbf{X})$  as

- Extensive function of state
- Monotonically-increasing function of  $E$

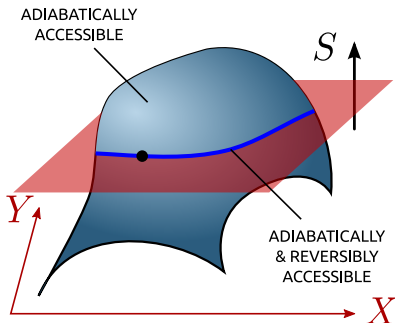
- Define the temperature as  $(\partial E / \partial S)_{\mathbf{X}} = [(\partial S / \partial E)_{\mathbf{X}}]^{-1} = T > 0$

- If it is possible to obtain state  $B$  *adiabatically* from state  $A$ , then  $S(B) \geq S(A)$

$$\Delta S_{\text{ad}} \geq 0$$

Second Law

- If a process is reversible, then one can also reach *adiabatically*  $A$  from  $B$ , that implies  $S(B) = S(A)$



# Entropy and reversible heat

- Consider a system defined by  $S$ ,  $E$ , and mechanical variables  $\mathbf{X}$ . For a reversible process one can cast the EOS into  $S = S(E, \mathbf{X})$
- Compare the differentials of  $S$  and  $E$

$$\begin{array}{lcl}
 \text{total differential of } S(E, \mathbf{X}) & & \text{first law} \\
 \overbrace{dS = \left(\frac{\partial S}{\partial E}\right)_{\mathbf{X}} dE + \sum_i \left(\frac{\partial S}{\partial X_i}\right)_{E, \mathbf{X}'_i} dX_i} & & \overbrace{dE = dQ_{\text{rev}} + dW_{\text{rev}}} \\
 \\
 \underbrace{\frac{\partial S}{\partial E} = T^{-1}}_{\frac{1}{T}} & & \text{rev. work} \\
 dS = \frac{1}{T} dE + \sum_i \left(\frac{\partial S}{\partial X_i}\right)_{E, \mathbf{X}'_i} dX_i & & dE = dQ_{\text{rev}} + \sum_i \frac{\partial E}{\partial X_i} dX_i
 \end{array}$$

- For an adiabatic, reversible process  $dS = 0$  and  $dQ = 0$

$$0 = \sum_i \frac{1}{T} \frac{\partial E}{\partial X_i} dX_i + \sum_i \left(\frac{\partial S}{\partial X_i}\right)_{E, \mathbf{X}'_i} dX_i \Rightarrow \left(\frac{\partial E}{\partial X_i}\right)_{S, \mathbf{X}'_i} = -T \left(\frac{\partial S}{\partial X_i}\right)_{E, \mathbf{X}'_i}$$

- Considering a reversible but non-adiabatic process

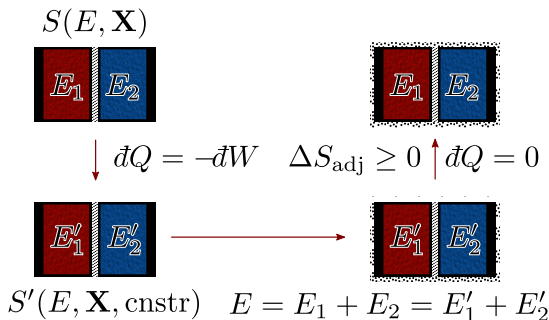
$$\boxed{TdS = dQ_{\text{rev}}}, \quad dE = TdS + \sum_i \left(\frac{\partial E}{\partial X_i}\right) dX_i$$

Clausius principle

Many classical books define the entropy starting from the reversible heat. Here we *postulate* it, and derive Clausius's principle from the postulated properties of  $S$ .

# Internal constraints and equilibrium

- Consider a system to which we applied an internal constraint - e.g. we fix the partitioning of  $E$  between two subsystems
  - We start in equilibrium, and make an arbitrary transformation that only changes the partitioning of energy between the two subsystems. This gives a state with a different entropy  $S'$  but same energy  $E = E_1 + E_2$ : from the first law,  $dQ + dW = 0$
  - We relax back to equilibrium adiabatically. From the axioms:  $S' < S$
- The equilibrium partitioning is the one that maximizes the entropy:  $\Delta S_{\text{adj}} \geq 0$  results in a general **maximum-entropy principle**



# A variational principle for $E$

- Under the conservation conditions  $E = E_1 + E_2$ ,  $\mathbf{X} = \mathbf{X}_1 + \mathbf{X}_2$ , and given the maximum entropy principle

$$S(E, \mathbf{X}, \text{cnstr}) = S(E_1, \mathbf{X}_1) + S(E_2, \mathbf{X}_2) \leq S(E, \mathbf{X})$$

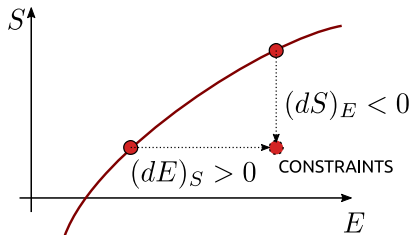
Recall that  $\partial S / \partial E > 0$ . Then, if

$$S(E', \mathbf{X}) = S(E, \mathbf{X}, \text{cnstr})$$

it must be that  $E' < E$ . That is, introducing constraints at constant entropy necessarily implies an increase of internal energy.

- If we introduce infinitesimal constraints  $\delta Y$  around equilibrium, we can express this condition as

$$\delta E_{S, \mathbf{X}} = E(S, \mathbf{X}, \delta Y) - E(S, \mathbf{X}) \approx \left( \frac{\partial E}{\partial Y} \right)_{S, \mathbf{X}, \delta Y=0} \delta Y \geq 0$$



# Thermal equilibrium

- What happens if we tried to partition energy between the two subsystems, at constant total energy?

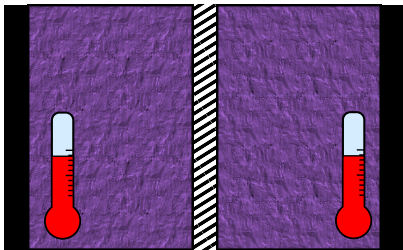
maxent principle    extensive entropy

$$\overbrace{0 \geq \delta S_{E,\mathbf{x}}}^{\text{maxent principle}} = \overbrace{\delta S_1 + \delta S_2}^{\text{extensive entropy}} = \left( \frac{\partial S_1}{\partial E_1} \right)_{\mathbf{x}, \delta E_1=0} \delta E_1 + \left( \frac{\partial S}{\partial E_2} \right)_{\mathbf{x}, \delta E_2=0} \delta E_2$$

- Due to the constant-energy condition,  $\delta E_2 = -\delta E_1$ , and considering that  $\partial S / \partial E = 1/T$

$$\frac{1}{T_1} \delta E_1 + \frac{1}{T_2} \delta E_2 = \left( \frac{1}{T_1} - \frac{1}{T_2} \right) \delta E_1 \leq 0 \quad \text{for all } \delta E_1, \text{ that implies } T_1 = T_2$$

$$T_2 = T_1$$





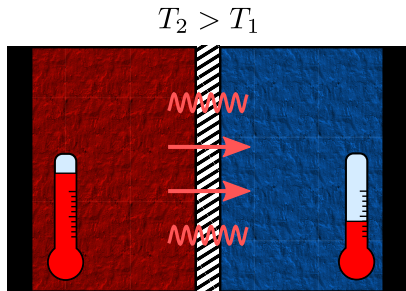
# Convergence to thermal equilibrium

- Now consider an initial state  $T_1 \neq T_2$ . An adiabatic spontaneous evolution will have  $\Delta S_1 + \Delta S_2 = \Delta S > 0$ .

$$\left(\frac{\partial S_1}{\partial E_1}\right)_x \Delta E_1 + \left(\frac{\partial S}{\partial E_2}\right)_x \Delta E_2 > 0 \quad \rightarrow \quad \left(\frac{1}{T_1} - \frac{1}{T_2}\right) \Delta E_1 > 0$$

- The maximum entropy condition implies that energy flows from the hot to the cold subsystem

$$\left(\frac{1}{T_1} - \frac{1}{T_2}\right) \Delta E_1 > 0 \quad T_2 > T_1 \rightarrow \frac{1}{T_2} < \frac{1}{T_1} \rightarrow \Delta E_1 > 0$$



# Legendre transforms

- Consider a function of  $N$  variables  $f(x_1, \dots, x_N)$ . One can write its differential

$$df = \sum_i \frac{\partial f}{\partial x_i} dx_i.$$

- Say we wanted to define a function, related to  $f$ , that instead has a differential form that depends on another set of variables  $u_i$ .
  - Consider  $g = f - \sum_i x_i u_i$

$$dg = \sum_i \frac{\partial f}{\partial x_i} dx_i - \sum_i u_i dx_i - \sum_i x_i du_i$$

- If we set  $u_i = \frac{\partial f}{\partial x_i}$  we can cancel the differentials  $dx_i$ . This is the Legendre transform of  $f$

$$g(u_1, \dots) = f - \sum_i x_i \frac{\partial f}{\partial x_i}$$

- Obviously, the transform can be applied to a subset of the  $x_i$ 's

# Thermodynamic potentials

- The most important term of  $dE$  in terms of mechanical boundary conditions is  $-pdV$ , that can be supplemented by composition variables.  $E$  is a natural function of  $S, V, n_i$ , so -- introducing the chemical potential  $\mu_i = (\partial E / \partial n_i)_{S, V, n'_i}$

$$dE = TdS - pdV + \sum_i \mu_i dn_i.$$

- One can Legendre-transform the entropy term, obtaining the Helmholtz free energy

$$A = E - TS, \quad dA = -SdT - pdV + \sum_i \mu_i dn_i$$

... or the volume term obtaining the enthalpy

$$H = E + pV, \quad dH = TdS + Vdp + \sum_i \mu_i dn_i$$

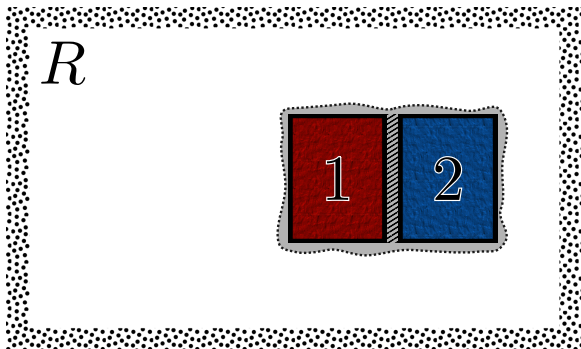
... or both obtaining the Gibbs free energy

$$G = E - TS + pV, \quad dG = -SdT + Vdp + \sum_i \mu_i dn_i$$

# A variational principle for $G$

- Consider a composite system 1 + 2 enclosed in a temperature/pressure reservoir  $R$ , at  $T^R$  and  $p^R$

$$\text{adiabaticity+constant-}V \rightarrow d(E^1 + E^2 + E^R) = 0, d(V^1 + V^2 + V^R) = 0$$



# A variational principle for $G$

- Consider a composite system 1 + 2 enclosed in a temperature/pressure reservoir  $R$ , at  $T^R$  and  $p^R$

$$\text{adiabaticity+constant-}V \rightarrow d(E^1 + E^2 + E^R) = 0, d(V^1 + V^2 + V^R) = 0$$

- Equilibrium condition:  $d(S^1 + S^2 + S^R) = 0$

$$dS^1 + dS^2 = -dS^R, \quad dV^1 + dV^2 = -dV^R, \quad dE^1 + dE^2 = -dE^R$$

- Using differential  $dE = TdS - PdV$

$$\text{constant-}E \rightarrow 0 = T^1 dS^1 + T^2 dS^2 - p^1 dV^1 - p^2 dV^2 - p^R dV^R + T^R dS^R$$

$$0 = (T^1 - T^R) dS^1 + (T^2 - T^R) dS^2 - (p^1 - p^R) dV^1 - (p^2 - p^R) dV^2$$

- Equilibrium implies  $T^1 = T^2 = T^R = T$ ,  $p^1 = p^2 = p^R = p$

- Now consider the 1 + 2 subsystem, and remember that

$$dG = d(E - TS + pV). \text{ With the } T \text{ and } p \text{ constraint}$$

$$\begin{aligned} 0 &= dE_1 + dE_2 + dE^R = dE_1 + dE_2 + TdS^R - pdV^R = \\ &= d(E_1 + E_2) - Td(S_1 + S_2) + pd(V_1 + V_2) = (d(G_1 + G_2))_{T,p} \end{aligned}$$

# Maxwell relations

- Considering double derivatives of thermodynamic potentials reveals relations between macroscopic quantities

$$\frac{\partial^2 E}{\partial V \partial S} = \left( \frac{\partial T}{\partial V} \right)_S, \quad \frac{\partial^2 E}{\partial S \partial V} = - \left( \frac{\partial p}{\partial S} \right)_V \rightarrow \boxed{\left( \frac{\partial T}{\partial V} \right)_S = - \left( \frac{\partial p}{\partial S} \right)_V}$$

- Similar equations hold for the other potentials

$$\frac{\partial^2 H}{\partial S \partial p} \rightarrow \boxed{\left( \frac{\partial T}{\partial p} \right)_S = \left( \frac{\partial V}{\partial S} \right)_p}$$

$$\frac{\partial^2 A}{\partial T \partial V} \rightarrow \boxed{\left( \frac{\partial S}{\partial V} \right)_T = \left( \frac{\partial p}{\partial T} \right)_V}$$

$$\frac{\partial^2 G}{\partial T \partial p} \rightarrow \boxed{- \left( \frac{\partial S}{\partial p} \right)_T = \left( \frac{\partial V}{\partial T} \right)_p}$$

# Constrained derivatives of a function

- Consider a function  $z = z(x, y)$

$$dz = \left( \frac{\partial z}{\partial x} \right)_y dx + \left( \frac{\partial z}{\partial y} \right)_x dy$$

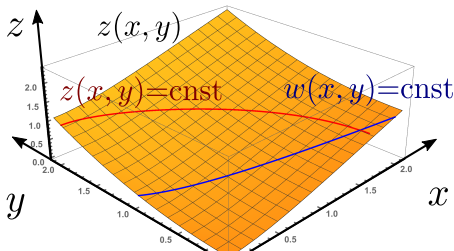
- If one requires constant  $z$ , the relation between the differentials is

$$\left( \frac{\partial y}{\partial x} \right)_z = - \left( \frac{\partial z}{\partial x} \right)_y / \left( \frac{\partial z}{\partial y} \right)_x \rightarrow \left( \frac{\partial z}{\partial x} \right)_y = - \left( \frac{\partial z}{\partial y} \right)_x \left( \frac{\partial y}{\partial x} \right)_z$$

- Now consider a derivative along another constraining function

$$w = w(x, y)$$

$$dz = \left( \frac{\partial z}{\partial x} \right)_y dx + \left( \frac{\partial z}{\partial y} \right)_x \left( \frac{\partial y}{\partial x} \right)_w dx \rightarrow \left( \frac{\partial z}{\partial x} \right)_w = \left( \frac{\partial z}{\partial x} \right)_y + \left( \frac{\partial z}{\partial y} \right)_x \left( \frac{\partial y}{\partial x} \right)_w$$



# Specific heat(s)

- ❶ Recall definitions of heat capacity (e.g.  $(dE)_V = TdS = C_V dT$ )

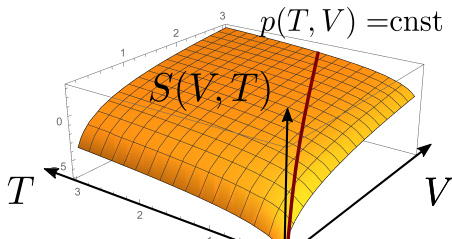
$$C_V = \left( \frac{\partial E}{\partial T} \right)_V = \left( \frac{\partial E}{\partial S} \right)_V \left( \frac{\partial S}{\partial T} \right)_V = T \left( \frac{\partial S}{\partial T} \right)_V ; C_P = \left( \frac{\partial H}{\partial T} \right)_P = T \left( \frac{\partial S}{\partial T} \right)_P$$

- ❷ Take  $S = S(T, V)$  and move along a constant- $p$  line

$$(dS)_P = \left( \frac{\partial S}{\partial T} \right)_V dT + \left( \frac{\partial S}{\partial V} \right)_T (dV)_P = \left( \frac{\partial S}{\partial T} \right)_V dT + \left( \frac{\partial S}{\partial V} \right)_T \left( \frac{\partial V}{\partial T} \right)_P dT$$

- ❸ This provides a relation between the heat capacities, the isothermal compressibility and the thermal expansion coefficient

$$\frac{C_P - C_V}{T} = \left( \frac{\partial S}{\partial V} \right)_T \left( \frac{\partial V}{\partial T} \right)_P = \left( \frac{\partial p}{\partial T} \right)_V \left( \frac{\partial V}{\partial T} \right)_P = - \left( \frac{\partial p}{\partial V} \right)_T \left[ \left( \frac{\partial V}{\partial T} \right)_P \right]^2$$





# Euler's Theorem for homogeneous functions

- A function is said to be homogeneous of degree  $n$  if

$$f(\lambda x_1, \lambda x_2, \dots, \lambda x_m) = \lambda^n f(x_1, x_2, \dots, x_m)$$

- Take the  $\lambda$ -derivative of both sides

$$\sum_i f'_i(\lambda x_1, \lambda x_2, \dots, \lambda x_m) x_i = n \lambda^{n-1} f(x_1, x_2, \dots, x_m)$$

- For  $\lambda = 1$

$$\sum_i x_i \frac{\partial f}{\partial x_i}(x_1, x_2, \dots, x_m) = n f(x_1, x_2, \dots, x_m)$$

# Gibbs-Duhem equation

- The energy is a homogeneous function of  $S, V, n_i$  so

$$E(S, V, n_i) = \frac{\partial E}{\partial S} S + \frac{\partial E}{\partial V} V + \sum_i \frac{\partial E}{\partial n_i} n_i = TS - pV + \sum_i \mu_i n_i$$

- From the definition of Gibbs free energy,  $G(T, p, n_i) = E - TS + pV = \sum_i \mu_i n_i$
- The total differential of  $E$  is

$$dE = TdS + SdT - pdV - Vdp + \sum_i [\mu_i dn_i + n_i d\mu_i]$$

but we know that the differential of  $E$  reads

$$dE = TdS - pdV + \sum_i \mu_i dn_i$$

so

$$SdT - Vdp + \sum_i n_i d\mu_i = 0$$

Gibbs-Duhem equation

# Multi-phase equilibrium

- Consider an isolated system containing  $P$  phases and  $M$  components. Each phase can be seen as a subsystem, and the interface terms ignored.

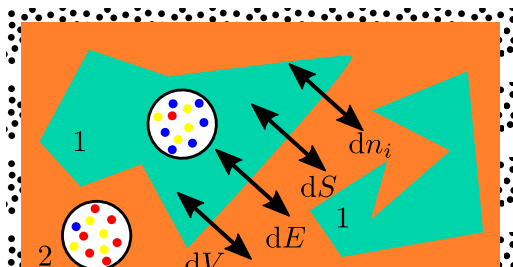
$$\delta E = \sum_{i=1}^P \delta E_i = \sum_{i=1}^P T^i \delta S^i - p^i \delta V^i + \sum_{j=1}^M \mu_j^i \delta n_j^i$$

- Being an isolated system, several conservation constraints must be enforced

$$\sum_i \delta S^i = 0, \quad \sum_i \delta V^i = 0, \quad \sum_i \delta n_j^i = 0$$

- The only way to guarantee  $\delta E \geq 0$  (minimum energy principle) for any value of the changes in the  $\delta$ .

$$T^1 = \dots = T^P = T, \quad p^1 = \dots = p^P = p, \quad \mu_j^1 = \dots = \mu_j^P = \mu_j$$



# Chemical potential and mass transport

- Consider a situation with  $\mu_j^1 > \mu_j^2$ . The system is out of equilibrium, and the spontaneous direction of evolution is that such that  $\Delta E < 0$ . At constant  $T$  and  $p$  throughout the system the only non-zero term in the energy differential will be

$$\mu_j^1 \Delta n_j^1 + \mu_j^2 \Delta n_j^2 < 0$$

- Mass balance implies  $\Delta n_j^2 = -\Delta n_j^1$ , i.e.

$$(\mu_j^1 - \mu_j^2) \Delta n_j^1 < 0$$

- For  $\mu_j^1 > \mu_j^2$  this implies  $\Delta n_j^1 < 0$ , i.e. components flow from the phase with higher chemical potential to that with lower  $\mu$ .

# Conditions for stable equilibrium

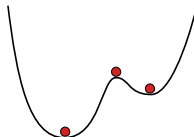
- Take a system in equilibrium, for which  $\delta E = 0$ . Then, one has to check whether the second-order variation is positive,  $\delta^2 E \geq 0$
- Considering an isolated system, with two subsystems that can only exchange heat, one gets

$$0 \leq \frac{\partial^2 E^1}{\partial (S^1)^2} (\delta S^1)^2 + \frac{\partial^2 E^2}{\partial (S^2)^2} (\delta S^2)^2 = \left( \frac{\partial^2 E^1}{\partial (S^1)^2} + \frac{\partial^2 E^2}{\partial (S^2)^2} \right) (\delta S^1)^2$$

- Considering  $(\partial^2 E / \partial S^2)_{V,n} = (\partial T / \partial S)_{V,n} = T / C_V$ , and that  $T_1 = T_2$  because of equilibrium,

$$\left( \frac{T}{C_V^1} + \frac{T}{C_V^2} \right) \geq 0$$

that implies  $T / C_V \geq 0$  since one could take any arbitrary subsystem



# Generalized equilibrium conditions

- Consider a thermodynamic potential  $\Phi$  (any of  $E, H, A, G$ ) that depends on some extensive variables  $X$  and some intensive variables  $u, z$ . Take  $x$  to be the variable conjugate to  $X$ , i.e.  $x = \partial\Phi/\partial X$ . Then the second-order differential will be e.g.

$$0 \leq \left[ \frac{\partial^2 \Phi^1}{\partial (X^1)^2} + \frac{\partial^2 \Phi^2}{\partial (X^2)^2} \right] (\delta X_1)^2 + \dots$$

- The positivity condition has to apply to each term separately, so we don't need to consider the terms in the differential containing other extensive variables.
- Taking into account the possibility of arbitrarily subdividing the system - so the conditions is not specific to subsystem 1 or 2 - one gets conditions of the form

$$\frac{\partial^2 \Phi}{\partial X^2} = \frac{\partial x}{\partial X} \geq 0$$

# Molar quantities and molar fractions

- Often one wants to refer to the properties of a system independently of its absolute size.
- It is then possible to introduce “molar” quantities, e.g.
  - Molar volume,  $v = V/n$
  - Molar fractions  $x_i = n_i/n$  (defining  $n = \sum_i n_i$ )
  - Molar thermodynamic potentials, e.g. molar Gibbs free energy  $g = G/n$  (NB:  $g \equiv \mu$ !)
- If derivatives are done at constant system size, there are similar relationships between extensive and molar quantities, e.g.

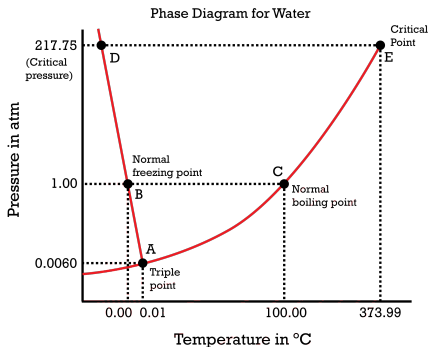
$$\left(\frac{\partial \mu}{\partial \rho}\right)_T = \frac{1}{n} \left(\frac{\partial G}{\partial \rho}\right)_T = \frac{V}{n} = v$$

$$\left(\frac{\partial \mu}{\partial T}\right)_\rho = \frac{1}{n} \left(\frac{\partial G}{\partial T}\right)_\rho = -\frac{S}{n} = -s$$

# Gibbs Phase Rule

- Consider a system with  $M$  components and  $P$  phases, described in terms of intensive variables -  $p$ ,  $T$  and  $M$  molar fractions  $x_j^i = n_j^i / \sum_j n_j^i$
- Equilibrium between the different phases implies  $M(P - 1)$  equations connecting the chemical potentials,  $\mu_j^i = \mu_j^{i'}$ , plus  $P$  equations connecting the molar fractions within each phase ( $\sum_j x_j^i = 1$ )
- This leaves a number of independent degrees of freedom  $f$  which is

$$f = 2 + MP - P - M(P - 1) = 2 + M - P$$





# Phase transitions and phase lines

- A phase line separates the stability range of two phases. Determined by

$$\mu_1(p, T) = \mu_2(p, T)$$

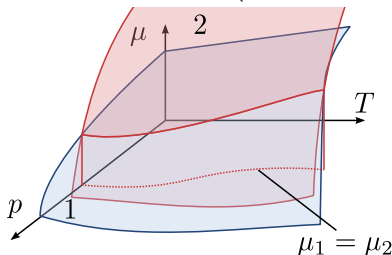
- The properties of the system may have a discontinuity (1st-order phase transition)

$$v_1 - v_2 = \left( \frac{\partial \mu_1}{\partial p} \right)_T - \left( \frac{\partial \mu_2}{\partial p} \right)_T$$

At critical points the two surfaces can be tangent, so it is possible not to have a discontinuity (second-order phase transition)

- We can compute the slope of coexistence line (Clausius-Clapeyron eqn.)

$$\frac{\partial p}{\partial T} = - \left( \left( \frac{\partial \mu_1}{\partial p} \right)_T - \left( \frac{\partial \mu_2}{\partial p} \right)_T \right)^{-1} \left( \left( \frac{\partial \mu_1}{\partial T} \right)_p - \left( \frac{\partial \mu_2}{\partial T} \right)_p \right) = \frac{s_1 - s_2}{v_1 - v_2}$$





# Entropy derivatives

- Derivatives of  $E$  and  $S$  are related due to the fundamental relation  $S(E, V)$

