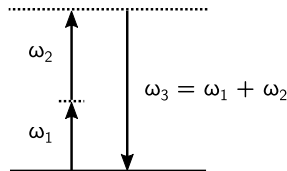
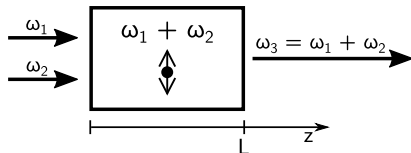


Topics covered	No	Lecture/Date
Introductory presentation; Basic of laser operation I: dispersion theory, atoms	1	11. 09. 2024
Basic of laser operation II: dispersion theory, atoms	2	18. 09. 2024
Laser systems I: 3 and 4 level lasers, gas lasers, solid state lasers, applications	3	25. 09. 2024
Laser systems II: semi-conductor lasers, external cavity lasers, applications	4	02. 10. 2024
Noise characteristics of lasers: linewidth, coherence, phase and amplitude noise, OSA (1)	5	09. 10. 2024
Noise characteristics of lasers: linewidth, coherence, phase and amplitude noise, OSA (2)	6	16. 10. 2024
Optical detection	7	30. 10. 2024
Optical fibers: light propagation in fibers, specialty fibers and dispersion (GVD)	8	06. 11. 2024
Ultrafast lasers I.: Passive mode locking and ultrafast lasers	9	13. 11. 2024
Ultrafast lasers II: mode locking, optical frequency combs / frequency metrology	10	20. 11. 2024
Ultrafast lasers III: pulse characterization, applications	11	27. 11. 2024
Nonlinear frequency conversion I: theory, frequency doubling, applications	12	04. 12. 2024
Nonlinear frequency conversion II: optical parametric amplification (OPA)	13	11. 12. 2024
Laboratory visits (lasers demo)	14	20. 12. 2024

- Difference frequency
- Parametric amplification
- Threshold of OPOs

Sum-frequency



Slowly varying envelope approximation:

$$\left| \frac{d^2 A_3}{dz^2} \right| \ll \left| k_3 \frac{dA_3}{dz} \right|.$$

Wave-vector mismatch

$$\frac{dA_3}{dz} = \frac{2id_{\text{eff}}\omega_3^2}{k_3c^2} A_1 A_2 e^{i\Delta k z},$$

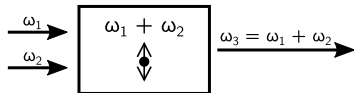
where $\Delta k = k_1 + k_2 - k_3$.

$$\frac{dA_1}{dz} = K_1 A_3 e^{-i\Delta k z}, \quad K_1 = \frac{2i\omega_1^2 d_{\text{eff}}}{k_1 c^2} A_2^*,$$

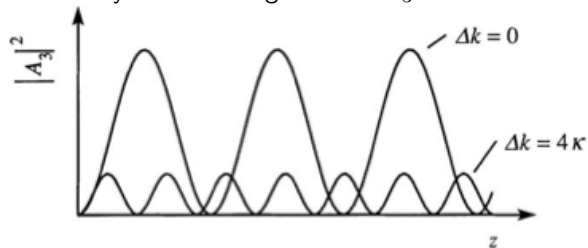
$$\frac{dA_3}{dz} = K_3 A_1 e^{+i\Delta k z}, \quad K_3 = \frac{2i\omega_3^2 d_{\text{eff}}}{k_3 c^2} A_2,$$

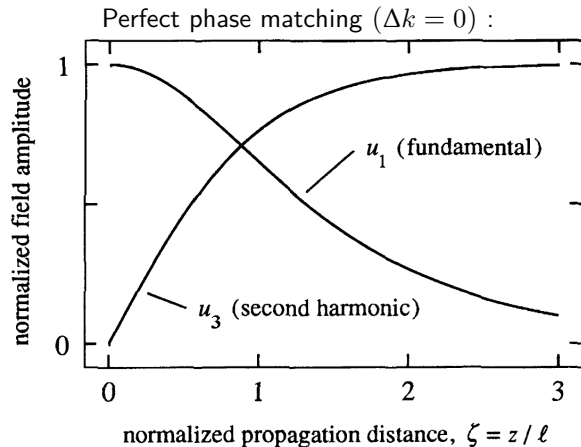
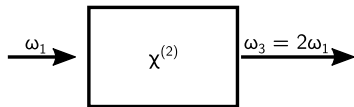
Assume wave A_2 constant:

$$\frac{d^2 A_1}{dz^2} = -\kappa^2 A_1, \quad \kappa^2 \equiv -K_1 K_3 = \frac{4\omega_1^2 \omega_3^2 d_{\text{eff}}^2 |A_2|^2}{k_1 k_3 c^4}.$$



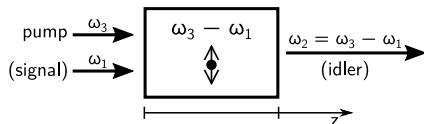
Oscillatory behavior in generated A_3 field



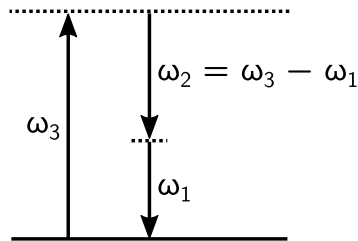


$$u_1(z)^2 + u_2(z)^2 = 1$$

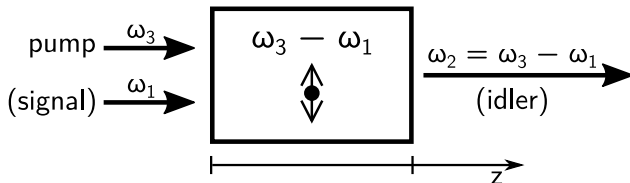
Difference-frequency



The actual frequency values of the *signal* ω_2 and *idler* ω_1 are determined by the phase matching condition.



Difference-frequency



$$\frac{dA_1}{dz} = \frac{2i\omega_1^2 d_{\text{eff}}}{k_1 c^2} A_3 A_2^* e^{i\Delta k z}$$

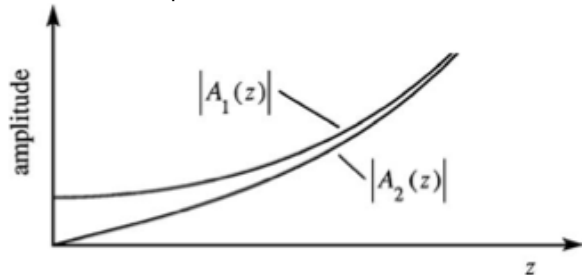
$$\frac{dA_2}{dz} = \frac{2i\omega_2^2 d_{\text{eff}}}{k_2 c^2} A_3 A_1^* e^{i\Delta k z}$$

Assumption: pump ω_3 is strong and undepleted

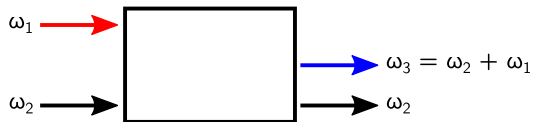
$$A_1(z) = A_1(0) \cosh \kappa z$$

$$A_2(z) = i \left(\frac{n_1 \omega_2}{n_2 \omega_1} \right)^{1/2} \frac{A_3}{|A_3|} A_1^*(0) \sinh \kappa z$$

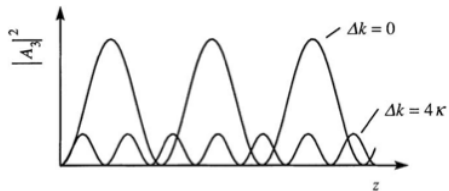
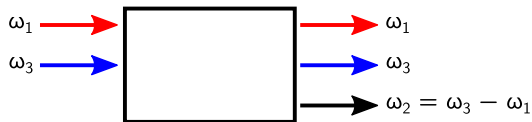
Parametric amplification



Sum

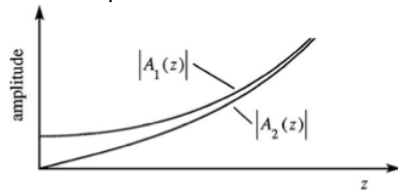


Difference



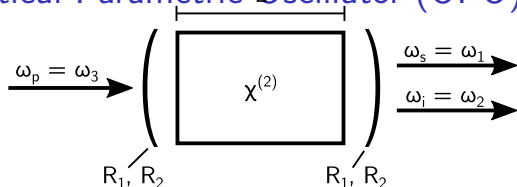
Oscillatory behavior

Parametric amplification



Gain: amplitude grows exponentially

Optical Parametric Oscillator (OPO)

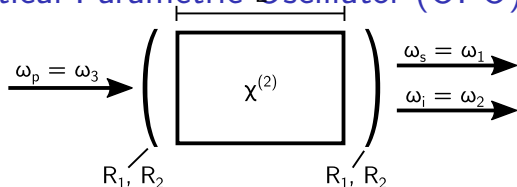


General solution for nonzero Δk (see exercises):

$$A_1(z) = \left[A_1(0) \left(\cosh gz - \frac{i\Delta k}{2g} \sinh gz \right) + \frac{\kappa_1}{g} A_2^*(0) \sinh gz \right] e^{i\Delta k z/2},$$

$$A_2(z) = \left[A_2(0) \left(\cosh gz - \frac{i\Delta k}{2g} \sinh gz \right) + \frac{\kappa_2}{g} A_1^*(0) \sinh gz \right] e^{i\Delta k z/2}$$

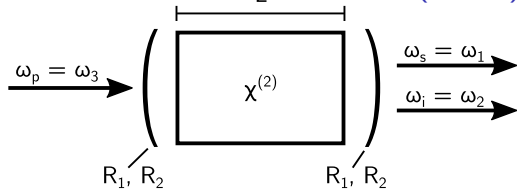
Optical Parametric Oscillator (OPO)



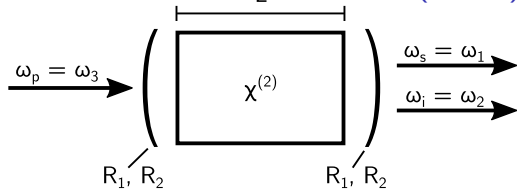
General solution for nonzero Δk (see exercises):

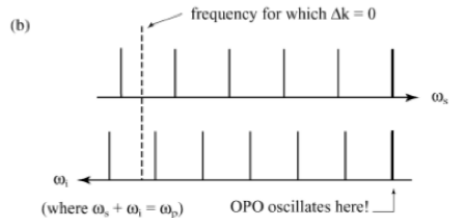
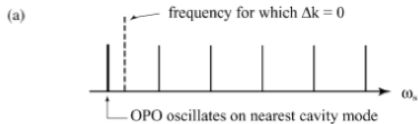
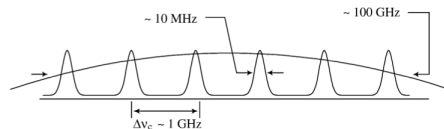
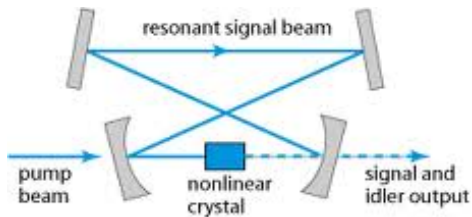
$$A_1(z) = \left[A_1(0) \left(\cosh gz - \frac{i\Delta k}{2g} \sinh gz \right) + \frac{\kappa_1}{g} A_2^*(0) \sinh gz \right] e^{i\Delta k z/2},$$
$$A_2(z) = \left[A_2(0) \left(\cosh gz - \frac{i\Delta k}{2g} \sinh gz \right) + \frac{\kappa_2}{g} A_1^*(0) \sinh gz \right] e^{i\Delta k z/2}$$

Optical Parametric Oscillator (OPO)



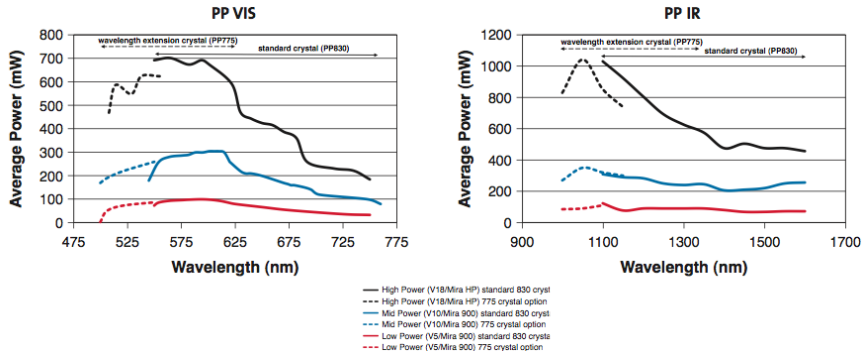
Optical Parametric Oscillator (OPO)





Tuning Range (nm)	
Signal SHG ^{4,5}	550 to 740
Signal ^{4,5}	1100 to 1600
Idler (option)	1750 to 3300
Nominal Pump Wavelength (nm)	
830	

Typical Tuning Curves for Femtosecond Mira-OPO PP-Automatic



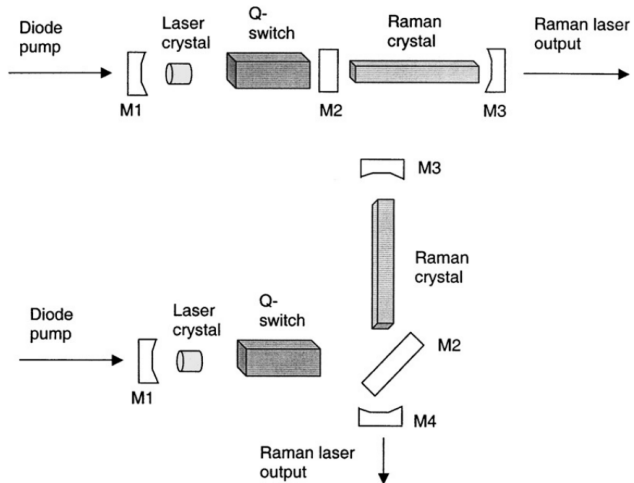
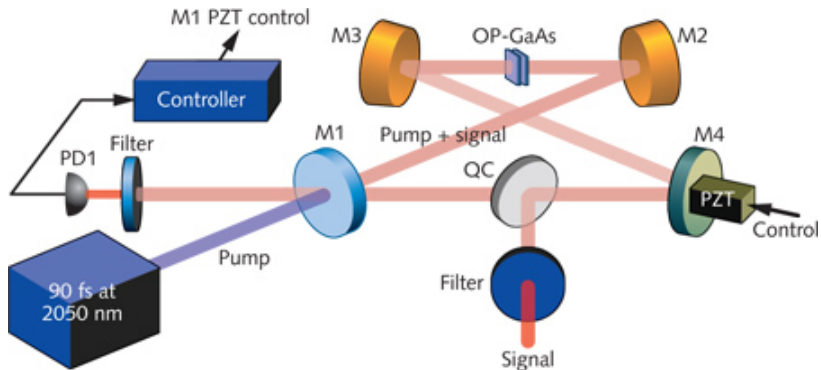


Fig. 14. Schematic diagrams showing coupled cavity Raman laser configurations (a) linear configuration and (b) folded configuration.



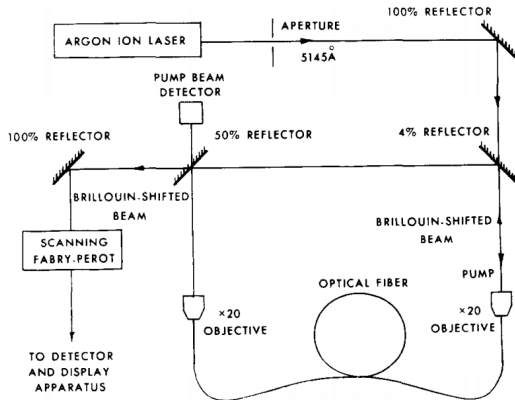
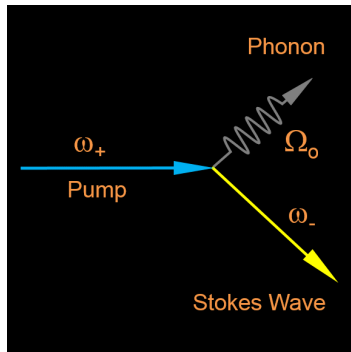


FIG. 1. Schematic of Brillouin ring-laser apparatus. The ring consists of the optical fiber together with the beam paths defined by the 4% and 50% partial reflectors. The pump-beam throughput is monitored by the pump-beam detector.