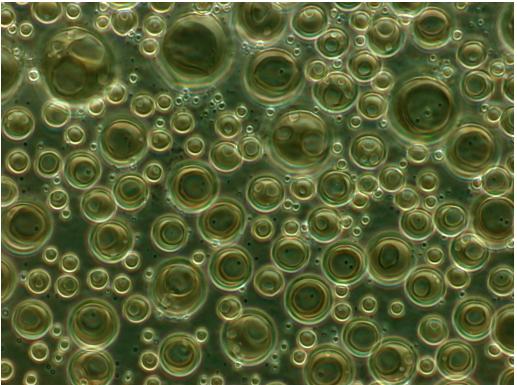
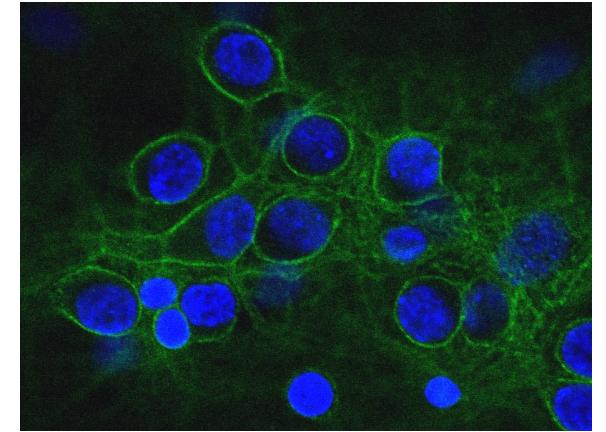
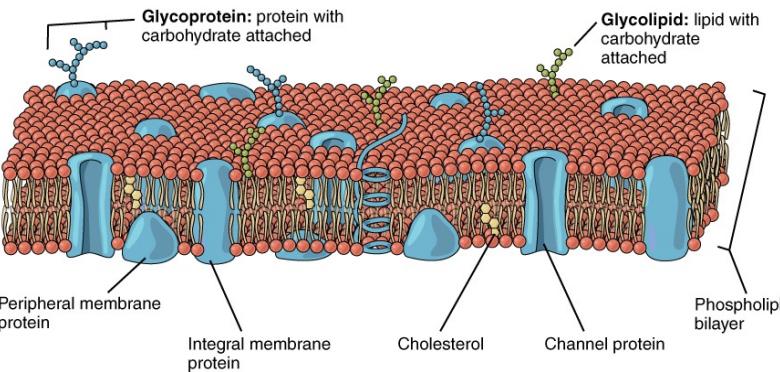
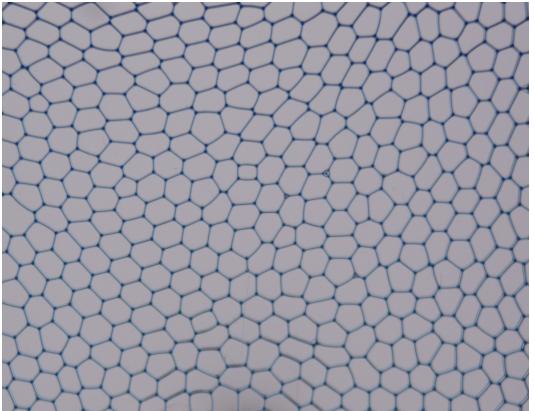


ME470: Mechanics of Soft and Biological Matter

Lecture4: Idea Chain & Freely Jointed Chain

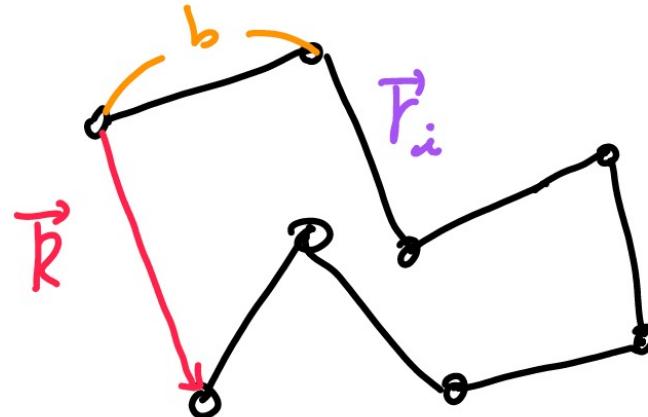


Sangwoo Kim

MESOBIO – IGM – STI – EPFL

Red Blood Cells

Ideal chain: polymer model in the flexible limit



Assumptions

- n segments of length b (Kuhn length)
- Inextensible ($L_c = nb$)
- Freely rotation, no internal energy change ($dU = 0$)

$$\vec{R} = \sum_{i=1}^n \vec{r}_i \quad (\text{end-to-end vector})$$

$$\langle \vec{R} \rangle = 0 \quad (\text{random orientation of } \vec{r}_i)$$

$$\langle R^2 \rangle = \langle \vec{R} \cdot \vec{R} \rangle = nb^2 \quad \rightarrow \quad \langle R^2 \rangle \sim n$$

Same as random walk

Random walk



Probability of the chain having a specific length



Free energy & force-displacement relation

Probability of at distance r with n step for 1D random walk

$$P_{1d}(n, r) = \frac{1}{2^n} \binom{n}{\frac{n+r/b}{2}} = \frac{1}{2^n} \frac{n!}{\left(\frac{n+r/b}{2}\right)! \left(\frac{n-r/b}{2}\right)!}$$

Binomial coefficient

In the limit of large n 

$$P_{1d}(n, r) = \frac{1}{\sqrt{2\pi\langle r^2 \rangle}} e^{-r^2/2\langle r^2 \rangle}$$

EPFL Ideal chain (IC)

Here,

$$\vec{R} = R_x \hat{e}_x + R_y \hat{e}_y + R_z \hat{e}_z$$

$$\langle R^2 \rangle = 3\langle r^2 \rangle \quad \rightarrow \quad \langle r^2 \rangle = \frac{\langle R^2 \rangle}{3} = \frac{nb^2}{3}$$

$$\rightarrow P_{1d}(n, R_i) = \sqrt{\frac{3}{2\pi\langle R^2 \rangle}} e^{-3R_i^2/2\langle R^2 \rangle} \quad i = x, y, z$$

$$\rightarrow P_{3d}(n, R) = \left(\frac{3}{2\pi\langle R^2 \rangle} \right)^{3/2} e^{-3R^2/2\langle R^2 \rangle}$$

Gaussian distribution!

Now, translate probability distribution function to free energy

$$F = -TS$$

$$S = k_B \ln \Omega(n, R) = k_B \ln[P_{3d}(n, R)\Omega_{tot}]$$

$$S \sim -\frac{3k_B R^2}{2nb^2} + \frac{3}{2}k_B \ln\left(\frac{3}{2\pi nb^2}\right) + k_B \ln \Omega_{tot}$$

S_0 : constant



$$F = -TS = k_B T \frac{3R^2}{2nb^2} - TS_0$$

Under external force, \vec{F} , in the direction of \vec{R}

$$G = -TS - FR$$

$$dG = 0$$

$$\Rightarrow \frac{\partial G}{\partial R} = \frac{3k_B T}{nb^2} R - F = 0$$



$$F = \left(\frac{3k_B T}{nb^2} \right) R$$

k_{sp} : spring constant

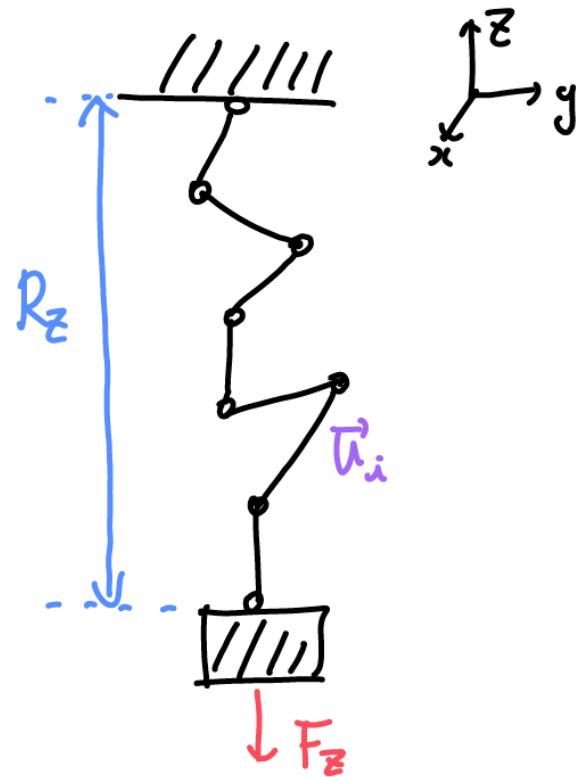
Note

- Non-zero force for non-zero R .
- Linear relation between force-displacement \rightarrow ENTROPIC spring.
- As T increases, stiffness increases.
- Valid only for flexible polymer with small R .
- Kuhn length is related to the persistence length, $b = 2l_p$

IC limitation: linear response beyond $L = nb$



FJC for realistic description at $R \sim L$



Assumptions

- Inextensible segments (same as IC)
 - End-to end vector
- Chain extended in direction only
- Describe microstates by directional angle, $(\phi_i, \theta_i) = \Theta$
$$u_{i,x} = \sin \theta_i \cos \phi_i$$
$$u_{i,y} = \sin \theta_i \sin \phi_i$$
$$u_{i,z} = \cos \theta_i$$
- Consider a system, chain and weight,
$$U = -F_Z R_Z$$

→ Use canonical ensemble (constant T, Boltzmann distribution)

Microscopic description: θ_i is an angle w.r.t z-axis

$$R_z = \vec{R} \cdot \hat{e}_z = b \sum_{i=1}^n \cos \theta_i \quad \Rightarrow \quad U = -F_z b \sum_{i=1}^n \cos \theta_i$$

Probability: $P(\Theta) = \frac{1}{Z} e^{-U(\Theta)/k_B T}$

$$Z = \int_{\Theta} \exp\left(-\frac{U(\Theta)}{k_B T}\right) d\Theta$$

$$\rightarrow \frac{U(\Theta)}{k_B T} = -\kappa \sum_{i=1}^n \cos \theta_i \quad \kappa \equiv \frac{bF_z}{k_B T}$$

$$\rightarrow Z = \prod_{i=1}^n \int_0^{2\pi} \int_0^\pi \exp(-\kappa \cos \theta_i) \sin \theta_i d\theta_i d\phi_i = z^n$$

$$\rightarrow z = 2\pi \int_0^\pi \exp(-\kappa \cos \theta) \sin \theta d\theta = \frac{4\pi}{\kappa} \sinh \kappa$$

We seek $\langle R_z \rangle = \int_{\Theta} P(\Theta) R_z d\Theta = \frac{1}{Z} \int_{\Theta} \exp\left(\frac{\kappa R_z}{b}\right) R_z d\Theta$

One can show

$$\int_{\Theta} \exp\left(\frac{\kappa R_z}{b}\right) R_z d\Theta = b \frac{\partial Z}{\partial \kappa}$$



$$\langle R_z \rangle = \frac{b}{Z} \frac{\partial Z}{\partial \kappa} = b \frac{\partial(\ln Z)}{\partial \kappa} = bn \frac{\partial(\ln z)}{\partial \kappa}$$

$$\langle R_z \rangle = nb \left[\coth\left(\frac{bF_z}{k_B T}\right) - \frac{k_B T}{bF_z} \right]$$

Note: this could be written as

$$\langle R_z \rangle = k_B T \frac{\partial(\ln Z)}{\partial F_z}$$

Which is generally true (for any spring)

Exercise: $F_z \ll 1$ (Taylor expansion around F_z), show

→ $F = \left(\frac{3k_B T}{nb^2} \right) R_z + H.O.T \quad (\text{IC recovered})$

As $F_z \rightarrow \infty$, $\coth(*) \rightarrow 1$, and $\langle R_z \rangle \rightarrow nb = L$