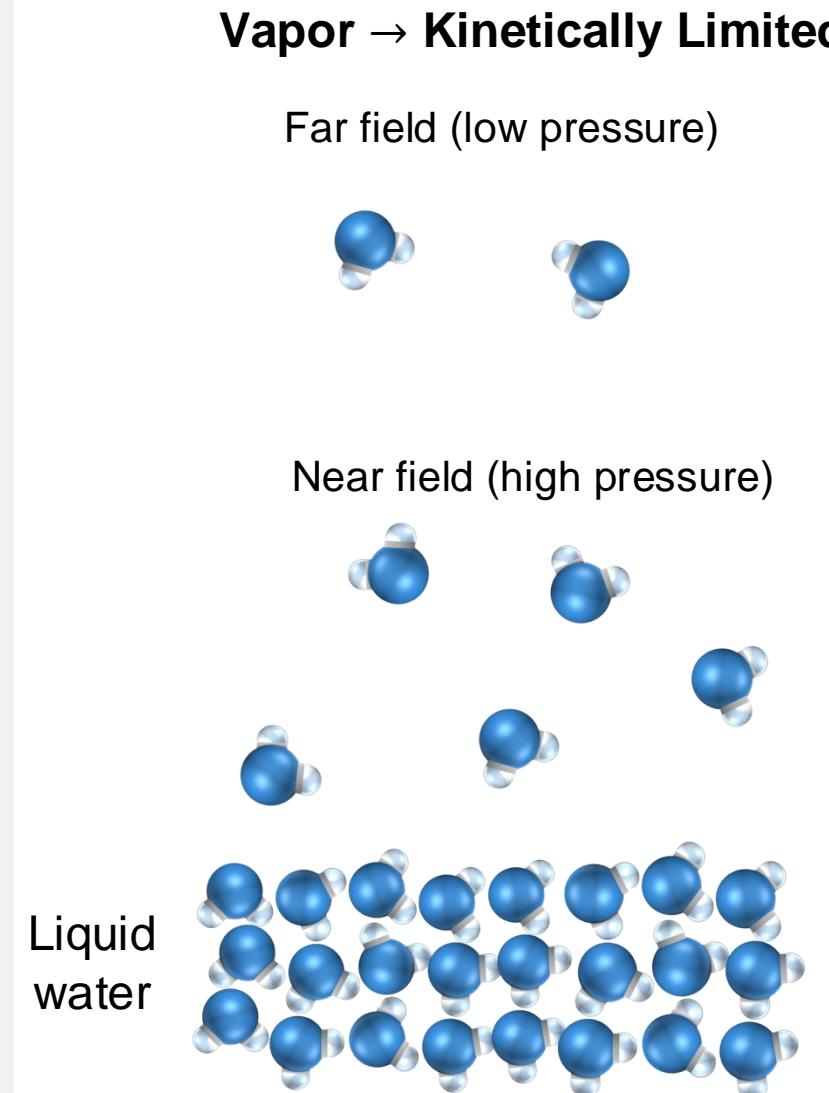
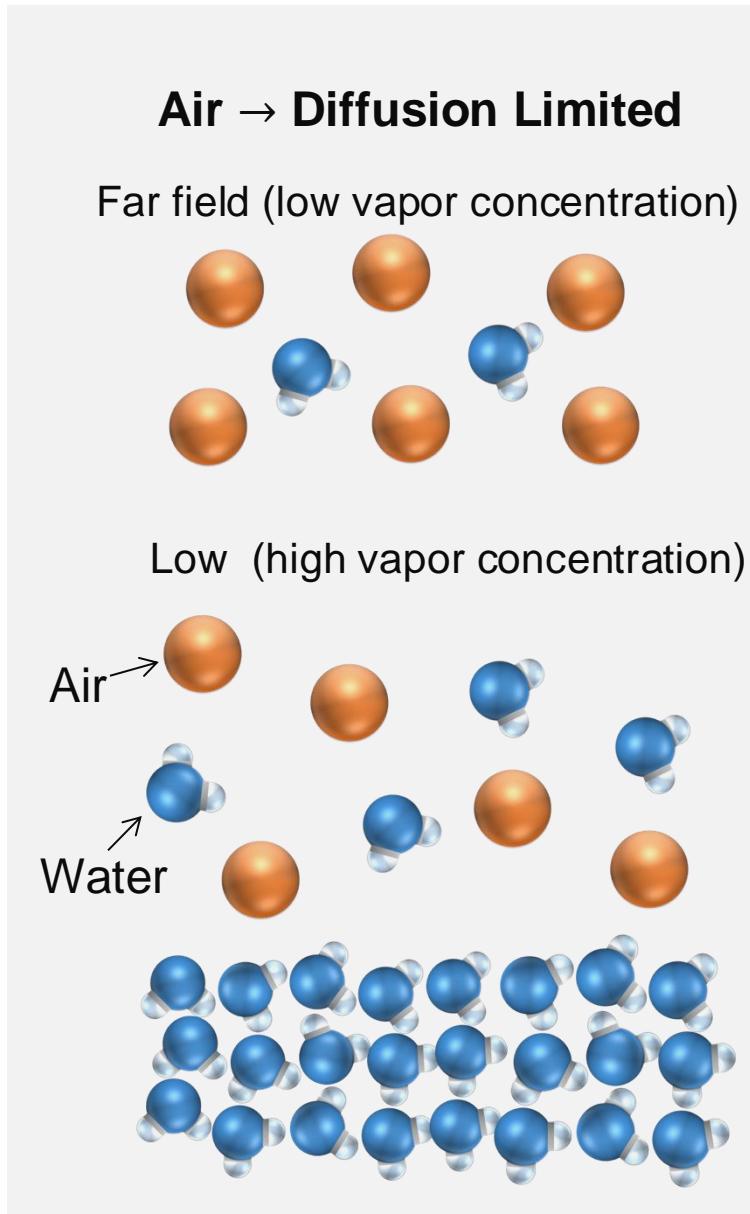


Zhengmao Lu
Energy Transport Advances
Laboratory
EPFL Mechanical Engineering

2024 Fall Semester

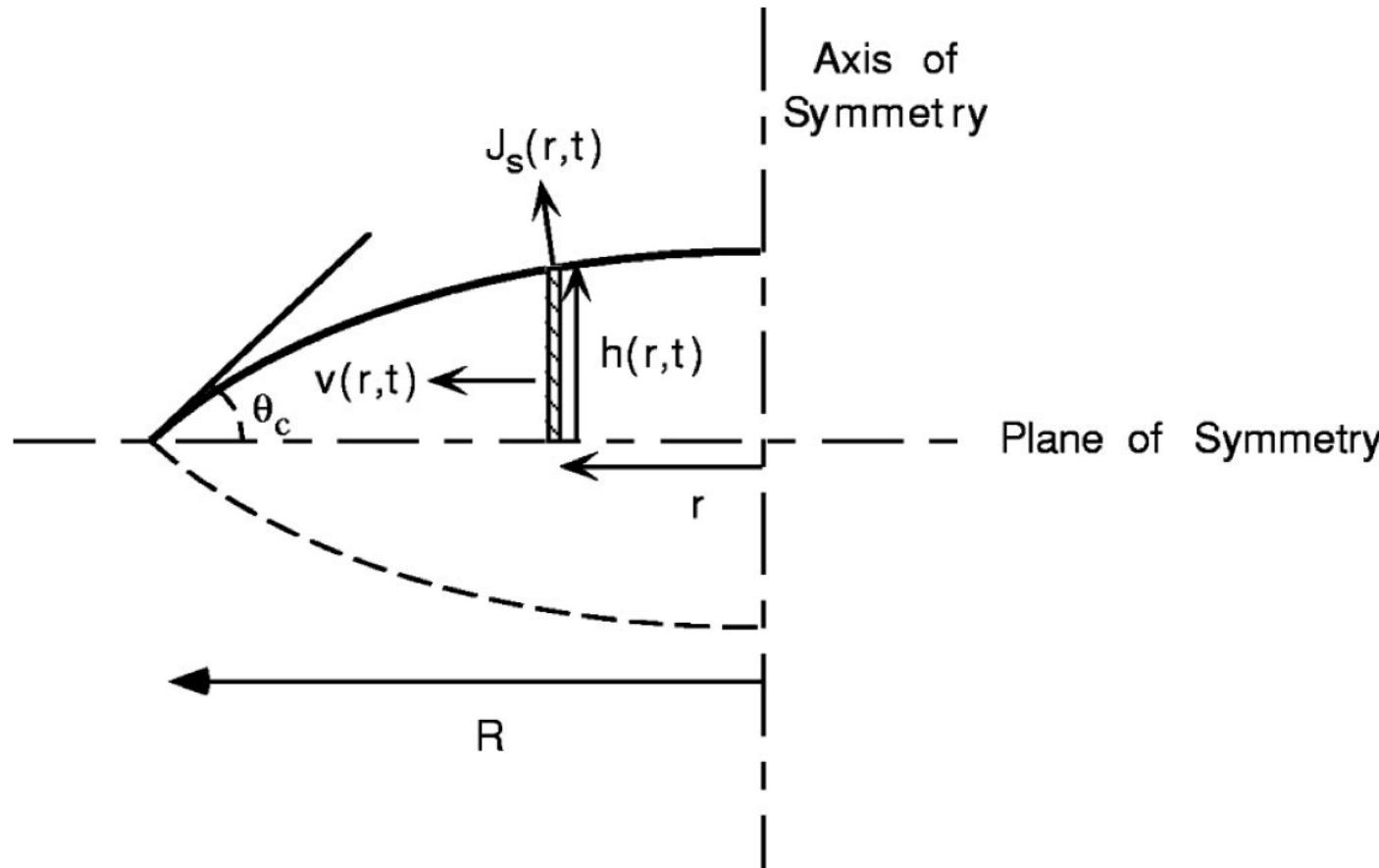
Photo Credit: Trougnouf

Last Week



- Fick's Law of Diffusion
 - Physical meaning of gradient and divergence operators
- Heat and mass transfer analogy
- Coffee ring effects

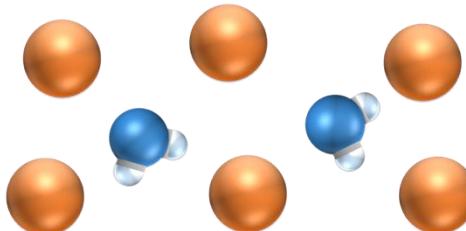
Coffee Ring Effects



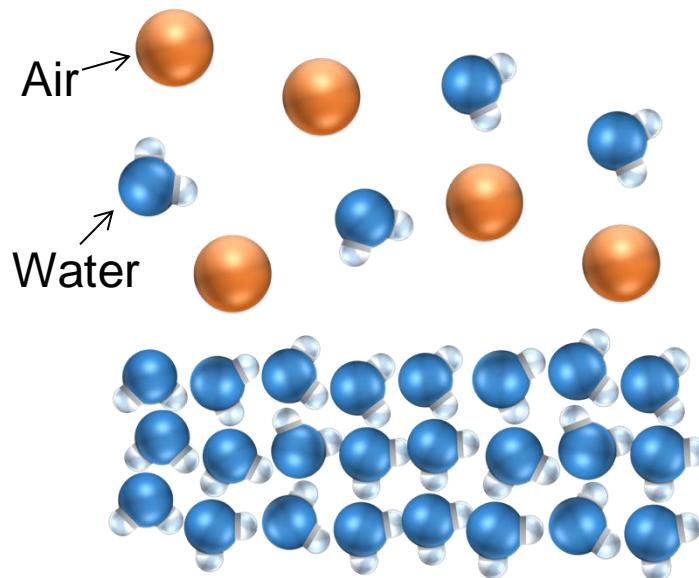
Fundamental Picture of Evaporation

Air → Diffusion Limited

Far field (low vapor concentration)

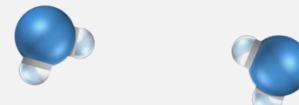


Low (high vapor concentration)

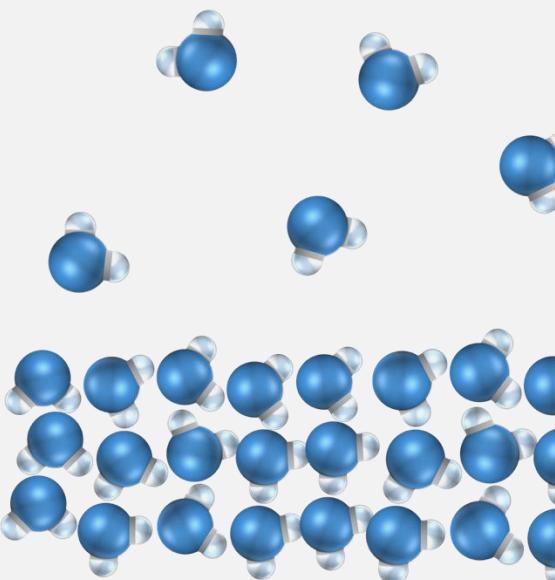


Vapor → Kinetically Limited

Far field (low pressure)



Near field (high pressure)



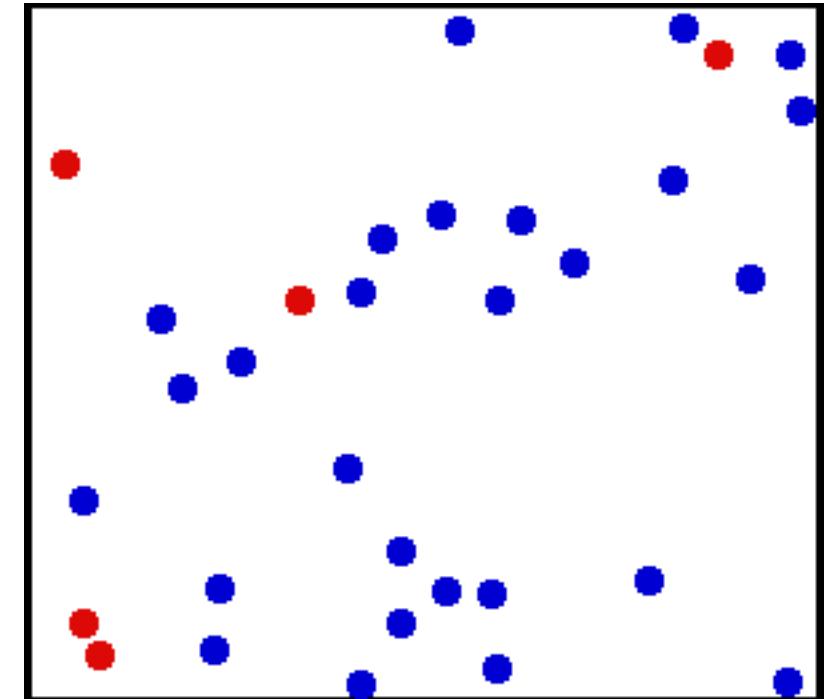
Intended Learning Objectives Today

- Understand basic assumptions of the **kinetic theory of gases**
- Relate **macroscopic quantities** to microscopic molecular motion
- Derive and understand the limit of **Schrage equation** for evaporation

Reading materials: **Carey** Chapter 4.5, Appendix I

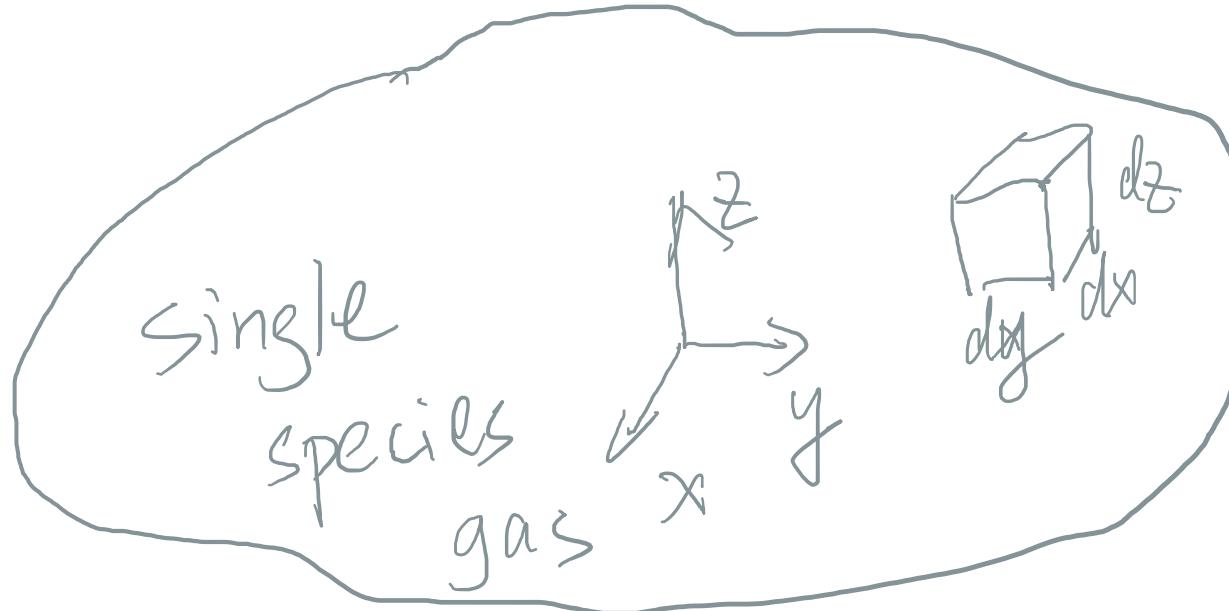
Crash Course on Kinetic Theory of Gases

- Consider gas as a **large number of randomly moving particles** that collide with one another every now and then
- Collisions are elastic: **kinetic energy is conserved** before and after
- Between collisions, particles are not affected by any force field



Credit: A. Greg

Velocity Distribution Function



The fraction of (or the probability of finding) molecules with Cartesian velocities (u, v, w) in the ranges u to $u + du$, v to $v + dv$, w to $w + dw$ in a unit volume is written as

$$\frac{dn_{uvw}}{n} = f(u, v, w) dudvdw$$

n : total number of molecules in a unit volume
 $n = \rho/m$

Velocity Distribution Function

$$\int f(u, v, w) dudv dw = \int \frac{dn_{uvw}}{n} dudv dw = 1$$

f can be seen as a probability density function

Marginal distribution $f_x(u) = \int dv \int dw f(u, v, w)$

f_x is the probability density function for u $\int f_x du = 1$

We can define $f_y(v)$, $f_z(w)$ similarly

Average Properties

Average velocity in x-direction $u_0 = \int f u du dv dw = \int f_x u du$

Similarly, we can define average velocity in y- and z- direction: v_0, w_0

Average kinetic energy $\bar{e}_k = \int f \frac{m}{2} (u^2 + v^2 + w^2) du dv dw$

$$\bar{e}_k = \int f \frac{m}{2} [(u_r + u_0)^2 + (v_r + v_0)^2 + (w_r + w_0)^2] du dv dw$$

u_r, v_r, w_r are relative velocities of each molecule in x-, y-, and z-directions

$$\bar{e}_k = \frac{m}{2} (u_0^2 + v_0^2 + w_0^2) + \int f \frac{m}{2} (u_r^2 + v_r^2 + w_r^2) du dv dw = e_{kb} + \bar{e}_{kr}$$

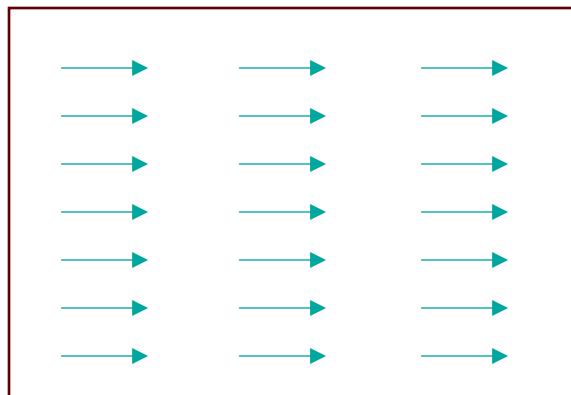
Homework

Temperature in Kinetic Theory

$$\frac{3}{2} k_B T = \bar{e}_{kr}$$

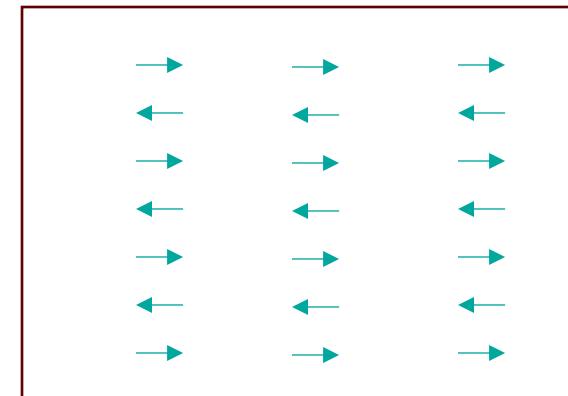
k_B : Boltzmann constant 1.38×10^{-23} [J/K]

Situation A



All molecules moving in the same direction at 10 m/s

Situation B



Higher temperature

Half of the molecules moving in one direction 5 m/s and the other half moving in the opposite direction at 5 m/s

Maxwell-Boltzmann Distribution

$$\frac{dn_{uvw}}{n} = f(u, v, w) dudvdw$$

In equilibrium, f takes a Gaussian form

$$f \propto \exp\left(-\frac{e_k}{k_B T}\right)$$

Kinetic energy of each molecule

$$e_k = \frac{1}{2} m(u^2 + v^2 + w^2)$$

$$\int f dudvdw = 1 \Rightarrow \int C \exp\left(-\frac{m}{2k_B T}(u^2 + v^2 + w^2)\right) dudvdw = 1$$

$$\Rightarrow C = \left(\frac{m}{2\pi k_B T}\right)^{\frac{3}{2}}$$

Check the Gaussian integral $\int e^{-x^2} dx = \sqrt{\pi}$

Maxwell-Boltzmann Distribution

$$f_{MB}(u, v, w) = \left(\frac{m}{2\pi k_B T} \right)^{\frac{3}{2}} \exp \left[-\frac{m}{2k_B T} (u^2 + v^2 + w^2) \right]$$

Marginal M-B distribution in x-direction

$$f_{MBx}(u) = \int dv \int dw f_{MB}(u, v, w) = \left(\frac{m}{2\pi k_B T} \right)^{\frac{1}{2}} \exp \left(-\frac{mu^2}{2k_B T} \right)$$

Similarly, we can obtain $f_{MBy}(v)$, $f_{MBz}(w)$

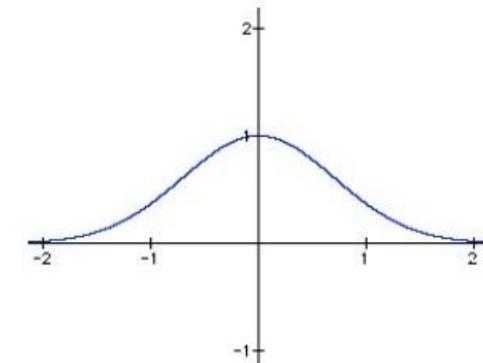
$$f_{MB} = f_{MBx}(u) f_{MBy}(v) f_{MBz}(w)$$

Maxwell-Boltzmann Distribution

In standard M-B distribution

Average velocity in x-direction $u_0 = \int f_{MBx} u du = \int \left(\frac{m}{2\pi k_B T} \right)^{\frac{1}{2}} \exp\left(-\frac{mu^2}{2k_B T}\right) u du = 0$

Odd function times even function



Similarly, $v_0=0, w_0=0$

$$\bar{e}_{kr} = \bar{e}_k = \int f_{MB} \frac{m}{2} (u^2 + v^2 + w^2) du dv dw = \frac{3}{2} k_B T$$

The parameter T we put in the M-B distribution happens to represent temperature

In the case that the vapor is moving at a bulk velocity (u_0, v_0, w_0) , but otherwise is in equilibrium, we can take the frame of reference that moves at the bulk vapor velocity.

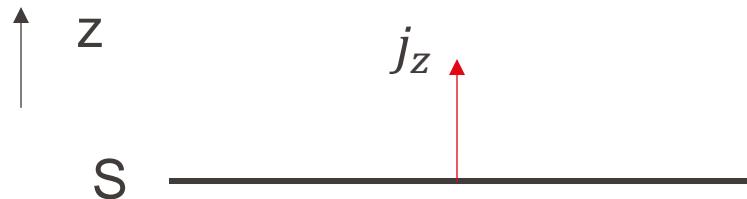
In this reference frame, the bulk vapor is static and M-B applies

$$f(u, v, w) = f_{MB}(u - u_0, v - v_0, w - w_0)$$
$$= \left(\frac{m}{2\pi k_B T} \right)^{\frac{3}{2}} \exp \left[-\frac{m}{2k_B T} ((u - u_0)^2 + (v - v_0)^2 + (w - w_0)^2) \right]$$

Marginal distribution $f_x(u) = \int dv \int dw f(u, v, w) = f_{MBx}(u - u_0)$

$$u_0 = \int f_x u du = \int u f_{MBx}(u - u_0) du \quad \text{Consistent}$$

Mass Flux Across a Surface



How to determine the molecular flux across a surface if the velocity distribution function is known

j_z : the rate at which molecules pass through surface S per unit area

What matters is velocity distribution in the direction perpendicular to the surface $f_z(w)dw$

The molecular flux due to molecules with z-velocity between w and $w+dw$ is $nf_z(w)dw \cdot w$

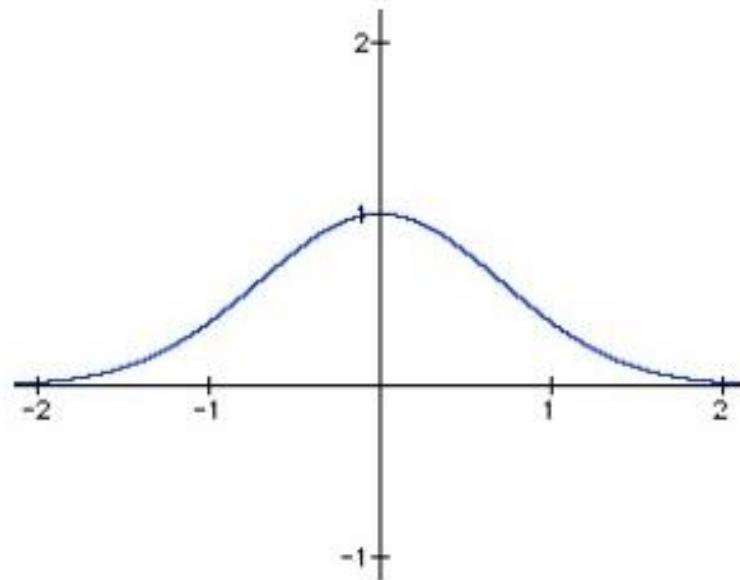
$$j_z = n \int f_z(w) w dw$$

$$\text{Mass flux } m_z'' = m j_z = \rho \int f_z(w) w dw$$

For standard M-B, $m_z'' = 0$

For drifted M-B, $m_z'' = \rho w_0$

One Way Mass Flux



With symmetric velocity distribution such as M-B, although the net molecular flux is zero is zero, there are two one-way molecular fluxes negating each other.

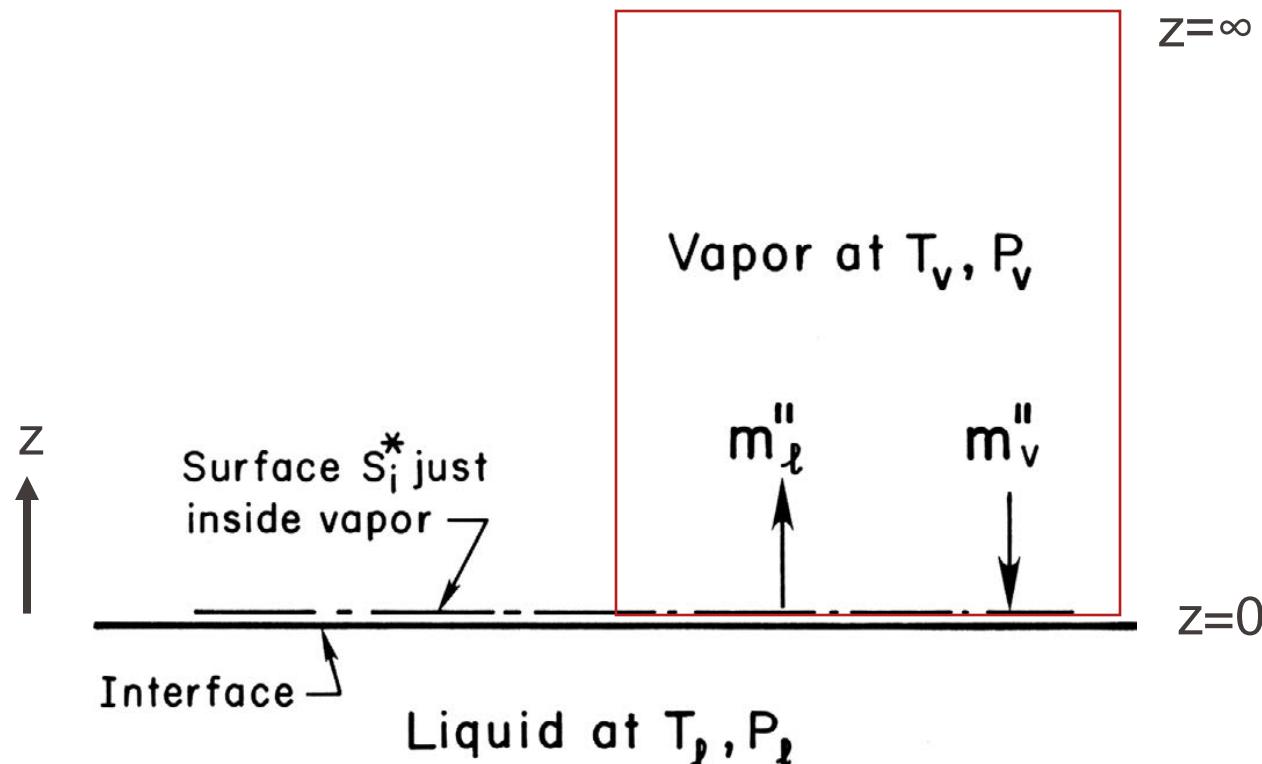
For standard M-B

$$j_{z^+} = \int_0^{\infty} n f_{MBz} w dw = \int_0^{\infty} n \left(\frac{m}{2\pi k_B T} \right)^{\frac{1}{2}} \exp \left(-\frac{mw^2}{2k_B T} \right) w dw = n \left(\frac{k_B T}{2\pi m} \right)^{\frac{1}{2}} [m/s]$$

$$j_{z^-} = -j_{z^+}$$

$$m''_{z^+} = \rho \left(\frac{k_B T}{2\pi m} \right)^{\frac{1}{2}}$$

Liquid-Vapor Interfacial Transport



Far away from the surface

$$\rho_v = \frac{P_v}{R T_v} \quad R: \text{specific gas constant}$$

$$R = \frac{k_B}{m}; \quad R = \frac{\bar{R}}{M}; \quad \bar{R} = k_B N_A$$

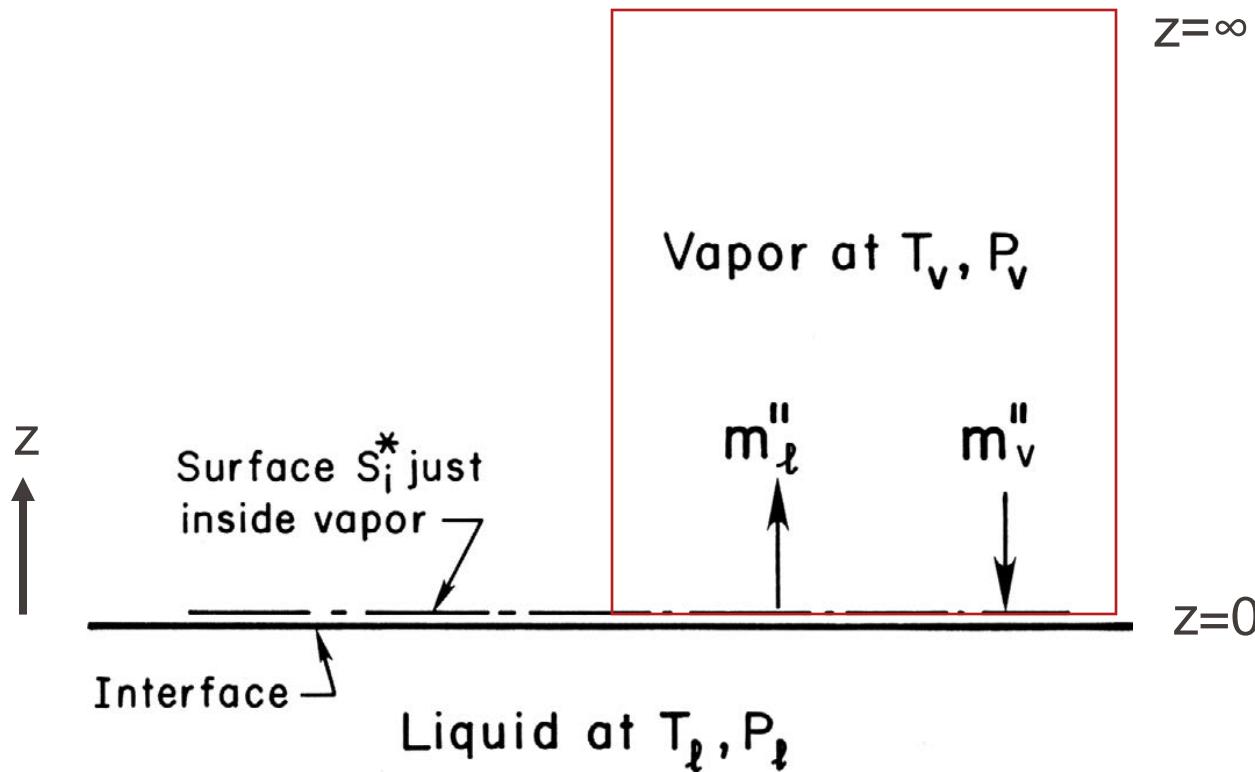
$$f_\infty = f_{MB}(u, v, w - w_0) \Big|_{T_v}$$

$$= \left(\frac{m}{2\pi k_B T_v} \right)^{\frac{3}{2}} \exp \left[-\frac{m}{2k_B T_v} (u^2 + v^2 + (w - w_0)^2) \right]$$

z-direction opposite to Figure 4.10 in Carey

w_0 unknown bulk vapor velocity at $z=\infty$; mass flux in the system $\rho_v w_0$

Liquid-Vapor Interfacial Transport



At surface S_i^* , m'' is due to
1) molecules emitted from liquid surface

$$m''_e = \hat{\sigma}_e \rho_e \left(\frac{k_B T_l}{2\pi m} \right)^{\frac{1}{2}}$$

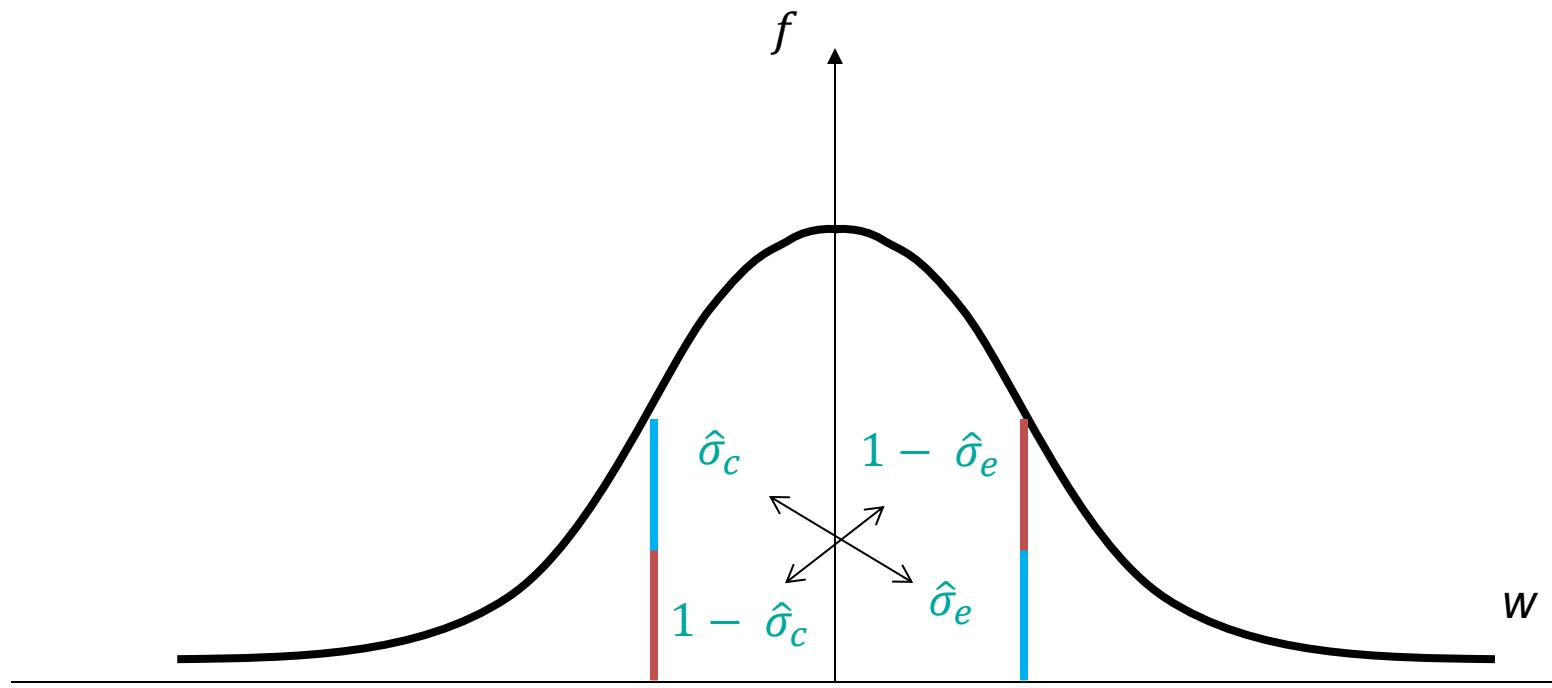
$$\rho_e = P_l / RT_l$$

(one-way flux from equilibrium vapor at $z = 0$, with evaporation coefficient $\hat{\sigma}_e$)

2) vapor molecules reflected from liquid surface $(1 - \hat{\sigma}_c) |m''_v|$

$\hat{\sigma}_c$: condensation coefficient/probability

Evaporation/Condensation Coefficient

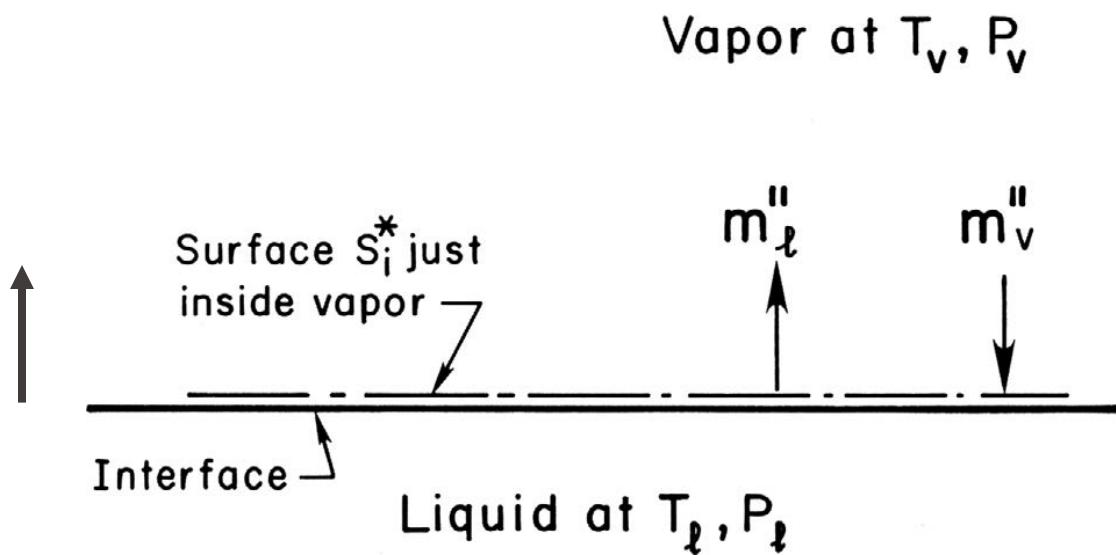


In equilibrium, $\hat{\sigma}_c = \hat{\sigma}_e = \hat{\sigma}$

Accommodation coefficient

Analogous to Kirchhoff's law, emissivity = absorptivity

Hertz-Knudsen Equation



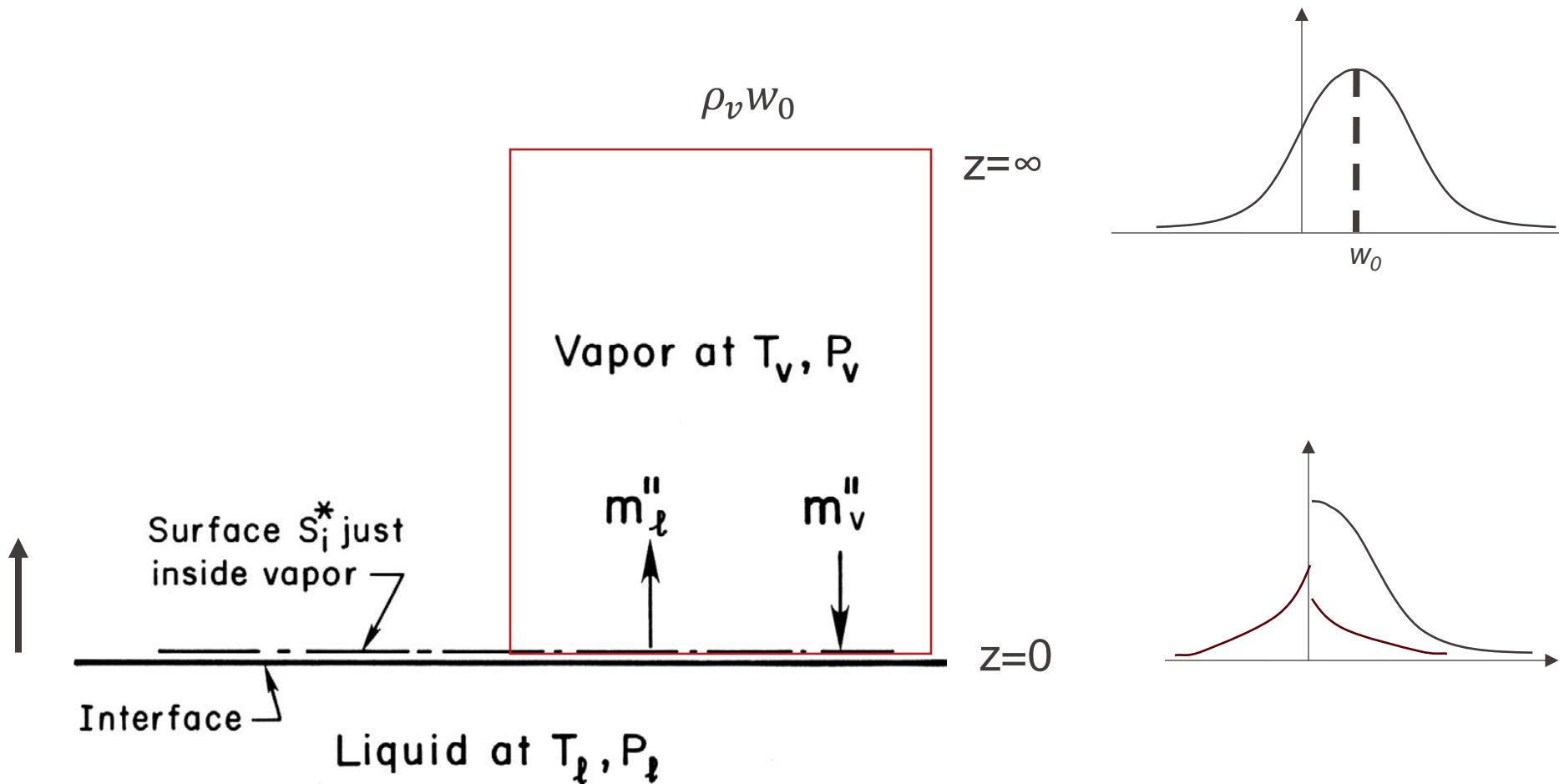
$$|m_v''| = \rho_v \left(\frac{k_B T_v}{2\pi m} \right)^{\frac{1}{2}}$$

$$m_l'' = \hat{\sigma}_e m_e'' + (1 - \hat{\sigma}_c) |m_v''|$$

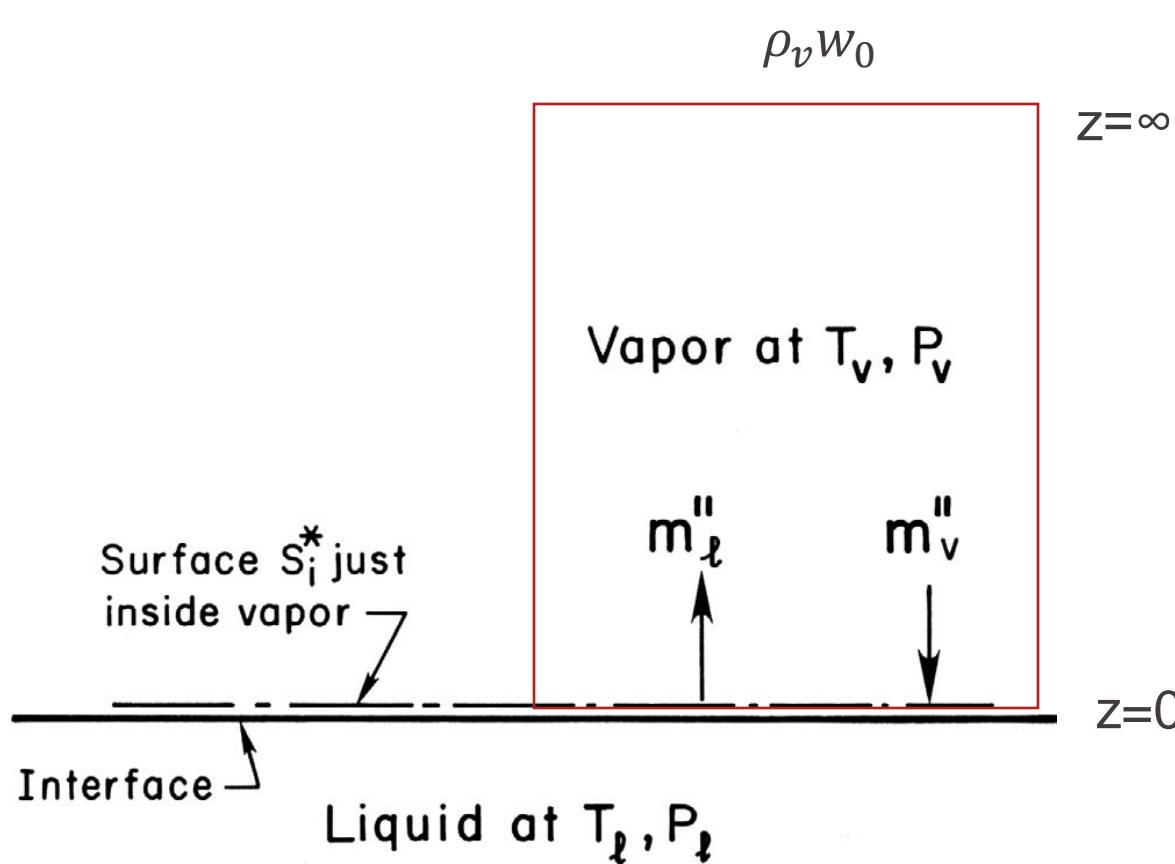
$$m_{net}'' = m_l'' - m_v'' = \hat{\sigma}_e m_e'' - \hat{\sigma}_c |m_v''|$$

$$[m_{net}'']_{HK} = \hat{\sigma}_e \rho_e \left(\frac{k_B T_l}{2\pi m} \right)^{\frac{1}{2}} - \hat{\sigma}_c \rho_v \left(\frac{k_B T_v}{2\pi m} \right)^{\frac{1}{2}}$$

Key Assumption in Schrage Equation



$$m_v'' = -m \int_{-\infty}^0 n_{\infty} f_{\infty z} w dw = \rho_v \int_{-\infty}^0 \left(\frac{m}{2\pi k_B T_v} \right)^{\frac{1}{2}} \exp \left(-\frac{m(w - w_0)^2}{2k_B T_v} \right) w dw = m_v''(w_0)$$



Mass balance

$$m_l'' - m_v'' = \rho_v w_0$$

$$\begin{aligned} m_l'' &= \hat{\sigma} m_e'' + (1 - \hat{\sigma}) m_v'' \\ &= \hat{\sigma} \frac{P_l}{RT_l} \left(\frac{k_B T_l}{2\pi m} \right)^{\frac{1}{2}} + (1 - \hat{\sigma}) m_v''(w_0) \end{aligned}$$

$$\hat{\sigma} \frac{P_l}{RT_l} \left(\frac{k_B T_l}{2\pi m} \right)^{\frac{1}{2}} - \hat{\sigma} m_v''(w_0) = \rho_v w_0$$

Solve for w_0

$$q_{evap}'' = \rho_v w_0 h_{lv}$$

Schrage Equation

When $\frac{1}{2} mw_0^2 \ll k_B T_v$, the evaporation heat flux can be written in a closed form

$$q''_{evap} = \left(\frac{2\hat{\sigma}}{2 - \hat{\sigma}} \right) h_{lv} (2\pi R)^{-\frac{1}{2}} \left(\frac{P_l}{\sqrt{T_l}} - \frac{P_v}{\sqrt{T_v}} \right)$$

z-direction defined differently from Carey

When $\hat{\sigma} = 0$, liquid surface is like an impermeable wall and there is no evaporation

Additional comment: Schrage's assumption about the velocity distribution has implications in energy and momentum balance/imbalance as well (which will result in three equations with one unknown, causing inconsistencies)

- Understand basic assumptions of the **kinetic theory of gases**
- Relate **macroscopic quantities** to microscopic molecular motion
- Derive and understand the limit of **Schrage equation** for evaporation

Reading materials: **Carey** Chapter 4.5, Appendix I