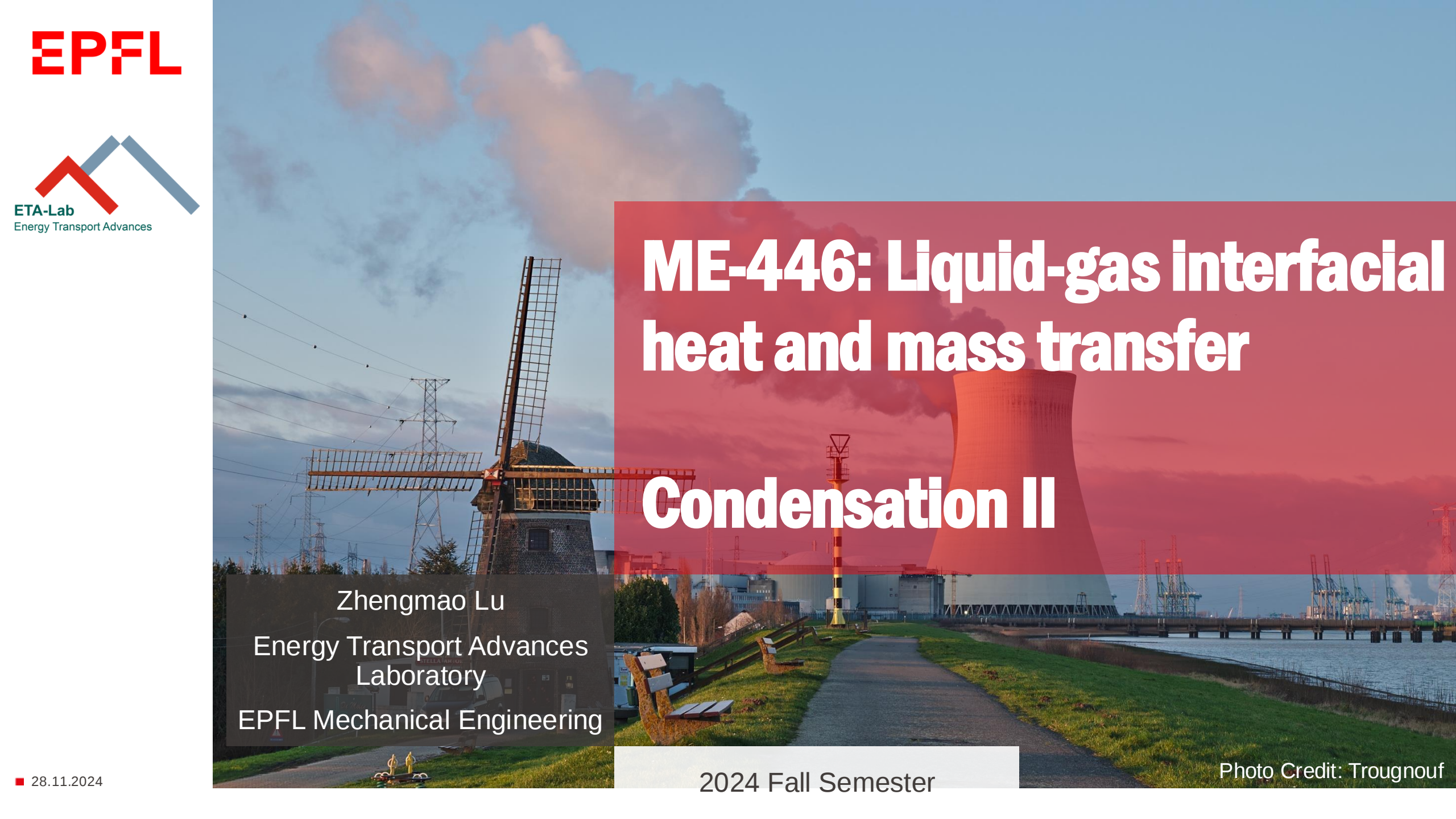


The background image is a composite. The left side shows a traditional wooden windmill with a lattice-structured sail, situated in a grassy field with power lines in the background. The right side shows a large industrial cooling tower emitting a plume of white steam, with a body of water and industrial cranes in the distance. A semi-transparent red rectangle is overlaid on the right side, containing the main title text.

ME-446: Liquid-gas interfacial heat and mass transfer

Condensation II

Zhengmao Lu
Energy Transport Advances
Laboratory
EPFL Mechanical Engineering

2024 Fall Semester

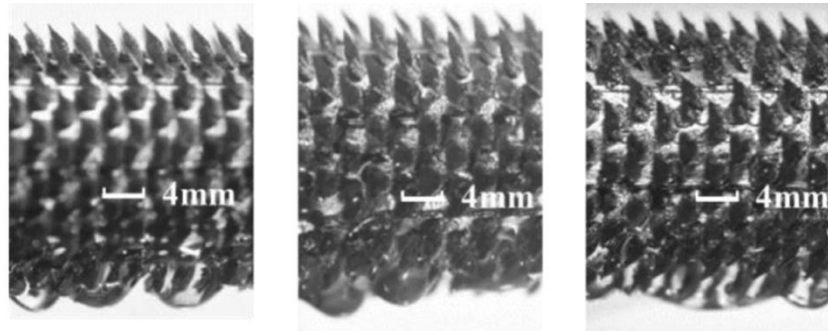
Photo Credit: Trougnouf

- Nucleation in condensation
- Rose's analysis of dropwise condensation
- Nusselt's analysis of filmwise condensation

Intended Learning Objective Today

- Typical condensation enhancement strategies
- Jumping-droplet condensation
- Design principles for lubricant infused surface
- Effect of noncondensable gases

Finned Tube Condenser



Gu et al., *International Journal of Heat and Mass Transfer* 2020

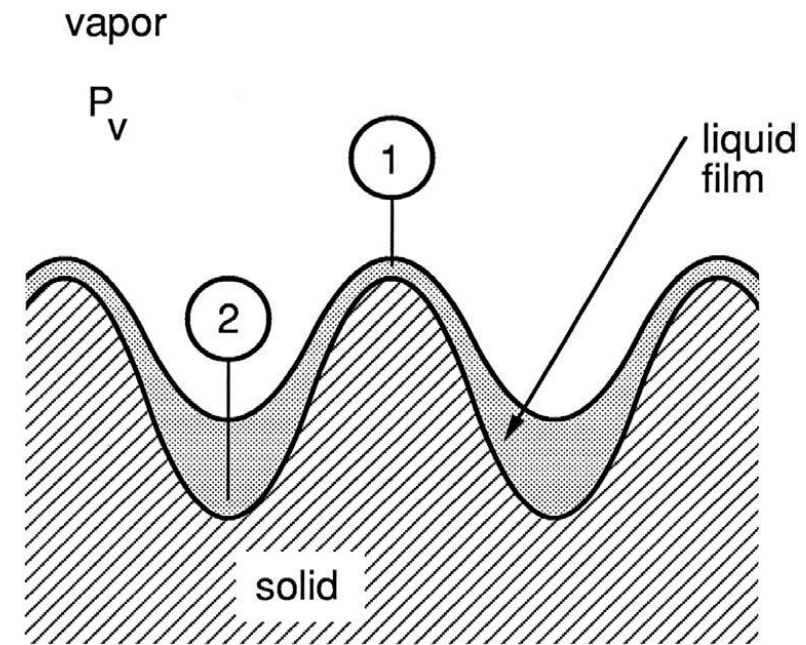
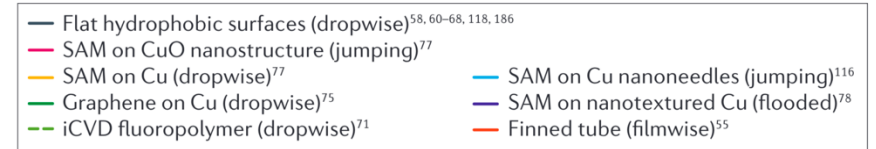
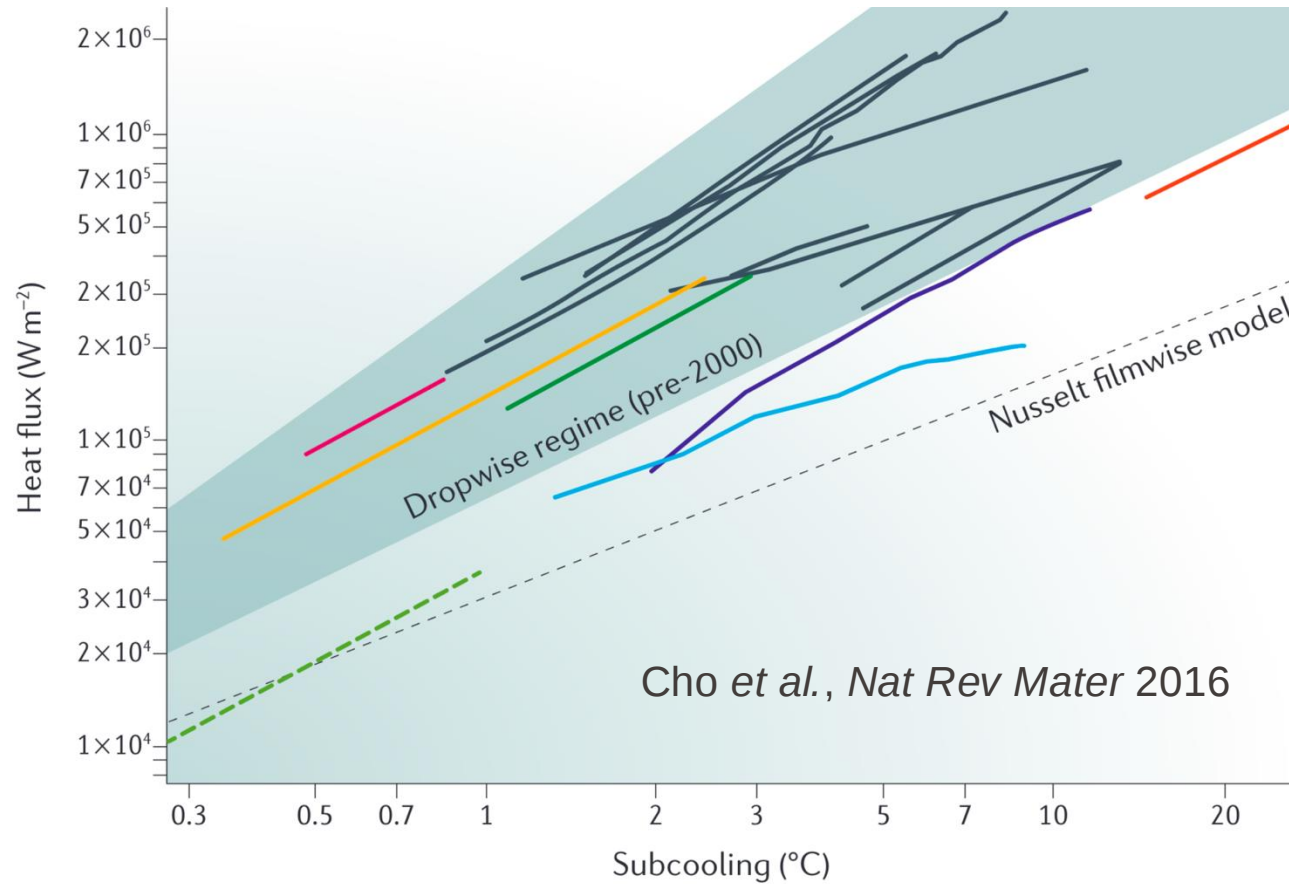
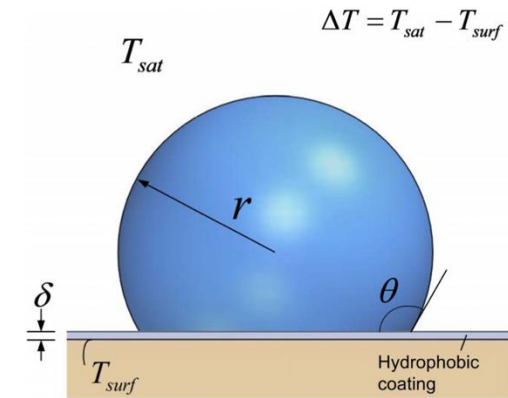


FIGURE 9.26 in Carey

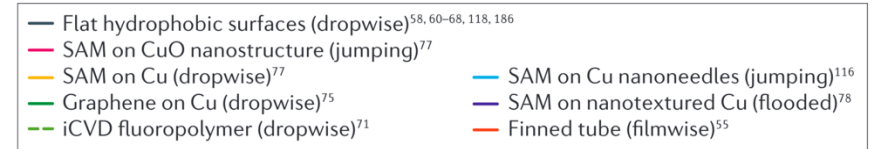
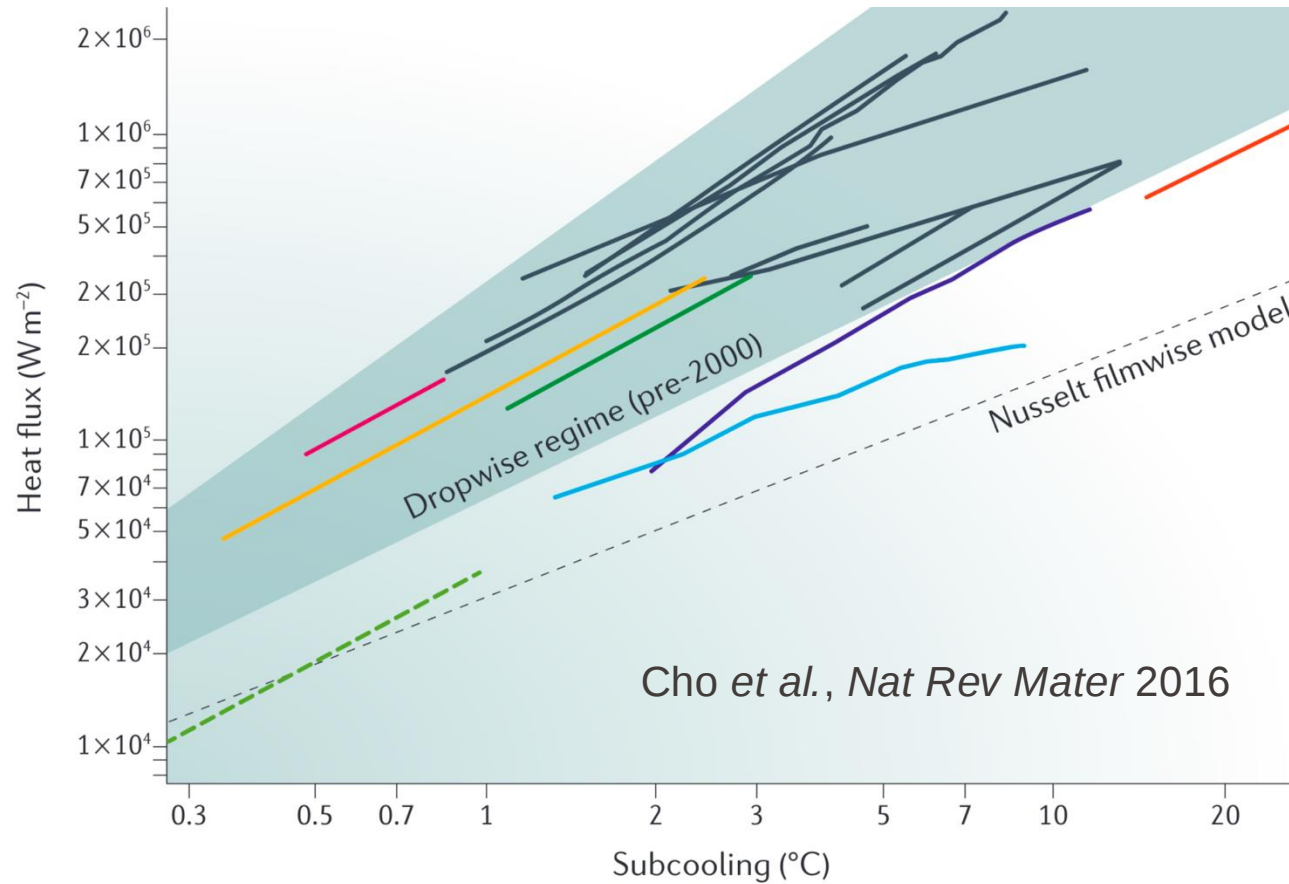
Increase condensation heat transfer area



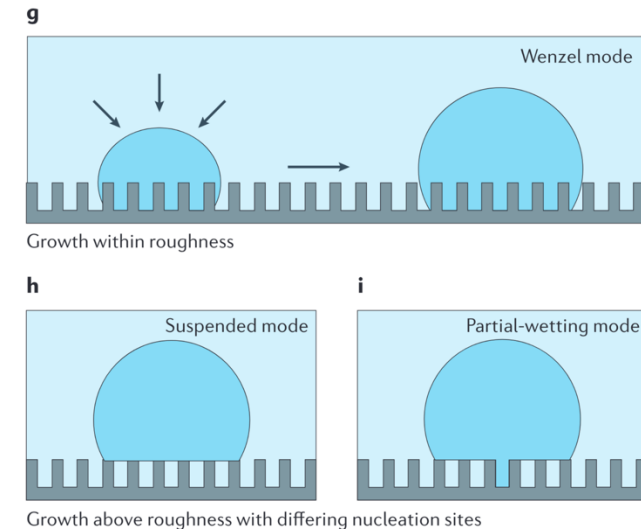
Flat Hydrophobic Coating



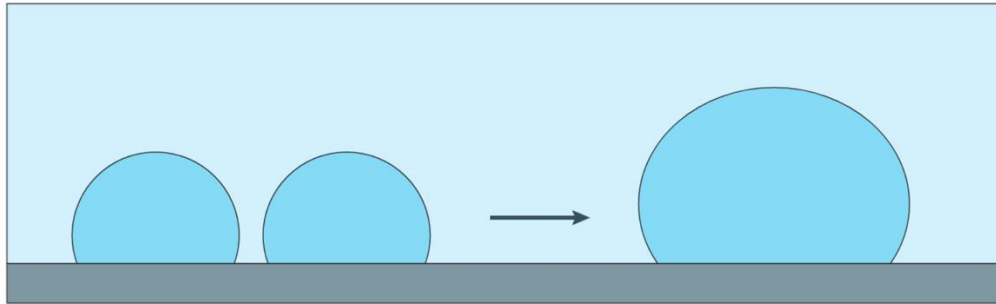
- Increase contact angle and decrease contact angle hysteresis
- Contact angle cannot be too large, otherwise not enough contact area for heat transfer



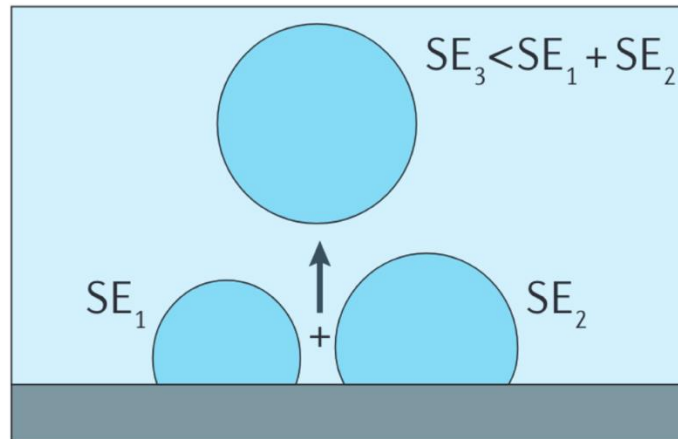
Surface Structure + Hydrophobic Coating



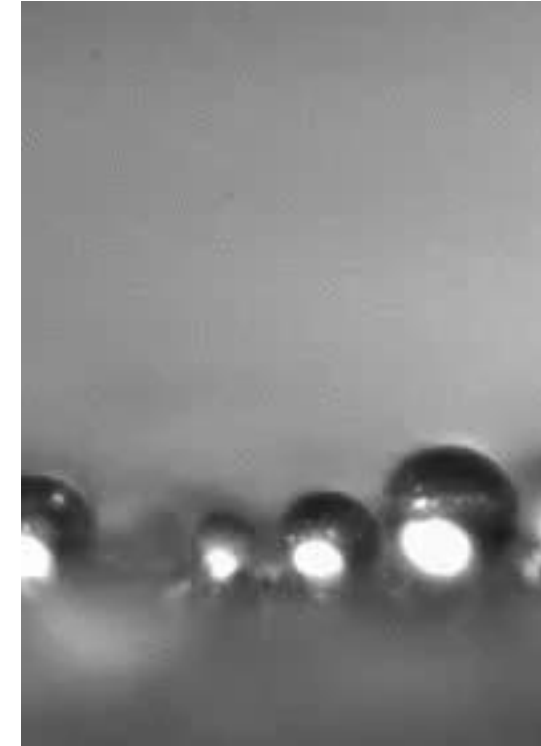
Potential flooding issue due to too many nucleation sites



Coalescence

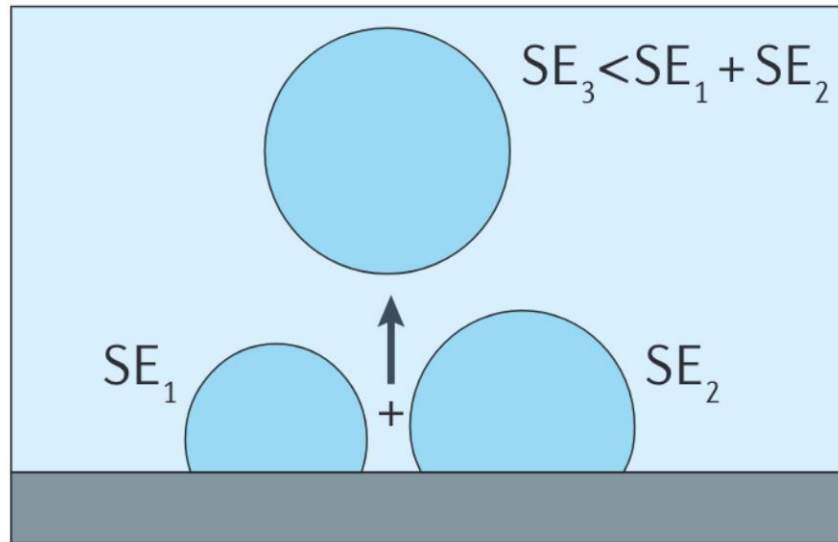


Coalescence departure



<https://doi.org/10.1103/PhysRevLett.103.184501>

Jumping Droplet Condensation



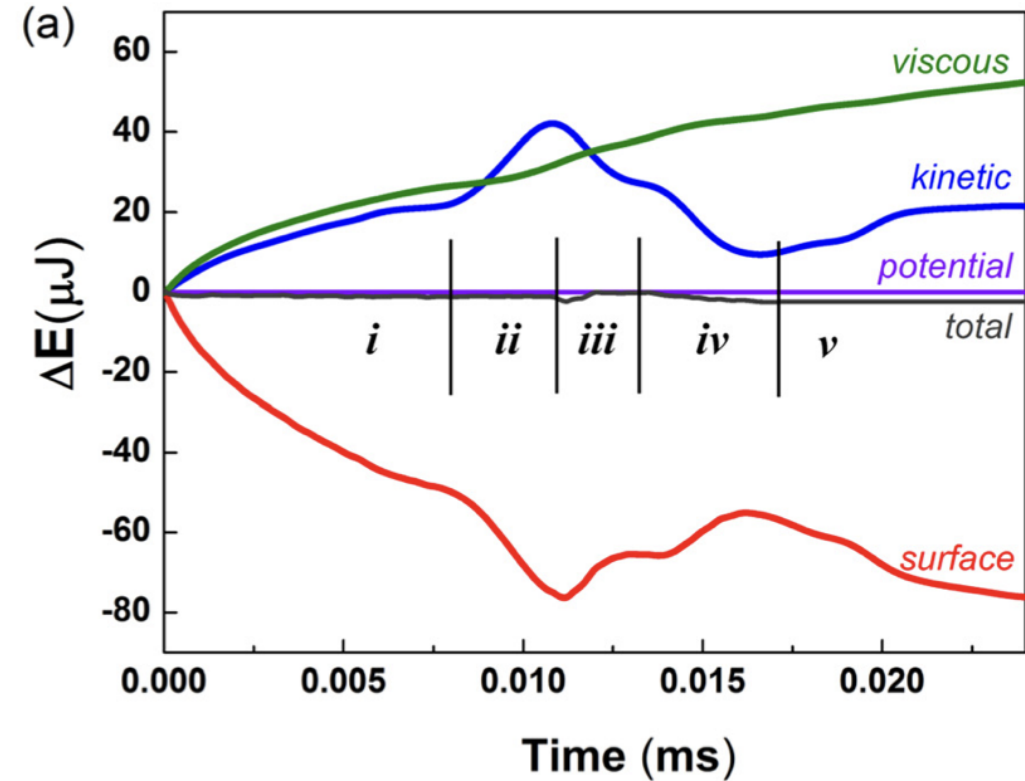
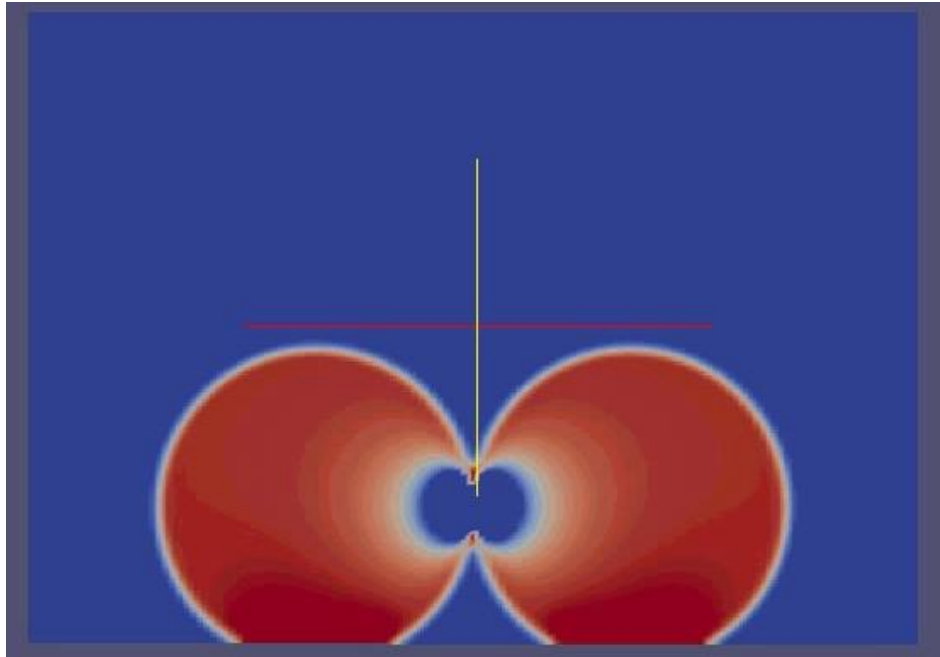
Coalescence departure

$$\Delta E_s \sim \sigma \Delta A \sim \sigma R^2$$

$$KE \sim \frac{1}{2} \rho R^3 U^2$$

$$U \sim \sqrt{\frac{\sigma}{\rho R}}$$

Viscous dissipation ignored



Appl. Phys. Lett. 103, 161601 (2013)

Only possible when the surface is superhydrophobic

Distribution of Droplet Radii in Dropwise Condensation

- Probability density function

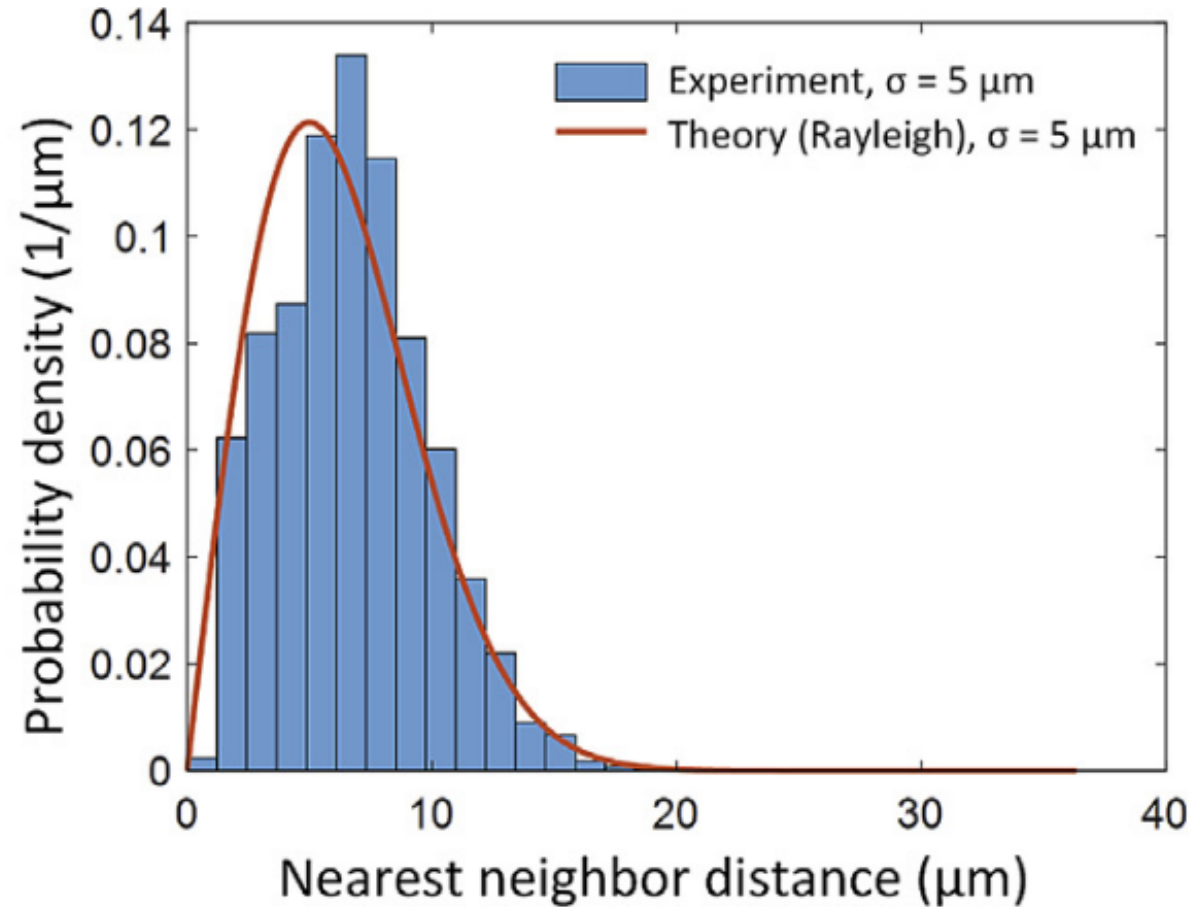
$$A(r) = \frac{r^{-2/3}}{3r_{max}^{1/3}} \quad r_{max} = K_3 \sqrt{\frac{\sigma}{\rho g}} \quad \text{for } r_e < r \leq r_{max}$$

Average droplet radius

$$h_{dc} = \frac{1}{\Delta T_t} \int_{r_e}^{r_{max}} \frac{q_d}{2\pi r^2} A(r) dr$$

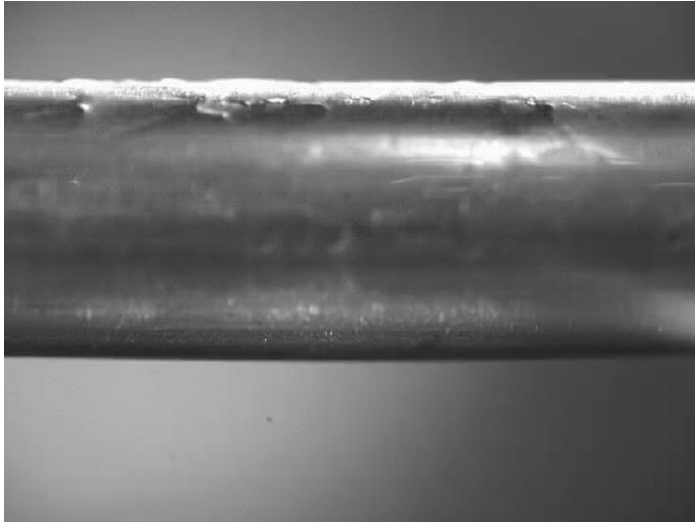
$$\bar{r} = \int_{r_e}^{r_{max}} r A(r) dr \approx \frac{1}{4} r_{max} \sim 300 \mu m$$

Distribution for Jumping Droplet Condensation



Since contacting neighboring droplet will cause jumping removal, droplet radius should be around half the nearest neighbor distance

Jumping-droplet mode will result in smaller average droplet sizes on the surface and better heat transfer

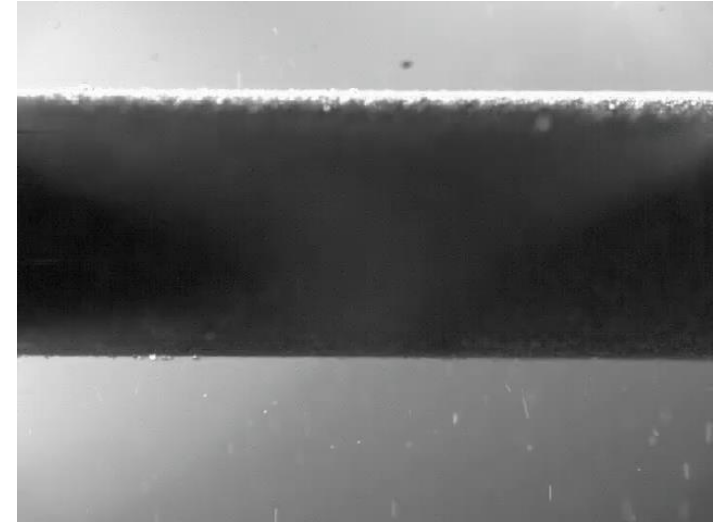


Filmwise condensation



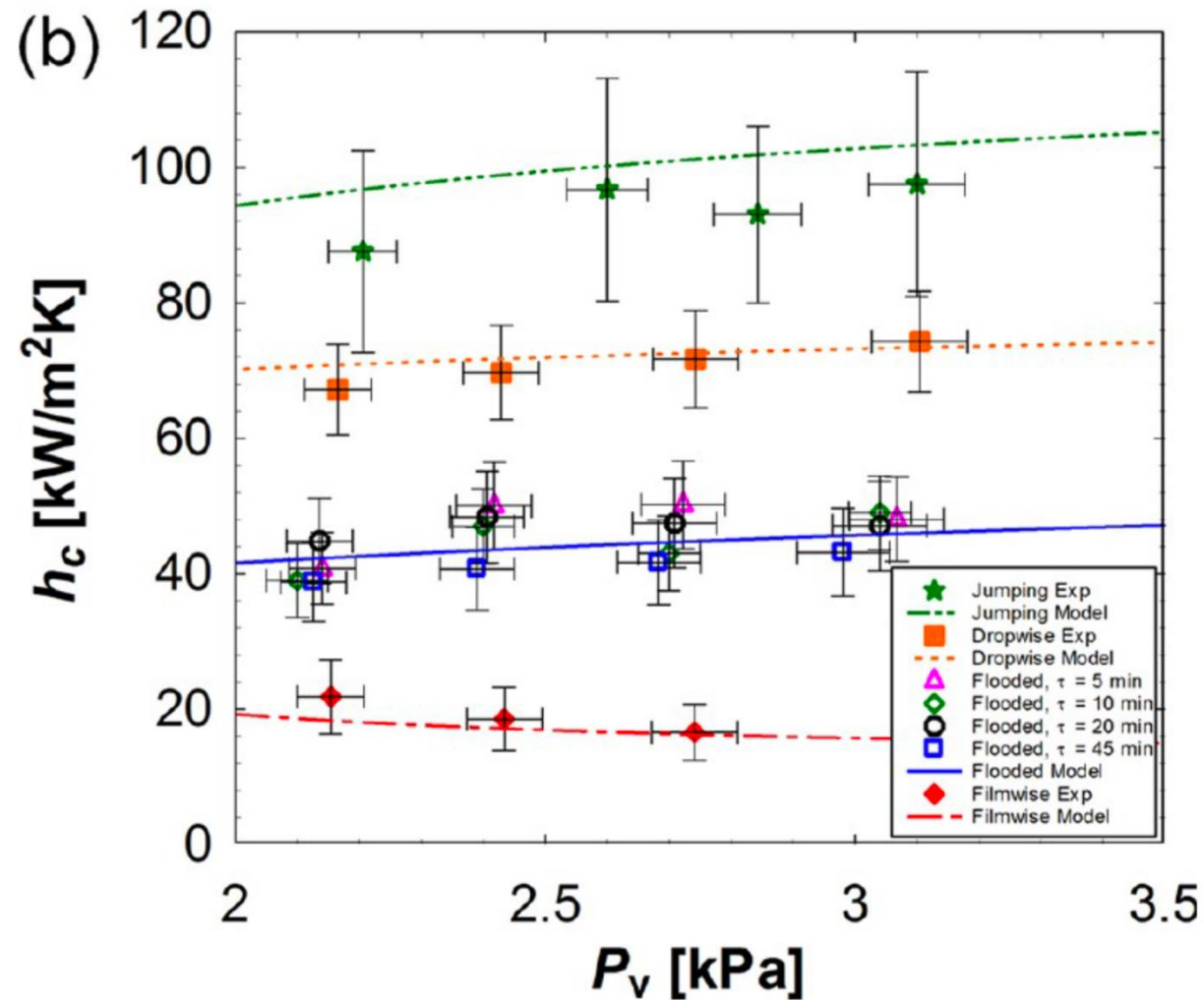
Dropwise condensation

Superhydrophobic surface



Jumping-droplet
condensation

Miljkovic *et al.*, *Nano Lett.* (2013)



Jumping-droplet

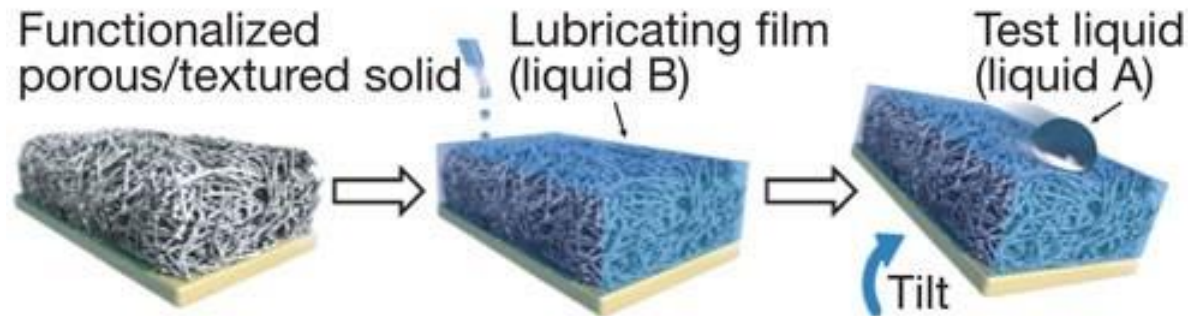
>

Dropwise

>

Filmwise

Lubricant Infused Surface (LIS)



Nature volume 477, pages 443–447 (2011)



Spreading Coefficient

$$S_{xy} = \gamma_y - (\gamma_{xy} + \gamma_x)$$

$S_{xy} \geq 0$ implies x can spread on y

(I) $S_{ld} \not\geq 0$, cloaking (II) $S_{dl} \not\geq 0$, spreading



(III) $S_{ls} \not\geq -\gamma_l R$ (IV) $S_{ls(d)} \not\geq -\gamma_{dl} R$



(V) $\gamma_{dl} \not\geq 0$, miscible



Legend:

- Impinging Droplet
- Lubricant
- Solid Surface

Possible ways to fail

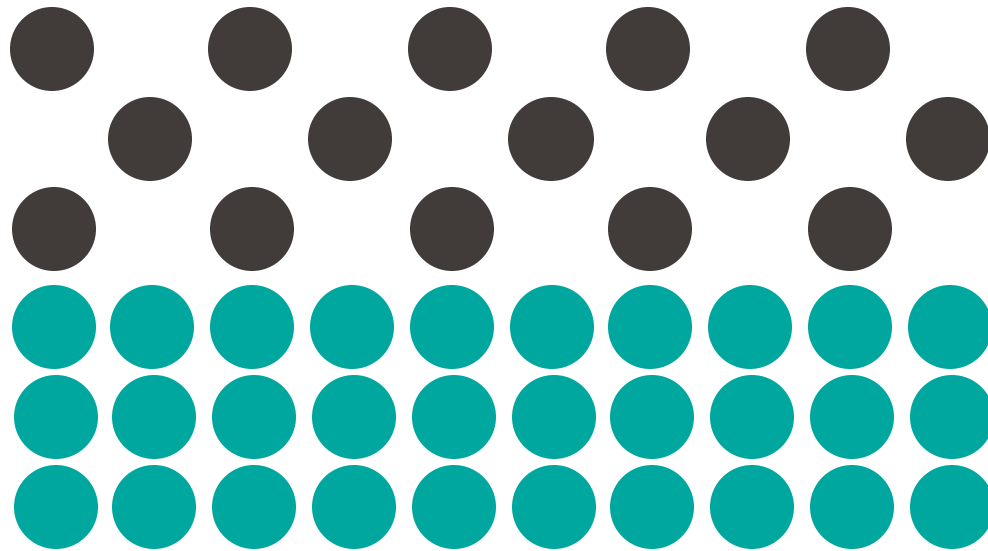
(I) Lubricant cloaking $S_{ld} \geq 0$

(II) Droplet spreading $S_{dl} \geq 0$

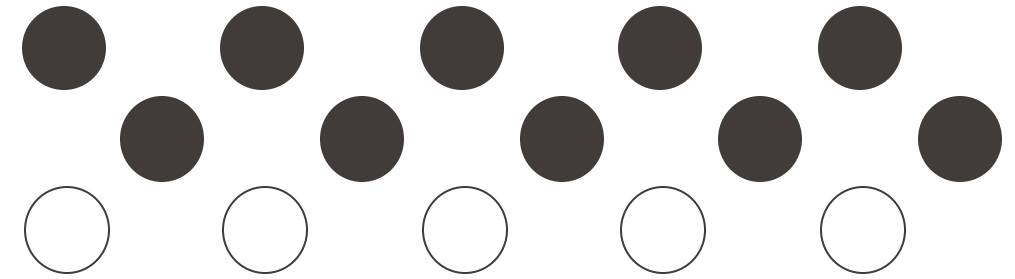
(III) No infusing $S_{ls} \leq \frac{r-1}{r-\phi} \gamma_l$

(IV) No infusing $S_{ls(d)} \leq \frac{r-1}{r-\phi} \gamma_{dl}$

(V) Miscible

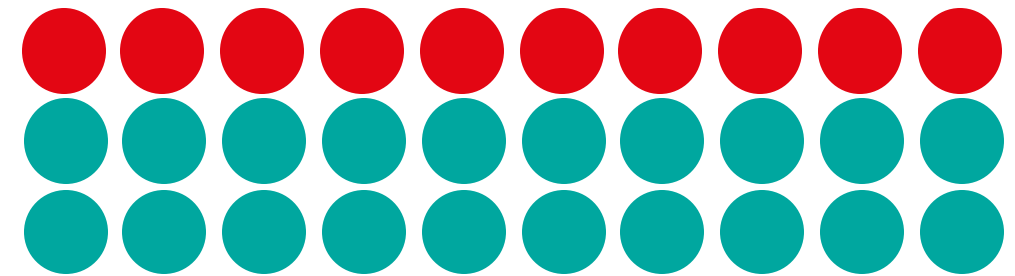


w_{ab}



σ_b

σ_a



$$\sigma_{ab} = \sigma_a + \sigma_b - w_{ab}$$

w_{ab} depends on intermolecular interactions

van Oss, Chaudhury, and Good (vOCG Model)

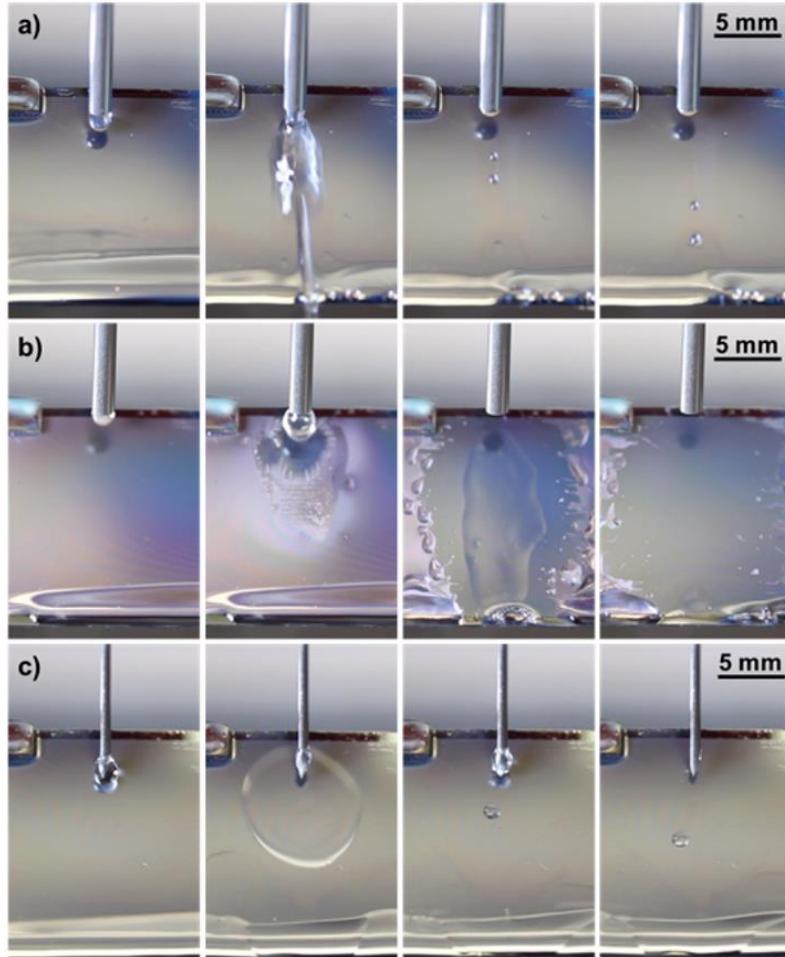
Langmuir 1992,8, 2877-2879

$$\gamma_A^{tot} = \gamma_A^{LW} + 2\sqrt{\gamma_A^+ \gamma_A^-}$$

$$\gamma_{AB}^{tot} = \gamma_A^{LW} + \gamma_B^{LW} - 2\sqrt{\gamma_A^{LW} \gamma_B^{LW}} + 2\sqrt{\gamma_A^+ \gamma_A^-} + 2\sqrt{\gamma_B^+ \gamma_B^-} - 2\sqrt{\gamma_A^+ \gamma_B^-} - 2\sqrt{\gamma_B^+ \gamma_A^-}$$

Phenomenological, Lifshitz-van der Waals component + polar component

Metallic interactions not considered



Diiodomethane (CH_2I_2) dropped onto a LIS of methanol infused in SiO_2 pillar

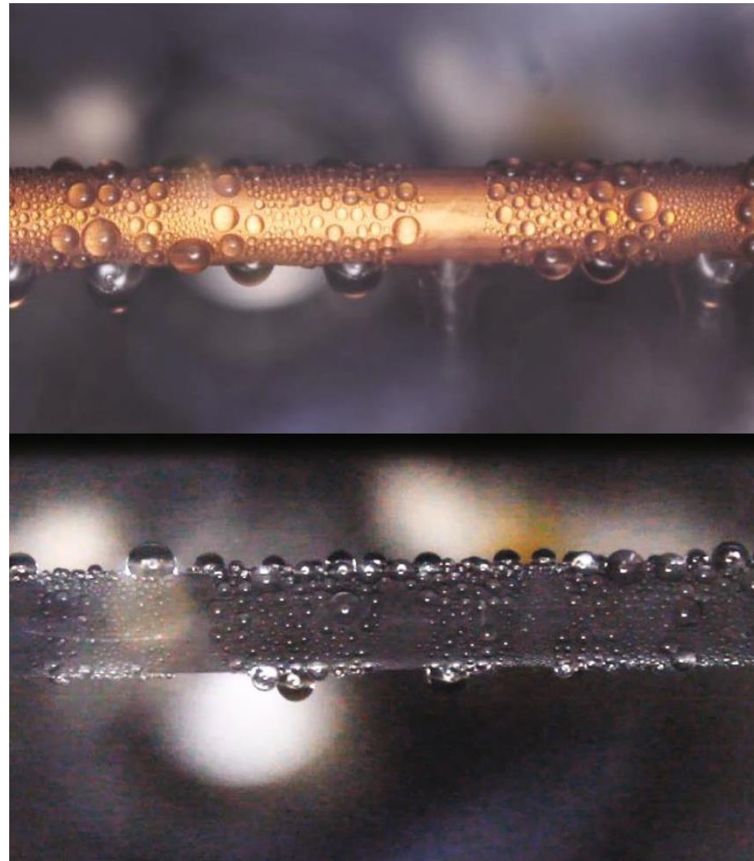
Methanol dropped onto a LIS of diiodomethane infused in SiO_2 pillar

Heptane dropped onto a LIS of methanol infused in SiO_2 pillars

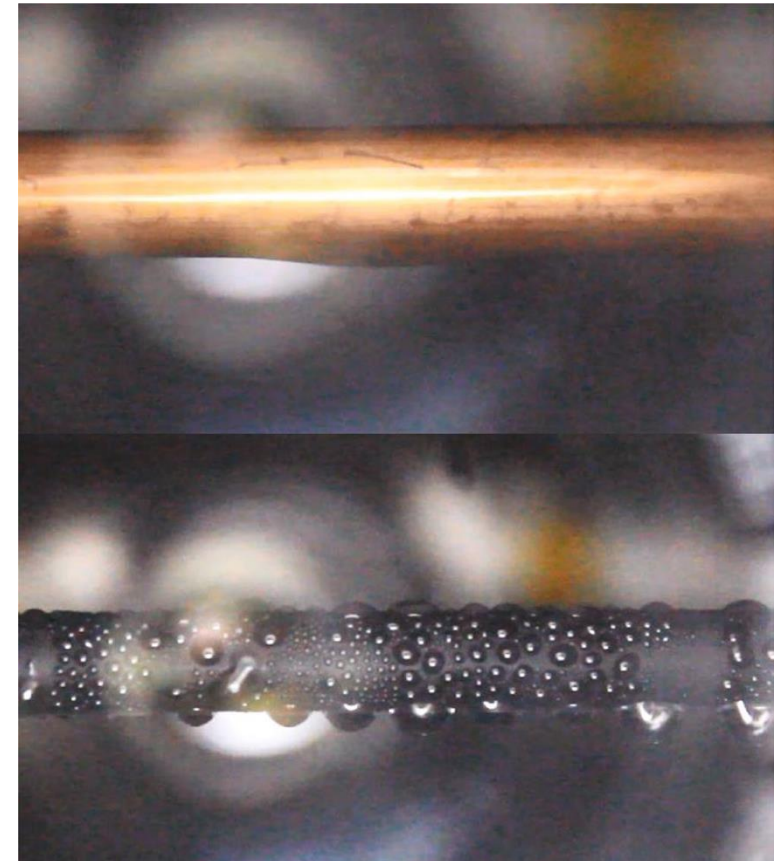
Water (72 mN/m)

Toluene (28 mN/m)

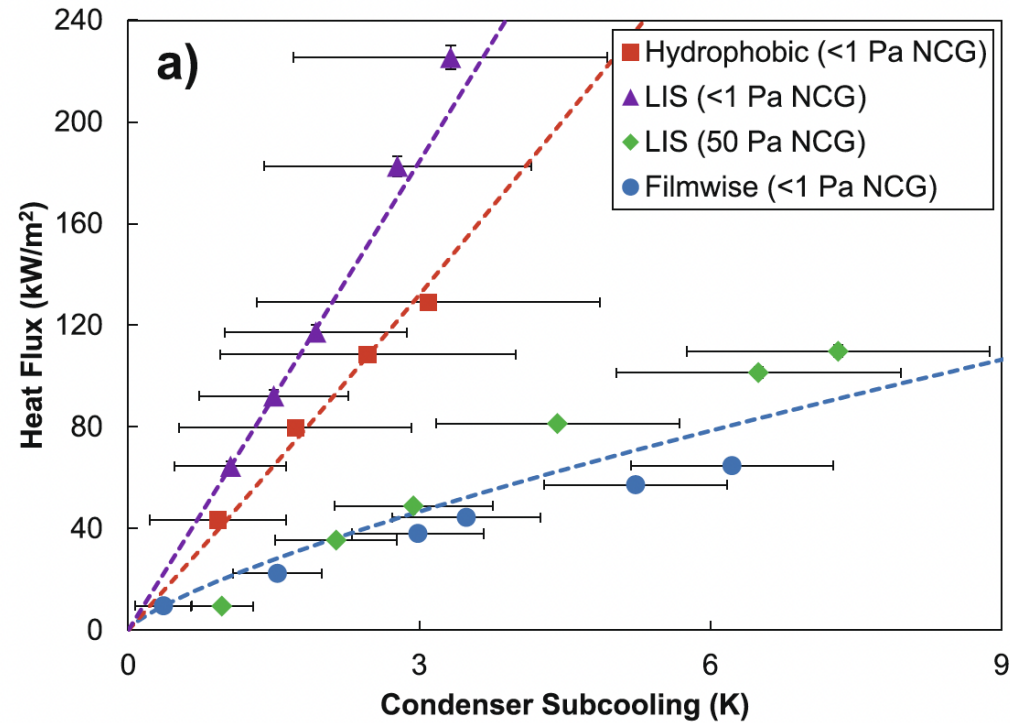
Regular
hydrophobic



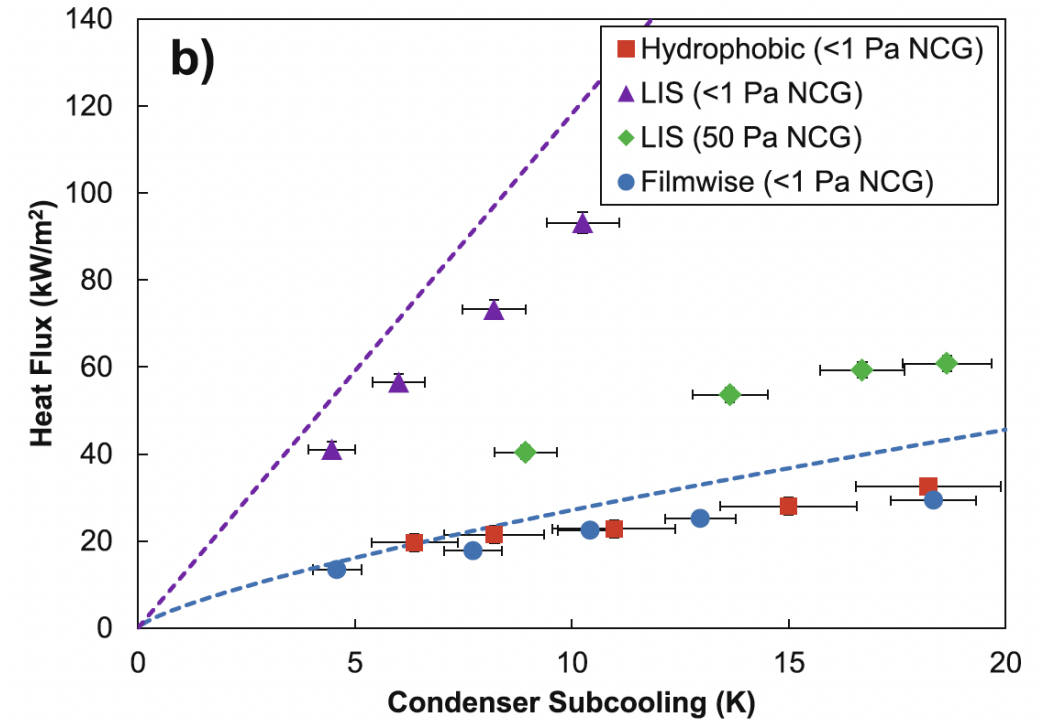
LIS



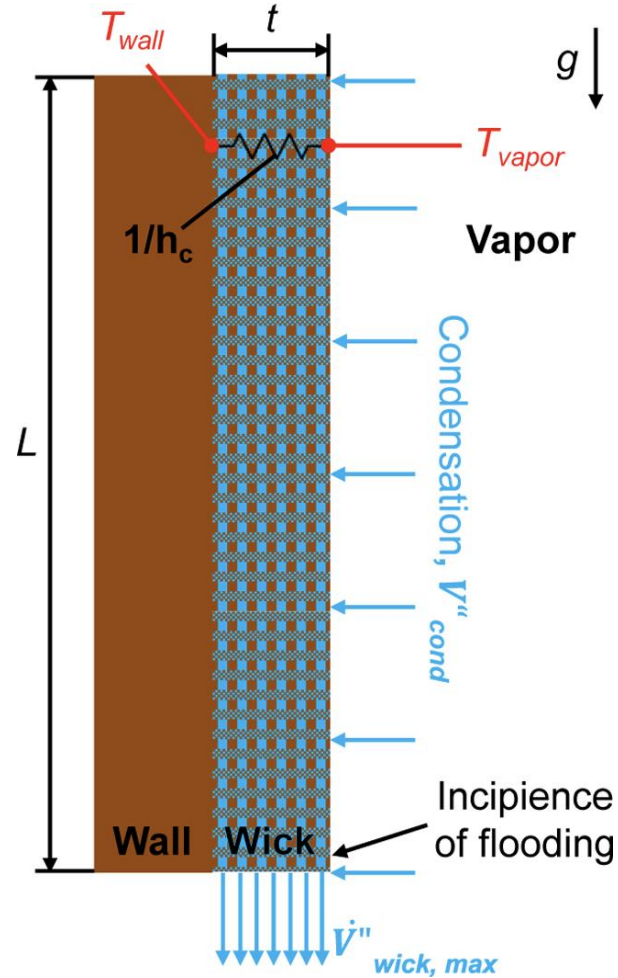
Water (72 mN/m)



Toluene (28 mN/m)



Preston, D.J. et al. Sci Rep 8, 540 (2018)



Langmuir 2018, 34, 4658–4664

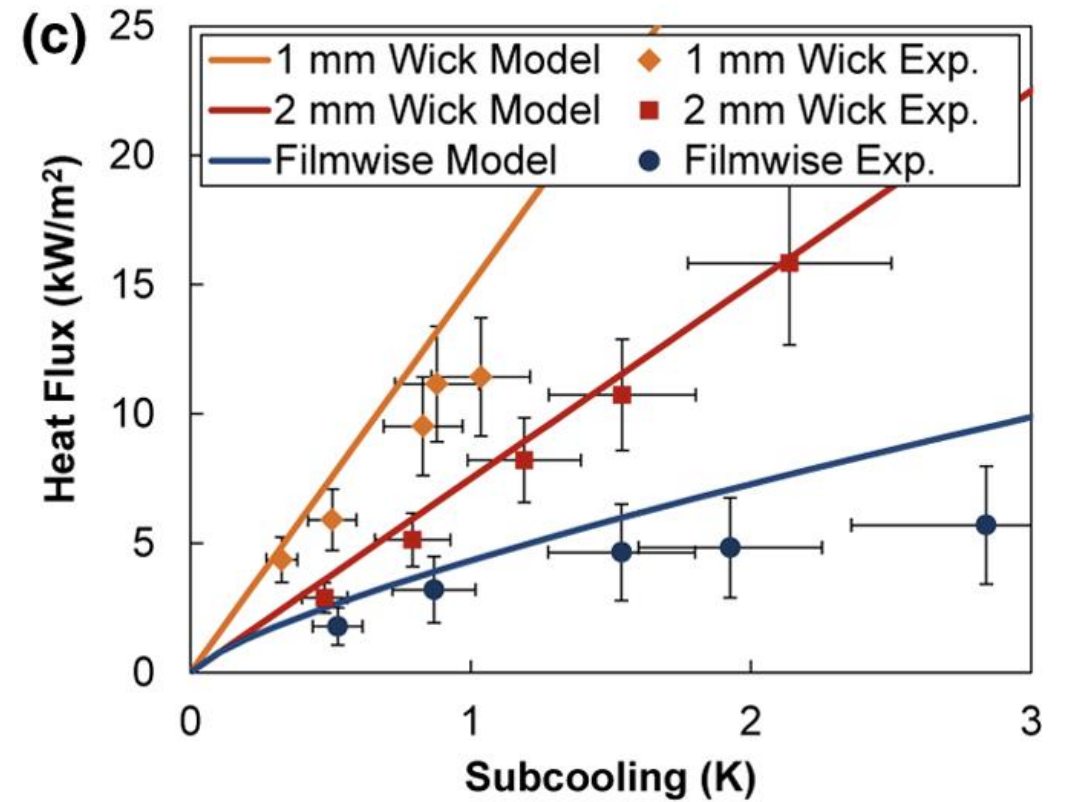
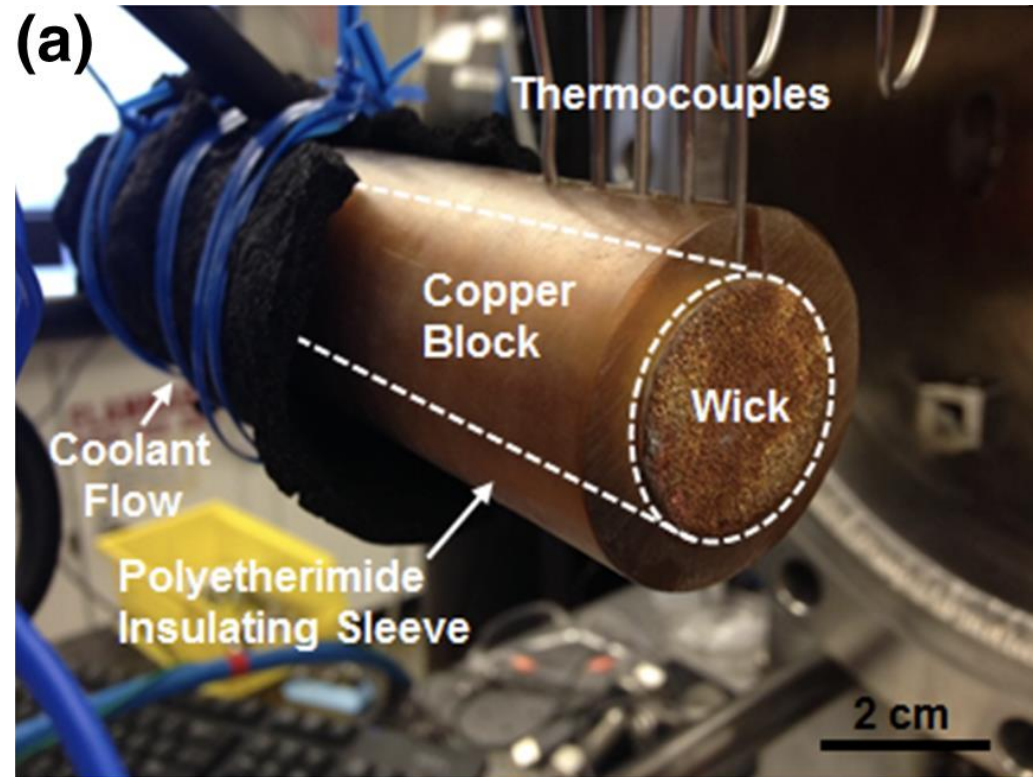
$$h_c = \frac{k_{wick}}{t}$$

$$\dot{m}''_{cond} h_{fg} = h_c \Delta T$$

$$\dot{V}''_{wick, max} = \frac{\dot{m}''_{cond} L}{\rho t} = \frac{K}{\mu} \left| \frac{dP}{dx} \right|_{max}$$

$$\left| \frac{dP}{dx} \right|_{max} = \rho g$$

$$\Delta T < \frac{K \rho^2 g h_{fg} t^2}{L k_{wick} \mu}$$



Langmuir 2018, 34, 4658–4664