

**ME-445 AERODYNAMICS**  
**Exercise 06**  
**Week 5**

# Formula sheet

## Cylindrical coordinates

$$\nabla \vec{u} = \left( \frac{\partial v_r}{\partial r}, \frac{1}{r} \frac{\partial v_\theta}{\partial \theta}, 0 \right)$$

$$\nabla \cdot \vec{u} = \frac{1}{r} \frac{\partial (rv_r)}{\partial r} + \frac{1}{r} \frac{\partial v_\theta}{\partial \theta}$$

$$\nabla \times \vec{u} = \left( 0, 0, \frac{1}{r} \left[ \frac{\partial (rv_\theta)}{\partial r} - \frac{\partial v_r}{\partial \theta} \right] \right)$$

## Potential flow

$$v_r = \frac{\partial \phi}{\partial r} = \frac{1}{r} \frac{\partial \psi}{\partial \theta}, \quad v_\theta = \frac{1}{r} \frac{\partial \phi}{\partial \theta} = -\frac{\partial \psi}{\partial r}$$

$$\text{Uniform parallel flow} \quad w = \phi + i\psi = U_\infty e^{-i\alpha} z$$

$$\text{Potential vortex in } z_0 \quad w = -\frac{i\gamma}{2\pi} \ln(z - z_0)$$

$$\text{Point source or sink in } z_0 \quad w = \frac{Q}{2\pi} \ln(z - z_0)$$

$$\text{Source-sink doublet in } z_0 \quad w = \frac{\mu}{2\pi(z - z_0)}$$

$$\frac{dw}{dz} = u - iv$$

Milne-Thomson circle theorem:

$$g(z) = w(z) + \overline{w \left( \frac{a^2}{\bar{z}} \right)}$$

## Thin airfoil theory

For a camber line with:

$$\frac{dy_c}{dx} = A_0 + \sum_{n=1}^{\infty} A_n \cos n\theta$$

$$\frac{x}{c} = \frac{(1 - \cos \theta)}{2}$$

we know:

$$k = 2U_\infty \left[ (\alpha - A_0) \frac{\cos \theta + 1}{\sin \theta} + \sum_{n=1}^{\infty} A_n \sin n\theta \right]$$

$$A_0 = \frac{1}{\pi} \int_0^\pi \frac{dy_c}{dx} d\theta$$

$$A_n = \frac{2}{\pi} \int_0^\pi \frac{dy_c}{dx} \cos n\theta d\theta$$

$$C_l = 2\pi\alpha + \pi(A_1 - 2A_0)$$

$$C_{m,1/4} = -\frac{\pi}{4}(A_1 - A_2)$$

$$x_{cp} = \frac{1}{4} + \frac{\pi}{4C_1}(A_1 - A_2)$$

## Finite wings with $AR = b^2/S$

Sign convention:

if induced velocity points downward:  $w(y) > 0, \alpha_i(y) > 0$

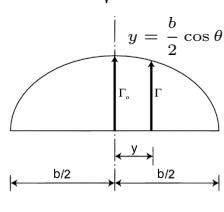
if induced velocity points upward:  $w < 0, \alpha_i < 0$

Prandtl's lifting-line theory

$$U_\infty \alpha_i(y_0) = w(y_0) = -\frac{1}{4\pi} \int_{-b/2}^{b/2} \frac{(d\Gamma/dy)}{y - y_0} dy$$

$$\alpha(y_0) = \alpha_{\text{eff}}(y_0) + \alpha_i(y_0)$$

$$\text{Elliptical loading } \Gamma(y) = \Gamma_0 \sqrt{1 - \left( \frac{2y}{b} \right)^2}$$

$$\begin{aligned} w &= \frac{\Gamma_0}{2b} \\ \alpha_i &= \frac{C_L}{\pi AR} \\ C_{D,i} &= \frac{C_L^2}{\pi AR} \end{aligned}$$


$$\text{General loading } \Gamma(\theta) = 2bU_\infty \sum_{n=1}^{\infty} A_n \sin n\theta$$

$$w(\theta) = U_\infty \sum_{n=1}^{\infty} nA_n \frac{\sin n\theta}{\sin \theta}$$

$$C_L = \pi A_1 AR$$

$$C_{D,i} = \frac{C_L^2}{\pi AR} (1 + \delta) \text{ with } \delta = \sum_{n=2}^{\infty} n (A_n/A_1)^2$$

## Boundary Layer

Flat plate **laminar** boundary layer

$$\frac{\delta}{x} = \frac{5}{\sqrt{Re_x}} \quad \text{boundary layer growth}$$

$$C_f = \frac{1.328}{\sqrt{Re_x}} \quad \text{skin friction drag coefficient}$$

Flat plate **turbulent** boundary layer

$$\frac{\delta}{x} = \frac{0.37}{Re_x^{1/5}} \quad \text{boundary layer growth}$$

$$C_f = \frac{0.074}{Re_x^{1/5}} \quad \text{skin friction drag coefficient}$$

## Miscellaneous

$\theta$	$0^\circ$	$30^\circ$	$45^\circ$	$60^\circ$	$90^\circ$
$\sin \theta$	0	$\frac{1}{2}$	$\frac{\sqrt{2}}{2}$	$\frac{\sqrt{3}}{2}$	1
$\cos \theta$	1	$\frac{\sqrt{3}}{2}$	$\frac{\sqrt{2}}{2}$	$\frac{1}{2}$	0

**water**

kinematic viscosity  $\nu = 1 \times 10^{-6} \text{ m}^2 \text{ s}^{-1}$   
 density  $\rho = 1000 \text{ kg m}^{-3}$

**air**

kinematic viscosity  $\nu = 1.5 \times 10^{-5} \text{ m}^2 \text{ s}^{-1}$   
 density  $\rho = 1.2 \text{ kg m}^{-3}$

$$\sin(x \pm y) = \sin x \cos y \pm \cos x \sin y$$

$$\cos(x \pm y) = \cos x \cos y \mp \sin x \sin y$$

$$\cos 2\theta = 2 \cos^2 \theta - 1$$

$$\sin 2\theta = 2 \sin \theta \cos \theta$$

$$\sin 3\theta = 3 \sin \theta - 4 \sin^3 \theta$$

$$\cos 3\theta = 4 \cos^3 \theta - 3 \cos \theta$$

$$\int_0^\pi \cos \theta d\theta = 0$$

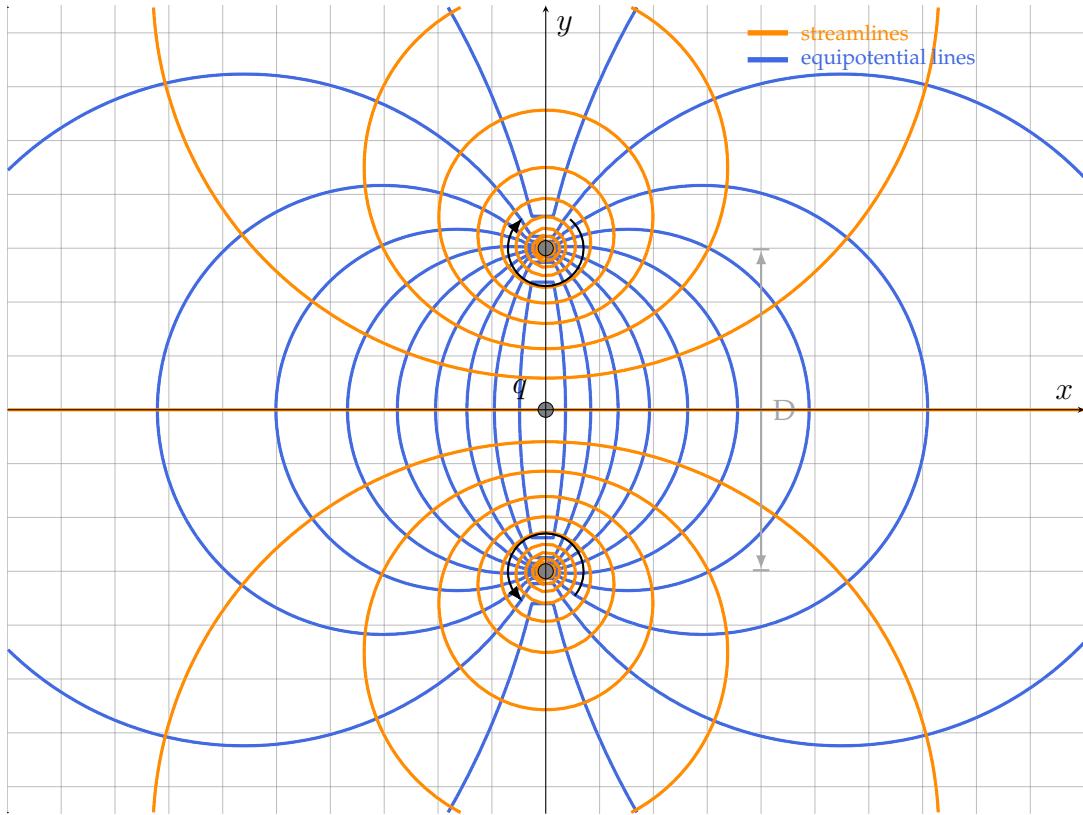
$$\int_0^\pi \sin \theta d\theta = 2$$

$$\int_0^\pi \cos^2 \theta d\theta = \int_0^\pi \sin^2 \theta d\theta = \frac{\pi}{2}$$

$$\int_0^\pi \frac{\cos n\theta}{\cos \theta - \cos \theta_1} d\theta = \pi \frac{\sin n\theta_1}{\sin \theta_1} \quad n = 0, 1, 2, \dots$$

$$\int_0^\pi \frac{\sin n\theta \sin \theta}{\cos \theta - \cos \theta_1} d\theta = -\pi \cos n\theta_1 \quad n = 1, 2, 3, \dots$$

1. Consider a clockwise and a counterclockwise potential vortex of strength  $G$  along  $y$  separated by a distance  $D$ .



(a) Find the resultant complex potential  $w(z)$ .

**Solution:**

With  $(0, 0)$  in the middle between the vortices:

$$w(z) = \frac{iG}{2\pi} \ln \left( z - i\frac{D}{2} \right) - \frac{iG}{2\pi} \ln \left( z + i\frac{D}{2} \right)$$

If the considered the strength positive if clockwise the following result is also correct.

$$w(z) = -\frac{iG}{2\pi} \ln \left( z - i\frac{D}{2} \right) + \frac{iG}{2\pi} \ln \left( z + i\frac{D}{2} \right)$$

The sign of  $G$  needs to change in the different terms and the sign in front of  $i\frac{D}{2}$

(b) Sketch the streamlines and equipotential lines in the above graph. Use a marker or colours (not red) to clearly distinguish between both and do not forget to add a legend.  
 (c) Find the magnitude and direction of the velocity  $\vec{u}_q$  at point  $q$  in between the two vortices in function of the parameters  $G$  and  $D$ .

**Solution:**

Considering  $G$  positive for the counterclockwise rotating vortex and the origin in between the vortices:

$$\begin{aligned} u - iv &= \frac{dw}{dz}(z) \\ &= \frac{iG}{2\pi} \frac{1}{\left( z - i\frac{D}{2} \right)} - \frac{iG}{2\pi} \frac{1}{\left( z + i\frac{D}{2} \right)} \end{aligned}$$

In this coordinate system  $z(q) = 0$ .

$$\begin{aligned} u_p - iv_p &= \frac{dw}{dz}(p) \\ &= -\frac{iG}{2\pi} \frac{1}{i\frac{D}{2}} - \frac{iG}{2\pi} \frac{1}{i\frac{D}{2}} \\ &= -\frac{2G}{\pi D} \end{aligned}$$

$$\begin{aligned} u_q &= -\frac{2G}{\pi D} \\ v_q &= 0 \end{aligned}$$

Alternatively, from the symmetry of the set-up, we know that the induced velocity is in the negative  $x$ -direction and has a magnitude of  $2 \frac{G}{2\pi D/2} = \frac{2G}{\pi D}$

(d) Now, add a horizontal uniform free stream flow with velocity  $u_\infty = \frac{1}{2}|\vec{u}_q|$  to the vortex pair, with  $\vec{u}_q$  the velocity found in the previous part. Find the new resultant complex potential  $w(z)$ .

**Solution:** ! Solutions depend on the choice of the origin of the coordinate system !

The complex potential for the flow is  $w(z) = \frac{iG}{2\pi} \ln \left( z - i\frac{D}{2} \right) - \frac{iG}{2\pi} \ln \left( z + i\frac{D}{2} \right) + u_\infty z$

(e) Find the location of all stagnation points. Write your solution(s) in function of the parameters  $G$  and  $D$ .

**Solution:** Considering  $G$  positive for the counterclockwise rotating vortex and the origin in between the vortices:

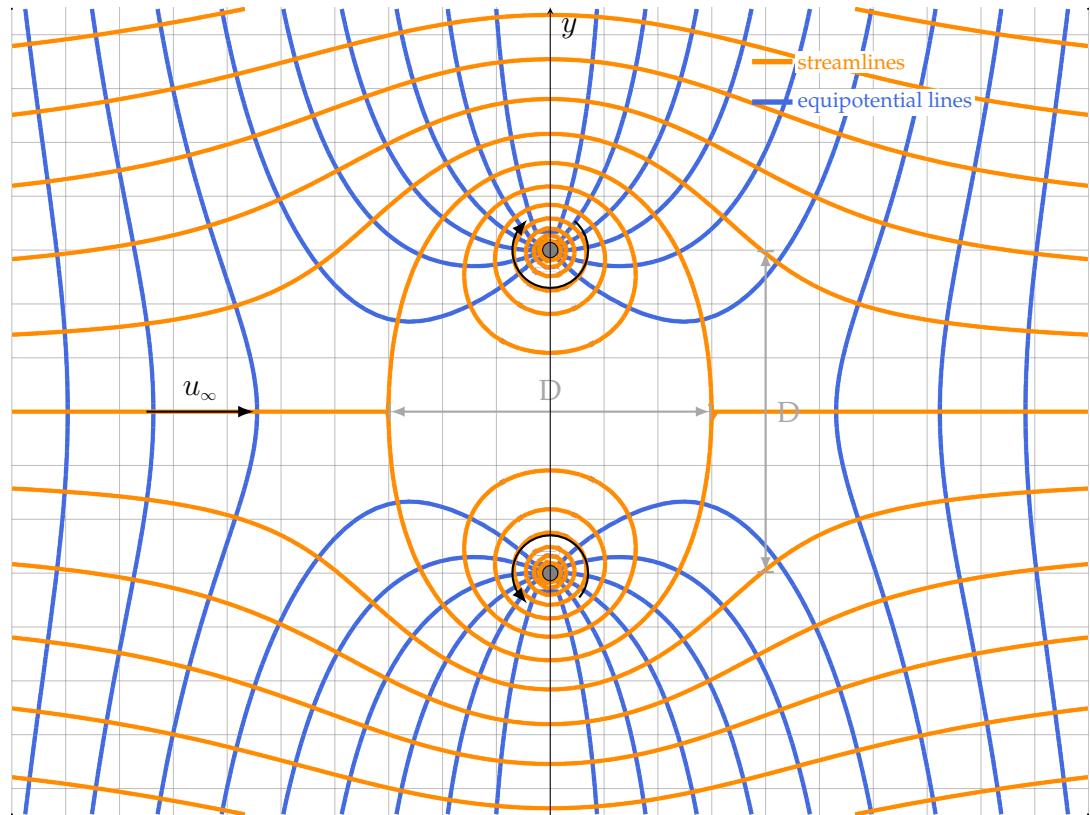
$$u - iv = \frac{dw}{dz}(z) = \frac{iG}{2\pi} \frac{1}{(z - i\frac{D}{2})} - \frac{iG}{2\pi} \frac{1}{(z + i\frac{D}{2})} + u_\infty$$

The vertical velocity component along the  $x$ -axis is zero everywhere. There will be 2 stagnation points. The stagnation points will be on the  $x$ -axis. We need to find the  $x$ -location for which the  $u$  velocity component is zero.

$$\begin{aligned} 0 &= u(x, y=0) \\ &= \frac{iG}{2\pi} \left( \frac{1}{x - i\frac{D}{2}} - \frac{1}{x + i\frac{D}{2}} \right) + u_\infty \\ &= \frac{iG}{2\pi} \left( \frac{iD}{x^2 + D^2/4} \right) + u_\infty \\ \Rightarrow \frac{2GD}{\pi} \left( \frac{1}{4x^2 + D^2} \right) &= u_\infty \\ \Rightarrow x &= \pm \sqrt{\frac{GD}{2\pi u_\infty} - \frac{D^2}{4}} \quad \text{with } u_\infty = 0.5u_p = \frac{G}{\pi D} \\ \Rightarrow x &= \pm \sqrt{\frac{D^2}{4}} \end{aligned}$$

stagnation points in  $(x, y) = (\pm \frac{D}{2}, 0)$

(f) Sketch the new streamline pattern in the graph below.



(g) Find the pressure coefficient in point  $q$

**Solution:**

The velocity in point  $q$  was  $(u_q, v_q) = (-\frac{2G}{\pi D}, 0)$  before including the horizontal uniform free stream  $u_\infty = \frac{G}{\pi D}$ . The new velocity components in point  $q$  are thus  $(u_q, v_q) = (-\frac{G}{\pi D}, 0) = (-u_\infty, 0)$  and the pressure coefficient  $c_p(q) = 1 - (u_q^2/u_\infty^2)$  hence  $c_p = 0$ .

(h) Find the total circulation  $\Gamma$  in the area enclosed by the large rectangle in the figure below.

**Solution:**  $\Gamma = 0$

(i) Find the total circulation  $\Gamma$  in the area enclosed by the circle in the figure below.

**Solution:**  $\Gamma = -G$

