

HYDRODYNAMICS

CORRECTION WEEK 11

Exercise 1

Part 1

1. In the absence of volumic forces, the equations of motion of a perfect, incompressible fluid are the Euler equations. It is not a potential flow since the flow field is not rotation free.

$$\partial \vec{u} / \partial t + (\vec{u} \cdot \nabla) \vec{u} + \nabla p / \rho = 0 \quad \text{and} \quad \nabla \cdot \vec{u} = 0.$$

2. The flow is stationary, the acceleration of the fluid is $(\vec{u} \cdot \nabla) \vec{u}$, being:

$$(\vec{u} \cdot \nabla) \vec{u} = \text{rot}(\vec{u}) \times \vec{u} + \nabla \left(\frac{1}{2} \|\vec{u}\|^2 \right) = \omega \vec{e}_z \times \vec{u} + \nabla \left(\frac{1}{2} \|\vec{u}\|^2 \right).$$

Or, the flow field being two dimensional and incompressible, there exists a function $\psi(x, y)$ such as: $\vec{u} = (\partial \psi / \partial y) \vec{e}_x - (\partial \psi / \partial x) \vec{e}_y$. Consequently:

$$\vec{e}_z \times \vec{u} = (\partial \psi / \partial x) \vec{e}_x + (\partial \psi / \partial y) \vec{e}_y = \nabla \psi.$$

Then assuming ω being constant, one deduces that:

$$\text{rot} \vec{u} \times \vec{u} = \omega \nabla \psi = \nabla(\omega \psi),$$

and the acceleration becomes the derivative of a potential:

$$(\vec{u} \cdot \nabla) \vec{u} = \nabla(\omega \psi + \frac{1}{2} \|\vec{u}\|^2).$$

Since the pressure appears also as a gradient, we transformed the Euler equations into the gradient of a scalar potential.

3. Since the Euler equation appears as a scalar potential, we have independence of the integration path and the integral for any scalar potential becomes:

$$\int_P \nabla \phi \cdot dr = \phi(B) - \phi(A),$$

for an arbitrary integration path P between position A and B . In our case this gives:

$$\rho \omega \psi + \frac{1}{2} \rho \|\vec{u}\|^2 + p = C,$$

where C is a constant.

4. The force exerted by a fluid on an obstacle is: $\vec{F} = - \int \int_{\Sigma} p \vec{n} dS$. Or, using preceding results,

$$\vec{F} = \rho \omega \int \int_{\Sigma} \psi \vec{n} dS + \frac{\rho}{2} \int \int_{\Sigma} \|\vec{u}\|^2 \vec{n} dS - C \int \int_{\Sigma} \vec{n} dS.$$

The integral of the normal around a closed interface is zero. Since the streamline ψ is constant on the obstacle, not only the last integral but also the first are zero.

Part 2

1. $\text{rot } \vec{U} = -S\vec{e}_z$.
2. $\text{rot } \vec{u} = \text{rot } (\vec{U} + \nabla\phi) = -S\vec{e}_z$ because $\text{rot } \nabla\phi = 0$. Applying the incompressibility condition, we find $\Delta\phi = 0$.
3. On Σ , the slip condition $\vec{u}|_\Sigma \cdot \vec{n} = 0$ becomes:

$$0 = (\vec{U} + \nabla\phi)|_\Sigma \cdot \vec{e}_r = (V + SR \sin(\theta)) \cos(\theta) + (\partial\phi/\partial r)|_\Sigma.$$

4. The Laplacian in polar coordinates is given as:

$$\Delta\phi = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial\phi}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2\phi}{\partial\theta^2},$$

the two functions $\phi = \Gamma\theta/2\pi$ and $\phi = A \ln(r)$ are harmonics, they verify $\Delta\phi = 0$.

5. Since $\Delta \ln(r) = 0$, also $\nabla \Delta \ln(r) = 0 = \Delta \nabla \ln(r)$, by linear combination $\Delta(\vec{B} \cdot \nabla \ln(r)) = 0$ for all vectors \vec{B} being constant. By iteration this is the same for \vec{C} .

6. In matching all the boundary conditions of Part 2.3 and identifying coefficients, one obtains:

$$A = 0, \quad B_1 = -VR^2, \quad B_2 = 0, \quad C_{11} = C_{22}, \quad C_{12} = \frac{1}{8}SR^4.$$

7. The velocity components are:

$$u_r = V \left(1 - \frac{R^2}{r^2} \right) \cos(\theta) + \frac{Sr}{2} \left(1 - \frac{R^4}{r^4} \right) \sin(2\theta)$$

$$u_\theta = \frac{\Gamma}{2\pi r} - V \left(1 + \frac{R^2}{r^2} \right) \sin(\theta) - \frac{Sr}{2} \left(1 - \left(1 + \frac{R^4}{r^4} \right) \cos(2\theta) \right).$$

Without shear ($S=0$), one recovers the potential flow with circulation Γ around a cylinder of radius R .

Part 3

3. At $r = R$ one verifies $u_r = 0$, because the fluid streams around the cylinder. For u_θ , still on the boundary Σ , one obtains:

$$(u_\theta^2)|_\Sigma = C^2 - 4KV \sin(\theta) + 4(V^2 - CSR) \sin^2(\theta) + 8SVR \sin^3(\theta) + 4S^2R^2 \sin^4(\theta),$$

where $C = \Gamma/(2\pi R) + SR/2$.

2. From part 1.4, the force is expressed as

$$\vec{F} = \frac{\rho}{2} \int \int_\Sigma ||\vec{u}||^2 \vec{n} dS = \frac{\rho}{2} \int_{z=0}^L \int_{\theta=0}^{2\pi} u_\theta^2 \vec{e}_r R d\theta dz,$$

projected on the Y and X axis:

$$F_x = \frac{\rho}{2} LR \int_0^{2\pi} u_\theta^2 \cos(\theta) d\theta, \quad F_y = \frac{\rho}{2} LR \int_0^{2\pi} u_\theta^2 \sin(\theta) d\theta.$$

The calculation gives $F_x = 0$, there is no drag.

3. After the calculation the exerted force on the cylinder is:

$$\vec{F} = \rho V L (2\pi S R^2 - \Gamma) \vec{e}_y.$$

The force is directed perpendicular to the flow (lift). The first term comes from shear and the second from Joukowski.