

# Networked Control Systems (ME-427)- Exercise session 5

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1. **Stabilizing state-feedback design.** Consider the NCS in Figure 1,

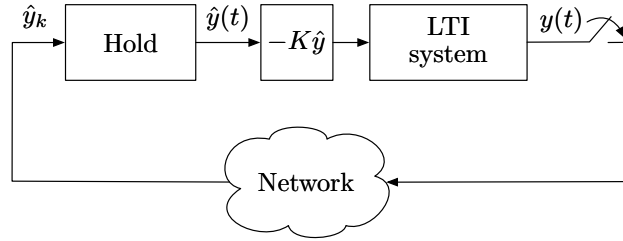


Figure 1: Networked control system

where the LTI system is the first-order model

$$\begin{cases} \dot{x} = -x - 5u \\ y = x \end{cases}.$$

Let  $T = 0.5$  and  $\tau = 0.2$  be the nominal sampling time and network induced delay, respectively. Find by hand all values of  $K$  stabilizing the NCS.

**Hint:** Recall the Jury's criterion: the roots of  $\phi(\lambda) = \lambda^2 + \alpha\lambda + \beta$  verify  $|\lambda| < 1$  if and only if

$$\begin{aligned} \beta &> -\alpha - 1 \\ \beta &> \alpha - 1 \\ \beta &< 1 \end{aligned}.$$

**Solution:** Given that  $A = -1$ ,  $B = -5$ ,  $C = 1$ ,  $T = 0.5$ , and  $\tau = 0.2$ , one has

$$\begin{aligned} \psi(T, \tau) &= \begin{bmatrix} e^{AT} - BK\Gamma(T - \tau) & -BK e^{A(T-\tau)}\Gamma(\tau) \\ 1 & 0 \end{bmatrix} \\ &= \begin{bmatrix} e^{-0.5} + 5K\Gamma(0.3) & 5K e^{-0.3}\Gamma(0.2) \\ 1 & 0 \end{bmatrix}. \end{aligned}$$

Approximately,

$$\begin{aligned} e^{-0.5} &= 0.6065 \\ e^{-0.3} &= 0.7408 \end{aligned}.$$

$$\Gamma(s) = 1 - e^{-s} \rightarrow \Gamma(0.3) = 0.2592 \quad \Gamma(0.2) = 0.18$$

Therefore,

$$\psi(0.5, 0.2) = \begin{bmatrix} 0.6065 + K \times 1.2939 & K \times 0.6716 \\ 1 & 0 \end{bmatrix}.$$

By computing the characteristic polynomial of  $\psi$  and using Jury's conditions, one has

$$-K \times 0.6716 > 0.6065 + K \times 1.2939 - 1 \quad (1a)$$

$$-K \times 0.6716 > -0.6065 - K \times 1.2939 - 1 \quad (1b)$$

$$-K \times 0.6716 < 1 \quad (1c)$$

- From (1a),  $-K \underbrace{(0.6716 + 1.2939)}_{1.9655} > -0.3935 \rightarrow K < \frac{0.3935}{1.9655} = 0.1595$
- From (1b),  $-K \underbrace{(0.6716 - 1.2939)}_{-0.6223} > -1.6065 \rightarrow K > \frac{-1.6065}{0.6223} = -2.5816$
- From (1c),  $-K < \frac{1}{0.6716} \rightarrow K > -1.4890$

Conclusion:  $K \in (-1.4890, 0.1595)$ .

2. **Remote control with delay compensation.** Consider the cart-stick balancer system in Figure 2,

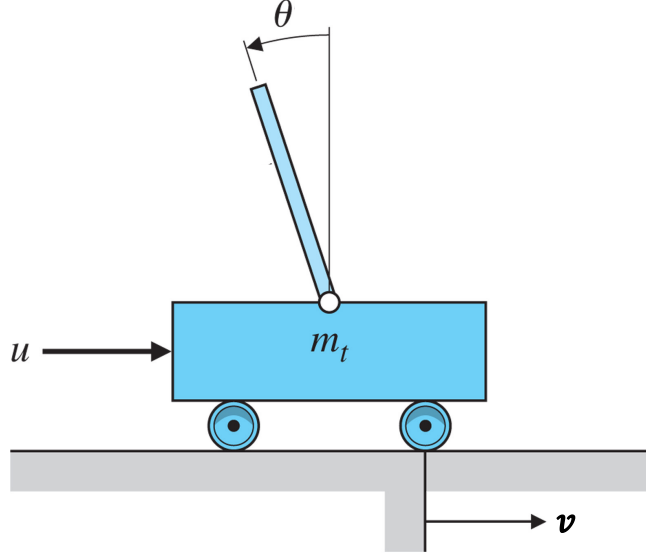


Figure 2: Cart-stick balancer.

with states  $x_1$ : stick angle  $\theta/10$ ,  $x_2$ : stick angular velocity  $\dot{\theta}$ ,  $x_3$ : cart velocity  $v$ . The input  $u$  is the voltage to the motor driving the wheels. The measured output  $y = \theta$  is the stick angle. The control goal is to maintain the stick vertical by moving the cart through  $u$ . Consider the remote controller with delay compensation defined in Figure 3 with uniform sampling period  $T = 0.1$  s.

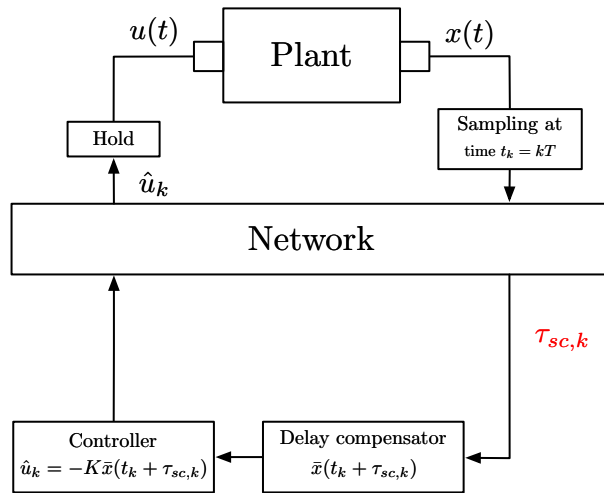


Figure 3: Remote controller with delay compensation.

Setting  $x^T = [x_1 \ x_2 \ x_3]$  one has the linearized model

$$\dot{x} = \underbrace{\begin{bmatrix} 0 & 1 & 0 \\ 31.33 & 0 & 0.016 \\ -31.33 & 0 & -0.216 \end{bmatrix}}_A x + \underbrace{\begin{bmatrix} 0 \\ -0.649 \\ 8.649 \end{bmatrix}}_B u$$

Recall from the lectures that, setting  $\delta_k = T + \tau_{sc,k+1} - \tau_{sc,k}$ , the closed-loop NCS model is given by the discrete-time system

$$\begin{aligned} x(t_{k+1} + \tau_{sc,k+1}) &= \tilde{A}_k x(t_k + \tau_{sc,k}) \\ \tilde{A}_k &= e^{A\delta_k} - \Gamma(\delta_k)BK, \quad \Gamma(\delta_k) = \int_0^{\delta_k} e^{As} ds \end{aligned} \quad (2)$$

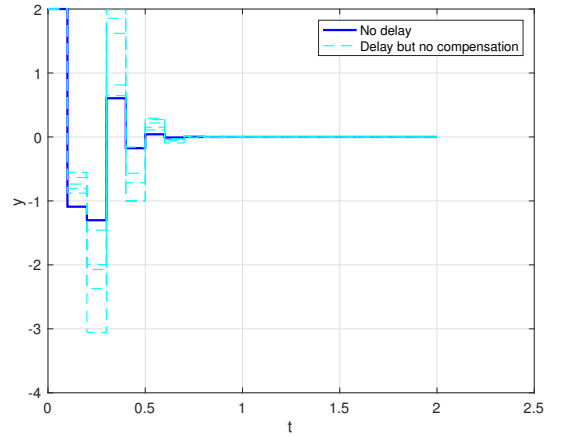
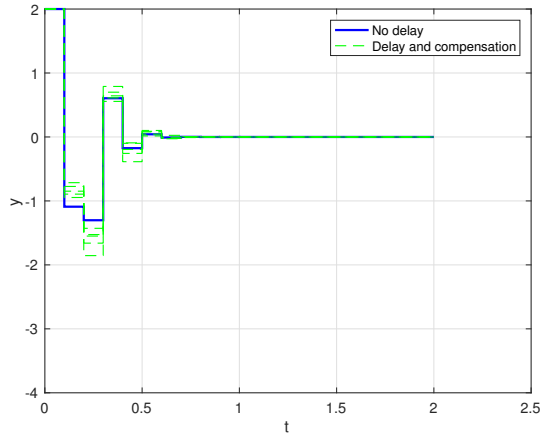
A simulator of the NCS is provided by the file `NCS_car_stick_balancer.m` available on moodle. The .m file is configured for running the *nominal experiment* defined by

$$t_0 = 0$$

$$x(0) = [0.2 \ 0.3 \ -0.5]^T$$

$$K = [-556.1829 \ -208.3171 \ -12.9905]$$

and it produces two plots, similar to the ones below



Both figures display the angular position of the stick (in degrees) and

- the blue line is the ideal NCS with  $\tau_{sc,k} = 0$ ,  $k = 0, 1, \dots$
- other lines are obtained extracting the values of  $\tau_{sc,k}$  five times from the uniform distribution on  $[\tau_{min}, \tau_{max}]$  (these parameters can be specified at the beginning of the file) and
  - using a delay-compensation controller, as seen in the lectures (green lines);
  - using an uncompensated controller (cyan lines).

(a) **Familiarize with the simulator.** Perform the following experiments.

- The default gain  $K$  has been produced by nominal design (see the lecture slides for the precise meaning of "nominal design") for placing the closed-loop eigenvalues in  $-0.42$ ,  $-0.49$ , and  $-0.56$ . Check stability in simulation by looking at the plots for
  - $\tau_{min} = \tau_{max} = 0$
  - $\tau_{min} = \tau_{max} = \tau < T$ . In this case performances are different if using delay compensation or not. Why ?

**Solution:** As seen in the lectures, considering the sampling interval  $[t_k, t_{k+1}]$ , the compensated controller produces the best possible control actions in the sub-interval  $[t_k + \tau_{sc,k}, t_{k+1}]$ , while the uncompensated controller does not.

- ii. Assume that performance of the NCS is acceptable if

$$|\theta(t_k)| < 15, \forall k = 0, 1, \dots \quad (3)$$

By increasing  $\tau = \tau_{min} = \tau_{max}$ , find  $\bar{\tau}$  such that (3) is verified by the delay-compensated controller, but not by the uncompensated controller.

**Solution:**  $\bar{\tau} \simeq 0.25T$  produces the desired behavior.

- iii. Run simulations with  $\tau_{sc,k}$  generated randomly in  $[0, \bar{\tau}]$ . The system behavior gets worse (for instance, oscillations are less dampened). Can you guess why ?

**Solution:** Nominal design implies that the controller has been synthesized for  $\tau_{sc,k}$  constant. This assumption, however, is not fulfilled in the simulation.

- iv. Can the NCS become unstable by increasing  $\bar{\tau}$  in the previous point ? Run simulations for answering.

**Solution:** Yes, for  $\bar{\tau} \simeq 0.45T$  unstable behaviors start appearing. Note that the car-stick-balancer is open-loop unstable. This is why network delays can have a particularly detrimental effect.

- (b) **Control design.** Network delays that can be tolerated for stability and performance depend on the eigenvalues of the nominal NCS. To see this,

- design a nominal gain  $K$  for placing the closed-loop eigenvalues in  $-0.12$ ,  $-0.14$ , and  $-0.16$  (so that NCS transients are shorter than before).

**Hint:** Fill in the missing code in `NCS-car_stick_balancer.m` for computing  $K$ .

**Solution:** See the MatLab code on moodle.

- run simulations with  $\tau_{sc,k}$  extracted randomly in  $[0, \bar{\tau}]$  and increase  $\bar{\tau}$  until unstable behaviors start appearing. How does  $\bar{\tau}$  compare with the result of point (2(a)iv) above?

**Solution:** Instability starts appearing for  $\bar{\tau} \simeq 0.85T$ . Therefore, compared to point (2(a)iv), the new controller brings more robustness to delays.