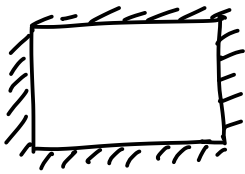


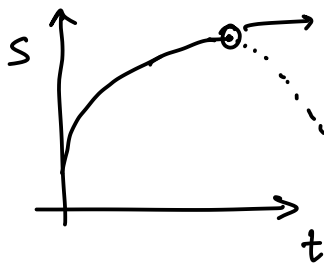
EQUILIBRIUM CRITERIA

Consider an isolated system $\rightarrow$ all extensive variables are constant

(eg) Volume can't change $\Rightarrow$ no p - V work



II Law: $dS \geq 0$



stop equilibrium $\rightarrow$ cannot evolve since entropy would decrease

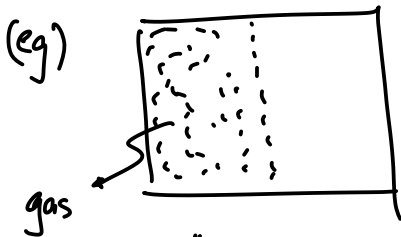
$$dS = \frac{du}{T} + \frac{p}{T} dV$$

$U \rightarrow$ constant

$V \rightarrow$ constant

what are we maximizing over?

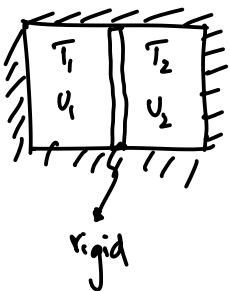
FIND EQUILIBRIUM STATE BY MAXIMIZING S OVER SOME INTERNAL EXTENSIVE VARIABLES



"internal" degree of freedom $\rightarrow$ volume of the gas

$S \rightarrow$ maximized when gas fills the whole volume.

① THERMAL EQUILIBRIUM:



$U = U_1 + U_2 = \text{constant}$ since no work or heat exchange with the environment

$$dV_1 = dV_2 = 0$$

Let U_1 be the independent internal extensive variable

$$dU_1 = T dS_1 - p dV_1 \quad \nearrow 0$$

$$\boxed{dU_1 = T_1 dS_1}$$

$$du = 0$$

$$\Rightarrow du_1 = -du_2$$

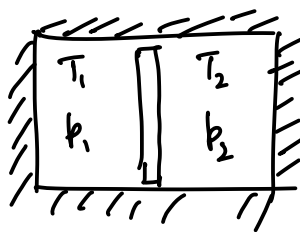
$$S = S_1 + S_2 \Rightarrow dS = dS_1 + dS_2 = \frac{du_1}{T_1} + \frac{du_2}{T_2} = du_1 \left(\frac{1}{T_1} - \frac{1}{T_2} \right)$$

$$S(u_1) \rightarrow \left[\frac{dS}{du_1} = \frac{1}{T_1} - \frac{1}{T_2} \right]$$

$$\text{only if } T_1 = T_2 \Rightarrow [dS = 0] \rightarrow \text{ENTROPY MAXIMIZED}$$

AND THERMAL

② THERMAL & MECHANICAL EQUILIBRIUM:



$$U = \text{constant}$$

$$= u_1 + u_2$$

$$du = 0 \Rightarrow du_1 = -du_2$$

$$V = \text{constant}$$

$$dV = 0 \Rightarrow dV_1 = -dV_2$$

fundamental equation:

$$dS_1 = \frac{du_1}{T_1} + \frac{p_1}{T_1} dV_1 \quad \& \quad dS_2 = \frac{du_2}{T_2} + \frac{p_2}{T_2} dV_2$$

2 independent internal extensive variables:

$$u_1 \& V_1$$

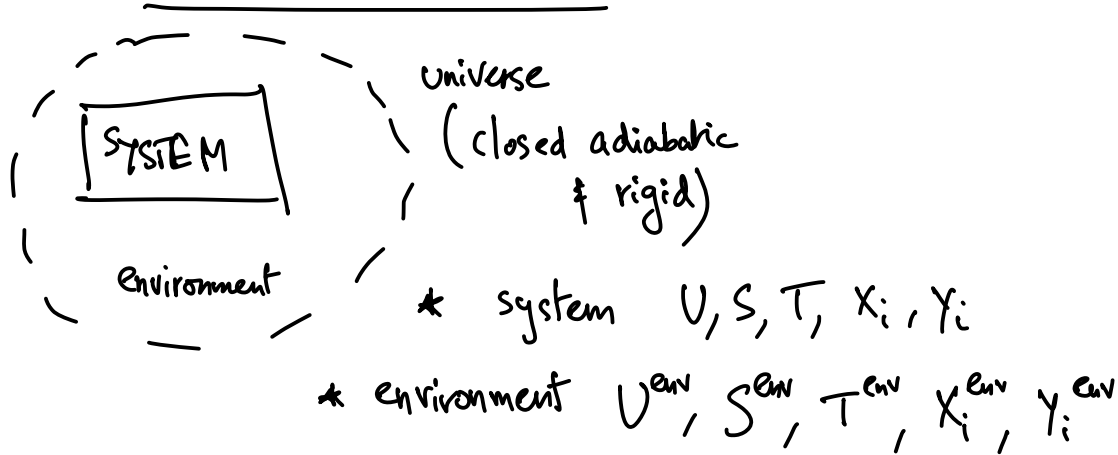
$$dS = \left(\frac{1}{T_1} - \frac{1}{T_2} \right) du + \left(\frac{p_1}{T_1} - \frac{p_2}{T_2} \right) dV_1$$

$$dS = 0 \rightarrow \text{max entropy.}$$

$$\Rightarrow \left(\frac{\partial S}{\partial u} \right)_{V_1} = 0 \Rightarrow T_1 = T_2 \quad ; \quad \left(\frac{\partial S}{\partial V_1} \right)_{u_1} = 0 \Rightarrow p_1 = p_2$$

INTENSIVE VARIABLES CONJUGATE TO FREELY VARYING INTERNAL EXTENSIVE VARIABLES ARE EQUAL BETWEEN ALL SUBSYSTEMS

* GENERAL EQUILIBRIUM CRITERIA:



$$U^{env} + U = \text{constant}$$

$$X_i^{env} + X_i = \text{Constant} \leftarrow \text{Conserved extensive variables}$$

initial state:

$$T = T^{env}$$

$$Y_i = Y_i^{env}$$

find eq^m state

$$T = T^{env}$$

$$Y_i = Y_i^{env}$$

environment is large enough such that transformation in the system does not affect intensive variables.

CHANGE OF STATE OF THE SYSTEM

$$\Delta U, \Delta X_i, \Delta S, \dots$$

for the environment: (EULER)

$$\Delta U^{env} = T^{env} \Delta S^{env} + \sum_i Y_i^{env} \Delta X_i^{env}$$

$$\Delta U^{env} = -\Delta U$$

$$\Delta X^{env} = -\Delta X$$

$$\Rightarrow -\Delta U = T^{\text{env}} \Delta S - \sum_i \gamma_i^{\text{env}} \Delta x_i$$

II Law $\Delta S^{\text{env}} + \Delta S \geq 0$

$$\Rightarrow \Delta S^{\text{env}} \geq -\Delta S$$

$$T^{\text{env}} \Delta S^{\text{env}} \geq -T^{\text{env}} \Delta S$$

$$-\Delta U + \sum_i \gamma_i^{\text{env}} \Delta x_i \geq -T^{\text{env}} \Delta S$$

$$\Rightarrow \boxed{0 \geq \Delta U - T^{\text{env}} \Delta S - \sum_i \gamma_i^{\text{env}} \Delta x_i}$$

- all freely varying extensive variables are system variables

- intensive variables are set by the environment

$$\Rightarrow \boxed{0 \geq \Delta U - T \Delta S - \sum_i \gamma_i \Delta x_i}$$

change of state can be irreversible
only end points need to be in eq^m

EQ^m UNDER DIFFERENT BOUNDARY CONDITIONS:

① fix all extensive variables

$$S_i, x_i = \text{constant}$$

$$\Rightarrow \Delta U \leq 0 \longrightarrow U \text{ has to be minimal}$$

U is the characteristic potential.

② fix T and all extensive mechanical variables

$$\Delta x_i = 0, \text{ since } x_i \text{ is fixed.}$$

$$\Delta U - T \Delta S \leq 0$$

$$\Delta F \leq 0$$

③ fix T & p:

$$\Delta U - T \Delta S + p \Delta V \leq 0$$

$$\boxed{\Delta G \leq 0}$$

CHEMICAL POTENTIALS & CHEMICAL WORK:

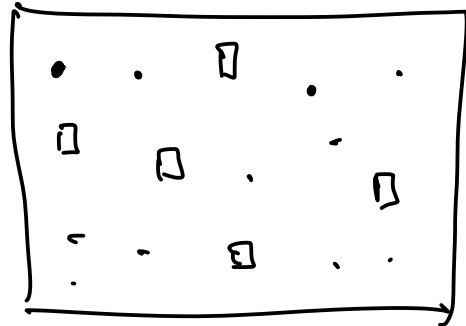
Work terms we have discussed so far:

p - V work } → mechanical
 T - S work }

E - P work } → electrical

What about chemical? Consider:

$p \leftrightarrow V$ conjugate
 $\uparrow$ intensive $\uparrow$ extensive



• → Oxygen
 $\square$ → nitrogen

$\mu_i \leftrightarrow N_i$ → number of moles or atoms of specie i
 $\uparrow$ intensive $\uparrow$ extensive
 μ_i is chemical potential

$$\delta W_{\text{chemical}} = \sum_{i=1}^c \mu_i dN_i$$

FUNDAMENTAL EQUATION OF THERMO: Assume p - V & μ_i - N_i work

$$du = Tds - pdv + \sum_{i=1}^c \mu_i dN_i$$

* EULER RELATION WITH GIBBS FREE ENERGIES

Consider a system with C chemical species where we control T , p , and N_i :

characteristic potential:

$$G(T, p, N_1, N_2, \dots, N_C) = U - TS + pV$$

$$dG = Vdp - SdT + \sum_{i=1}^C \mu_i dN_i \Rightarrow \underline{\text{Derive EOS}}$$

Say we multiply the number of atoms of each specie by $\alpha \Rightarrow$ size of the system changes by a factor α

$$\Rightarrow \alpha G(T, p, N_1, N_2, \dots, N_C)$$

$$= G(T, p, \alpha N_1, \alpha N_2, \dots, \alpha N_C)$$

Differentiating both sides of the equation with respect to α at fixed T, p

$$\text{LHS} = \frac{\partial}{\partial \alpha} (\alpha G(T, p, N_1, \dots, N_C)) = G(T, p, N_1, N_2, \dots, N_C)$$

$$\text{RHS} = \frac{\partial G(T, p, \alpha N_1, \alpha N_2, \dots)}{\partial \alpha} = \sum_{i=1}^C \frac{\partial G}{\partial (\alpha N_i)} \times \left(\frac{\partial (\alpha N_i)}{\partial \alpha} \right)$$

$$RHS = \sum_{i=1}^c \frac{\partial G}{\partial (\alpha N_i)} N_i$$

evaluate LHS and RHS at $\alpha=1$

$$\Rightarrow G = \left(\frac{\partial G}{\partial N_1} \right)_{T, p, N_{j \neq 1}} N_1 + \left(\frac{\partial G}{\partial N_2} \right)_{T, p, N_{j \neq 2}} N_2 + \dots = \sum_{i=1}^c \left(\frac{\partial G}{\partial N_i} \right)_{T, p, N_{j \neq i}} N_i$$

From The Equation of state for G

$$\mu_i = \left(\frac{\partial G}{\partial N_i} \right)_{T, p, N_{j \neq i}}$$

$$\Rightarrow \boxed{G = \sum_{i=1}^c \mu_i N_i}$$

— Pure substance that forms a single phase

(g) A block of copper at room temperature and ambient pressure

$$G = N \mu \quad \begin{array}{l} \nearrow \text{number of moles} \\ \rightarrow \text{chemical potential} \end{array}$$

$$\boxed{\mu = \frac{G}{N}}$$

PHASE TRANSITIONS & ONE COMPONENT SYSTEMS:

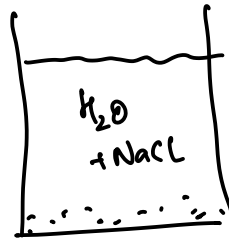
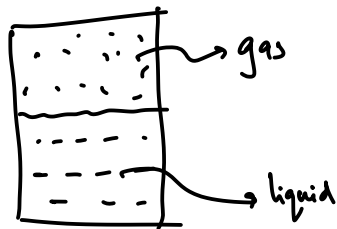
We will control $T, p \rightarrow$ look for states (phases) with lowest G

To find the lowest energy state we need to know how G changes with T, p .

$$\Rightarrow \boxed{dG = -SdT + Vdp}$$

* Reminder:

What is a phase?



Both containers have "distinct portions" with properties that are markedly different

(eg) ρ_{liquid} v/s $\rho_{\text{solid}} \rightarrow$ densities

each "distinct portion" $\rightarrow$ PHASE

* The shape of the Gibbs free energies:

$$dG = Vdp - SdT$$

$$\left(\frac{\partial G}{\partial p}\right)_T = V > 0$$

$$\left(\frac{\partial G}{\partial T}\right)_p = -S < 0$$

Curvature

$$\left(\frac{\partial^2 G}{\partial T^2}\right)_p = -\left(\frac{\partial S}{\partial T}\right)_p = -C_p/T < 0$$

$$\left(\frac{\partial^2 G}{\partial p^2}\right)_T = \left(\frac{\partial V}{\partial p}\right)_T = -V\kappa$$

< 0

* The phases and phase diagram of water:

Water is commonly known to have 3 PHASES

- Solid
- Liquid
- Gas

let $\alpha \rightarrow$ denote one of these phases of water

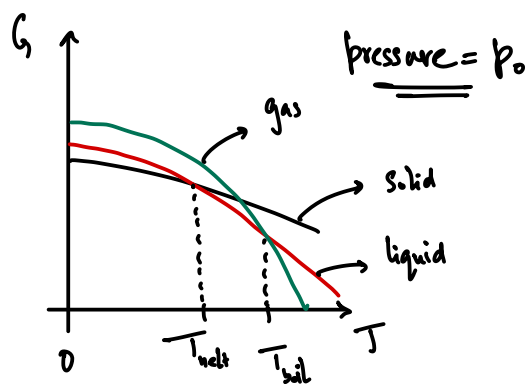
$$G^\alpha = U^\alpha - TS^\alpha + pV^\alpha \rightarrow \text{we control } T \text{ \& } p$$

$$\boxed{G^\alpha = H^\alpha - TS^\alpha}$$

Notice @ $T=0$

$$G^\alpha = H^\alpha$$

$$\text{Usually } \left[\begin{array}{l} S^{\text{gas}} > S^{\text{liquid}} > S^{\text{solid}} \\ H^{\text{gas}}(T=0) > H^{\text{liquid}}(T=0) > H^{\text{solid}}(T=0) \end{array} \right]$$



Recall for eq^m: $dG \leq 0$ @ G (the characteristic potential) is minimized

$\Rightarrow$ At any given temperature the phase with the lowest Gibbs free energy is the eq^m phase

$$\left[\begin{array}{l} T < T_{\text{melt}} \rightarrow \text{solid} \\ T_{\text{melt}} < T < T_{\text{boil}} \rightarrow \text{liquid} \\ T_{\text{boil}} < T \rightarrow \text{gas} \end{array} \right]$$

[REPEAT FOR SUBLIMATION]

$$\left[\begin{array}{l} \text{At } T = T_{\text{melt}} \\ (G^{\text{solid}} = G^{\text{liquid}}) < G^{\text{gas}} \\ \\ \text{At } T = T_{\text{boil}} \\ (G^{\text{liquid}} = G^{\text{gas}}) < G^{\text{solid}} \end{array} \right]$$