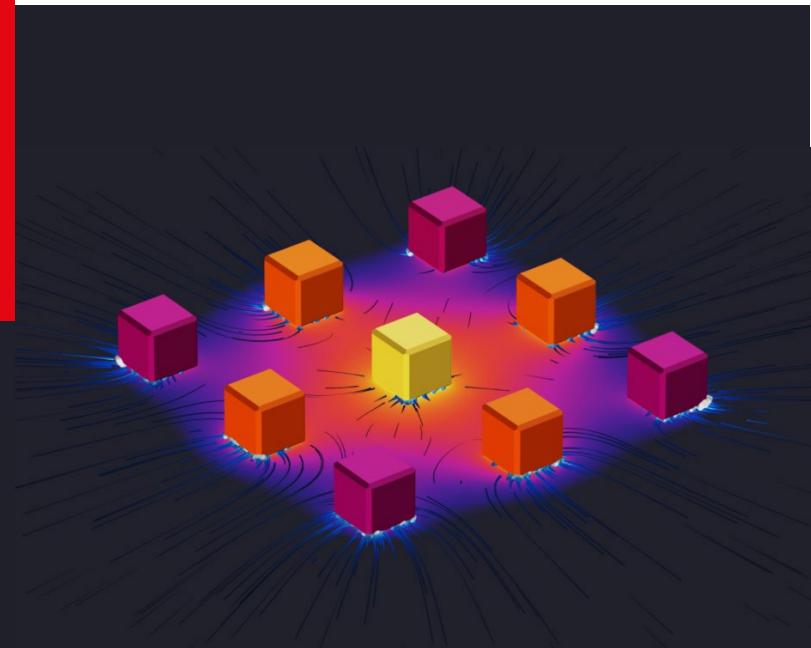


# Heat and Mass Transfer

## ME-341

*Instructor:* Giulia Tagliabue



# From Thermodynamics to Heat Transfer

Thermodynamics

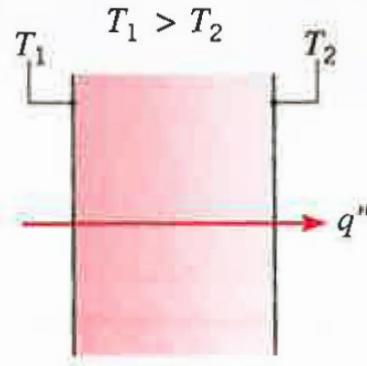


Heat Transfer

Although thermodynamics may be used to determine the amount of heat needed for a system to pass from one equilibrium state to another it does not acknowledge that heat transfer is inherently a non-equilibrium process. In fact, for heat transfer to occur there **MUST** be a TEMPERATURE GRADIENT. (Incropera, Ch. 1.3)

# Transport Laws

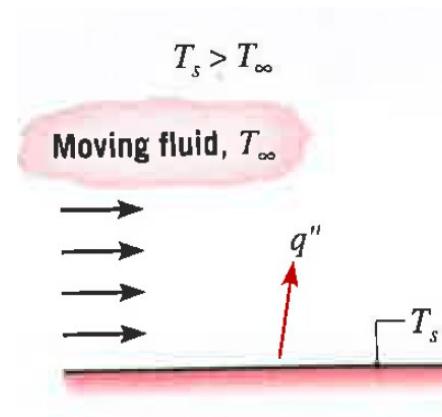
## Conduction



Fourier's Law

$$q'' = -k \frac{dT}{dx}$$

## Convection



Newton's Law

$$q'' = \bar{h} (T_s - T_\infty)$$

# Heat Transfer Mechanisms and Transport Laws

## Conduction

- Planar and radial systems
- With and without heat sources
- Steady-state and Transient

- Thermal resistances/Thermal circuits/Heat transfer coefficient U
- Dimensionless numbers (Re, Nu, Pr, Bi, Ra, Gr)
- Characteristic dimensions & reference temperature
- Mass/Momentum/**Energy conservation** equations

$$\frac{1}{\alpha} \frac{\partial T}{\partial t} = \nabla^2 T + \frac{\dot{q}}{k}$$

Conduction → Only Diffusion  
(Closed system)

## Convection

- Forced convection (External and Internal)
- Free convection
- Boiling and Condensation

- Thermal resistances/Thermal circuits/Heat transfer coefficient U
- Dimensionless numbers (Re, Nu, Pr, Bi, Ra, Gr)
- Characteristic dimensions & reference temperature
- Mass/Momentum/**Energy conservation** equations

$$\rho c_p \left( \frac{\partial T}{\partial t} + \vec{u} \cdot \nabla T \right) = k \nabla^2 T + \dot{q}$$

Convection → Diffusion + Advection  
(Open system)

Design a Heat Exchanger

# This lecture

- Introduction to Heat Exchangers
- The problem of the overall heat transfer coefficient
- RECAP of critical concepts

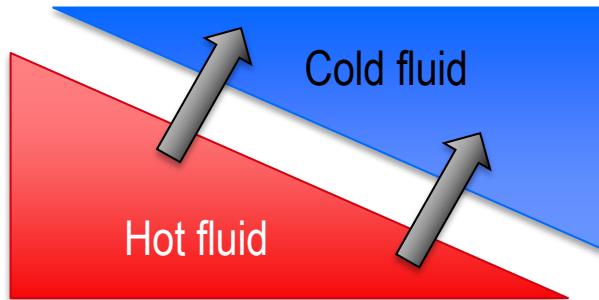
## Learning Objectives:

- Understand the concept and possible design of heat exchangers

# Introduction to Heat Exchangers

Power production  
(boilers/condensers)

Chemical  
Processing



Air-conditioning &  
Waste-heat recovery

Natural Systems

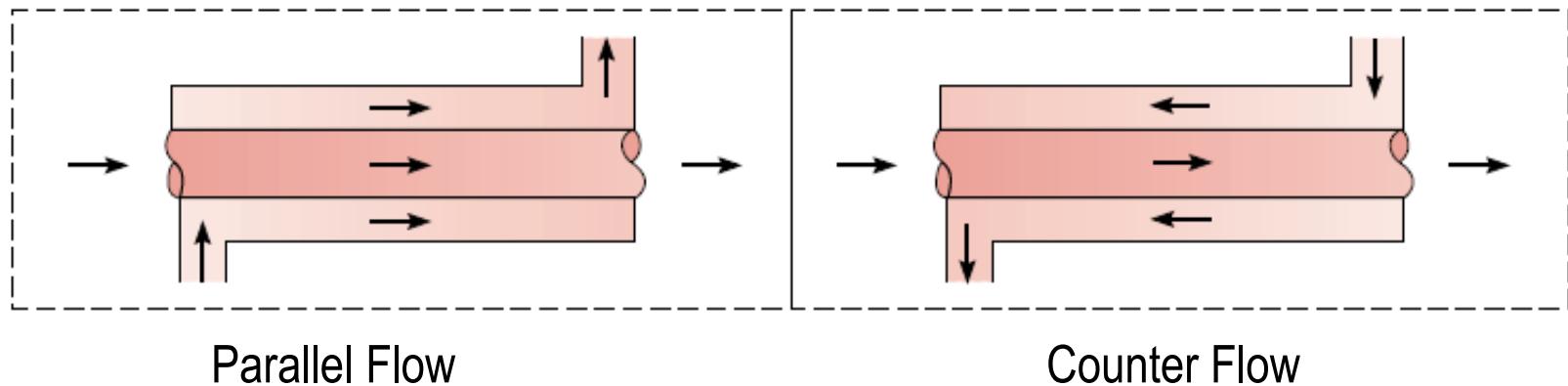
# Introduction to Heat Exchangers



Flow arrangement ?

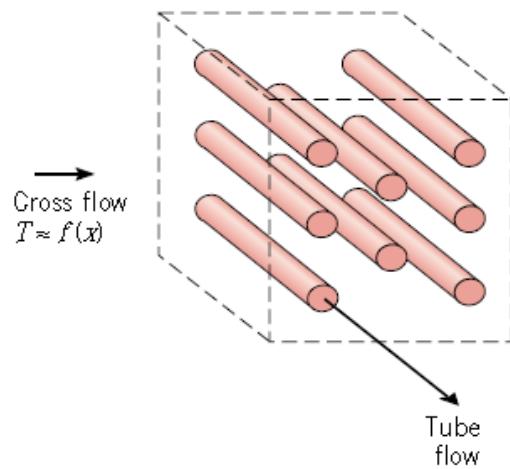
# Introduction to Heat Exchangers

## A. Concentric Flow

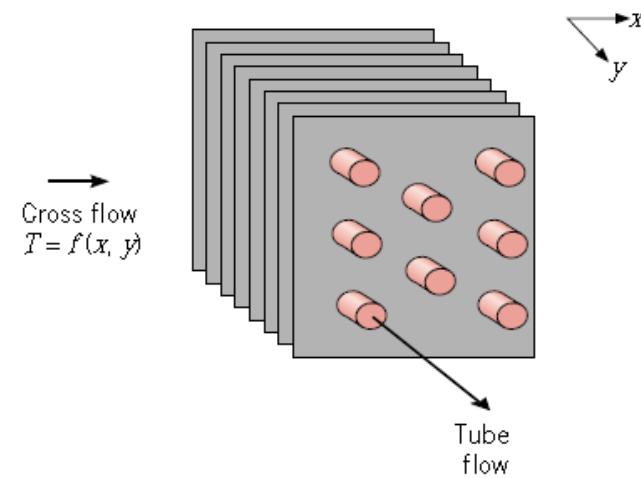


# Introduction to Heat Exchangers

## B. Cross-Flow



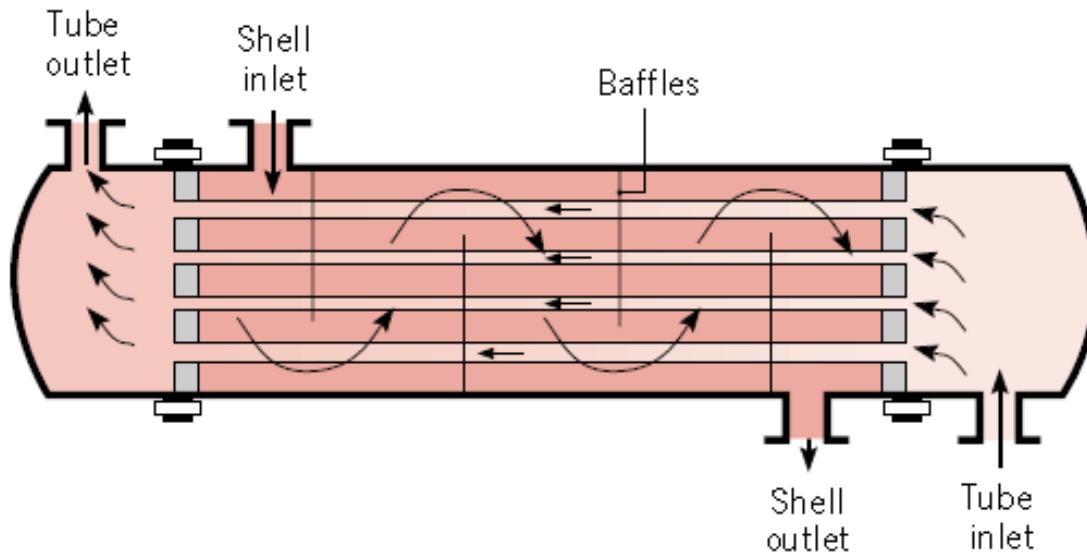
Mixed Flow (Unfinned)



Unmixed Flow (Finned)

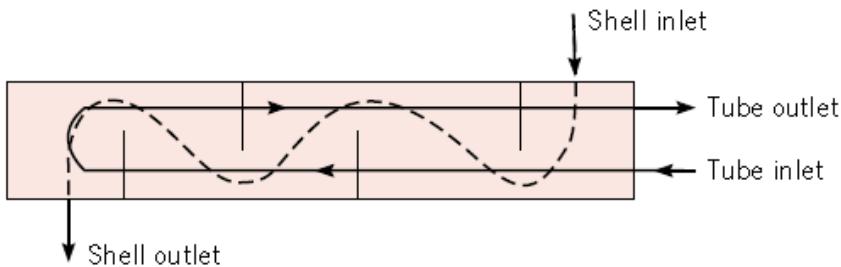
# Introduction to Heat Exchangers

## C. Shell-and-Tube

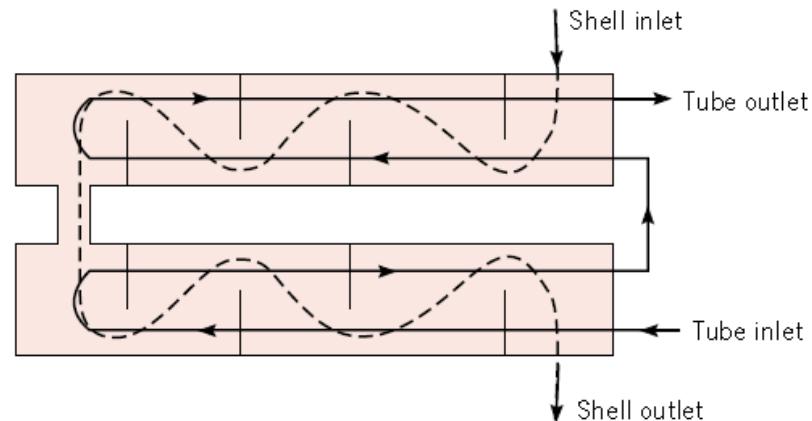


# Introduction to Heat Exchangers

## c. Shell-and-Tube



1 Shell pass  
2 Tube passes



2 Shell passes  
4 Tube passes

# This lecture



- Introduction to Heat Exchangers
- The problem of the overall heat transfer coefficient
- RECAP of critical concepts

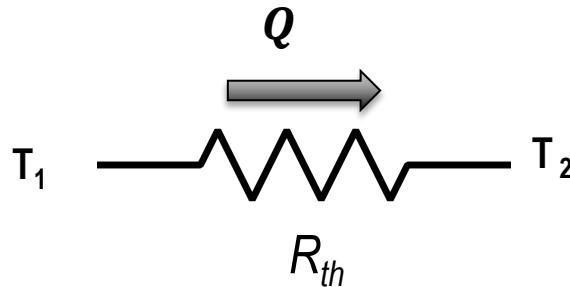
## Learning Objectives:



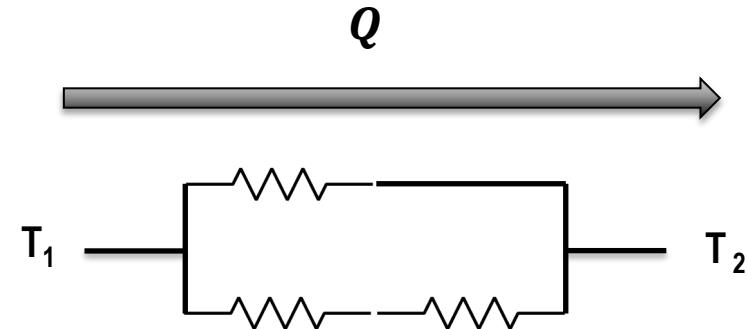
- Understand the concept and possible design of heat exchangers

# Overall Heat Transfer Coefficient

*Thermal Resistance & Thermal Circuits*



$$Q = \frac{(T_1 - T_2)}{R_{th}}$$



$$Q = \frac{(T_1 - T_2)}{R_{tot}}$$

# Overall Heat Transfer Coefficient

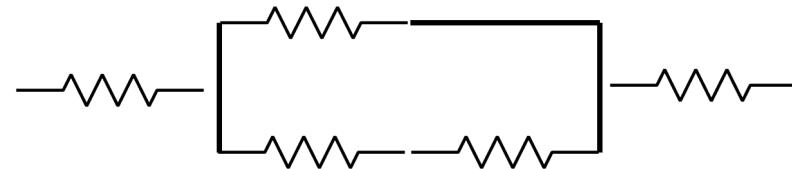
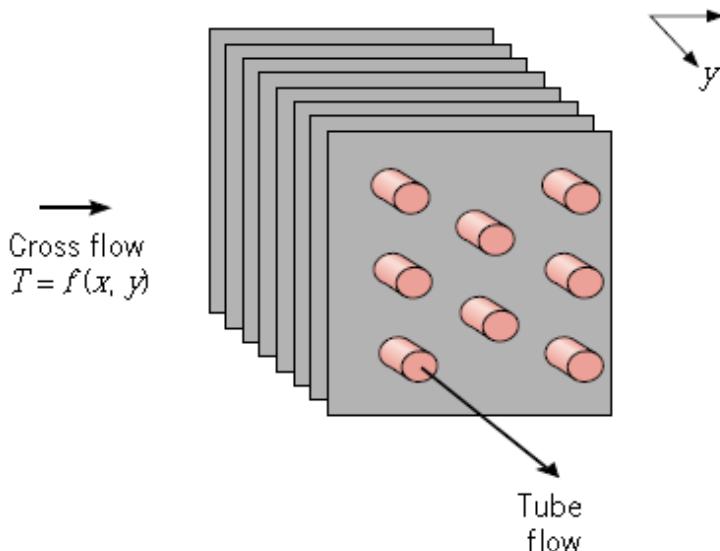
$$Q = \frac{\Delta T}{R_{tot}} = \mathbf{U} A \Delta T$$



$$U \equiv \frac{1}{R_{tot} A}$$



$$\frac{1}{U A} \equiv R_{tot}$$



*Note: we will discuss the expression for  $\Delta T$  later*

# Overall Heat Transfer Coefficient

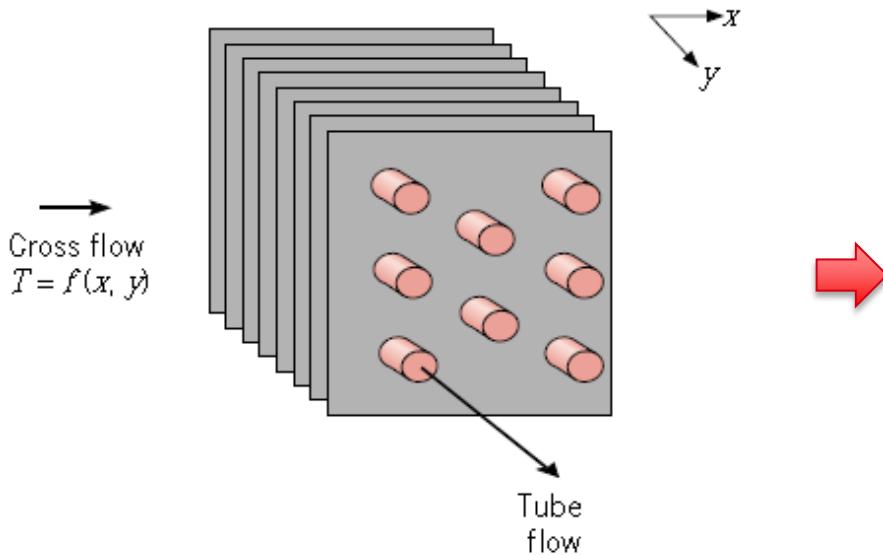
$$Q = \frac{\Delta T}{R_{tot}} = \mathbf{U} A \Delta T$$



$$U \equiv \frac{1}{R_{tot} A}$$



$$\frac{1}{U A} \equiv R_{tot}$$



- Conduction thermal resistances
  - Planar/radial conduction
- Convection thermal resistances
  - Internal and external
- Array of Fins
- Fouling

# This lecture

- Introduction to Heat Exchangers
- The problem of the overall heat transfer coefficient
- RECAP of critical concepts

## Learning Objectives:

- Understand the concept and possible design of heat exchangers

# Overall Heat Transfer Coefficient

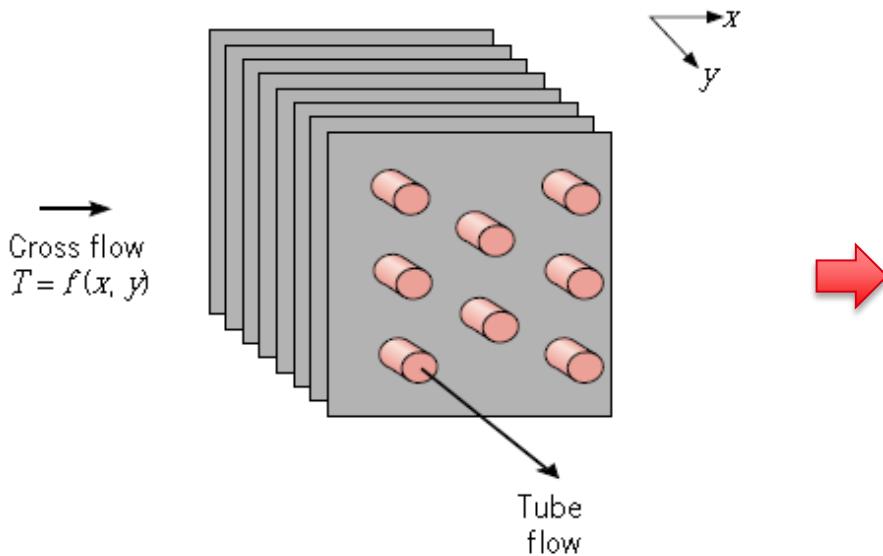
$$Q = \frac{\Delta T}{R_{tot}} = \mathbf{U} A \Delta T$$



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$$\frac{1}{U A} \equiv R_{tot}$$

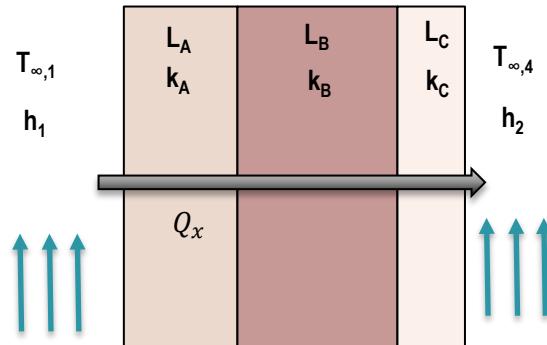


- Conduction thermal resistances
  - Planar/radial conduction
- Convection thermal resistances
  - Internal and external
- Array of Fins
- Fouling

# Conduction Thermal Resistance

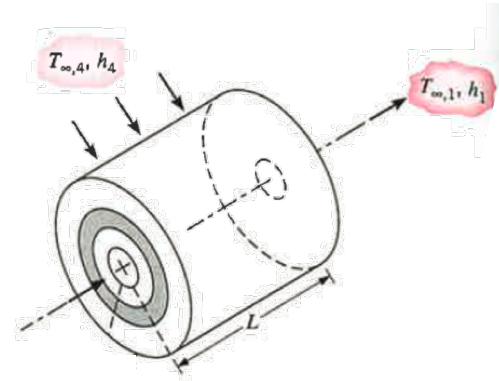
Planar wall

$$R_{th,cond} = \frac{L}{kA} \quad [ \text{K/W} ]$$



Radial System

$$R_{th,cond-cyl} = \frac{\ln(r_2/r_1)}{2\pi L k} \quad [ \text{K/W} ]$$



What is the critical assumption underlying these expressions ?

# Convection Thermal Resistances

Planar wall

$$R_{th,conv} = \frac{1}{hA} \quad [K/W]$$

Radial System

$$R_{th,conv} = \frac{1}{h2\pi rL} \quad [K/W]$$

Where  $h$  must be determined with the appropriate correlations!!



Determine the right correlation

# General methodology for calculating the convection coefficient

0. Identify the type of convection (Forced/External, Forced/Internal, Free, Boiling/Condensation)
1. Recognize the flow geometry (plate, cylinder, inner/outer flow etc.) **[GEOM]**
2. Specify the appropriate reference temperature and evaluate the pertinent fluid properties at that temperature  $T_f$ 
  - External convection over a plate/cylinder:  $T_f = (T_s + T_\infty)/2$
  - External convection over a bank of tubes:  $T_f = (T_{in} + T_{out})/2$
  - Internal convection:  $T_f = (T_{m,i} + T_{m,o})/2$
  - Free convection:  $T_f = (T_s + T_\infty)/2$
  - Boiling: a) film pool boiling  $T_l = T_{sat}$ ,  $T_v = T_f = (T_s + T_{sat})/2$ ; b) all other types of boiling  $T_l = T_v = T_{sat}$
  - Condensation (film):  $T_v = T_{sat}$ ,  $T_l = T_f = (T_s + T_{sat})/2$

*Note: If the necessary temperatures are unknown, we can use  $T_\infty$ ,  $T_{in}$  or  $T_{sat}$  to estimate all of the fluid properties. Once we obtain  $T_s$ ,  $T_{out}$ ,  $T_{m,o}$  we need to check whether it was reasonable.*
3. Calculate the Reynolds number (be careful to use the right characteristic dimension -  $x, L, D$  – and velocity -  $u_m, u_\infty$ ) or the Gr&Ra numbers. Determine the flow conditions (laminar/turbulent) **[FLOW]**
4. Decide whether a local or surface average coefficient is required **[Loc/Ave]**
5. Calculate Pr or get it from the table **[Pr]**
6. Select the appropriate correlation, determine Nu and the convection coefficient or directly h **[Nu, h]**

# (Radiation Thermal Resistances)

(Radiation Thermal Resistance)

Planar wall

$$R_{th,rad} = \frac{1}{h_{rad}A} \quad [\text{K/W}]$$

Radial System

$$R_{th,rad} = \frac{1}{h_{rad}2\pi rL} \quad [\text{K/W}]$$

where

$$Q_x = A\varepsilon\sigma(T_s^4 - T_{sur}^4) = Ah_{rad}(T_s - T_{sur})$$

→  $h_{rad} = \varepsilon\sigma(T_s^2 + T_{sur}^2)(T_s + T_{sur})$

# Overall Heat Transfer Coefficient

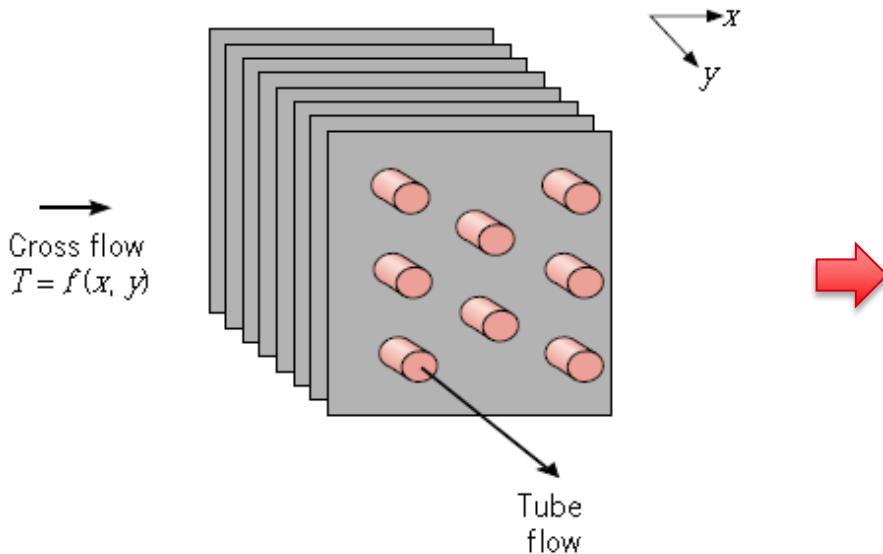
$$Q = \frac{\Delta T}{R_{tot}} = \mathbf{U} A \Delta T$$



$$U \equiv \frac{1}{R_{tot} A}$$

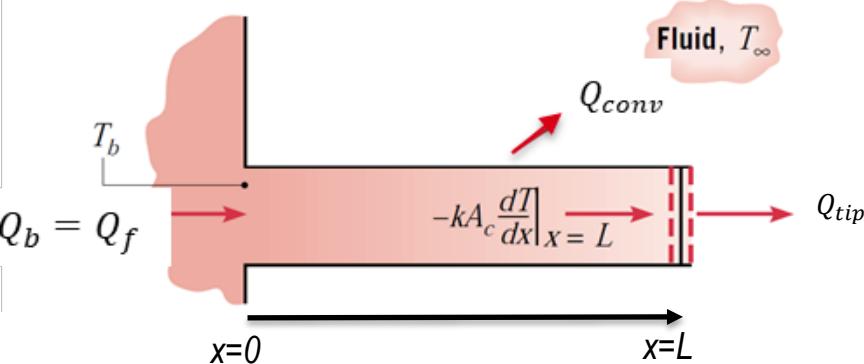


$$\frac{1}{U A} \equiv R_{tot}$$



- Conduction thermal resistances
  - Planar/radial conduction
- Convection thermal resistances
  - Internal and external
- **Array of Fins**
- Fouling

# Heat Transfer from Fin of Uniform Cross-Section



$$\frac{d^2\theta}{dx^2} - m^2\theta = 0 \quad \rightarrow \quad \theta = C_1 e^{mx} + C_2 e^{-mx}$$

**Boundary conditions:**

- Fin base  $T(x = 0) = T_b$
- Fin tip  $\theta_{x=0} = \theta_b$

1. Adiabatic  $\frac{d\theta}{dx} \Big|_{x=L} = 0$

2. Convection  $-kA_c \frac{d\theta}{dx} \Big|_{x=L} = hA_c(T(L) - T_\infty)$

3. Temperature  $\theta_{x=L} = \theta_L$

4. Infinite fin  $\theta_L \rightarrow 0$

# Heat Transfer from Fin of Uniform Cross-Section - Recap

**TABLE 3.4** Temperature distribution and heat loss for fins of uniform cross section

Case	Tip Condition ( $x = L$ )	Temperature Distribution $\theta/\theta_b$	Fin Heat Transfer Rate $Q_f$
A	Convection heat transfer: $h\theta(L) = -kd\theta/dx _{x=L}$	$\frac{\cosh m(L-x) + (h/mk) \sinh m(L-x)}{\cosh mL + (h/mk) \sinh mL} \quad (3.70)$	$M \frac{\sinh mL + (h/mk) \cosh mL}{\cosh mL + (h/mk) \sinh mL} \quad (3.72)$
B	Adiabatic $d\theta/dx _{x=L} = 0$	$\frac{\cosh m(L-x)}{\cosh mL} \quad (3.75)$	$M \tanh mL \quad (3.76)$
C	Prescribed temperature: $\theta(L) = \theta_L$	$\frac{(\theta_L/\theta_b) \sinh mx + \sinh m(L-x)}{\sinh mL} \quad (3.77)$	$M \frac{(\cosh mL - \theta_L/\theta_b)}{\sinh mL} \quad (3.78)$
D	Infinite fin ( $L \rightarrow \infty$ ): $\theta(L) = 0$	$e^{-mx} \quad (3.79)$	$M \quad (3.80)$
$\theta \equiv T - T_\infty$		$m^2 \equiv hP/kA_c$	
$\theta_b = \theta(0) = T_b - T_\infty$		$M \equiv \sqrt{hPkA_c} \theta_b$	

# Efficiency and Thermal Resistance (1 Fin)

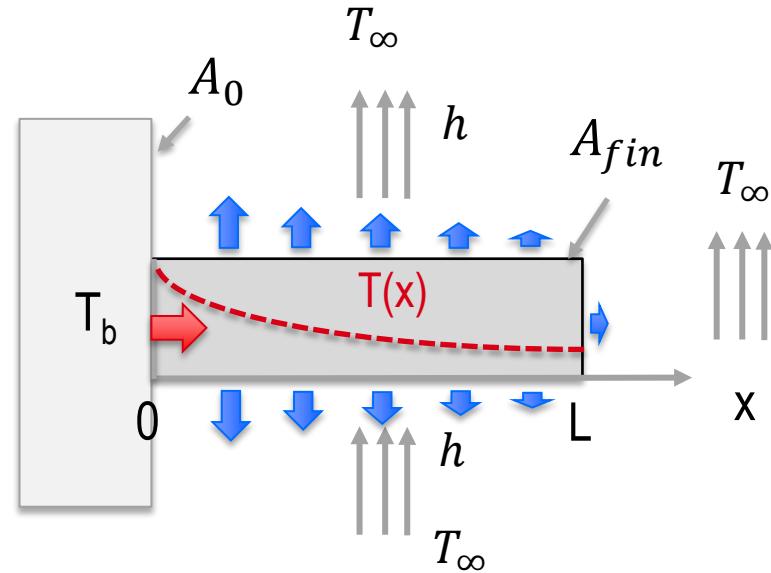
$$Q_f = Q_{b,cond} = -kA \frac{d\theta}{dx} \Big|_{x=0}$$

If  $T_b$  is the temperature of the fin base:

$$\Rightarrow \eta_f \equiv \frac{Q_f}{Q_{f,max}} = \frac{Q_f}{hA_f(T_b - T_\infty)} = \frac{Q_f}{hA_f\theta_b}$$

$$\Rightarrow Q_f = \eta_f h A_f (T_b - T_\infty)$$

$$\Rightarrow R_f \equiv \frac{(T_b - T_\infty)}{Q_f} = \frac{1}{hA_f\eta_f}$$



# Efficiency and Thermal Resistance (1 Fin)

TABLE 3.4 Temperature distrib

Case	Tip Condition ( $x = L$ )	Fin Heat Transfer Rate $Q_f$
A	Convection heat transfer: $h\theta(L) = -kd\theta/dx _{x=L}$	$M \frac{\sinh mL + (h/mk) \cosh mL}{\cosh mL + (h/mk) \sinh mL} \quad (3.72)$
B	Adiabatic $d\theta/dx _{x=L} = 0$	$M \tanh mL \quad (3.76)$
C	Prescribed temperature: $\theta(L) = \theta_L$	$M \frac{(\cosh mL - \theta_L/\theta_b)}{\sinh mL} \quad (3.78)$
D	Infinite fin ( $L \rightarrow \infty$ ): $\theta(L) = 0$	$M \quad (3.80)$

$\theta \equiv T - T_\infty$        $m^2 \equiv hP/kA_c$   
 $\theta_b = \theta(0) = T_b - T_\infty$        $M \equiv \sqrt{hPkA_c}\theta_b$

$$M = \sqrt{hPkA_c}\theta_b$$

$$\eta_f \equiv \frac{Q_f}{hA_f\theta_b} = \frac{M \tanh mL}{hPL\theta_b} = \frac{\tanh mL}{mL}$$

$$R_f \equiv \frac{1}{hA_f\eta_f}$$

$$\eta_f \equiv \frac{Q_f}{hA_f\theta_b} = \frac{M}{hA_f\theta_b} = \frac{1}{mL}$$

$$R_f \equiv \frac{\theta_b}{Q_f} = \frac{\theta_b}{M} = \frac{1}{\sqrt{hPkA_c}}$$

# Efficiency and Thermal Resistance (Fin Array)

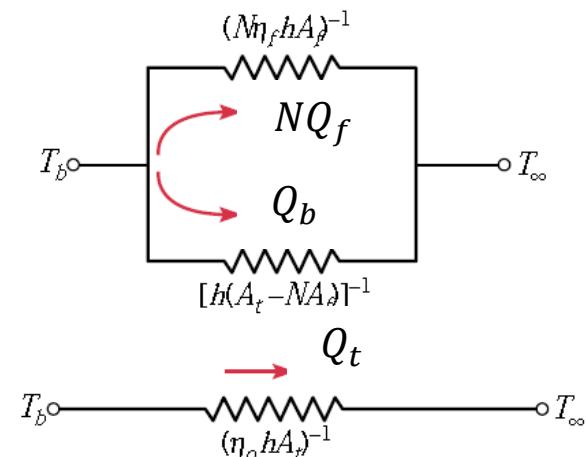
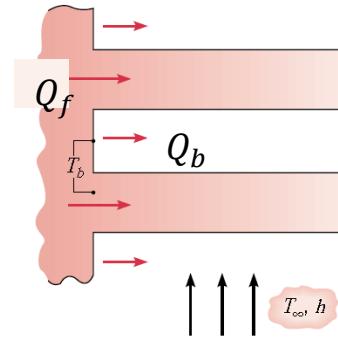
$$\eta_o \equiv \frac{Q_t}{Q_{t,max}} = \frac{Q_t}{hA_t(T_b - T_\infty)} = \frac{NQ_f + Q_b}{h(NA_f + A_b)(T_b - T_\infty)}$$

→  $\eta_o \equiv 1 - \frac{NA_f}{A_t} (1 - \eta_f)$  *Overall efficiency*

*Single fin efficiency*

→  $R_o \equiv \frac{(T_b - T_\infty)}{Q_t} = \frac{1}{\eta_o h A_t}$

Note: for the overall efficiency another common notation is  $\eta_t$

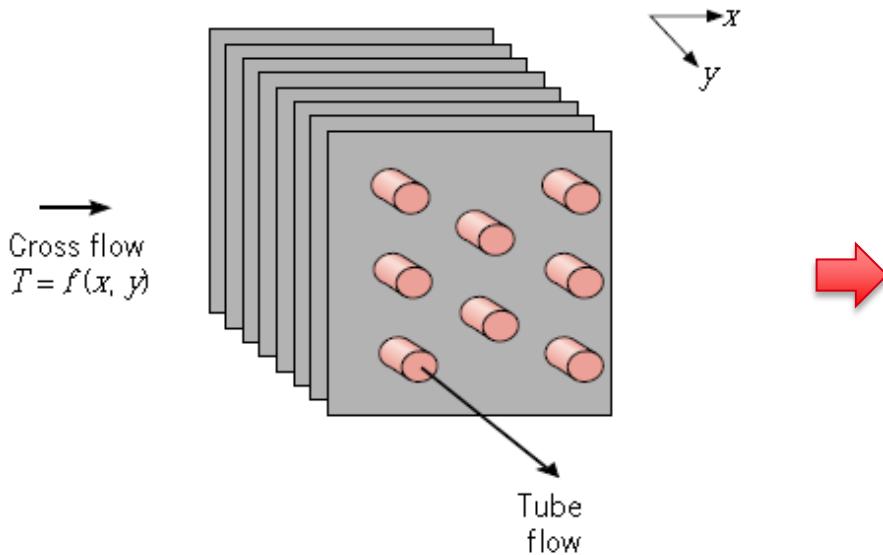


# Overall Heat Transfer Coefficient

$$Q = \frac{\Delta T}{R_{tot}} = \mathbf{U} A \Delta T \quad \rightarrow$$

$$U \equiv \frac{1}{R_{tot} A} \quad \rightarrow$$

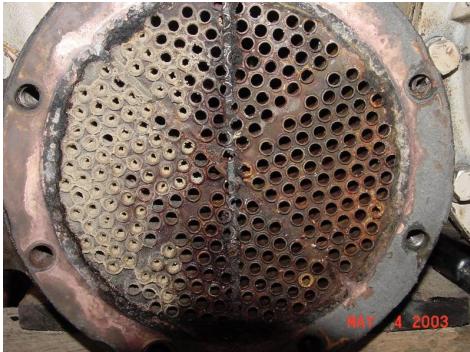
$$\frac{1}{U A} \equiv R_{tot}$$



- Conduction thermal resistances
  - Planar/radial conduction
- Convection thermal resistances
  - Internal and external
- Array of Fins
- **Fouling**

# Overall Heat Transfer Coefficient

## Fouling



Dramatic increase in thermal resistance due to poor conduction through the scaling layer

→ Introduce a *fouling* resistance per unit area (fouling factor)  $R_f''$

$$R_f'' \equiv AR_{foul} \quad \rightarrow \quad R_{foul} = \frac{R_f''}{A}$$

# This lecture



- Fouling
- The overall heat transfer coefficient

## Learning Objectives:

- Calculate the overall heat transfer coefficient

# Overall Heat Transfer Coefficient

$$Q = \frac{\Delta T}{R_{tot}} = \mathbf{U} A \Delta T$$

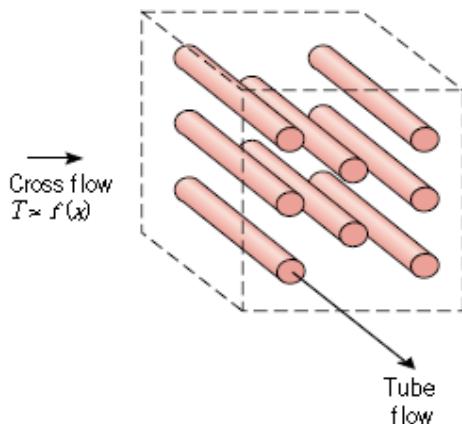


$$U \equiv \frac{1}{R_{tot} A}$$



$$\frac{1}{U A} \equiv R_{tot}$$

Example 1a: Without fouling



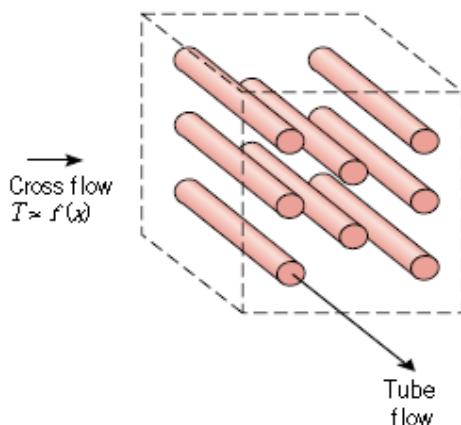
# Overall Heat Transfer Coefficient

$$Q = \frac{\Delta T}{R_{tot}} = \mathbf{U} A \Delta T$$

$$U \equiv \frac{1}{R_{tot} A}$$

$$\frac{1}{U A} \equiv R_{tot}$$

Example 1a: Without fouling



$$\frac{1}{U A} = R_{conv,out} + R_{cond} + R_{conv,in}$$

$$\frac{1}{U A} = \frac{1}{h_{out} A_{out}} + \frac{\ln(r_{out}/r_{in})}{2\pi k L} + \frac{1}{h_{in} A_{in}}$$

$h_{out}$  forced convection external flow  
 $h_{in}$  forced convection internal flow

# Overall Heat Transfer Coefficient

$$Q = \frac{\Delta T}{R_{tot}} = \mathbf{U} A \Delta T$$

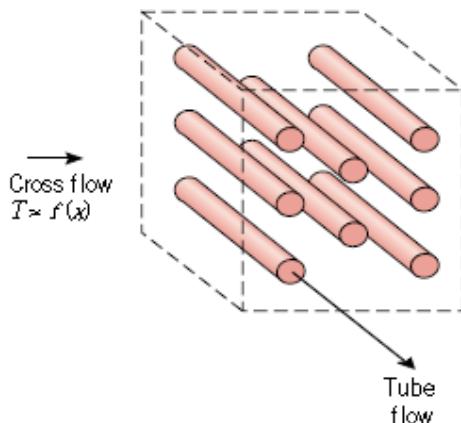


$$U \equiv \frac{1}{R_{tot} A}$$



$$\frac{1}{U A} \equiv R_{tot}$$

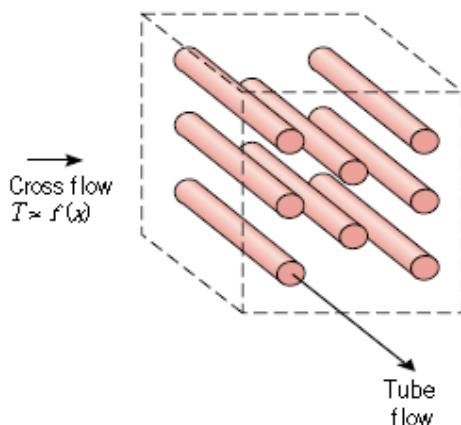
Example 1a: With fouling



# Overall Heat Transfer Coefficient

$$Q = \frac{\Delta T}{R_{tot}} = \mathbf{U} A \Delta T \quad \rightarrow \quad U \equiv \frac{1}{R_{tot} A} \quad \rightarrow \quad \frac{1}{U A} \equiv R_{tot}$$

Example 1a: With fouling



$$\frac{1}{U A} = R_{conv,out} + R_{foul,out} + R_{cond} + R_{foul,in} + R_{conv,in}$$

$$R_f'' \equiv A R_{foul} \quad \rightarrow \quad R_{foul} = \frac{R_f''}{A}$$

$$\frac{1}{U A} = \frac{1}{h_{out} A_{out}} + \frac{R_{f,o}''}{A_{out}} + \frac{\ln(r_{out}/r_{in})}{2\pi k L} + \frac{R_{f,i}''}{A_{in}} + \frac{1}{h_{in} A_{in}}$$

# Overall Heat Transfer Coefficient

$$Q = \frac{\Delta T}{R_{tot}} = \mathbf{U} A \Delta T$$

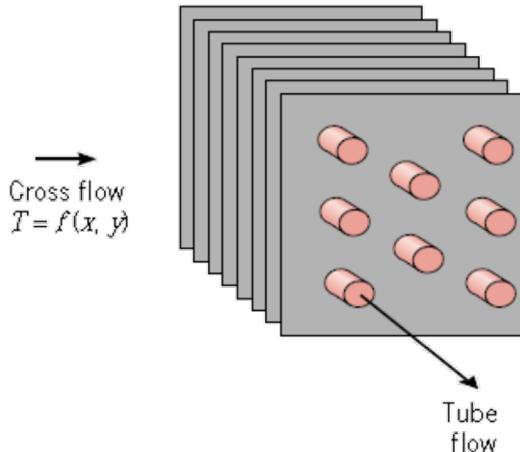


$$U \equiv \frac{1}{R_{tot} A}$$



$$\frac{1}{U A} \equiv R_{tot}$$

Example 2a: Finned, without fouling



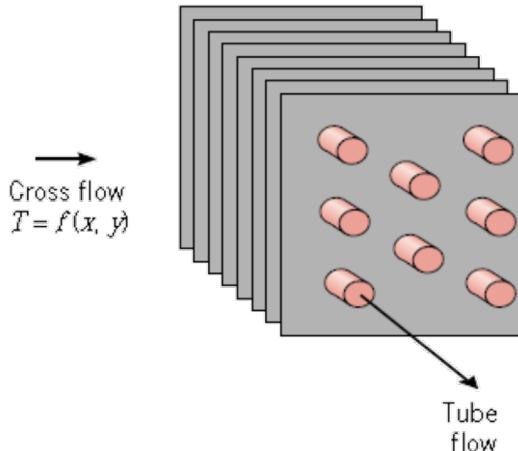
# Overall Heat Transfer Coefficient

$$Q = \frac{\Delta T}{R_{tot}} = \mathbf{U} A \Delta T$$

$$U \equiv \frac{1}{R_{tot} A}$$

$$\frac{1}{U A} \equiv R_{tot}$$

Example 2a: Finned, without fouling



$$\frac{1}{U A} = R_{conv,out} + R_{cond} + R_{conv,in}$$

$$R_{conv,out} = R_{fin\ array} \equiv \frac{(T_0 - T_\infty)}{Q_t} = \frac{1}{\eta_o h A_{total}}$$

$$\frac{1}{U A} = \frac{1}{\eta_o h_{out} A_{out}} + \frac{\ln(r_{out}/r_{in})}{2\pi k L} + \frac{1}{h_{in} A_{in}}$$

# Overall Heat Transfer Coefficient

$$Q = \frac{\Delta T}{R_{tot}} = \mathbf{U} A \Delta T$$

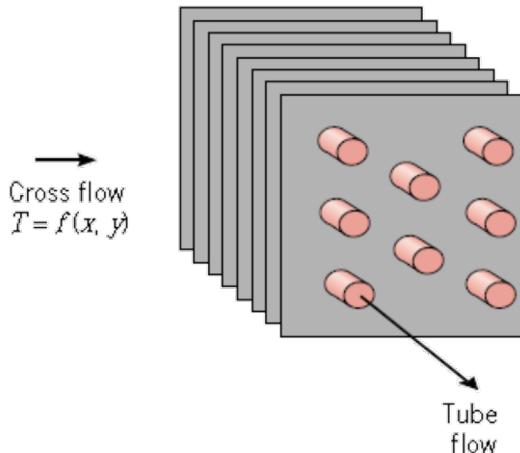


$$U \equiv \frac{1}{R_{tot} A}$$



$$\frac{1}{U A} \equiv R_{tot}$$

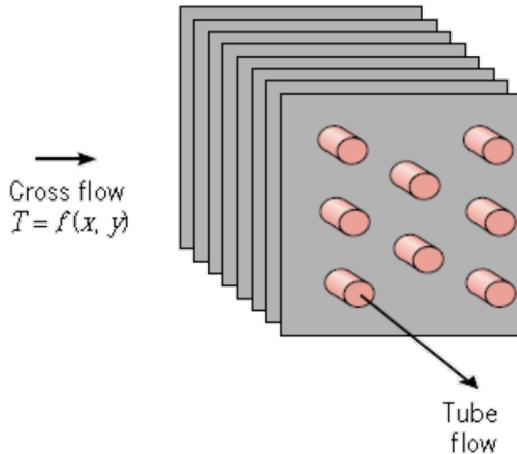
Example 2a: Finned, with fouling



# Overall Heat Transfer Coefficient

$$Q = \frac{\Delta T}{R_{tot}} = \mathbf{U} A \Delta T \quad \rightarrow \quad U \equiv \frac{1}{R_{tot} A} \quad \rightarrow \quad \frac{1}{U A} \equiv R_{tot}$$

Example 2a: Finned, with fouling



$$\frac{1}{U A} = R_{conv,out} + R_{foul,out} + R_{cond} + R_{foul,in} + R_{conv,in}$$

$$R_{overall \ fin \ array} \equiv \frac{(T_0 - T_\infty)}{Q_t} = \frac{1}{\eta_o h A_t} = \frac{1}{h(\eta_o A_t)} = \frac{1}{h A'_t}$$

$$R_{foul} = \frac{R_f''}{A'_t} = \frac{R_f''}{\eta_o A_t}$$

$$\frac{1}{U A} = \frac{1}{\eta_o h_{out} A_{out}} + \frac{R_{f,o}''}{\eta_o A_{out}} + \frac{\ln(r_{out}/r_{in})}{2\pi k L} + \frac{R_{f,i}''}{A_{in}} + \frac{1}{h_{in} A_{in}}$$

# Overall Heat Transfer Coefficient

$$Q = \frac{\Delta T}{R_{tot}} = \mathbf{U} A \Delta T \quad \rightarrow \quad U \equiv \frac{1}{R_{tot} A} \quad \rightarrow \quad \frac{1}{U A} \equiv R_{tot}$$

In the most general case we could have fins present also on the inner side:

$$\frac{1}{U A} = \frac{1}{\eta_{o,out} h_{out} A_{out}} + \frac{R_{f,o}''}{\eta_{o,out} A_{out}} + R_{cond} + \frac{R_{f,i}''}{\eta_{o,in} A_{in}} + \frac{1}{\eta_{o,in} h_{in} A_{in}}$$

Account for all the layers of conduction!!

# Overall Heat Transfer Coefficient

$$Q = \frac{\Delta T}{R_{tot}} = \mathbf{U} A \Delta T \quad \rightarrow \quad U \equiv \frac{1}{R_{tot} A} \quad \rightarrow \quad \frac{1}{U A} \equiv R_{tot}$$

Note:

$$\frac{1}{U A} \equiv R_{tot} = \frac{1}{U_{in} A_{in}} = \frac{1}{U_{out} A_{out}} = \frac{1}{U_{cold} A_{cold}} = \frac{1}{U_{hot} A_{hot}}$$

→  $U_{in} \equiv \frac{1}{R_{tot} A_{in}} \neq U_{out} \equiv \frac{1}{R_{tot} A_{out}}$        $U_{cold} \equiv \frac{1}{R_{tot} A_{cold}} \neq U_{hot} \equiv \frac{1}{R_{tot} A_{hot}}$

→ Calculate first the total heat transfer resistance  $R_{tot}$  then multiply by a specific area to determine the overall heat transfer coefficient with respect to a certain surface.

Note: Do not calculate U starting from  $R_{tot}''$  because it is likely you will mess up the areas (you can do it but you have to be extra careful as each term of the specific resistance will be normalized by a different area...)

# This lecture

-  Introduction to Heat Exchangers
-  The problem of the overall heat transfer coefficient
-  RECAP of critical concepts

## Learning Objectives:

-  Understand the concept and possible design of heat exchangers

# Next lecture

- The overall heat transfer coefficient

## Learning Objectives:

- Calculate the overall heat transfer coefficient