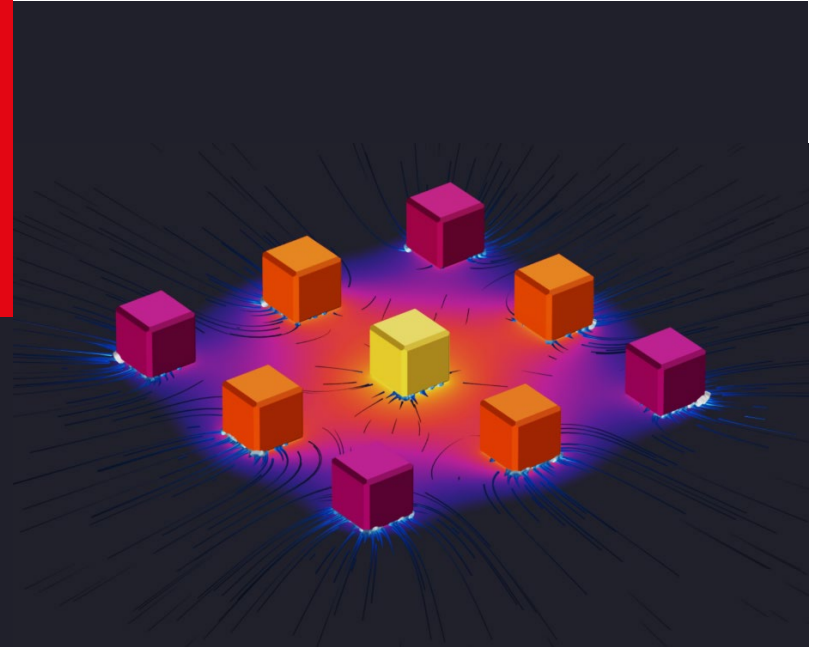


Heat and Mass Transfer ME-341

Instructor: Giulia Tagliabue



Spring Semester

Previously

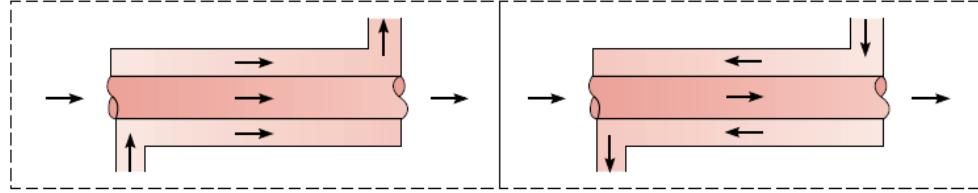
- ✓ ☒ Heat Exchangers Types
- ✓ ☒ Overall Heat Transfer Coefficient
- ✓ ☒ Parallel/Counter Flow Design
 - ✓ ☒ Temperature Profile and Total Heat Transfer

Learning Objectives:

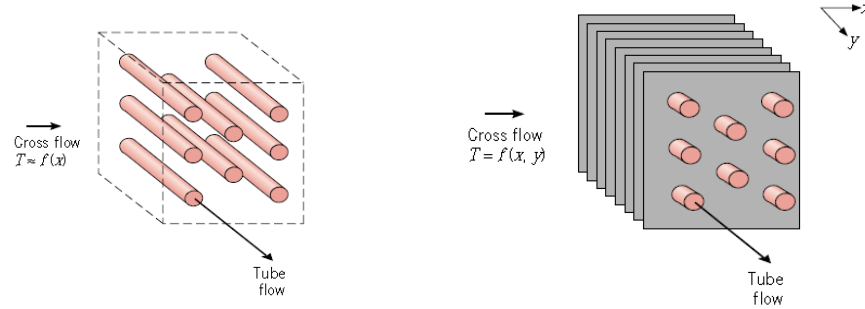
- ✓ ☒ Calculate the overall heat transfer coefficient
- ✓ ☒ Calculate the total heat transfer for parallel flow HE
- ✓ ☒ Calculate the total heat transfer for counter flow HE

Introduction to Heat Exchangers

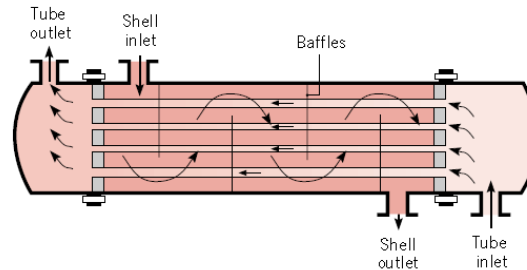
A. Concentric Flow



B. Cross-Flow



C. Shell-and-Tube



Overall Heat Transfer Coefficient

$$Q = \frac{\Delta T}{R_{tot}} = \mathbf{U} A \Delta T \quad \rightarrow \quad U \equiv \frac{1}{R_{tot} A} \quad \rightarrow \quad \frac{1}{UA} \equiv R_{tot}$$

In the most general case we could have fins present also on the inner side:

$$\frac{1}{UA} = \frac{1}{\eta_{o,out} h_{out} A_{out}} + \frac{R_{f,o}''}{\eta_{o,out} A_{out}} + \underbrace{R_{cond}} + \frac{R_{f,i}''}{\eta_{o,in} A_{in}} + \frac{1}{\eta_{o,in} h_{in} A_{in}}$$

Includes all the layers of conduction!!

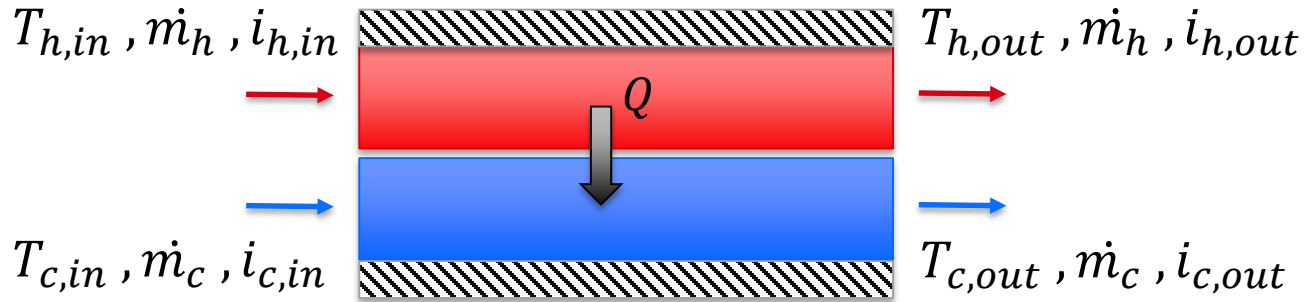
$$U_{in} \equiv \frac{1}{R_{tot} A_{in}} \neq U_{out} \equiv \frac{1}{R_{tot} A_{out}}$$

Parallel Flow Heat Exchanger

Energy balance

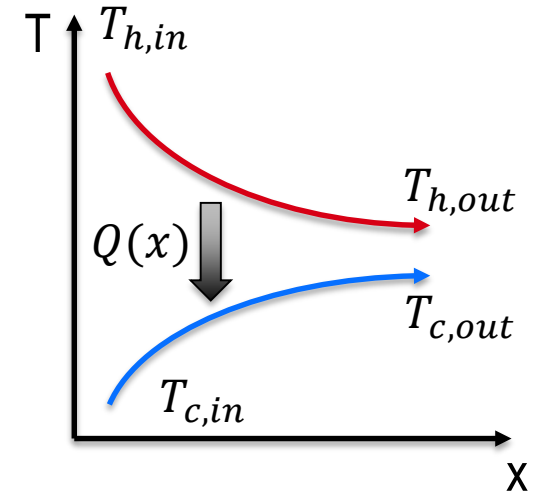
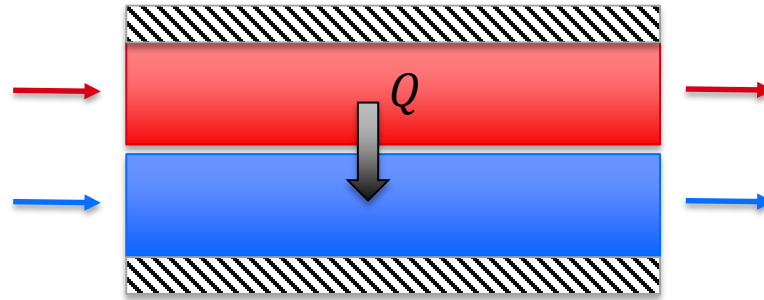
$i = \text{enthalpy}$

Not to confuse with
convection coefficient



Parallel Flow Heat Exchanger

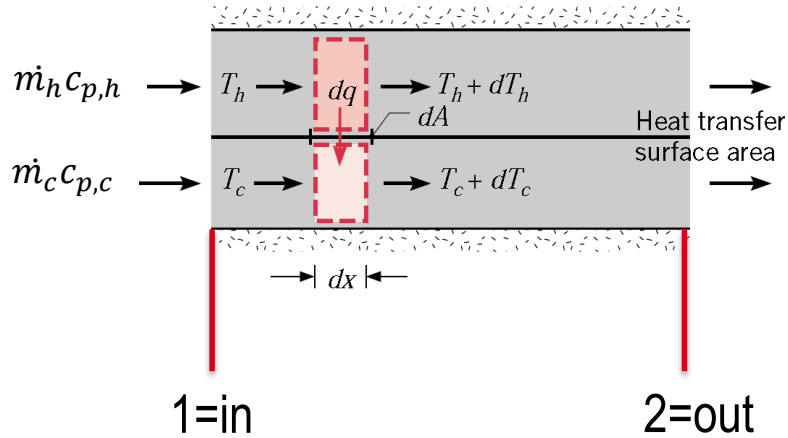
Temperature Profile



➡ What is an appropriate ΔT_m ?

Parallel Flow heat Exchanger

Temperature Profile and Total Heat Transfer



$$Q = UA \frac{\Delta T_2 - \Delta T_1}{\ln(\Delta T_2 / \Delta T_1)} = UA \Delta T_m$$

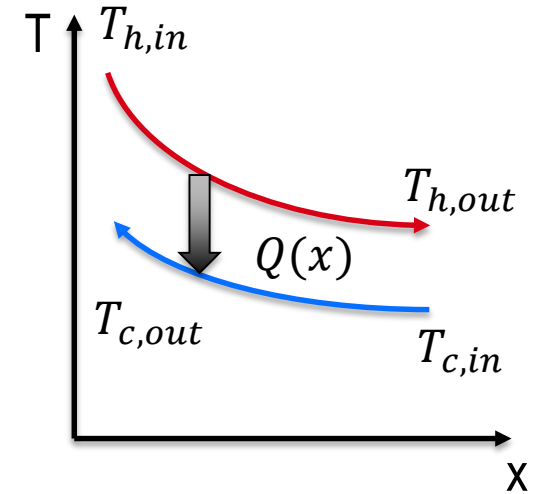
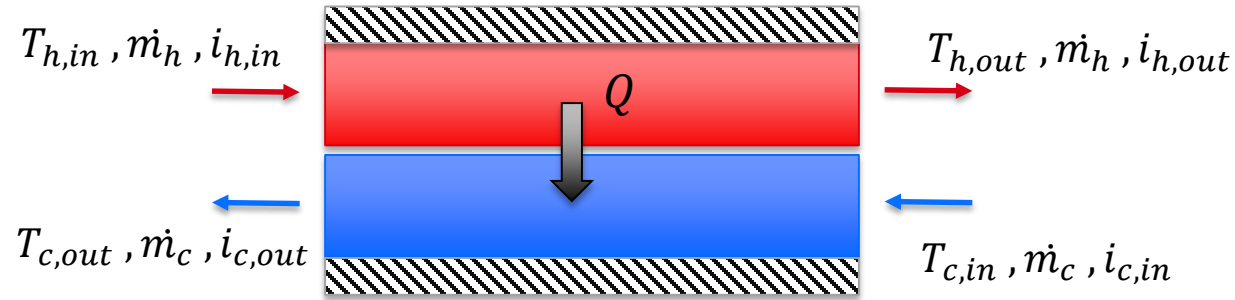
$$\Delta T_m = \frac{\Delta T_2 - \Delta T_1}{\ln(\Delta T_2 / \Delta T_1)}$$

$$\Delta T_1 = (T_{h,1} - T_{c,1}) = (T_{h,in} - T_{c,in})$$

$$\Delta T_2 = (T_{h,2} - T_{c,2}) = (T_{h,out} - T_{c,out})$$

Counter Flow Heat Exchanger

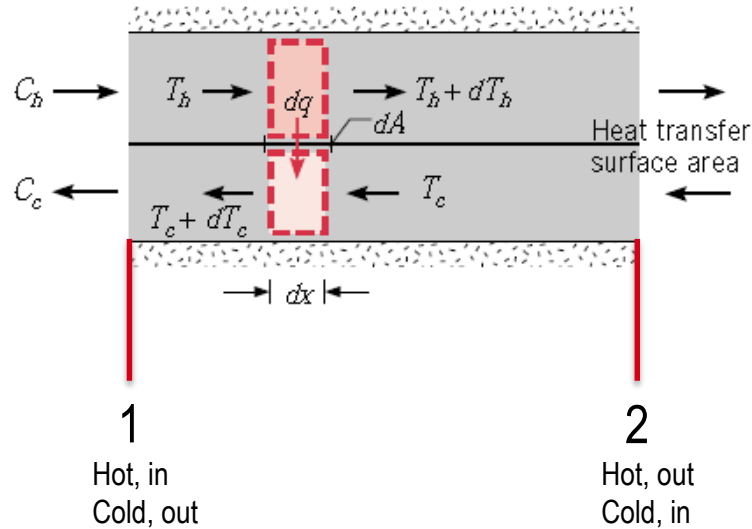
Temperature Profile



➡ What is an appropriate ΔT_m ?

Counter Flow heat Exchanger

Temperature Profile and Total Heat Transfer



$$Q = UA \frac{\Delta T_2 - \Delta T_1}{\ln(\Delta T_2 / \Delta T_1)} = UA \Delta T_m$$

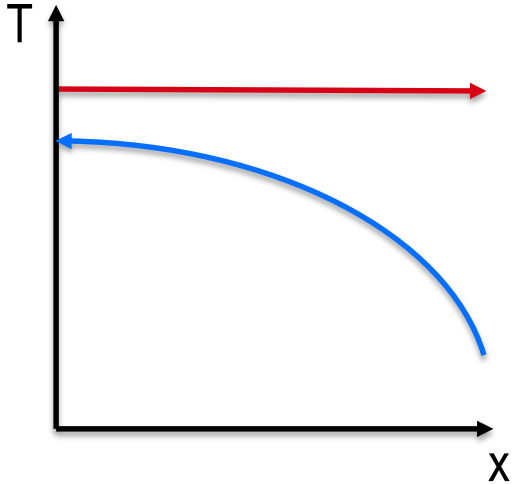
$$\Delta T_m = \frac{\Delta T_2 - \Delta T_1}{\ln(\Delta T_2 / \Delta T_1)}$$

$$\Delta T_1 = (T_{h,1} - T_{c,1}) = (T_{h,in} - T_{c,out})$$

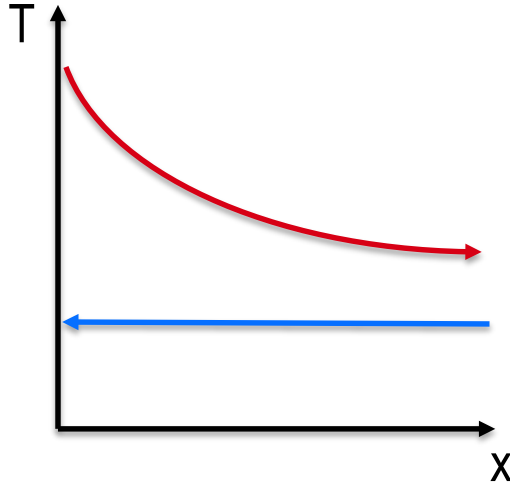
$$\Delta T_2 = (T_{h,2} - T_{c,2}) = (T_{h,out} - T_{c,in})$$

Special Operating Conditions

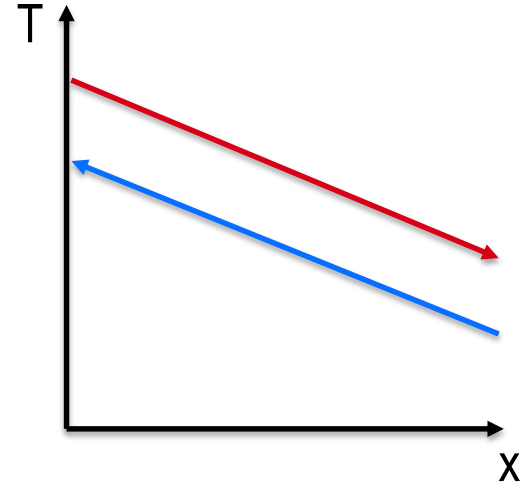
Representations Based on Counter Flow



- Condensing vapor on the hot-side
- $C_h \gg C_c$



- Evaporating liquid on the cold side
- $C_h \ll C_c$



- $C_h \sim C_c$

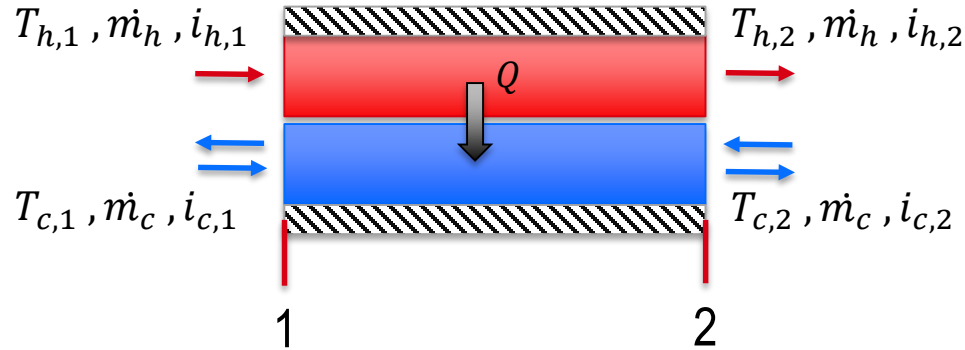
This Lecture

- ❑ Heat Exchanger Analysis/Design/Performance Calculation
 - ❑ Effectiveness-NTU method

Learning Objectives:

- ❑ Identify the design parameter for a heat exchanger
- ❑ Analyze the performance of a heat exchanger

Effectiveness-NTU Method



$$Q = -Q_h = -C_h(T_{h,out} - T_{h,in})$$

$$Q = Q_c = C_c(T_{c,out} - T_{c,in})$$

$$\Delta T_m = \frac{\Delta T_2 - \Delta T_1}{\ln(\Delta T_2 / \Delta T_1)}$$

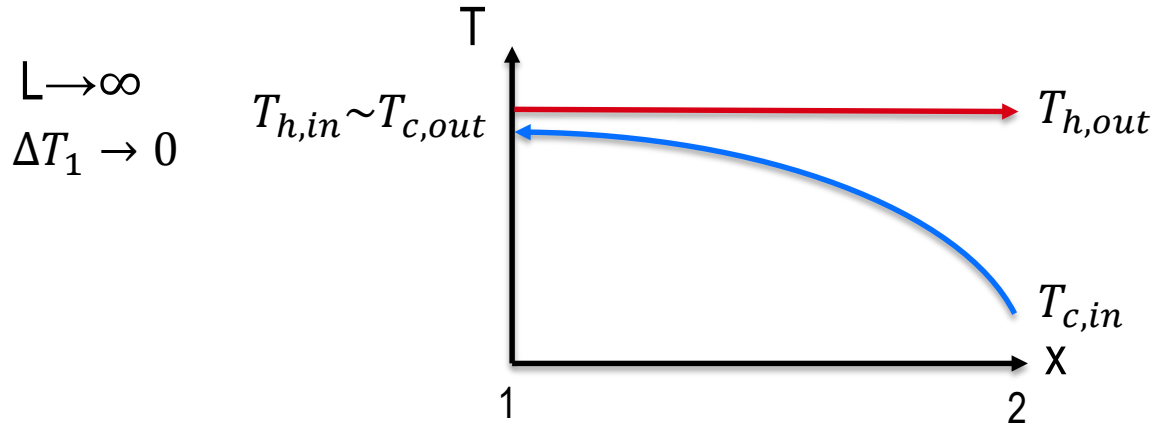
$$Q = UA \frac{\Delta T_2 - \Delta T_1}{\ln(\Delta T_2 / \Delta T_1)} = UA \Delta T_m$$

How do we design the heat exchanger if we do NOT know all the four temperatures ?
What about shell-tube heat exchangers where there are various flow configurations?

Effectiveness-NTU Method

We want to **determine the highest heat transfer** in the heat exchanger. We observe that:

➡ The maximum Q will be: $Q_{max} = C_{\min} \Delta T_{max} = C_{\min} (T_{max} - T_{min})$



$$C_h \gg C_c$$

$$\begin{aligned}
 Q_{max} &= C_c (T_{c,out} - T_{c,in}) \\
 &= C_c (T_{h,in} - T_{c,in})
 \end{aligned}$$

➡ The maximum ΔT occurs on the flow side with $C_{min} = \min(C_c, C_h)$

$$dq = -dq_h = -C_h dT_h$$

$$dq = dq_c = C_c dT_c$$

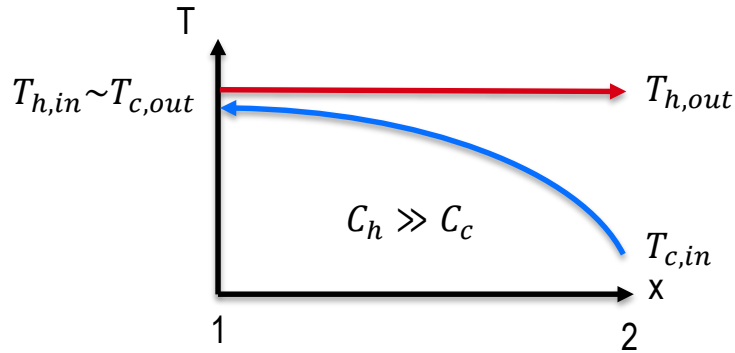


If $C_c \gg C_h$ then $|dT_c| \ll |dT_h|$ and viceversa.

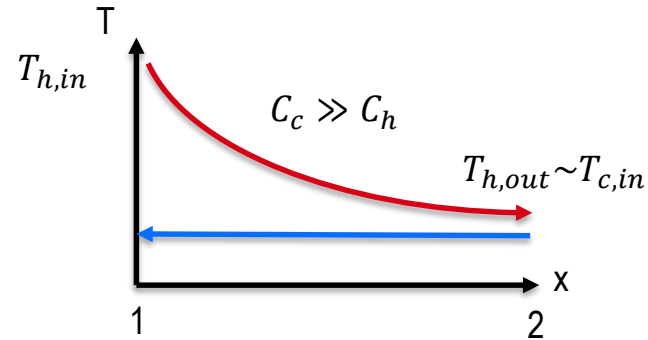
Effectiveness-NTU Method

We want to **determine the highest heat transfer** in the heat exchanger. We observe that:

➡ The maximum Q will be: $Q_{max} = C_{min}\Delta T_{max} = C_{min}(T_{max} - T_{min})$



$$\begin{aligned} Q_{max} &= C_c(T_{c,out} - T_{c,in}) \\ &= C_c(T_{h,in} - T_{c,in}) \end{aligned}$$



$$\begin{aligned} Q_{max} &= C_h(T_{h,in} - T_{h,out}) \\ &= C_h(T_{h,in} - T_{c,in}) \end{aligned}$$

Effectiveness-NTU Method

We want to determine the highest heat transfer for a given system.

The maximum Q will be: $Q_{max} = C_{min}\Delta T_{max} = C_{min}(T_{h,in} - T_{c,in})$

→ **Effectiveness** $\varepsilon \equiv \frac{Q}{Q_{max}}$ $\left\{ \begin{array}{l} \varepsilon = \frac{C_h(T_{h,in} - T_{h,out})}{C_{min}(T_{h,in} - T_{c,in})} \\ \varepsilon = \frac{C_c(T_{c,out} - T_{c,in})}{C_{min}(T_{h,in} - T_{c,in})} \end{array} \right. \quad 0 < \varepsilon < 1$

→ $Q = \varepsilon C_{min}(T_{h,in} - T_{c,in})$ If we know $\varepsilon, T_{h,in}, T_{c,in}$ we can determine Q

Effectiveness-NTU Method

We now observe that:

$$\varepsilon = \frac{Q}{Q_{max}} = \frac{UA\Delta T_{lm}}{C_{min}(T_{h,in} - T_{c,in})} = NTU \frac{\Delta T_{lm}}{(T_{h,in} - T_{c,in})}$$

Where we have defined the **number of heat transfer units NTU**, as: $NTU \equiv \frac{UA}{C_{min}}$

More generally, it can be shown that: $\varepsilon = f\left(NTU, \frac{C_{min}}{C_{max}}\right)$

Therefore the heat transfer in the heat exchanger can be determined once the physical properties ($C_{c,h}$), the heat exchanger design (UA) and the inlet temperatures of the working fluids are known.

Effectiveness-NTU Method

Parallel-flow Heat Exchanger

If $C_{min} = C_h$:

$$\varepsilon = \frac{(T_{h,in} - T_{h,out})}{(T_{h,in} - T_{c,in})}$$

And also we have:

$$\frac{C_{min}}{C_{max}} = \frac{\dot{m}_h c_{p,h}}{\dot{m}_c c_{p,c}} = \frac{T_{c,o} - T_{c,i}}{T_{h,i} - T_{h,o}}$$

➡ $T_{c,out} = \frac{C_{min}}{C_{max}}(T_{h,in} - T_{h,out}) + T_{c,in}$

Last week we derived:

$$\ln\left(\frac{\Delta T_2}{\Delta T_1}\right) = -UA\left(\frac{1}{C_h} + \frac{1}{C_c}\right)$$



$$\ln\left(\frac{T_{h,o} - T_{c,o}}{T_{h,i} - T_{c,i}}\right) = -\frac{UA}{C_{min}}\left(1 + \frac{C_{min}}{C_{max}}\right)$$



$$\frac{T_{h,o} - T_{c,o}}{T_{h,i} - T_{c,i}} = \exp\left[-NTU\left(1 + \frac{C_{min}}{C_{max}}\right)\right]$$

Effectiveness-NTU Method

Parallel-flow Heat Exchanger

If $C_{min} = C_h$:
$$\varepsilon = \frac{(T_{h,in} - T_{h,out})}{(T_{h,in} - T_{c,in})}$$

And also we have:
$$\frac{C_{min}}{C_{max}} = \frac{\dot{m}_h c_{p,h}}{\dot{m}_c c_{p,c}} = \frac{T_{c,o} - T_{c,i}}{T_{h,i} - T_{h,o}}$$

→
$$T_{c,out} = \frac{C_{min}}{C_{max}}(T_{h,in} - T_{h,out}) + T_{c,in}$$

$$\frac{T_{h,o} - T_{c,o}}{T_{h,i} - T_{c,i}} = \exp \left[-NTU \left(1 + \frac{C_{min}}{C_{max}} \right) \right]$$

→
$$\frac{T_{h,o} - T_{c,o}}{T_{h,i} - T_{c,i}} = \frac{T_{h,o} - T_{h,i} + T_{h,i} - T_{c,o}}{T_{h,i} - T_{c,i}} = \frac{(T_{h,o} - T_{h,i}) + (T_{h,i} - T_{c,i}) - (C_{min}/C_{max})(T_{h,i} - T_{h,o})}{T_{h,i} - T_{c,i}}$$

$-\varepsilon$

Effectiveness-NTU Method

Parallel-flow Heat Exchanger

$$\left. \begin{aligned} \frac{T_{h,o} - T_{c,o}}{T_{h,i} - T_{c,i}} &= \exp \left[-NTU \left(1 + \frac{C_{\min}}{C_{\max}} \right) \right] \\ \frac{T_{h,o} - T_{c,o}}{T_{h,i} - T_{c,i}} &= 1 - \varepsilon \left(1 + \frac{C_{\min}}{C_{\max}} \right) \end{aligned} \right\} \varepsilon = \frac{1 - \exp \{ -NTU [1 + (C_{\min}/C_{\max})] \}}{1 + (C_{\min}/C_{\max})}$$

This expression is general and it applies to any parallel heat exchanger irrespective of the fluid which has the minimum thermal capacity.

Similar expressions of $\varepsilon = \left(NTU, \frac{C_{\min}}{C_{\max}} \right)$ have been derived for other heat exchanger configurations and are summarized in the next table.

TABLE 11.3 Heat Exchanger Effectiveness Relations [5]

Flow Arrangement	Relation	
Concentric tube		
Parallel flow	$\varepsilon = \frac{1 - \exp[-NTU(1 + C_r)]}{1 + C_r}$	(11.28a)
Counterflow	$\varepsilon = \frac{1 - \exp[-NTU(1 - C_r)]}{1 - C_r \exp[-NTU(1 - C_r)]} \quad (C_r < 1)$	
	$\varepsilon = \frac{NTU}{1 + NTU} \quad (C_r = 1)$	(11.29a)
Shell-and-tube		
One shell pass (2, 4, ... tube passes)	$\varepsilon_1 = 2 \left\{ 1 + C_r + (1 + C_r^2)^{1/2} \right. \\ \left. \times \frac{1 + \exp[-(NTU)_1(1 + C_r^2)^{1/2}]}{1 - \exp[-(NTU)_1(1 + C_r^2)^{1/2}]} \right\}^{-1}$	(11.30a)
n Shell passes ($2n, 4n, \dots$ tube passes)	$\varepsilon = \left[\left(\frac{1 - \varepsilon_1 C_r}{1 - \varepsilon_1} \right)^n - 1 \right] \left[\left(\frac{1 - \varepsilon_1 C_r}{1 - \varepsilon_1} \right)^n - C_r \right]^{-1}$	(11.31a)
Cross-flow (single pass)		
Both fluids unmixed	$\varepsilon = 1 - \exp \left[\left(\frac{1}{C_r} \right) (NTU)^{0.22} \{ \exp[-C_r(NTU)^{0.78}] - 1 \} \right]$	(11.32)
C_{\max} (mixed), C_{\min} (unmixed)	$\varepsilon = \left(\frac{1}{C_r} \right) (1 - \exp \{ -C_r [1 - \exp(-NTU)] \})$	(11.33a)
C_{\min} (mixed), C_{\max} (unmixed)	$\varepsilon = 1 - \exp \{ -C_r^{-1} [1 - \exp \{ -C_r(NTU) \}] \}$	(11.34a)
All exchangers ($C_r = 0$)	$\varepsilon = 1 - \exp(-NTU)$	(11.35a)

$$C_r \equiv C_{\min} / C_{\max}$$

PHASE CHANGE!
($C_r = 0$)

TABLE 11.4 Heat Exchanger NTU Relations

Flow Arrangement	Relation
Concentric tube	
Parallel flow	$NTU = -\frac{\ln [1 - \varepsilon(1 + C_r)]}{1 + C_r} \quad (11.28b)$
Counterflow	$NTU = \frac{1}{C_r - 1} \ln \left(\frac{\varepsilon - 1}{\varepsilon C_r - 1} \right) \quad (C_r < 1)$
	$NTU = \frac{\varepsilon}{1 - \varepsilon} \quad (C_r = 1) \quad (11.29b)$
Shell-and-tube	
One shell pass (2, 4, . . . tube passes)	$(NTU)_1 = - (1 + C_r^2)^{-1/2} \ln \left(\frac{E - 1}{E + 1} \right) \quad (11.30b)$
	$E = \frac{2/\varepsilon_1 - (1 + C_r)}{(1 + C_r^2)^{1/2}} \quad (11.30c)$
n Shell passes ($2n, 4n, . . .$ tube passes)	Use Equations 11.30b and 11.30c with
	$\varepsilon_1 = \frac{F - 1}{F - C_r} \quad F = \left(\frac{\varepsilon C_r - 1}{\varepsilon - 1} \right)^{1/n} \quad NTU = n(NTU)_1 \quad (11.31b, c, d)$
Cross-flow (single pass)	
C_{\max} (mixed), C_{\min} (unmixed)	$NTU = -\ln \left[1 + \left(\frac{1}{C_r} \right) \ln(1 - \varepsilon C_r) \right] \quad (11.33b)$
C_{\min} (mixed), C_{\max} (unmixed)	$NTU = -\left(\frac{1}{C_r} \right) \ln [C_r \ln(1 - \varepsilon) + 1] \quad (11.34b)$
All exchangers ($C_r = 0$)	$NTU = -\ln(1 - \varepsilon) \quad (11.35b)$

$$C_r \equiv C_{\min} / C_{\max}$$

Effectiveness-NTU Method

$$C_r \equiv C_{\min}/C_{\max}$$

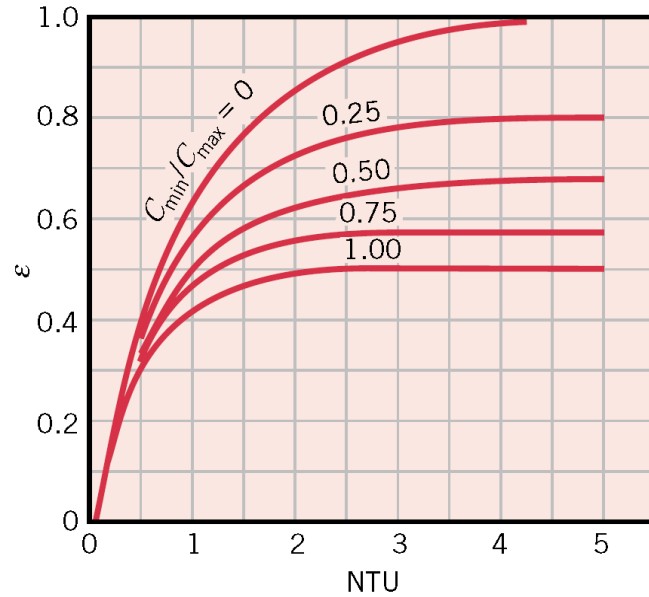


FIGURE 11.10 Effectiveness of a parallel-flow heat exchanger (Equation 11.28).

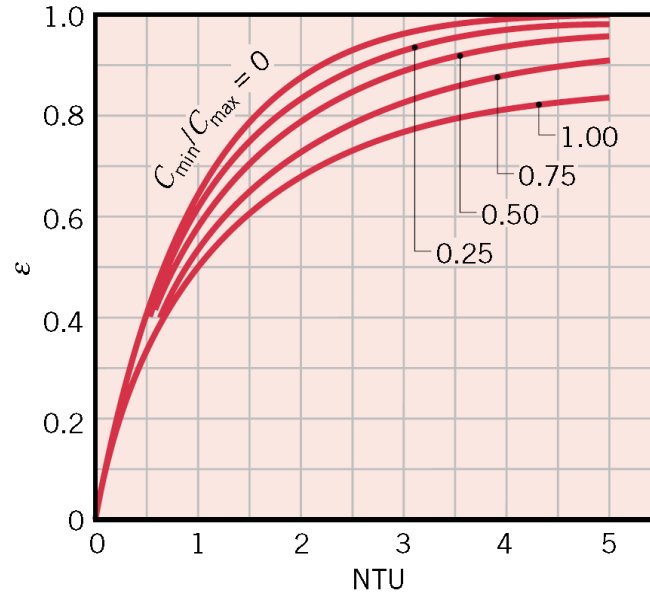


FIGURE 11.11 Effectiveness of a counterflow heat exchanger (Equation 11.29).

Effectiveness-NTU Method

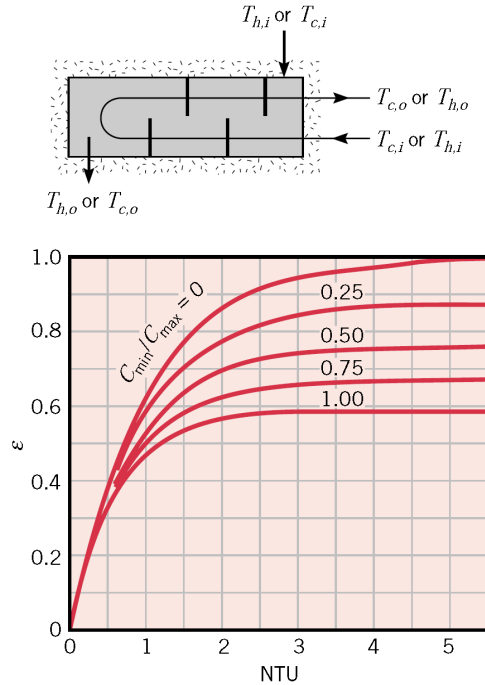


FIGURE 11.12 Effectiveness of a shell-and-tube heat exchanger with one shell and any multiple of two tube passes (two, four, etc. tube passes) (Equation 11.30).

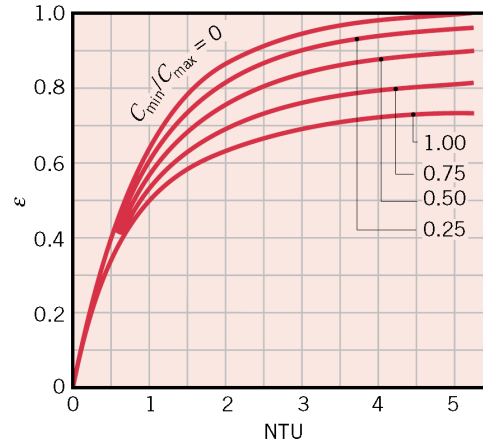
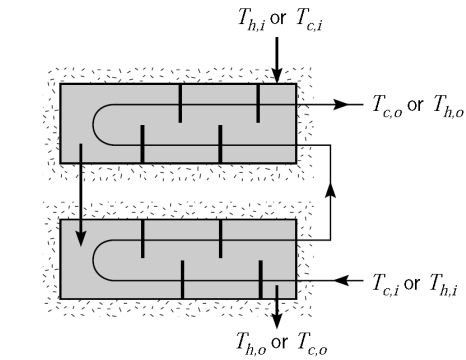


FIGURE 11.13 Effectiveness of a shell-and-tube heat exchanger with two shell passes and any multiple of four tube passes (four, eight, etc. tube passes) (Equation 11.31 with $n = 2$).

$$C_r \equiv C_{\min}/C_{\max}$$

Effectiveness-NTU Method

$$C_r \equiv C_{\min}/C_{\max}$$

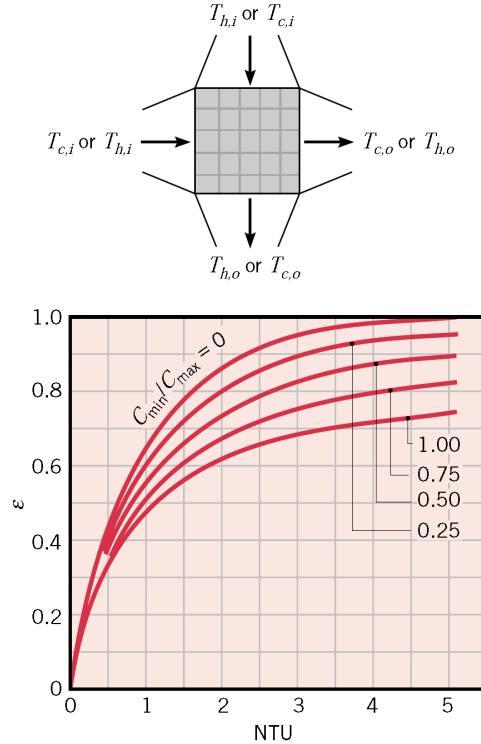


FIGURE 11.14 Effectiveness of a single-pass, cross-flow heat exchanger with both fluids unmixed (Equation 11.32).

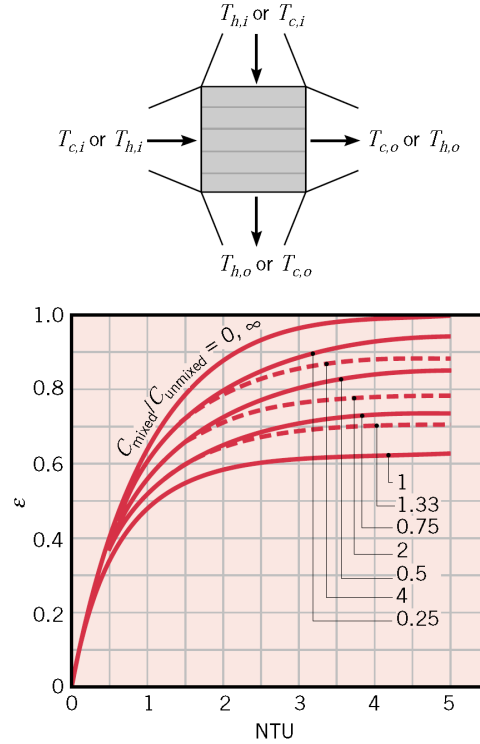


FIGURE 11.15 Effectiveness of a single-pass, cross-flow heat exchanger with one fluid mixed and the other unmixed (Equations 11.33, 11.34).

This Lecture



Heat Exchanger Analysis/Design/Performance Calculation



Effectiveness-NTU method

Learning Objectives:

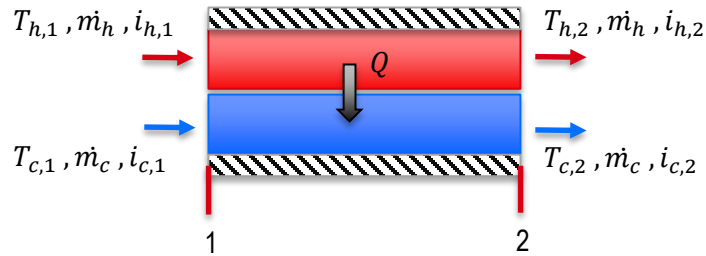


Identify the design parameter for a heat exchanger



Analyze the performance of a heat exchanger

Heat Exchanger Problems



Design problem:

All input and output temperatures are given, as well as flow rates.
We need to determine the appropriate heat exchanger area.

➡ Calculate ε and C_r , then NTU then A

Performance analysis problem:

We have a heat exchanger of prescribed dimensions, we know the inlet conditions and we need to determine the outlet conditions and the overall heat transfer.

➡ Calculate NTU and C_r and then determine ε

Next Lecture

- ❑ Design and performance Analysis of Heat Exchangers

Learning Objectives:

- ❑ Identify the design parameter for a heat exchanger
- ❑ Analyze the performance of a heat exchanger