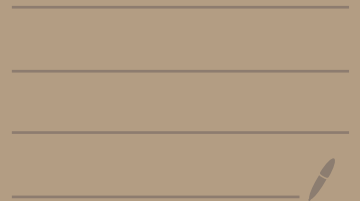


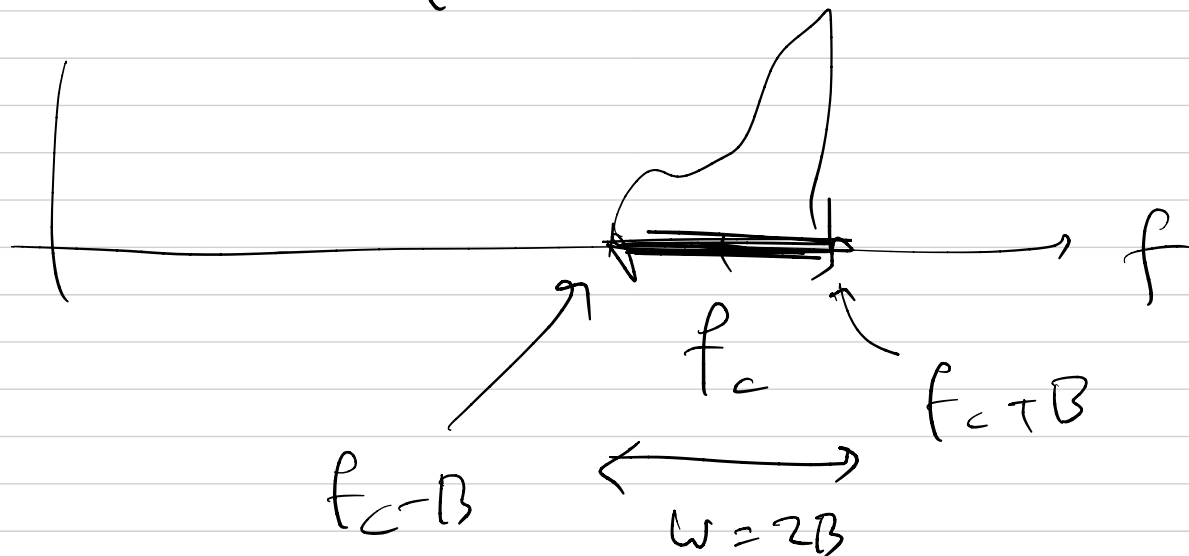
Principles of Digital Communication

May 19, 2021

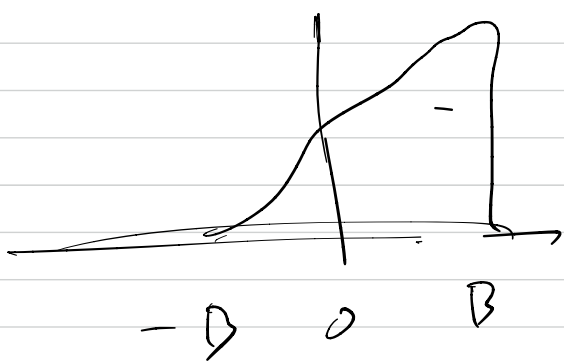


Reading was: "passband communication" 7.1-4).

We wish to communicate using signals that live on a frequency band:



Q: Can we design "everything" in base-band



and "simply" upconvert just before transmission

Ans: yes.

We notice: if $w(t)$ is a ^{real} waveform such that $w_F(f) = 0$ for $||f| - f_c| > B$,

then $w(t)$ can be written as

$$w(t) = \sqrt{2} \operatorname{Re} \{ w_E(t) e^{j 2\pi f_c t} \}$$

where $w_E(t)$ is low-pass ($w_{E,F}(f) = 0$ when $|f| > B$)

$w_E(t)$ is the "baseband equivalent" of $w(t)$ and is (in general) a $\mathbb{C}$ -valued signal

$$x(t) \sim x_E(t)$$

$$y(t) \sim y_E(t)$$

$$\langle x, y \rangle = \operatorname{Re} \{ \langle x_E, y_E \rangle \}$$

$$w(t) = \sqrt{2} \operatorname{Re} \{ w_E(t) \} \cos(2\pi f_c t)$$

$$= \sqrt{2} \operatorname{Im} \{ w_E(t) \} \sin(2\pi f_c t)$$

in-phase part
of $w(t)$

quadrature
-phase
part of $w(t)$

So: TX architecture:

$$i \in \{0, \dots, m-1\}$$



$$c_i \in \mathbb{C}^n$$



$$w_{E,i}(t) = \sum_{j=1}^n c_{ij} \psi_j(t)$$

complex, L -normal
system of waveforms,
baseband



$$w_i(t) = \operatorname{Re} \{ \sqrt{2} w_{E,i}(t) e^{j2\pi f_c t} \}$$

Note:

$$\begin{aligned}
 w_i(t) &= \sqrt{2} \operatorname{Re} \left\{ \sum_{j=1}^n c_{ij} \psi_j(t) e^{j\omega_c t} \right\} \\
 &= \sum_{j=1}^n \operatorname{Re} \{ c_{ij} \} \operatorname{Re} \{ \psi_j(t) e^{j\omega_c t} \} \sqrt{2} \\
 &\quad - \operatorname{Im} \{ c_{ij} \} \operatorname{Im} \{ \psi_j(t) e^{j\omega_c t} \} \sqrt{2}
 \end{aligned}$$

So, each $w_i(t)$ is a linear combination of $2n$ real waveforms:

$$\begin{aligned}
 &\operatorname{Re} \{ \psi_j(t) e^{j\omega_c t} \} \sqrt{2} \quad j=1, \dots, n \\
 &\operatorname{Im} \{ \psi_j(t) e^{j\omega_c t} \} \sqrt{2} \quad j=1, \dots, n
 \end{aligned}$$

Surprisingly, these $2n$ waveforms are an $\perp$ -normal basis (because ψ_j 's are $\perp$ -normal).

Because of this we know what to do at the

RCUR: we should form

$$\langle R(t), \operatorname{Re} \{ \sqrt{2} \psi_j(t) e^{j\omega_c t} \} \rangle \quad j=1, \dots, n$$

$$\text{and } \langle \operatorname{Im} \{ \psi_j(t) e^{j\omega_c t} \} \sqrt{2} \rangle \quad \text{"}$$

This is equivalent to:

$$\operatorname{Re} \{ \langle R(t), \sqrt{2} \psi_j(t) e^{+j2\pi f_c t} \rangle \},$$

$$\operatorname{Im} \{ \langle R(t), \sqrt{2} \psi_j(t) e^{j2\pi f_c t} \rangle \}$$

$$\equiv \operatorname{Re} \{ \langle R(t) e^{-j2\pi f_c t} \sqrt{2}, \psi_j(t) \rangle \},$$

$$\operatorname{Im} \{ \langle \quad, \quad \rangle \}$$

$$\equiv \langle R(t) e^{-j2\pi f_c t} \sqrt{2}, \psi_j(t) \rangle \quad j=1 \dots n$$

$$\equiv R(t) \xrightarrow{\sqrt{2} e^{-j2\pi f_c t}} \langle \cdot, \psi_j \rangle \quad j=1 \dots n$$

$= x_j$

TX

c

$\downarrow$

$c_i \in \mathbb{C}^n$

$\downarrow$

$w_{E,c}(t)$ complex, baseband

$\downarrow$

$w_c(t)$ real, passband

RX

$\uparrow$

$\uparrow$

$y = c_i + z \in \mathbb{C}^n$

$\uparrow$

$r_E(t) = w_{E,c}(t) + \tilde{N}(t)$

$\uparrow$

$R(t) = w_c(t) + N(t)$

add real
time parts
 $N(0, \frac{N_0}{2})$

The baseband equivalent noise is

$$\tilde{N}(t) = N(t) e^{-j2\pi f_c t} \sqrt{2}$$

$$= \underbrace{N(t) \sqrt{2} \cos(2\pi f_c t)} - j \underbrace{N(t) \sqrt{2} \sin(2\pi f_c t)}$$

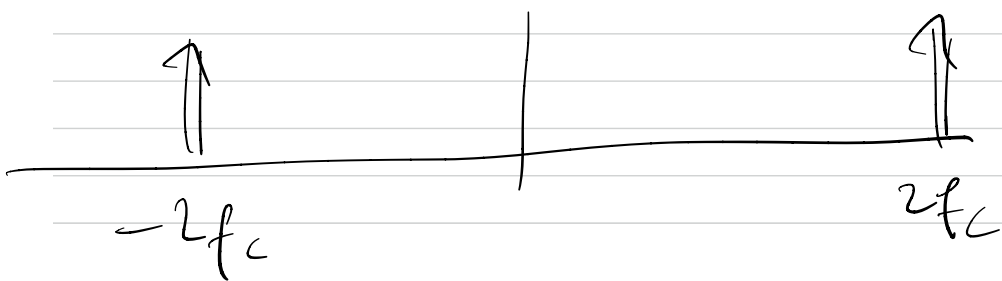
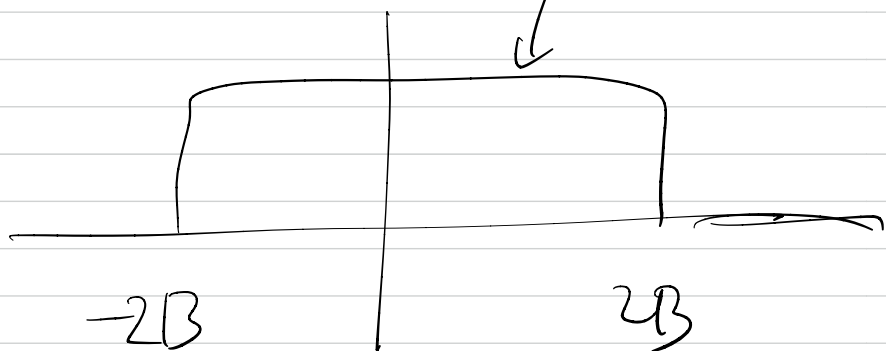
What we will do with $\tilde{N}(t)$ is to take its inner products with baseband waveforms $g(t)$.

$$\langle \tilde{N}, g \rangle = \langle N(t) \sqrt{2} \cos(2\pi f_c t), g \rangle - j \langle N(t) \sqrt{2} \sin(2\pi f_c t), g \rangle$$

$$\int N(t) \underbrace{[g^*(t) \sqrt{2} \cos(2\pi f_c t)]}_{a(t)} dt = \langle N, a \rangle$$

$$\int N(t) \underbrace{[g^*(t) \sqrt{2} \sin(2\pi f_c t)]}_{b(t)} dt = \langle N, b \rangle$$

$$\langle a, b \rangle = \int |g(t)|^2 \underbrace{\sin(4\pi f_c t)} dt = 0$$

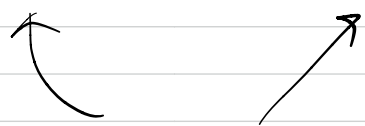


⇒ if we replace

$$\tilde{N}(t) = N(t) \sqrt{2} \cos(2\pi f_c t) - j N(t) \sqrt{2} \sin(2\pi f_c t)$$

by

$$\tilde{N}(t) = N_1(t) - j N_2(t)$$



independent AWGN

the receiver architecture will not see any difference

⇒ (7.4): baseband equivalent noise:

$$R_E(t) = w_E(t) + \tilde{N}(t)$$



Complex AWGN, with
independent $\text{Re}\{\}$ and $\text{Im}\{\}$
parts each of intensity $N_0/2$

$\tilde{c}_i$ c_i $w_{\tilde{c}_i}(t)$ $w_i(t)$ $\hat{c}_i$

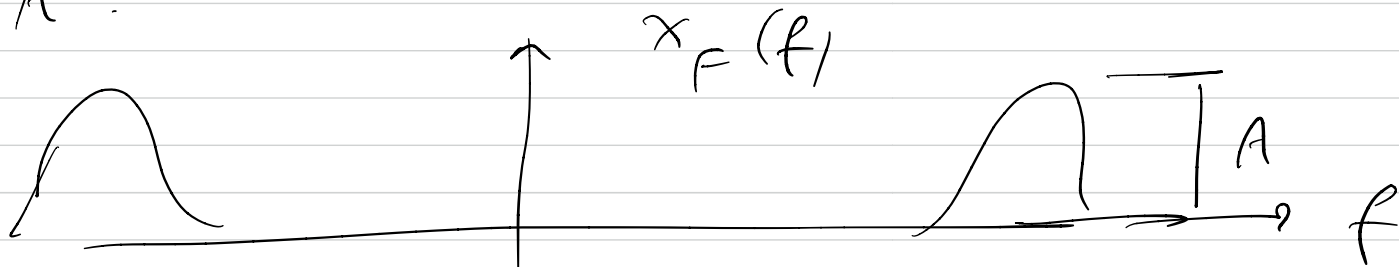
$$\gamma = c_i + z$$

$$r_{\tilde{c}_i}(t) = w_{\tilde{c}_i}(t) + \tilde{N}(t)$$

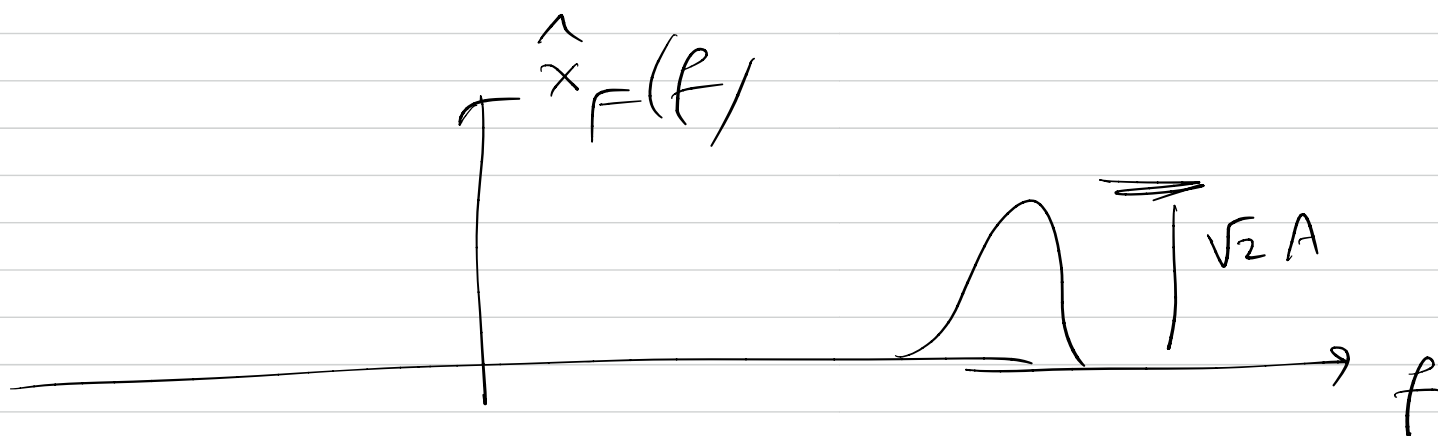
$$R(t) = w_i(t) + N(t).$$

Q: where are the $\sqrt{2}$'s coming from?

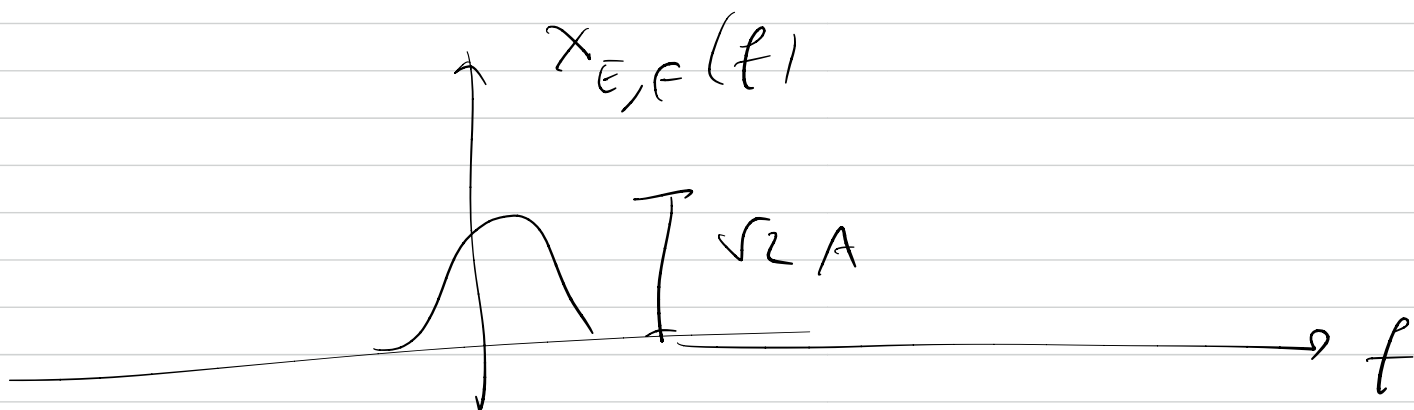
A: we have



bandpass
waveform



analytic
signal



baseband
equiv.

$$\|x\|^2 = \int |x(t)|^2 dt$$

$$= \|x_F\|^2 = \int |x_F(t)|^2 dt$$

$$= 2 \int_0^\infty |x_F(t)|^2 dt$$

$$= \frac{1}{\pi} \int_{-\infty}^\infty |\hat{x}_F(t)|^2 dt$$

$$= \int_{-\infty}^\infty \underbrace{|\sqrt{2} \hat{x}_F(t)|^2}_{|\hat{x}_F(t)|^2} dt$$