

Téléphone : +41 21 693 24 27
Fax : +41 21 693 28 68
E-mail : dimitrios.lignos@epfl.ch
Site web : <http://resslab.epfl.ch>
Address: EPFL ENAC IIC RESSLAB
GC B3 485, Station 18,
CH-1015, Lausanne

Exercise #3: Response to pulses and approximate analysis for short pulses

Problem 1

The 24-m-high full water tank shown in the figure is subjected to the force $p(t)$ shown in the figure caused by an aboveground explosion. The weight of the water when the tank is full is 160kN. The damping coefficient was measured from a free vibration test and was found to be, $c = 0.0063 \text{ kN} - \text{sec}/\text{mm}$ and its lateral stiffness $k = 0.5 \text{ kN}/\text{mm}$. Determine the following:

1. The natural vibration period and damping ratio of the structure with the tank full;
2. The maximum base shear and bending moment at the base of the tower supporting the tank.

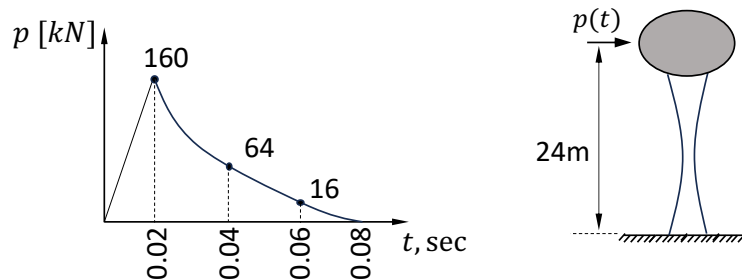


Figure 3.1

Problem 1 - Solution

1. For this water tank, when it is assumed to be full, the corresponding mass is as follows:

$$m = \frac{W}{g} = \frac{160kN}{9810 \text{ mm/s}^2} = 0.016kN - \text{sec}^2/\text{mm}$$

Therefore, the period of vibration can be estimated as follows:

$$T_n = 2\pi \sqrt{\frac{m}{k}} = 2\pi \sqrt{\frac{0.016kN - \text{sec}^2/\text{mm}}{0.5 \text{ kN/mm}}} = 1.13\text{sec}$$

Regarding the damping ratio, it is known that:

$$\zeta = \frac{c}{2\sqrt{km}} = \frac{0.0063kN - \text{sec/mm}}{2\sqrt{\frac{0.5kN}{\text{mm}} \cdot 0.016kN - \text{sec}^2/\text{mm}}} = 0.035 = 3.5\%$$

2. We should first check what is the ratio, t_d/T_n

$$\frac{t_d}{T_n} = \frac{0.08}{1.13} = 0.07$$

Because $t_d/T_n < 0.25$, the forcing function may be treated as a pure impulse of magnitude,

$$I = \int_0^{0.08} p(t) dt$$

NOTE: essentially if we integrate the acting force diagram versus time, we can estimate the amplitude of the equivalent impulse force.

The above integration cannot be done analytically as the function $p(t)$ is given at discrete points. As such, we can apply the trapezoidal rule (or other) to do the integration. Here, the integration rule is applied:

$$I = \int_0^{0.08} p(t) dt = \frac{0.02}{2} (0 + 2(160) + 2(64) + 2(16) + 0) = 4.80kN - \text{sec}$$

As the response has been transformed into a pure impulse, the displacement history of an SDF system under an impulse load, I causes free vibration of the SDF system due to the initial velocity, $\dot{u}(\tau) = I/m$ and initial displacement $u(\tau) = 0$ (see Slide 21); hence, the corresponding displacement after neglecting damping is as follows:

$$u(t) = \frac{I}{m\omega_n} \sin [\omega_n(t - \tau)] \text{ for } t \geq \tau$$

In slide 21 of the lecture notes, we looked at the case of a unit impulse (its amplitude is equal to 1). However, in our case the amplitude is equal to I .

In our case, $\tau = 0$, therefore,

$$u(t) = \frac{I}{m\omega_n} \sin(\omega_n t) \text{ for } t \geq 0$$

The above function maximizes when,

$$\frac{d(u(t))}{dt} = 0 \Rightarrow \cos(\omega_n t) = 0 \Rightarrow \omega_n t = \frac{\pi}{2} \Rightarrow t = \frac{\pi}{2\omega_n}$$

Substituting to the equation above, the maximum displacement may be computed as follows,

$$u_o = \frac{I}{m\omega_n} \sin\left(\omega_n \frac{\pi}{2\omega_n}\right) = \frac{I}{m\omega_n} \cdot 1 = \frac{I}{m\omega_n} = \frac{I}{(k/\omega_n^2)\omega_n} = \frac{I}{(k/\omega_n)} = \frac{I}{k} \frac{2\pi}{T_n}$$

NOTE: $\omega_n = \sqrt{k/m}$

Neglecting the effect of damping, the maximum displacement in this case may be estimated as follows:

$$u_o = \frac{I}{k} \frac{2\pi}{T_n} = \frac{4.80}{0.5} \frac{2\pi}{1.13} = 53mm$$

To be able to compute the associated shear force and moment, the equivalent static force, f_{so} acting on the system should be estimated. This may be done as follows,

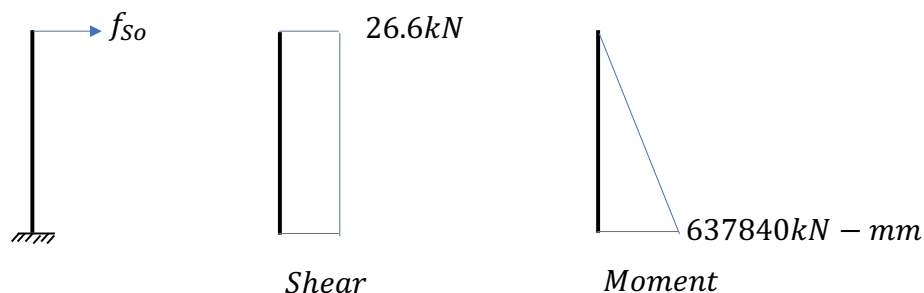
$$f_{so} = ku_o = \frac{0.5kN}{mm} \cdot 53mm = 26.6kN$$

As such, the base shear is simply calculated by equilibrium as shown in the figures below and,

$$V_b = f_{so} = 26.6kN$$

The moment at the base,

$$M_b = V_b h = 26.6kN \cdot 24000mm = 637840kN - mm$$



Problem 2

A one-storey building, idealized as a $h = 3.6\text{-m}$ -high frame with two columns hinged at the base and a rigid beam, has a natural period of 0.5 sec . Each column has a rectangular cross section of $270\text{ mm} \times 100\text{ mm}$. The Young's modulus of the material is 30 GPa . Neglecting damping, determine the maximum response of this frame due to a rectangular pulse force of amplitude 16 kN and duration $t_d = 0.2\text{ sec}$. Assume that the system is elastic. The response quantities of interest to be calculated are:

1. the displacement at the top of the frame; and
2. the maximum bending stress in the columns.

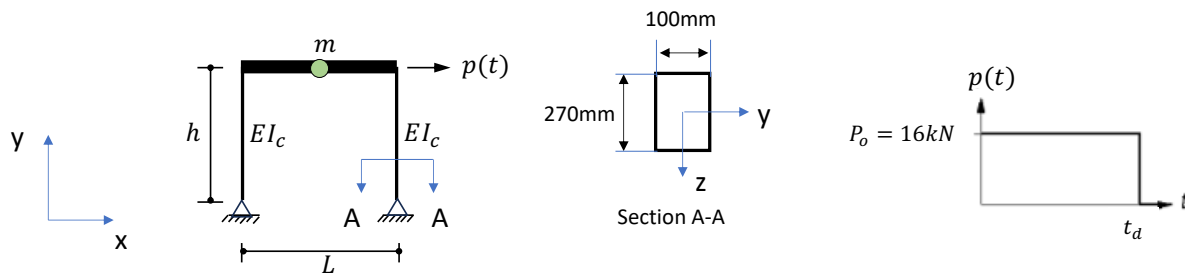


Figure 3.2

Problem 2 – Solution

The natural period of vibration is given ($T_n = 0.5$ sec). As such, we can compute the dynamic amplification factor, R_d . With that we can conduct simplified analysis of short pulses.

$$R_d = \frac{u_o}{(u_{st})_o} = 2 \sin\left(\frac{\pi t_d}{T_n}\right) = 2 \sin(0.4\pi) = 1.902$$

The corresponding lateral stiffness of the SDF system may be computed as follows:

$$K_{SDF} = 2K_{col} = 2\left(\frac{3EI_c}{h^3}\right) = 6 \cdot \frac{(30 \text{ kN/mm}^2) \cdot 164025000 \text{ mm}^4}{3600 \text{ mm}^4} = 0.63 \frac{\text{kN}}{\text{mm}}$$

NOTE: For the above calculation, the second moment of area of the column cross section should be computed (rectangular):

$$I_c = \frac{100 \cdot 270^3}{12} = 164025000 \text{ mm}^4$$

As such, the peak displacement of the steady state response may be estimated as follows:

$$(u_{st})_o = \frac{p_o}{K_{SDF}} = \frac{16 \text{ kN}}{0.63 \text{ kN/mm}} = 25.3 \text{ mm}$$

The peak displacement of the SDF response may be estimated as follows:

$$u_o = R_d(u_{st})_o = 1.902 \cdot 25.3 \text{ mm} = 48.09 \text{ mm}$$

Finally, the bending moment of the cross section (from Statics 2):

$$M = \frac{3EI_c}{h^2} u_o = \left(\frac{3 \cdot 30 \text{ kN/mm}^2 \cdot 164025000 \text{ mm}^4}{3600^2 \text{ mm}^2}\right) 48.09 \text{ mm} = 54777.6 \text{ kN} \cdot \text{mm}$$

Alternatively, we can find the bending moment from the equivalent static force,

$$f_{so} = p_o R_d = 16(1.902) = 30.4 \text{ kN}$$

Because both columns are identical, the force f_{so} is equally distributed to the those; and the corresponding moment is as follows:

$$M = \frac{f_{so}}{2} h = \frac{30.4 \text{ kN}}{2} 3600 \text{ mm} = 54777.6 \text{ kN} \cdot \text{mm}$$

The corresponding longitudinal stress due to flexure can then be calculated from principles of structural mechanics as follows:

$$\sigma = \frac{M}{I_c} \cdot \frac{b}{2} = \frac{54777.6kN - mm}{164025000mm^4} \cdot \frac{270mm}{2} = 0.045 \frac{kN}{mm^2} = 45MPa$$