

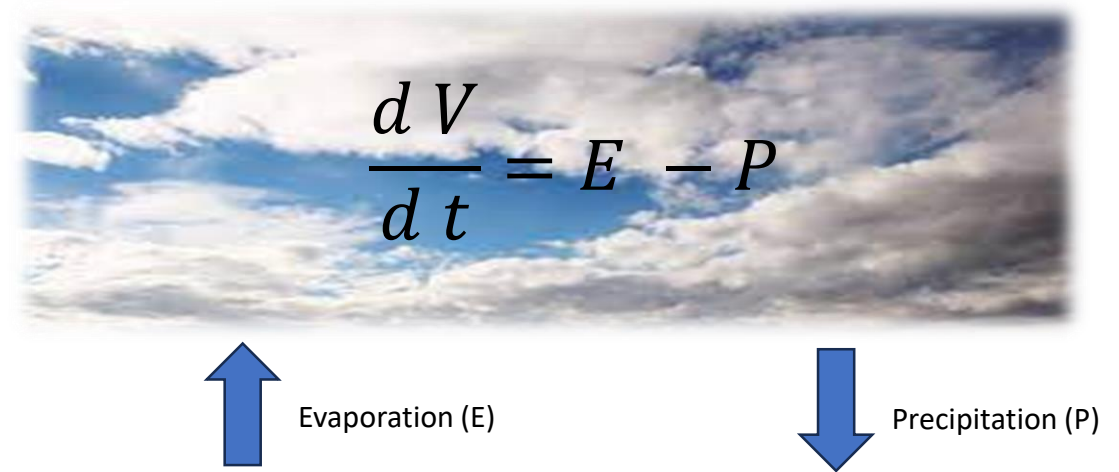
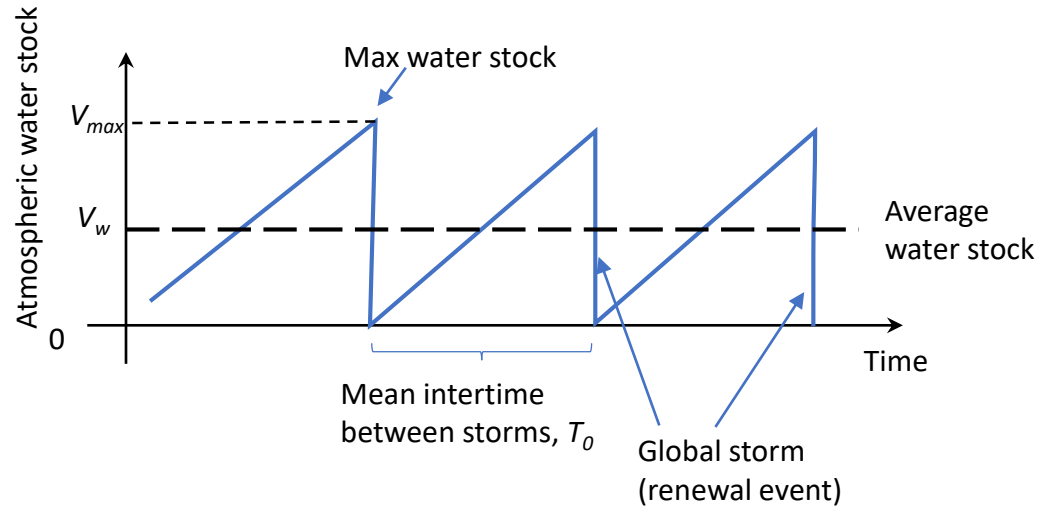
# Water Resources Engineering and Management

Exercices Lecture 2: global circulation; groundwater dynamics



24/02/2025

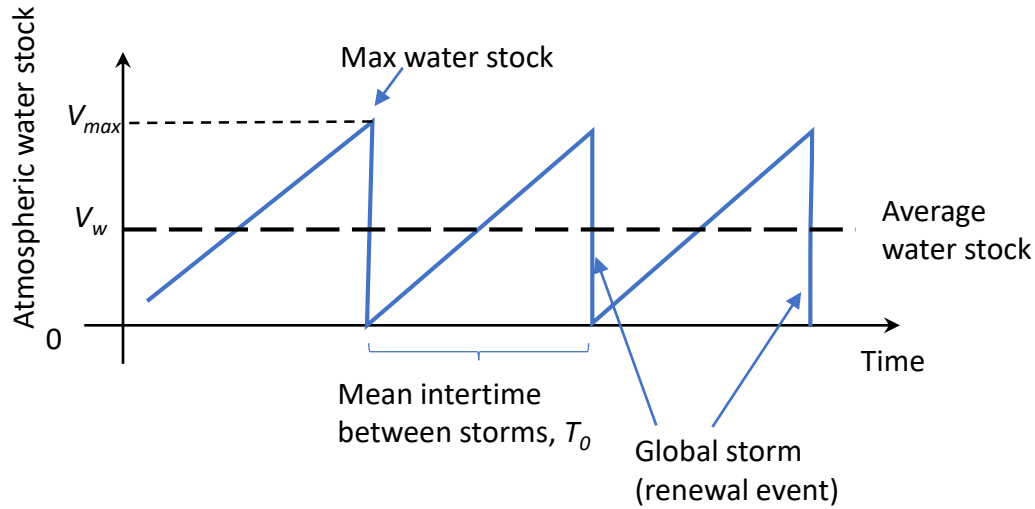
# Exercise 1. Assess the mean period for the renewal of water in the atmosphere (residence time)



## QUESTION

- The residence time,  $T_w$
- The relationship between  $T_w$  and  $T_0$

# Exercise 1. Assess the mean period for the renewal of water in the atmosphere (residence time) - SOLUTION

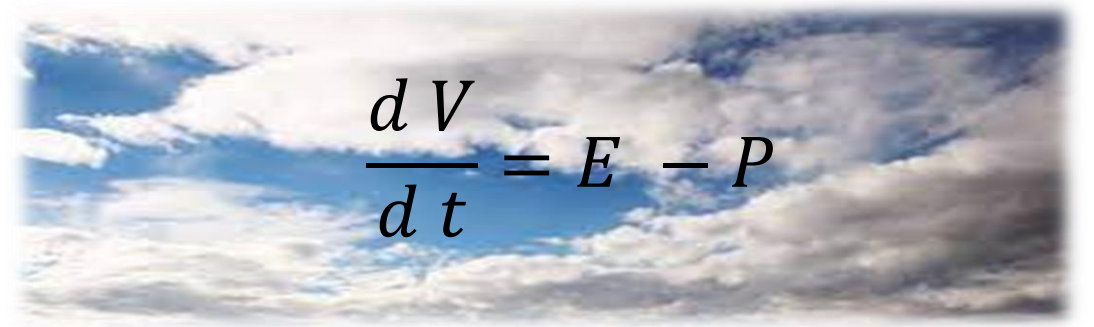


DATA - L2.1 (slide 14)

- World average H<sub>2</sub>O stock (mainly as water vapour) →  $V_w = 1.3 \cdot 10^{13} \text{ m}^3$
- Total world precipitation →  $P = 5.77 \cdot 10^{14} \text{ m}^3/\text{yr}$

HYPOTHESIS

- Permanent regime  $dV/dt=0 \rightarrow E=P, V=V_w$



Evaporation (E)



Precipitation (P)

$$E = \frac{V_w}{T_w} = P$$

$$T_w = \frac{V_w}{P} = 8.22 \text{ d}$$

$$T_w = \frac{V_w}{\left(\frac{V_{\max}}{T_0}\right)} = T_0 \frac{\frac{1}{2} V_{\max}}{V_{\max}} = \frac{T_0}{2}$$

## Exercise 2. Where would all the water go?

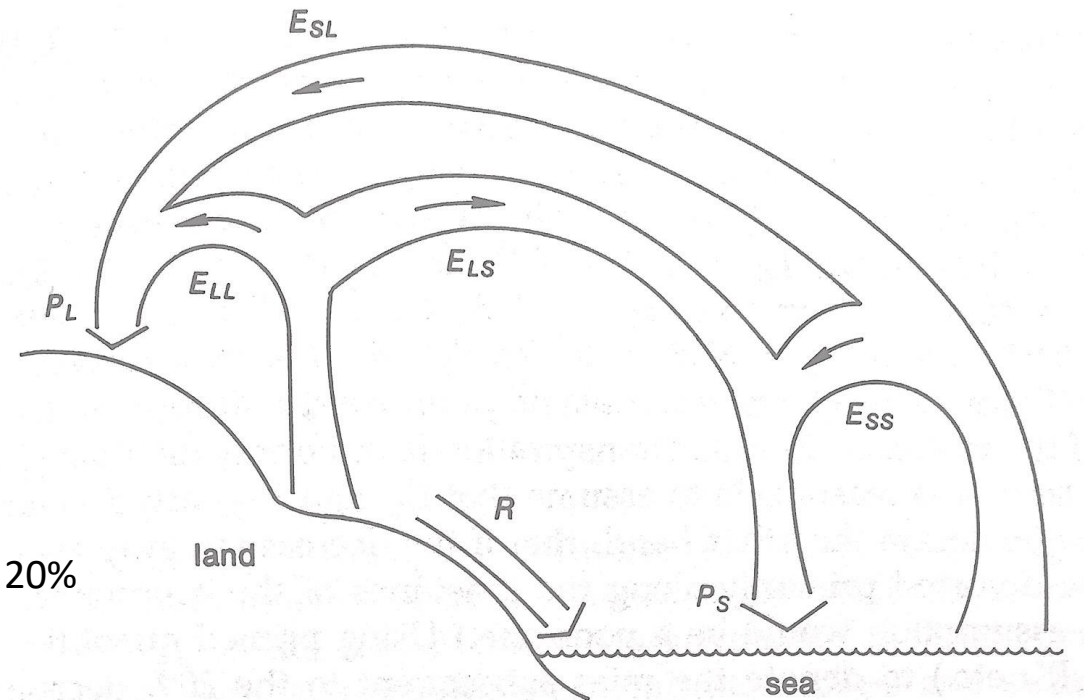
Assuming that evapotranspiration from the land surface decreases uniformly by 20% as a result of widespread deforestation, what changes would occur in global precipitation at the land surface and in average runoff from the land to the oceans?

This is not a residence time problem, but rather a box model problem

If you think that precipitation changes by 20%, you're wrong

### QUESTION

- The fluxes at the current state
- The altered fluxes if evaporation from land diminishes by 20%



Source: John Harte. Consider a spherical cow. University Science Book, 1988

# Exercise 2. Where would all the water go? - SOLUTION

DATA - L2.1 (slide 14)

- Total precipitation on land  $\rightarrow P_L = 110 \cdot 10^3 \text{ km}^3/\text{yr}$
- Total precipitation on sea  $\rightarrow P_S = 458 \cdot 10^3 \text{ km}^3/\text{yr}$
- Total flow from land to sea  $\rightarrow R = 44.8 \cdot 10^3 \text{ km}^3/\text{yr}$

4 unknowns fluxes:  $E_{LL}, E_{LS}, E_{SL}, E_{SS}$

$\rightarrow$  4 equations are required

## CURRENT STATE – BALANCING EQUATION

Sea:  $P_S + R = E_{SS} + E_{SL} \quad (1)$

Earth:  $P_L = E_{LL} + E_{LS} + R \quad (2)$

Atmosphere:  $E_{SL} + E_{LL} = P_L \quad (3a)$

$E_{SS} + E_{LS} = P_S \quad (3b)$

Constitutive Eq.:  $E_{LL} = 3E_{LS} \quad (4)$

L2.1 (slide 14)

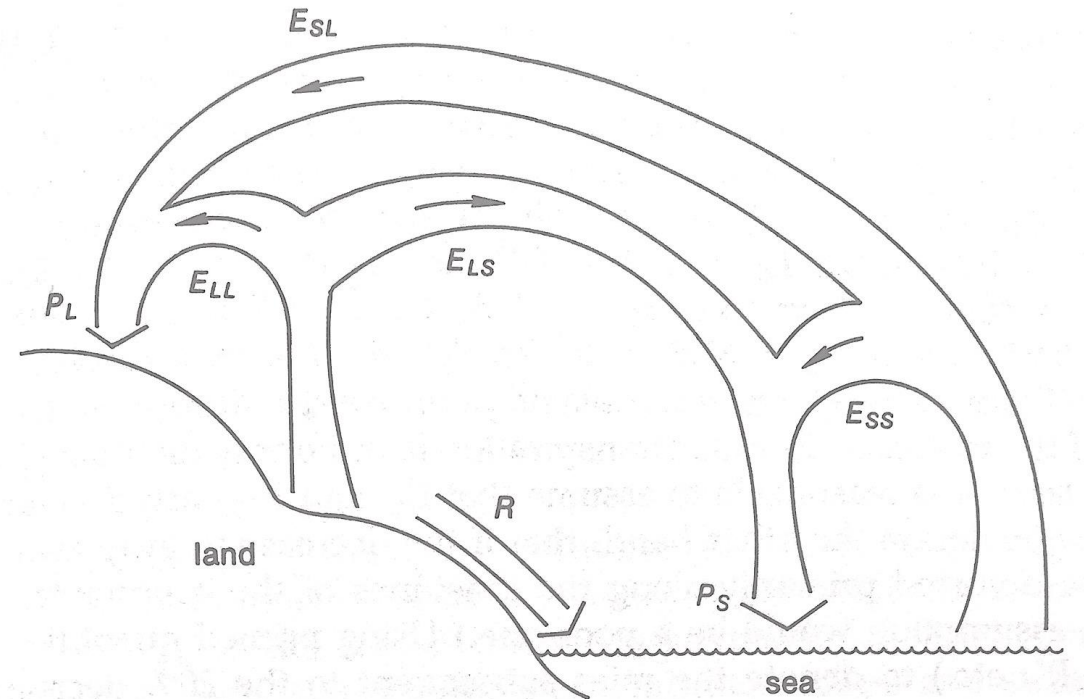
After reorganization:

$$E_{LL} = \frac{3}{4}(P_L - R) = 48.9 \cdot 10^3 \text{ km}^3/\text{yr}$$

$$E_{LS} = \frac{1}{4}(P_L - R) = 16.3 \cdot 10^3 \text{ km}^3/\text{yr}$$

$$E_{SL} = \frac{1}{4}P_L + \frac{3}{4}R = 61.1 \cdot 10^3 \text{ km}^3/\text{yr}$$

$$E_{SS} = P_S - \frac{1}{4}(P_L - R) = 441.7 \cdot 10^3 \text{ km}^3/\text{yr}$$



# Exercise 2. Where would all the water go? - SOLUTION

DATA - L2.1 (slide 14)

- Reducing factor for evaporation from land  $\rightarrow \alpha = 0.8$
- Modified total evaporation from land to land  $\rightarrow E'_{LL} = \alpha E_{LL}$
- Total evaporation from land to sea  $\rightarrow E'_{LS} = \alpha E_{LS}$
- Total evaporation from sea to land  $\rightarrow E'_{SL} = E_{SL}$
- Total evaporation from sea to sea  $\rightarrow E'_{SS} = E_{SS}$

## MODIFIED STATE – BALANCING EQUATION

Sea:  $P'_S + R' = E_{SS} + E_{SL}$  (1)

Earth:  $P'_L = E'_{LL} + E'_{LS} + R'$  (2)

Atmosphere:  $E_{SL} + E'_{LL} = P'_L$  (3a)

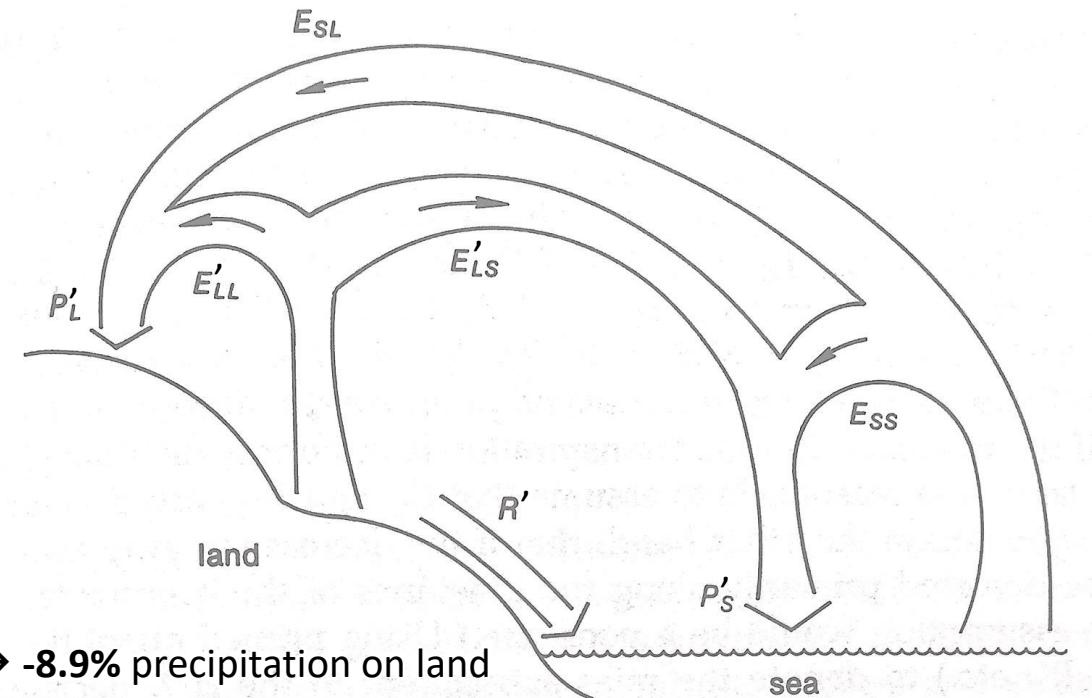
After reorganization:

$$P'_L = E_{SL} + \alpha E_{LL} = P_L - (1 - \alpha) E_{LL} = 100.2 \cdot 10^3 \text{ km}^3/\text{yr}$$

$$P'_S = E_{SS} + \alpha E_{LS} = P_S - (1 - \alpha) E_{LS} = 454.7 \cdot 10^3 \text{ km}^3/\text{yr}$$

$$R' = E_{SL} - \alpha E_{LS} = R + (1 - \alpha) E_{LS} = 48.1 \cdot 10^3 \text{ km}^3/\text{yr}$$

3 unknowns fluxes:  $P'_L, P'_S, R'$   $\rightarrow$  3 equations are required



$\rightarrow$  -8.9% precipitation on land

$\rightarrow$  -0.7% precipitation on sea

$\rightarrow$  +7.4% flow from land to sea (runoff)



# Exercise 3. Pumping test to define the soil conductivity, $K$

The average saturated hydraulic conductivity,  $K$ , of a given soil region is derived from field measurements. The following scheme is usually adopted for the phreatic groundwater flow.

## DATA

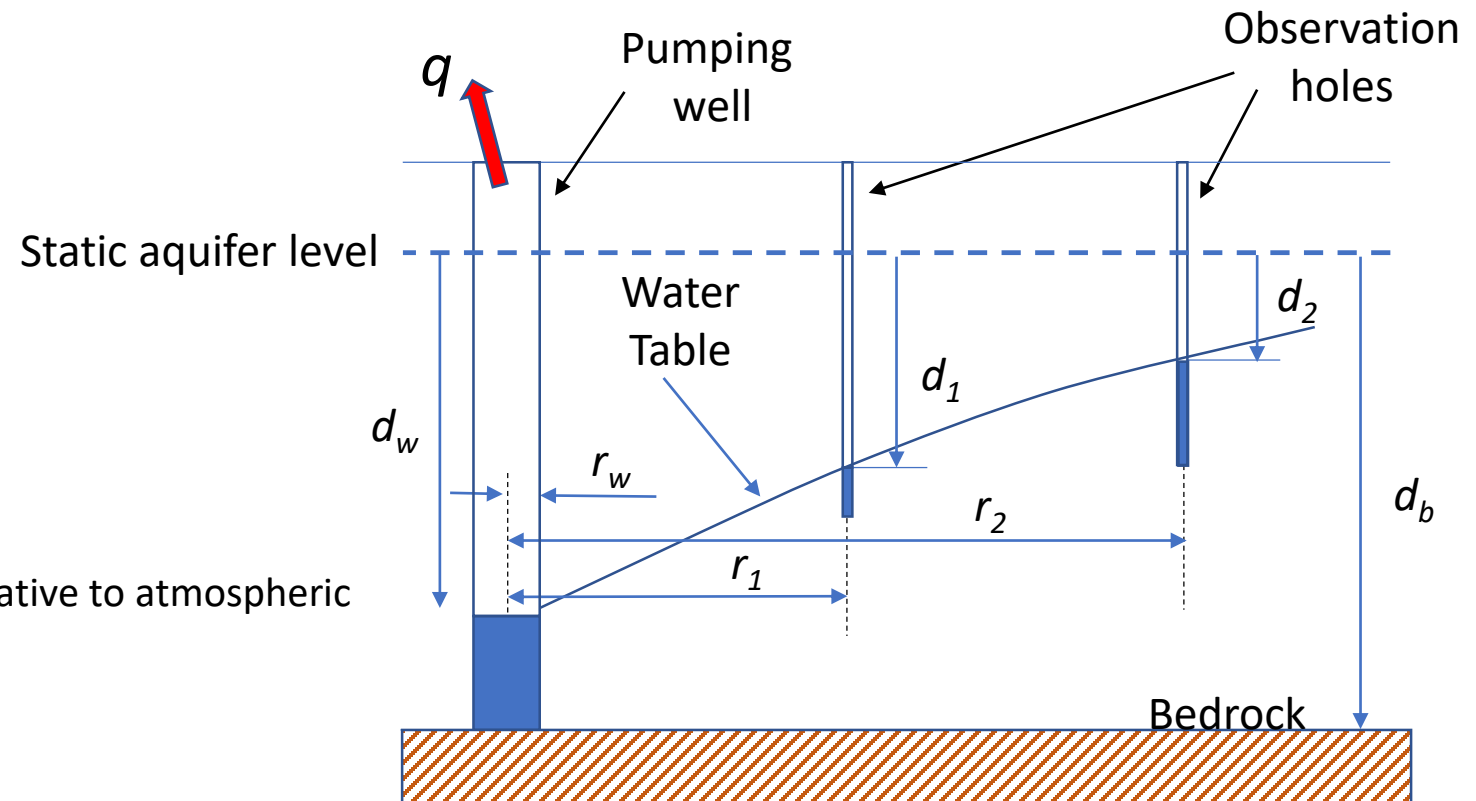
- Pumped flow  $\rightarrow q = 5 \text{ L/s}$
- Depth of impermeable bedrock  $\rightarrow d_b = 32 \pm 4.5 \text{ m}$
- Distance of 1<sup>st</sup> piezometric hole  $\rightarrow r_1 = 20 \text{ m}$
- Distance of 2<sup>nd</sup> piezometric hole  $\rightarrow r_2 = 55 \text{ m}$
- Water depth at 1<sup>st</sup> hole  $\rightarrow d_1 = 4.82 \text{ m}$
- Water depth at 2<sup>nd</sup> hole  $\rightarrow d_2 = 4.27 \text{ m}$
- Radius of the well  $\rightarrow r_w = 0.5 \text{ m}$

## HYPOTHESES

- Cylindrical simmetry
- Flow is horizontal (Dupuit-Forchmeier hypothesis)
- Suction above water table is ignored
- Free surface at water table and pressure here is 0 relative to atmospheric
- Hydraulic gradient constant at given radius  $dh/dr$

## QUESTIONS

- The hydraulic conductivity,  $K$
- The uncertainty in the value of the hydraulic conductivity,  $\Delta K$
- The depth within the well,  $d_w$



# Exercise 3. Pumping test to define $K$ - SOLUTION

$$h(r) = d_b - d(r) \quad \text{Height of the aquifer with respect to the bedrock}$$

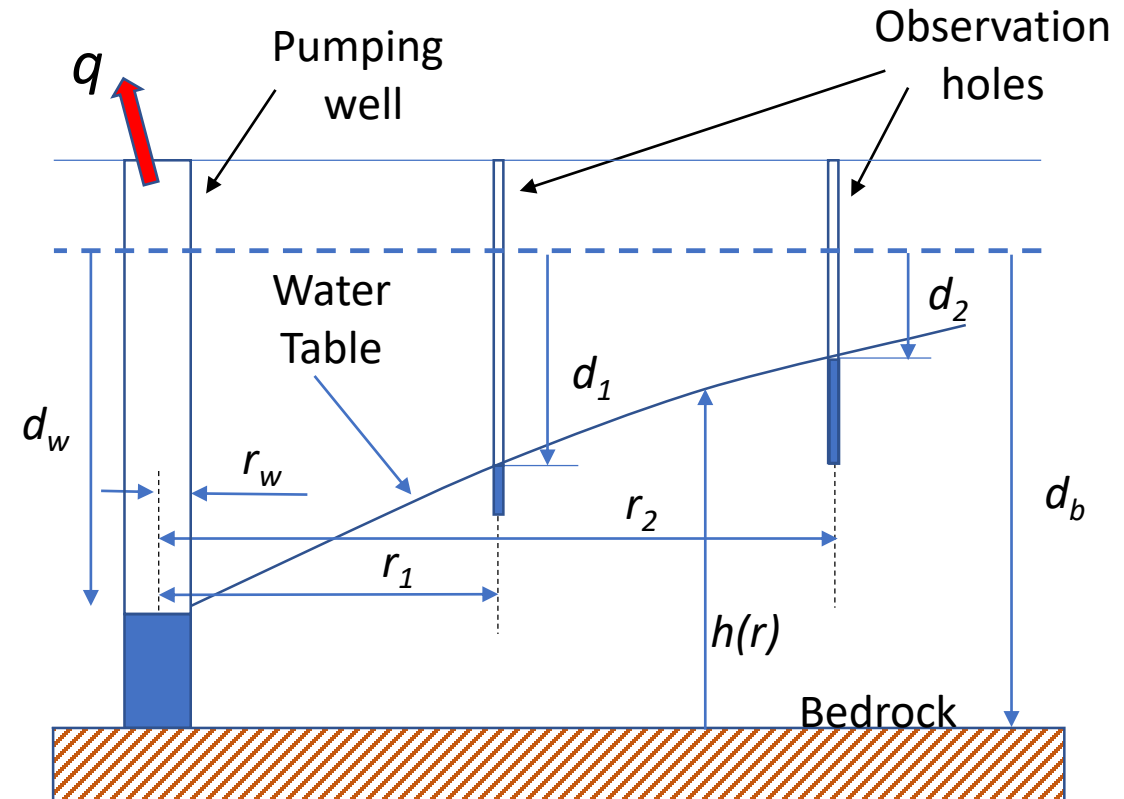
$$q = 2\pi r h(r) U(r) \quad \text{Continuity equation}$$

$$U(r) = K \frac{dh(r)}{dr} \quad \text{Darcy's law}$$

$$q = 2\pi r h(r) K \frac{dh(r)}{dr} \Rightarrow \frac{q}{2\pi K} \frac{dr}{r} = h dh$$

$$\frac{q}{2\pi K} \int_{r_1}^{r_2} \frac{1}{r} dr = \int_{h_1}^{h_2} h dh \Rightarrow \frac{q}{2\pi K} \log r \Big|_{r_1}^{r_2} = \frac{h^2}{2} \Big|_{h_1}^{h_2}$$

$$K = \frac{q \log(r_2/r_1)}{\pi (h_2^2 - h_1^2)} = 5.33 \cdot 10^{-5} \text{ m/s}$$





# Exercise 3. Pumping test to define $K$ - SOLUTION

$h(r) = d_b - d(r)$  Height of the aquifer with respect to the bedrock

$$K = \frac{q \log(r_2/r_1)}{\pi (h_2^2 - h_1^2)}$$

$$K = \frac{q}{\pi} \frac{\log(r_2/r_1)}{(d_b - d_2)^2 - (d_b - d_1)^2}$$

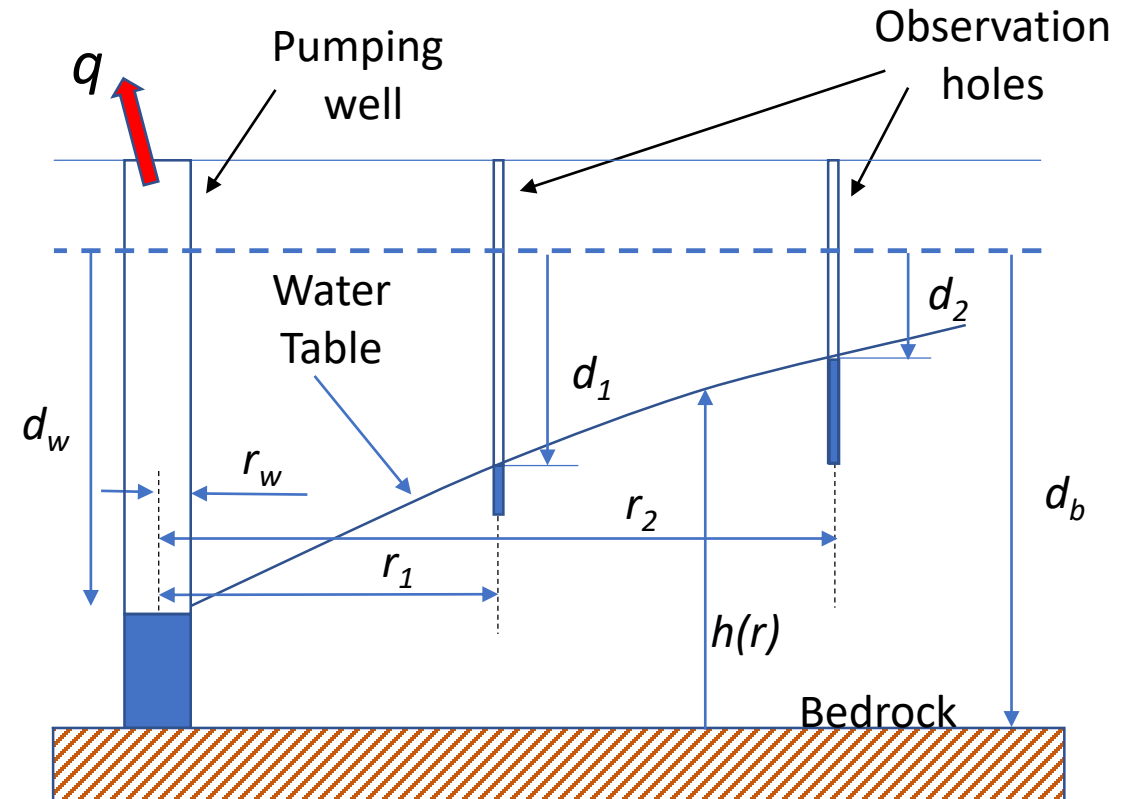
$$K = \frac{q \log(r_2/r_1)}{\pi} \frac{1}{d_1 - d_2} \frac{1}{2 d_b - d_1 - d_2}$$

Error propagation

$$\Delta f = \sqrt{\sum_{i=1}^n \left( \frac{\partial f}{\partial x_i} \Delta x_i \right)^2} \Rightarrow \Delta K = \left| \frac{\partial K}{\partial d_b} \Delta d_b \right|$$

$$\Delta K = \frac{q}{\pi} \log \frac{r_2}{r_1} \frac{1}{d_1 - d_2} \left| \frac{-2}{(2 d_b - d_1 - d_2)^2} \Delta d_b \right| = 8.74 \cdot 10^{-6} \text{ m/s}$$

$$\frac{\Delta K}{K} = 16.4 \% \quad \frac{\Delta d_b}{d_b} = 14.1 \%$$



# Exercise 3. Pumping test to define $K$ - SOLUTION

We can follow the same procedure as for Q1, but between the well and hole 2, then reorganizing for  $h_w$

$$K = \frac{q \log(r_2/r_w)}{\pi (h_2^2 - h_w^2)}$$

$$h_w = \sqrt{h_2^2 - \frac{q}{\pi K} \log(r_2/r_w)} = 25.07 \text{ m}$$

Similarly, between the well and hole 1

$$K = \frac{q \log(r_1/r_w)}{\pi (h_1^2 - h_w^2)}$$

$$h_w = \sqrt{h_1^2 - \frac{q}{\pi K} \log(r_1/r_w)} = 25.07 \text{ m}$$

