

Prestressing 1 Conceptual design

Literatures :

- Polycopié *Structures en béton : Conception, dimensionnement et vérification* chap. 6
- *Prestressed Concrete Bridges*, C. Menn
- TGC 7, *Dimensionnement des structures en béton*
- TGC 8, *Dimensionnement des structures en béton*



Introduction

Concrete → in compression during constructive stage

Bridges → Fundamental

Buildings → Large span or large loads

Advantages

- Slenderness ↑
- Cracking ↓
- Stiffness ↑
- Use of high steel strength

Invention → XIX century - start of XXe

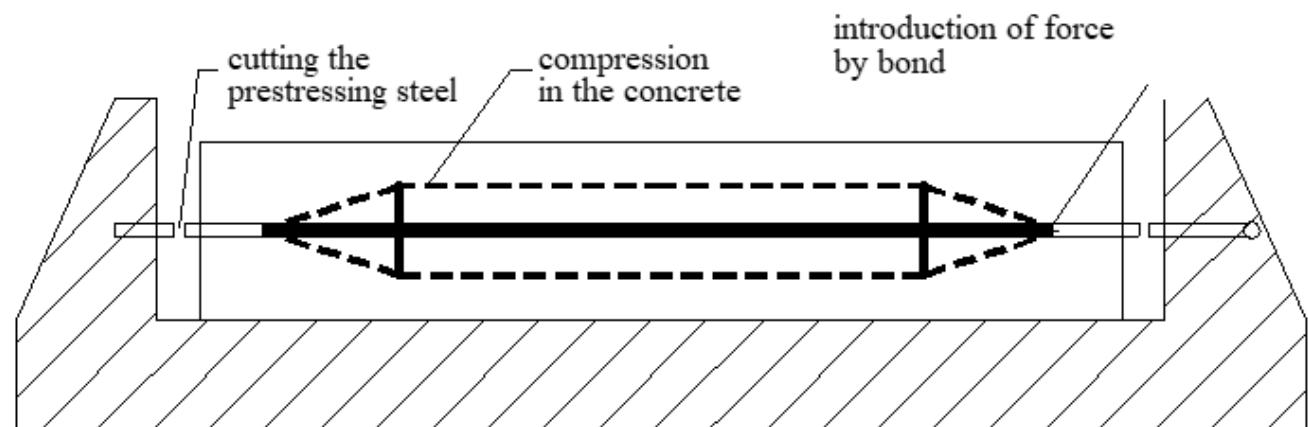
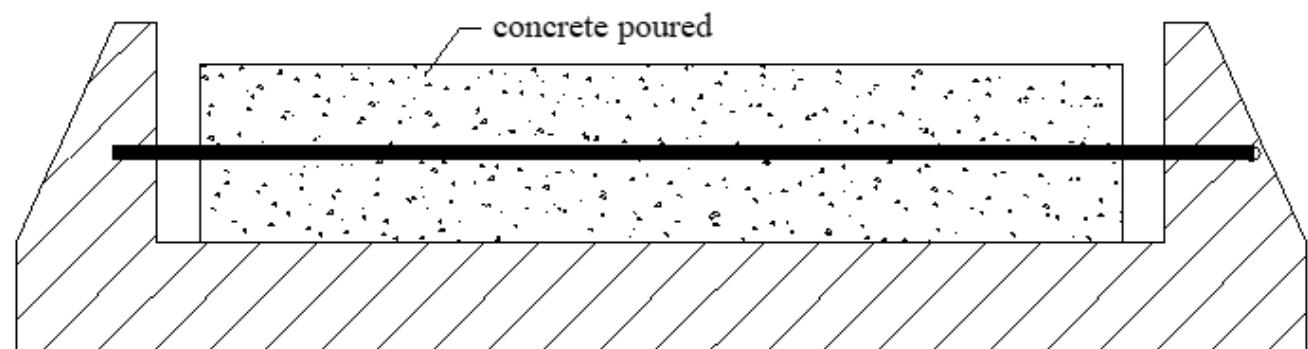
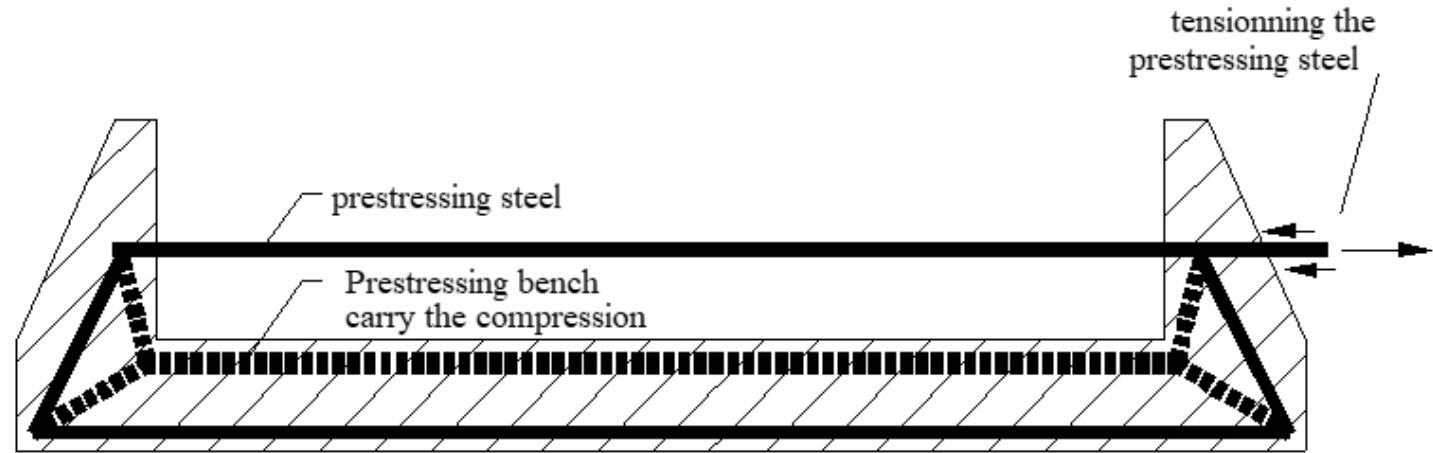
Main patent → 1928 (Eugène Freyssinet)

Types of prestressing

Pre-tensioning

Prestressing Process

- Placing of the tendons
- Tensionning
- Concrete
- Curing and demoulding
- Detensioning (cutting)



Types of prestressing

Pre-tensioning



Types of prestressing

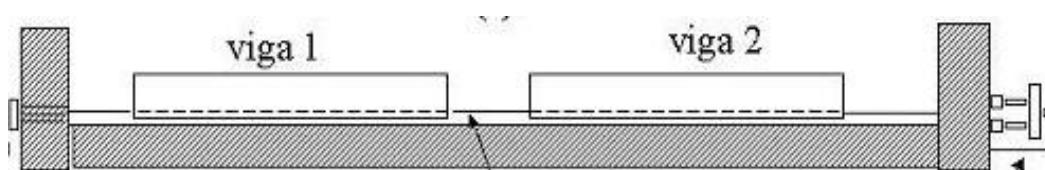
Pre-tensioning



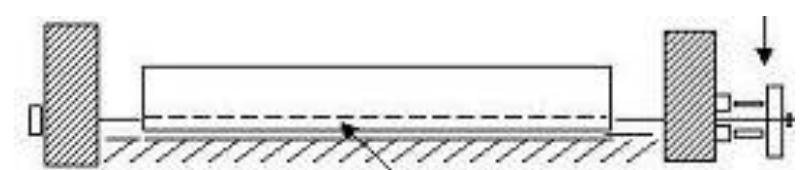
Types of prestressing

Pre-tensioning

Discontinuous



Continuous

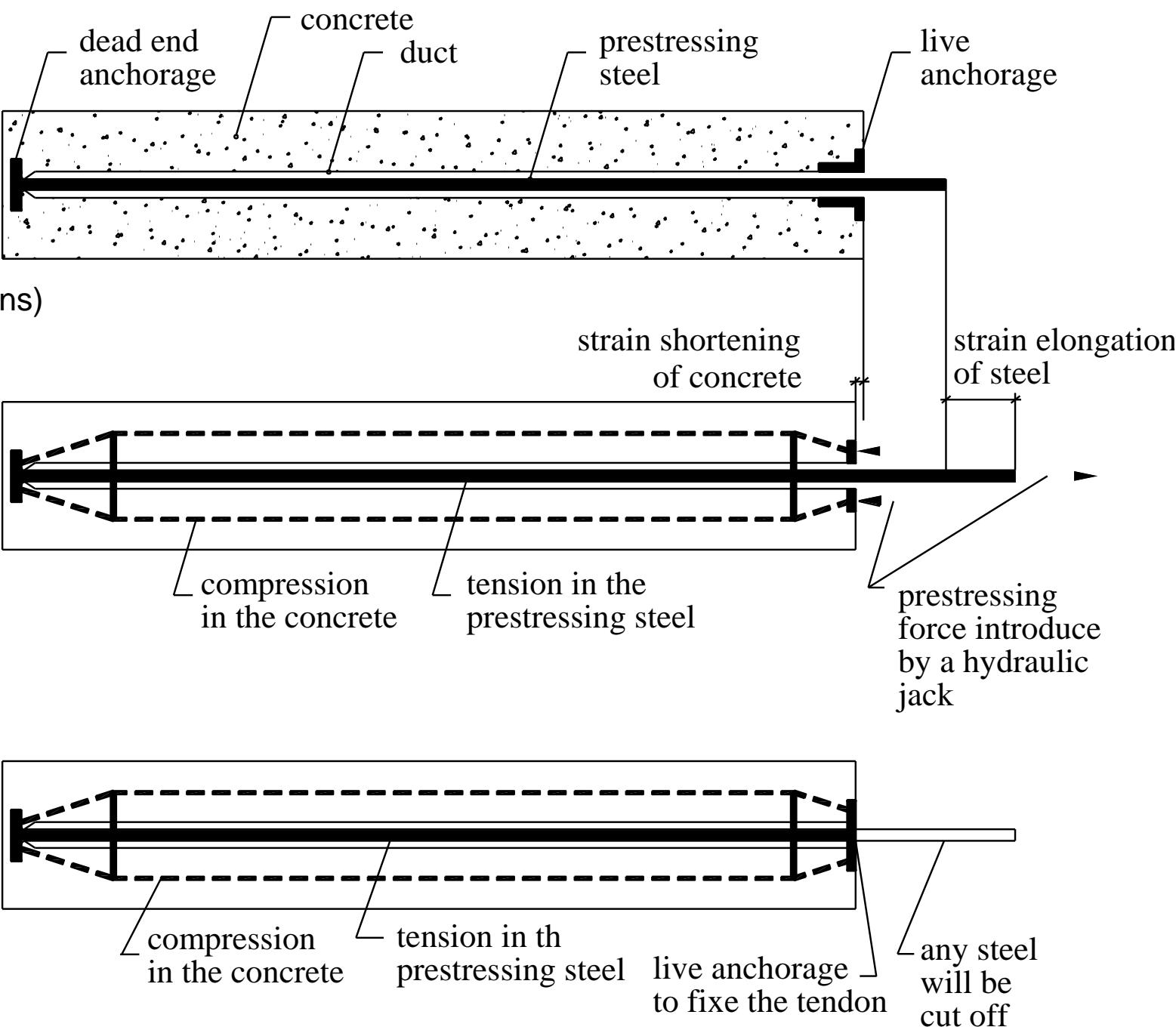


Types of prestressing

Post-tensioning

Prestressing Process

- Concrete with the duct + anchorages (+ tendons)
- Curing and demoulding
- Tensioning



Types of prestressing

Post-tensioning

Tendon = prestressing steel (e.g. strands) + anchorages + duct + grout

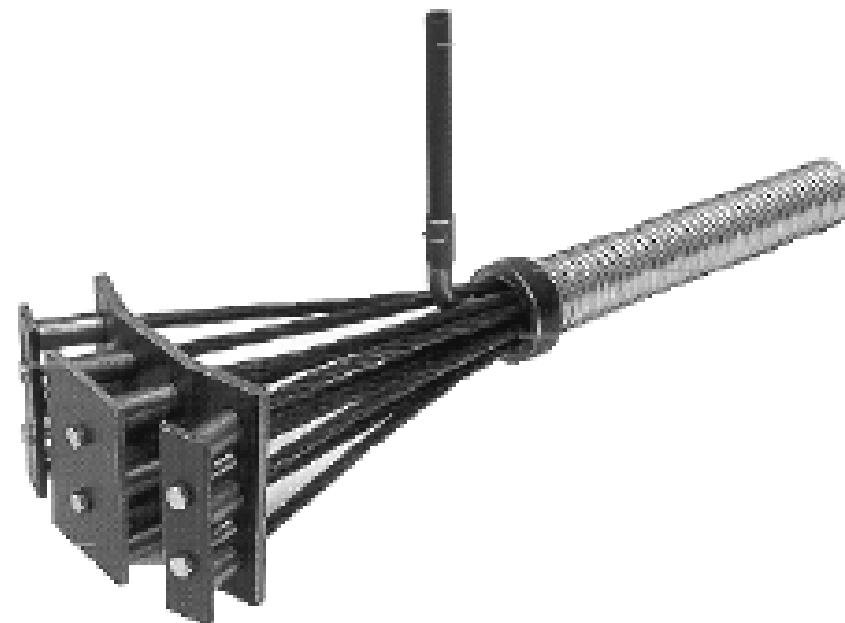
(câble = acier de précontrainte + têtes + gaine + coulis d'injection)



Live anchorage (tête mobile)



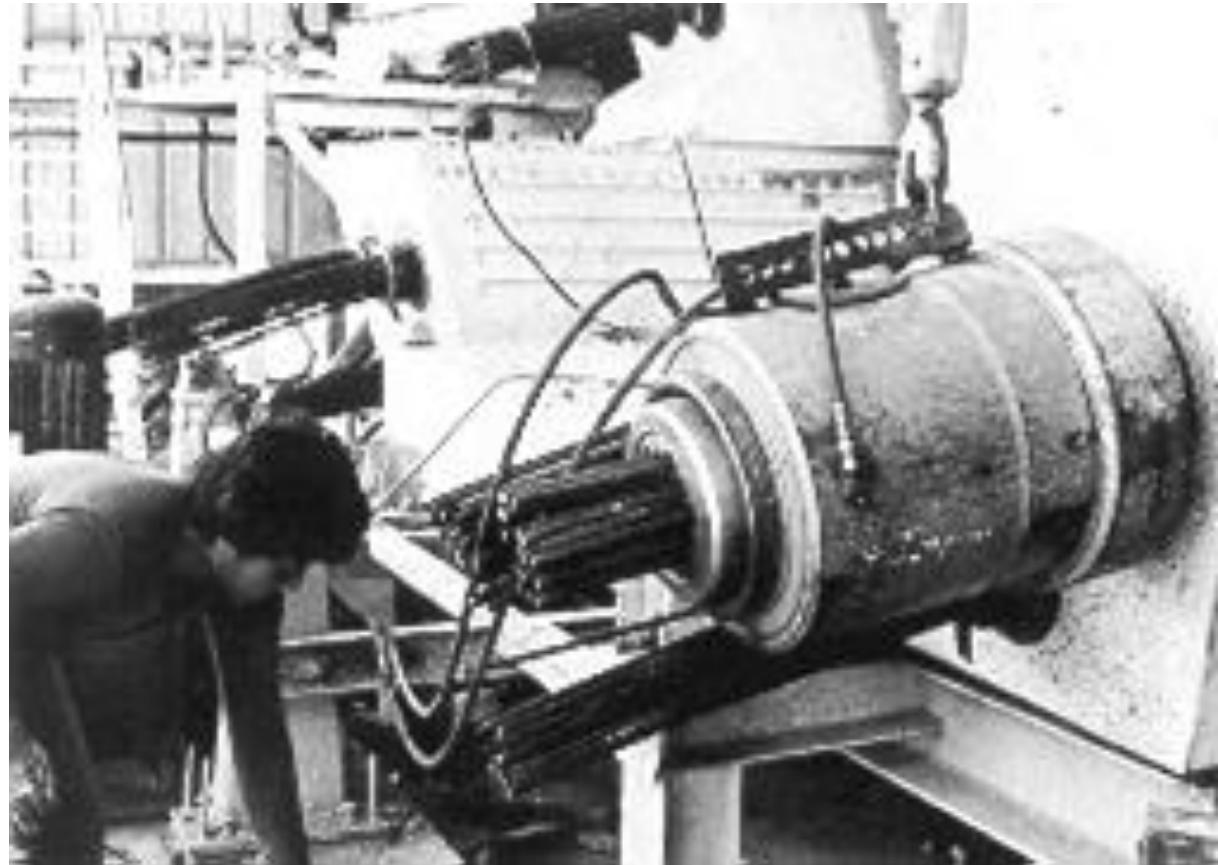
Dead end anchorage (tête fixe)



Types of prestressing

Post-tensioning

Jack



Types of prestressing

Post-tensioning

Internal



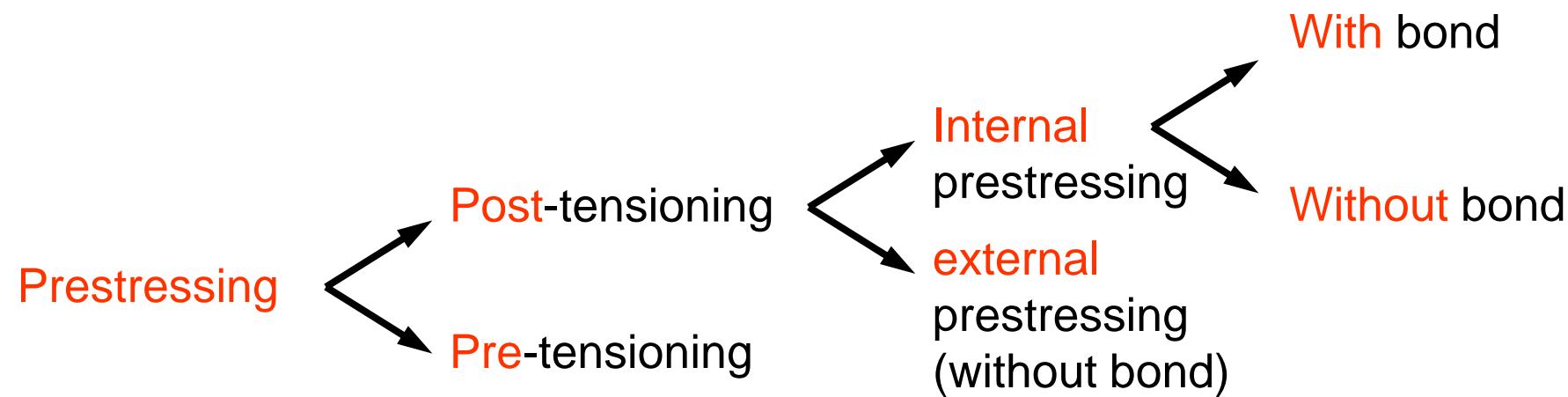
External



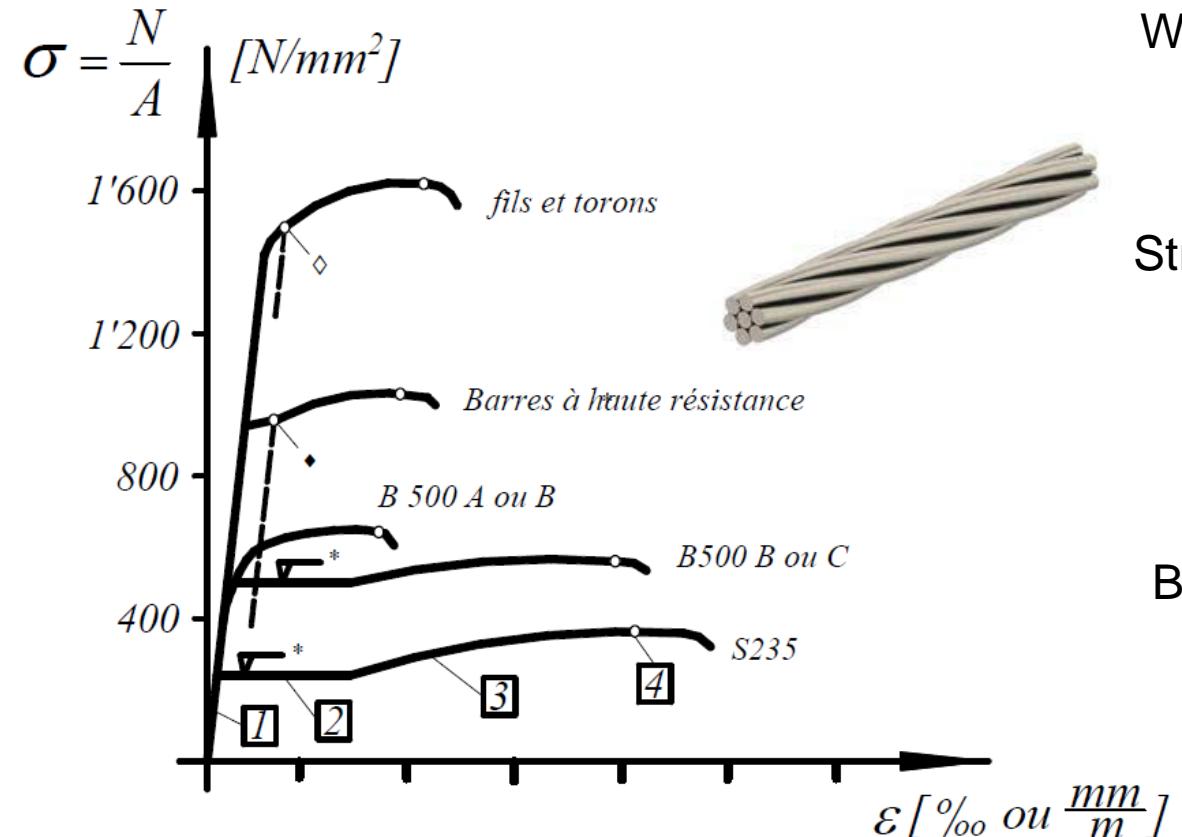
With or without bond

Without bond

Types of prestressing



Prestressing steel

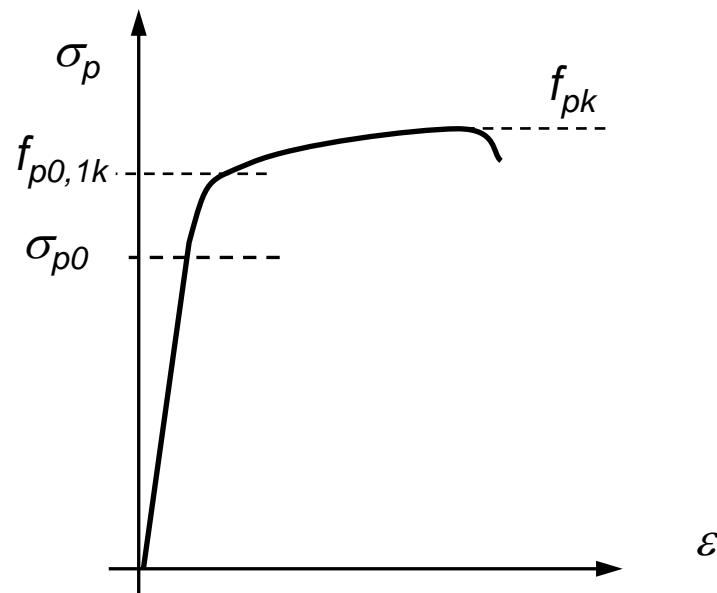
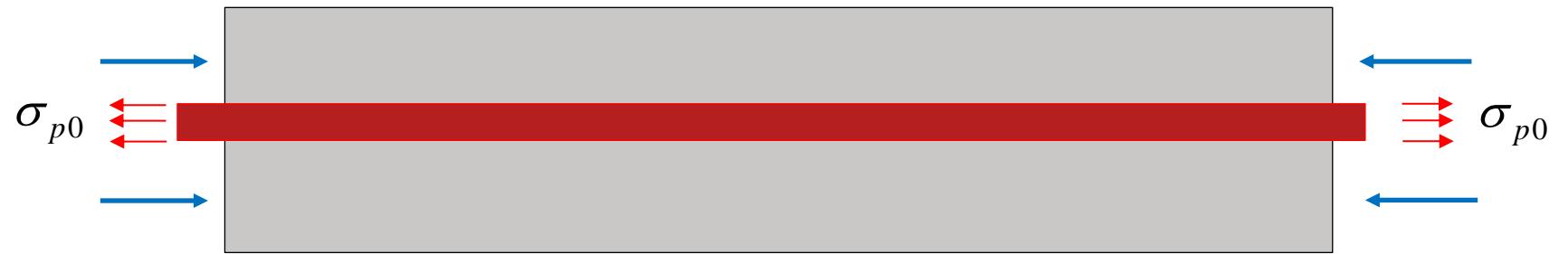


Wires
Strands
Bars

Produit	Diamètre \varnothing [mm]	Section A_p [mm 2]	Résistance à la traction f_{pk} [N/mm 2]	Limite d'écoulement $f_{p0,1k}$ [N/mm 2]	Désignation
Fils	3,0	7,1	1860	1600	Y1860C-3,0
	4,0	12,6	1860	1600	Y1860C-4,0
	5,0	19,6	1860	1600	Y1860C-5,0
	6,0	28,3	1770	1520	Y1770C-6,0
	7,0	38,5	1670	1440	Y1670C-7,0
	8,0	50,3	1670	1440	Y1670C-8,0
	10,0	78,5	1570	1300	Y1570C-10,0
Torons	12,9	100	1860	1600	Y1860S7-12,9
	15,3	140	1770 1860	1520 1600	Y1770S7-15,3 Y1860S7-15,3
	15,7	150	1770 1860	1520 1600	Y1770S7-15,7 Y1860S7-15,7
Barres (lisses ou nervurées)	20,0	314	1100	900	Y1100H-20,0
	26,0	531	1030 1050 1230	830 950 1080	Y1030H-26,0 Y1050H-26,0 Y1230H-26,0
	26,5	552	1030 1050 1230	830 950 1080	Y1030H-26,5 Y1050H-26,5 Y1230H-26,5
	32,0	804	1030 1050 1230	830 950 1080	Y1030H-32,0 Y1050H-32,0 Y1230H-32,0
	36,0	1018	1030 1050 1230	830 950 1080	Y1030H-36,0 Y1050H-36,0 Y1230H-36,0

[SIA 262, 2013]

Initial prestressing force



$$\sigma_{p0} \leq 0.70 \cdot f_{pk} \quad \text{After the initial prestressing force}$$

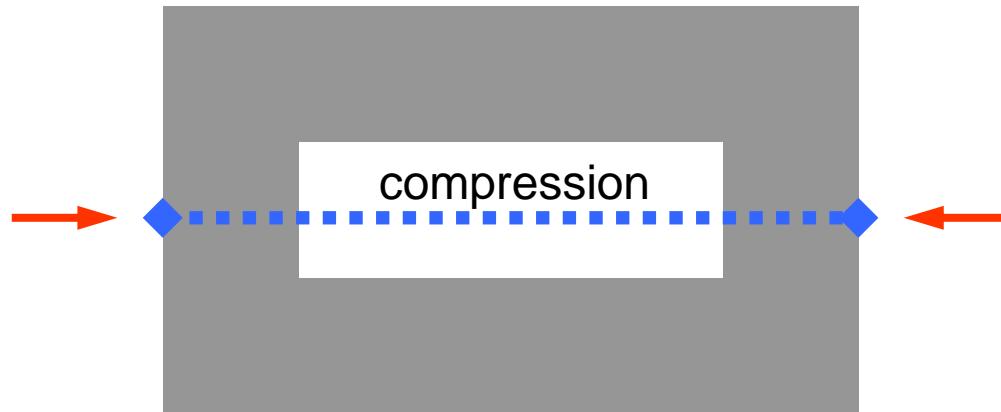
$$\sigma_{p0} \leq 0.75 \cdot f_{pk} \quad \text{During the initial prestressing force}$$

$$\sigma_{p\infty} \geq 0.45 \cdot f_{pk} \quad \text{at } t = \infty$$

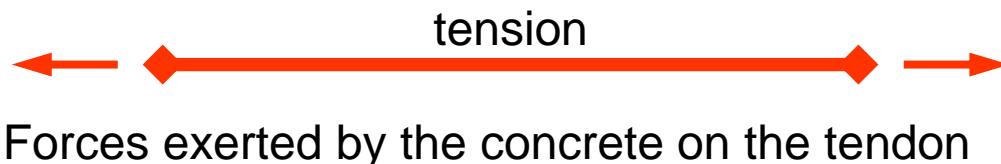
Approaches to considering prestressing

Self-equilibrated **system of Forces**

(prestressing considered as external action)



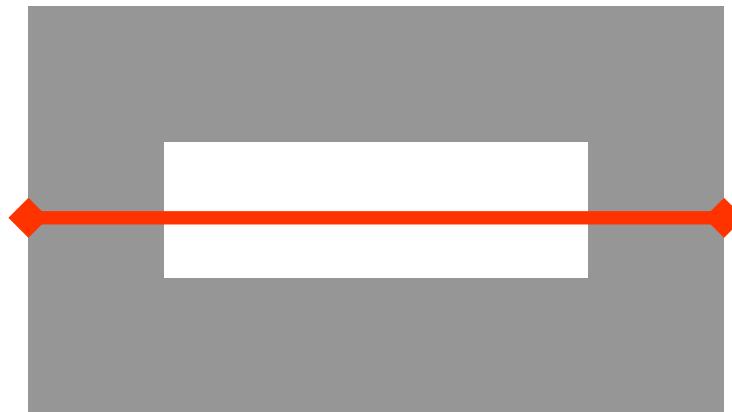
Forces exerted by the tendon on the concrete



Forces exerted by the concrete on the tendon

Self-equilibrated **state of stresses**

(prestressing considered on the side of the resistance)

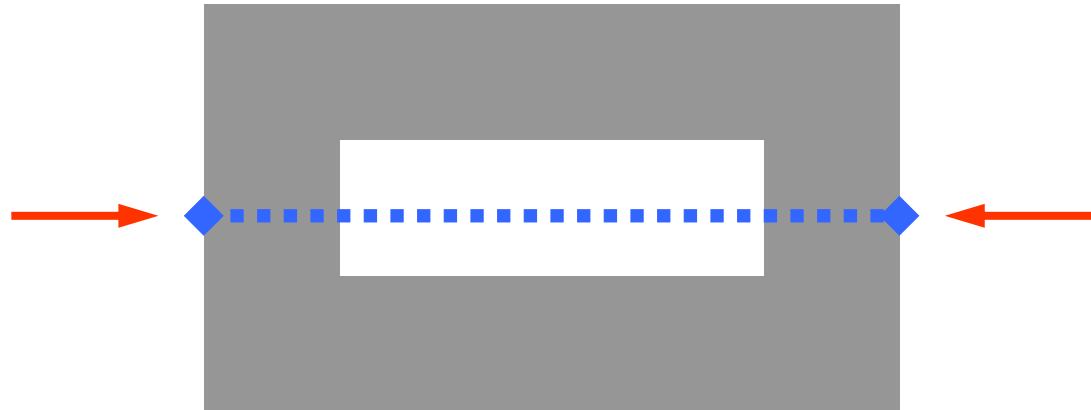


The system is composed by the concrete **with** the tendon. Prestressing induces internal forces and so deformation.

Approaches to considering prestressing

1) Anchorage forces

Self-equilibrated **system of Forces**



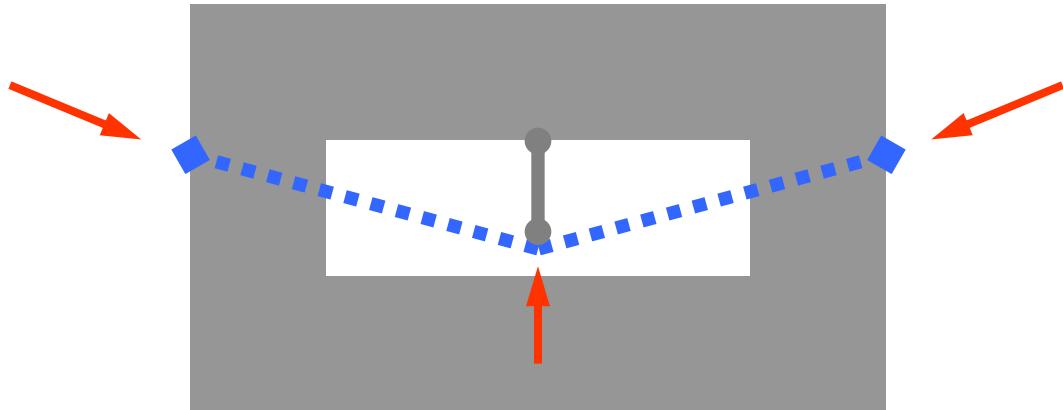
Self-equilibrated **state of stresses**



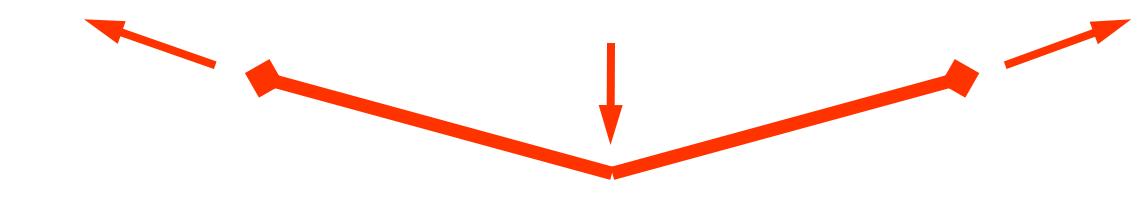
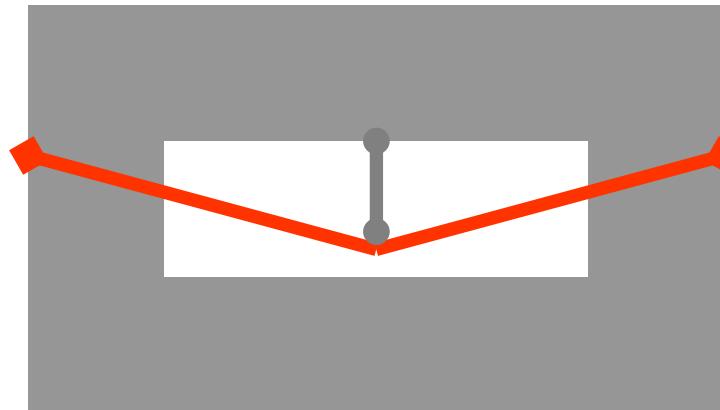
Approaches to considering prestressing

2) Deviation forces

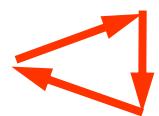
Self-equilibrated **system of Forces**



Self-equilibrated **state of stresses**



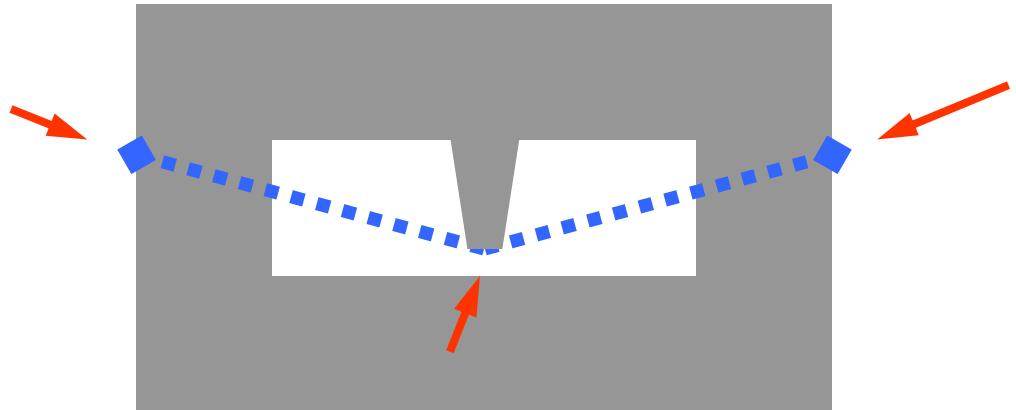
Deviation forces are in equilibrium with the anchorage forces



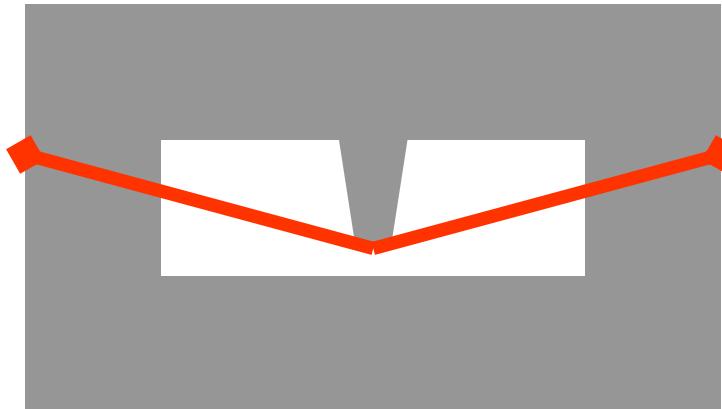
Approaches to considering prestressing

3) Friction forces

Self-equilibrated **system of Forces**



Self-equilibrated **state of stresses**

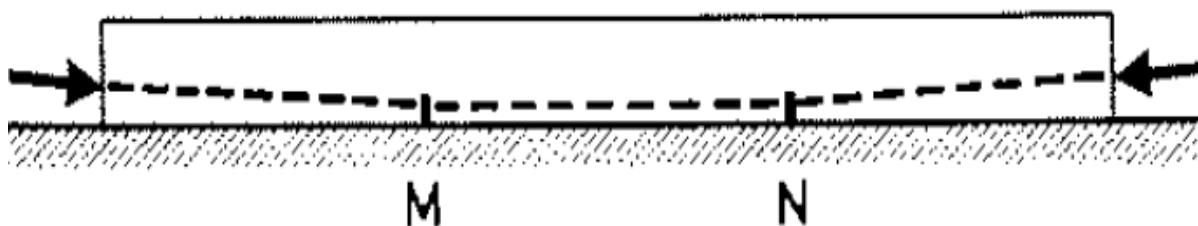


friction forces derive from a relative displacement between the tendon and the deviation element (when the tendon is tensioned for example)

Prestressing tendon geometry

Pre-tensioning

Deviators in intermediate cross sections (M y N) in the mould or the bench. They should resist vertical forces

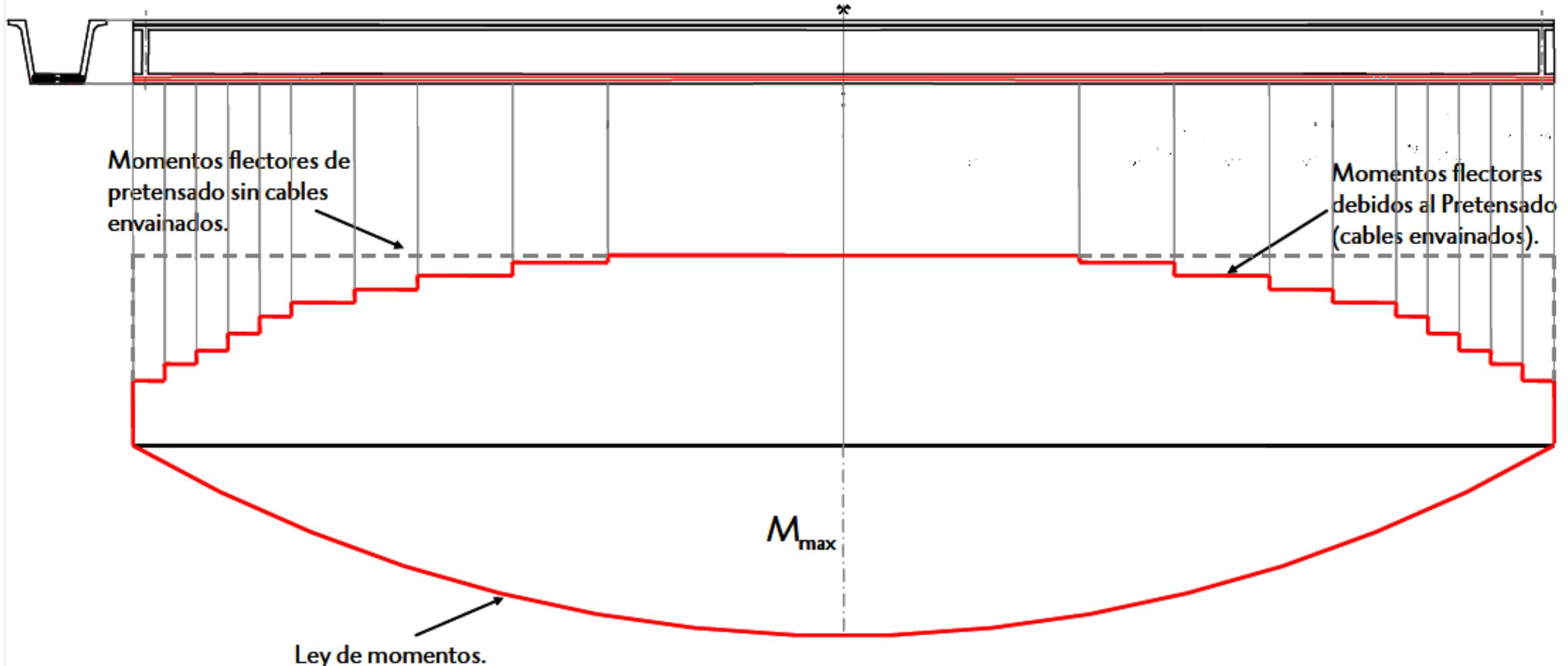


With several layers of **debonding** of strands



Prestressing tendon geometry

Pre-tensioning - Debonding



Prestressing tendon geometry

Pre-tensioning – Debonding : anchorage length

EN 1992-1-1:2004 (E)

Eurocode 2: Design of concrete structures -
Part 1-1: General rules and rules for buildings

8.10.2 Anchorage of pre-tensioned tendons

8.10.2.1 General

(1) In anchorage regions for pre-tensioned tendons, the following length parameters should be considered, see Figure 8.16:

- Transmission length, l_{pt} , over which the prestressing force (P_0) is fully transmitted to the concrete; see 8.10.2.2 (2),
- Dispersion length, l_{disp} over which the concrete stresses gradually disperse to a linear distribution across the concrete section; see 8.10.2.2 (4),
- Anchorage length, l_{bpd} , over which the tendon force F_{pd} in the ultimate limit state is fully anchored in the concrete; see 8.10.2.3 (4) and (5).

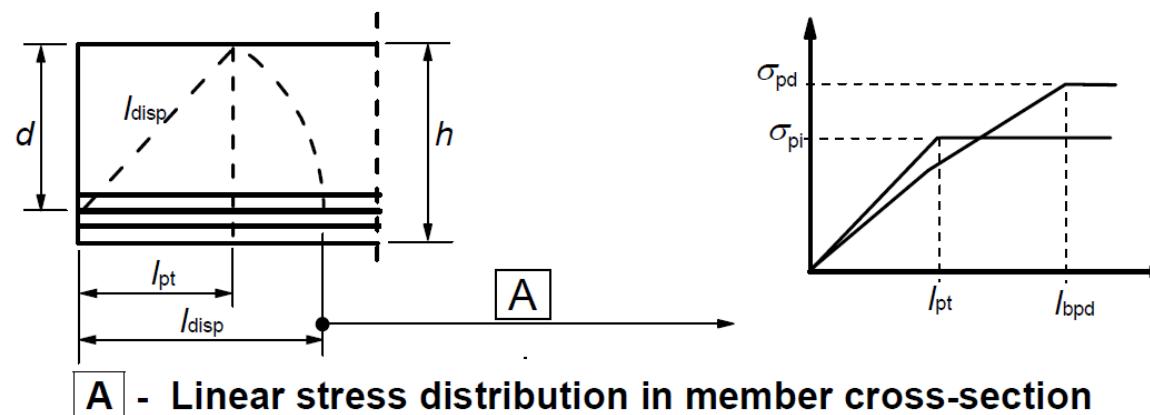
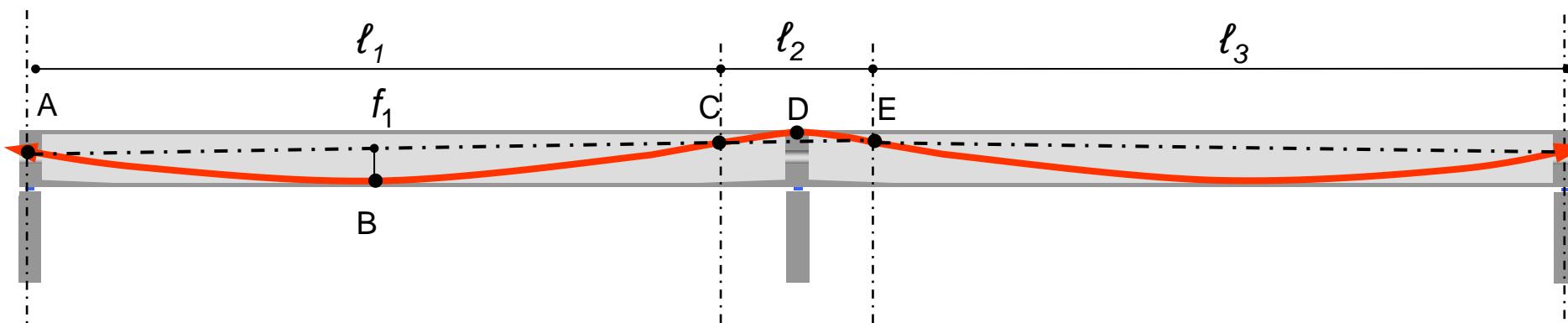
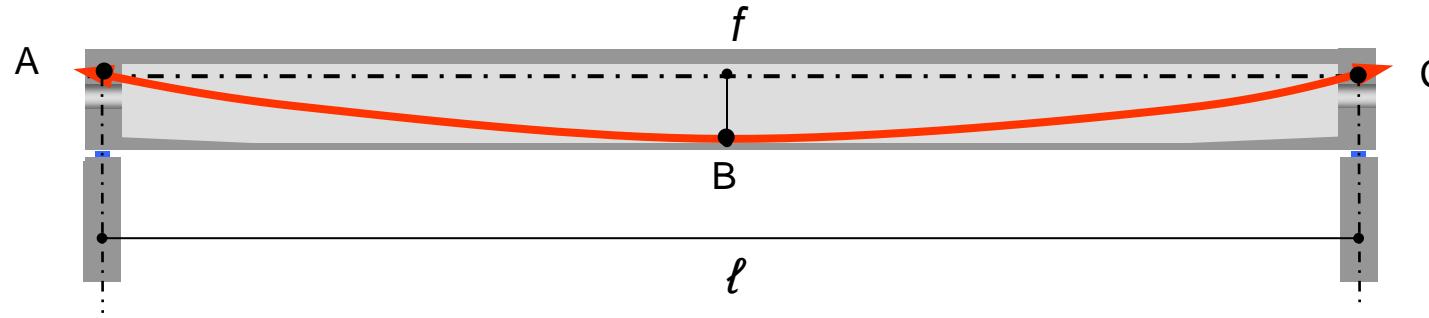


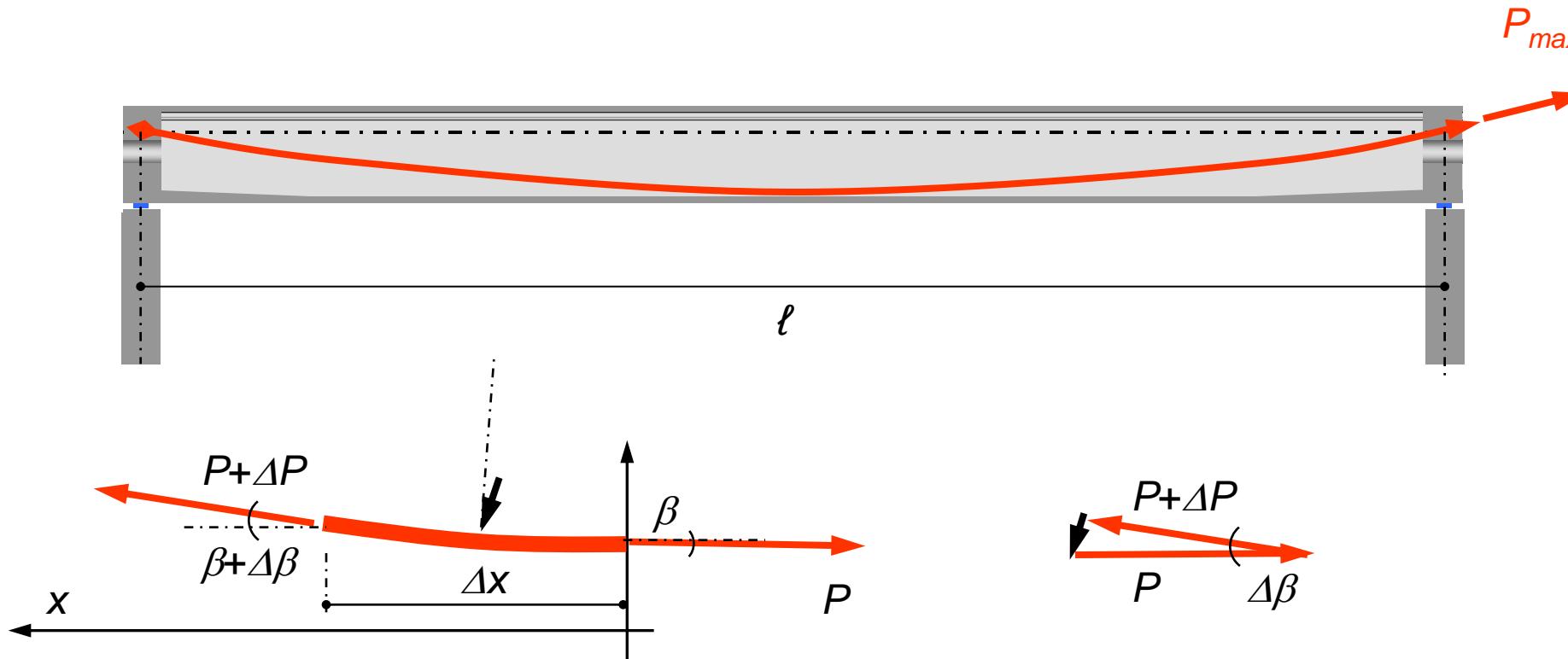
Figure 8.16: Transfer of prestress in pretensioned elements; length parameters

Prestressing tendon geometry

Post-tensioning



Immediate losses of prestress : due to friction

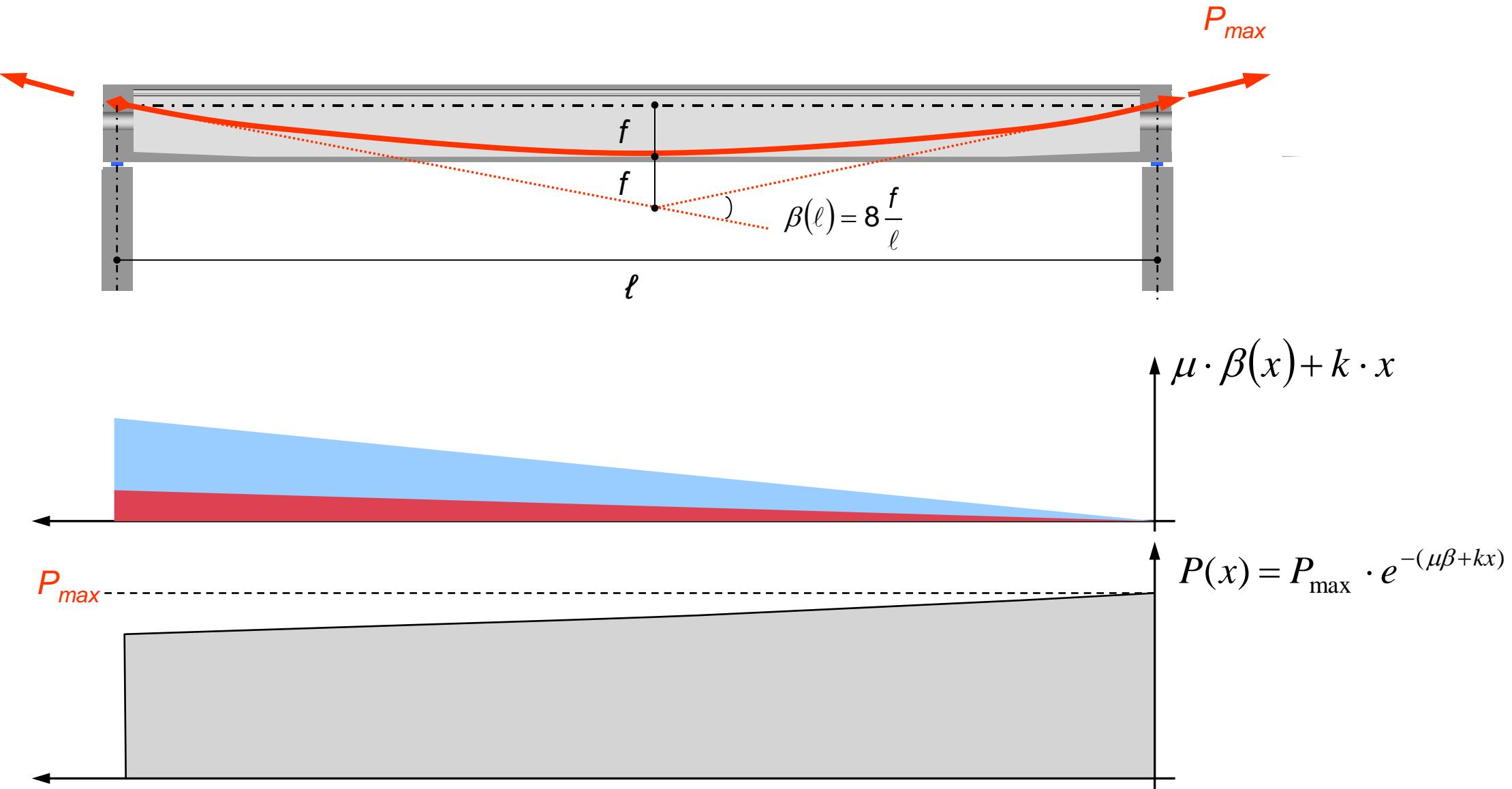


$$\Delta P = -P \cdot (\mu \cdot \Delta \beta + k \cdot \Delta x) \quad \rightarrow \quad P(x) = P_{\max} \cdot e^{-(\mu \beta + kx)}$$

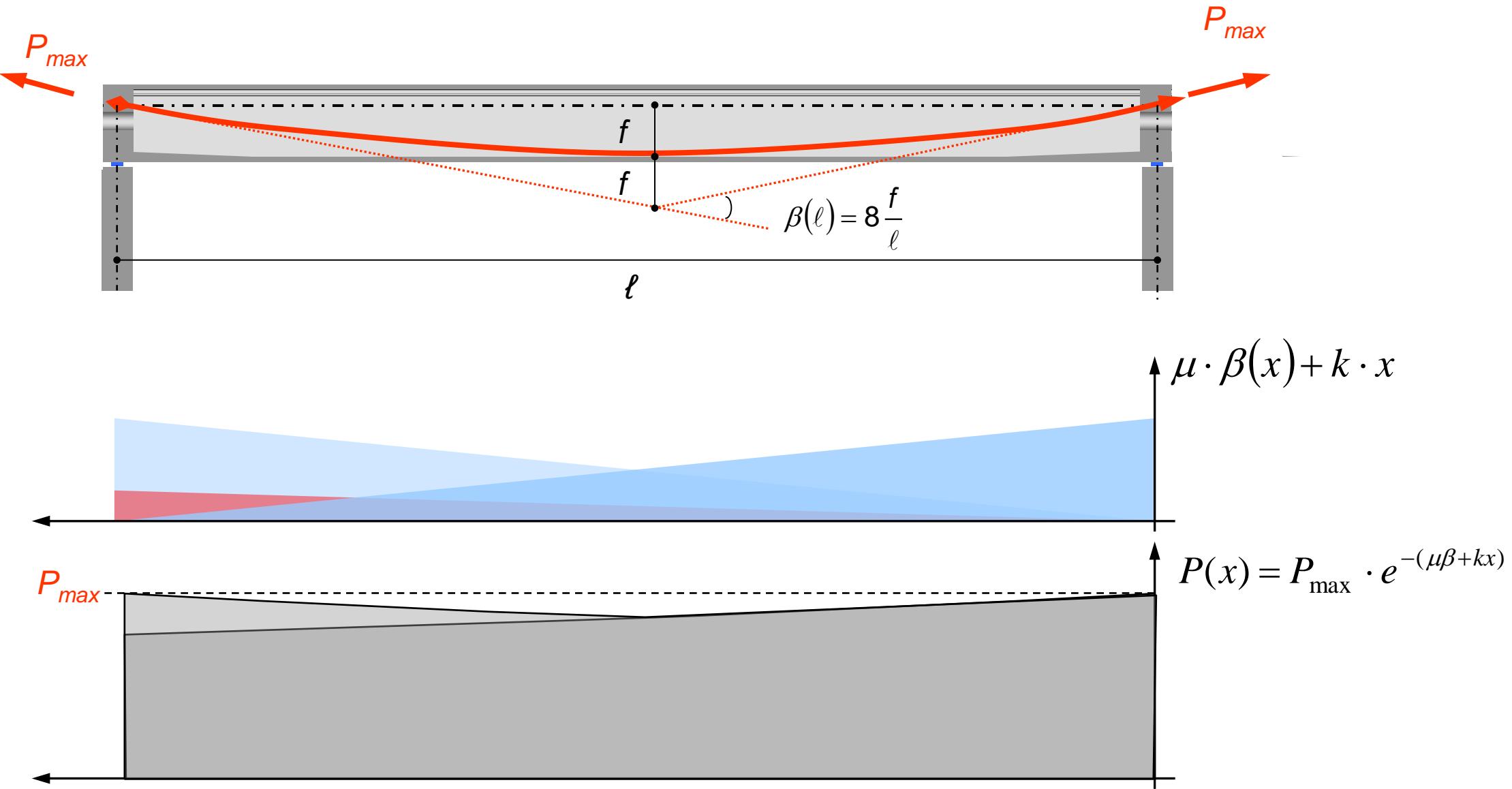
For example for strands

Duct type		
Metal	$\mu \approx 0.20$	$k \approx 0.0008 \text{ m}^{-1}$
Polymer (plastic)	$\mu \approx 0.14$	$k \approx 0.0010 \text{ m}^{-1}$

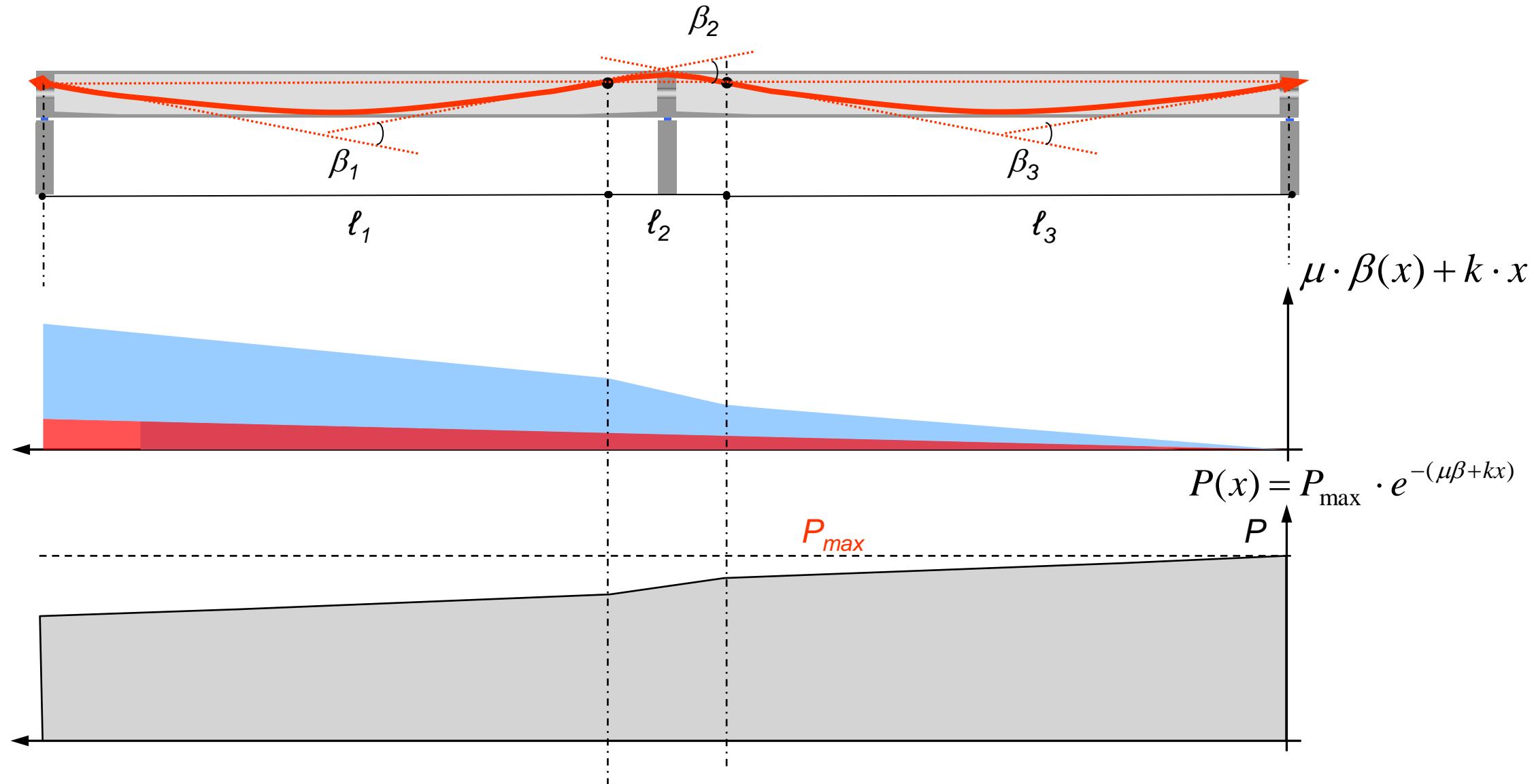
Immediate losses of prestress : due to friction



Immediate losses of prestress : due to friction

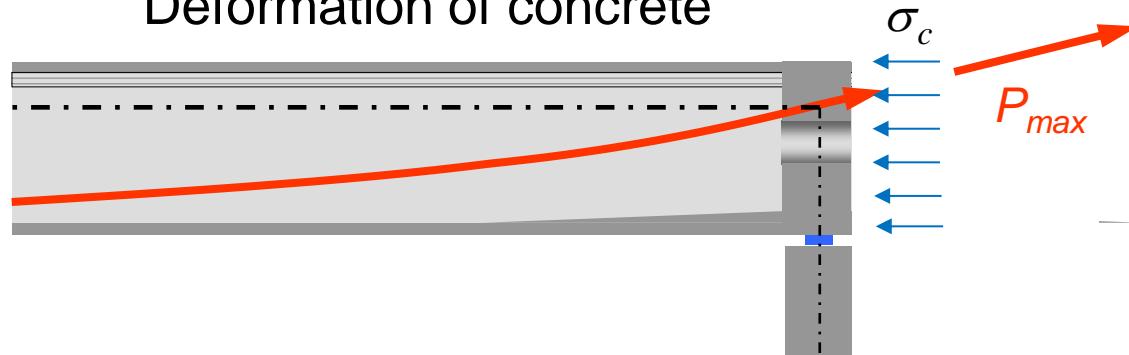


Immediate losses of prestress : due to friction

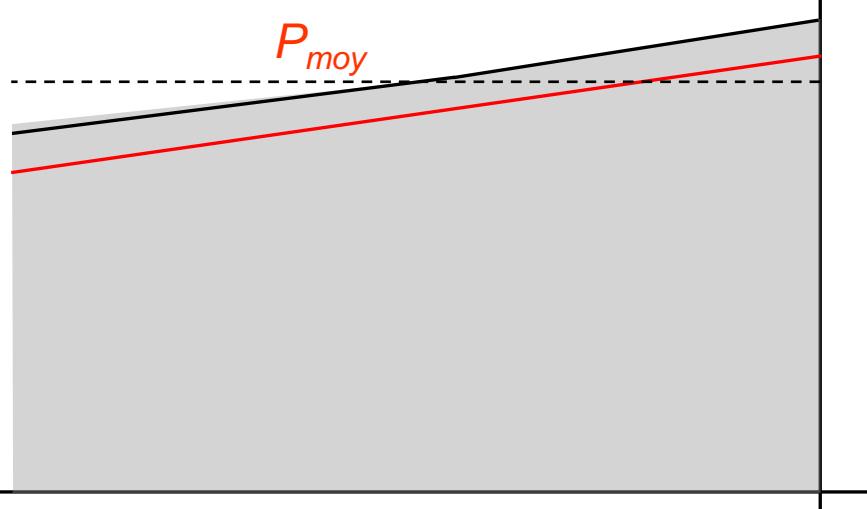


Immediate losses of prestress : others

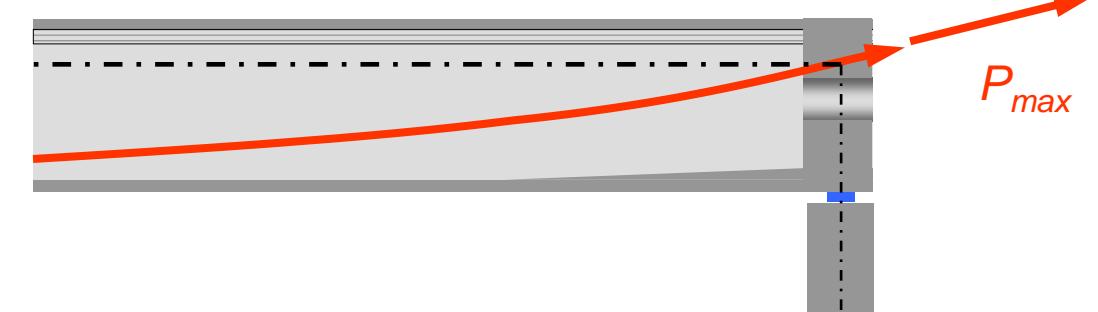
Deformation of concrete



$$\Delta\sigma_{p,el} = \varepsilon_{moy} \cdot E_p = \frac{\sigma_{cp}}{E_c} \cdot E_p = \frac{P_{moy}}{A_c \cdot E_{cm}} \cdot E_p$$

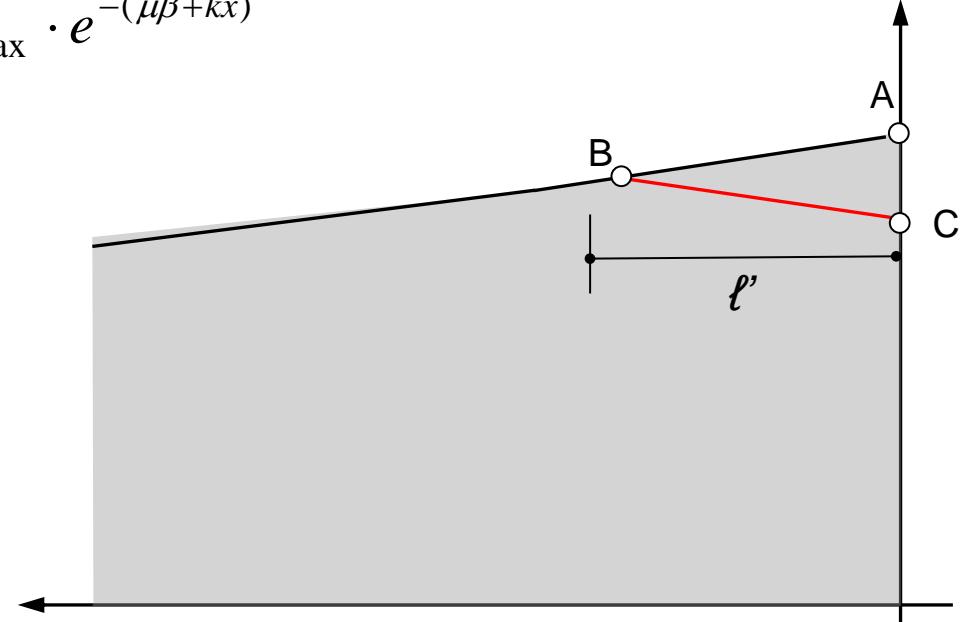


Wedge draw-in



$$P(x) = P_{max} \cdot e^{-(\mu\beta+kx)}$$

$$\Delta\sigma_{p,el}$$



This loss can be neglected by

- Sequence of prestressing
- Larger prestressing stresses

A_c : Cross sectional area of concrete

E_c : modulus of elasticity of concrete

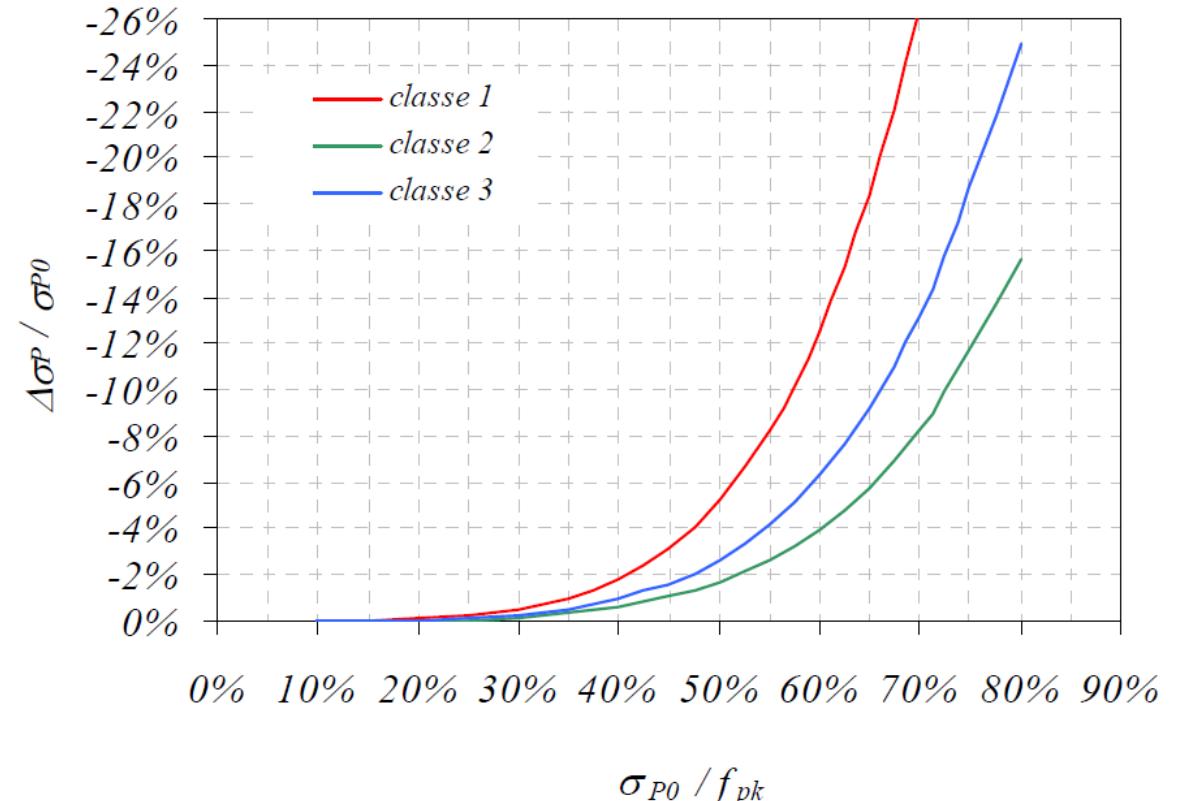
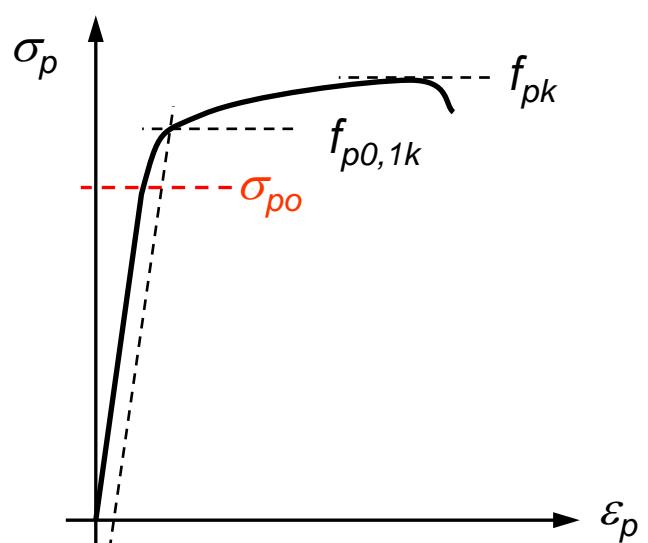
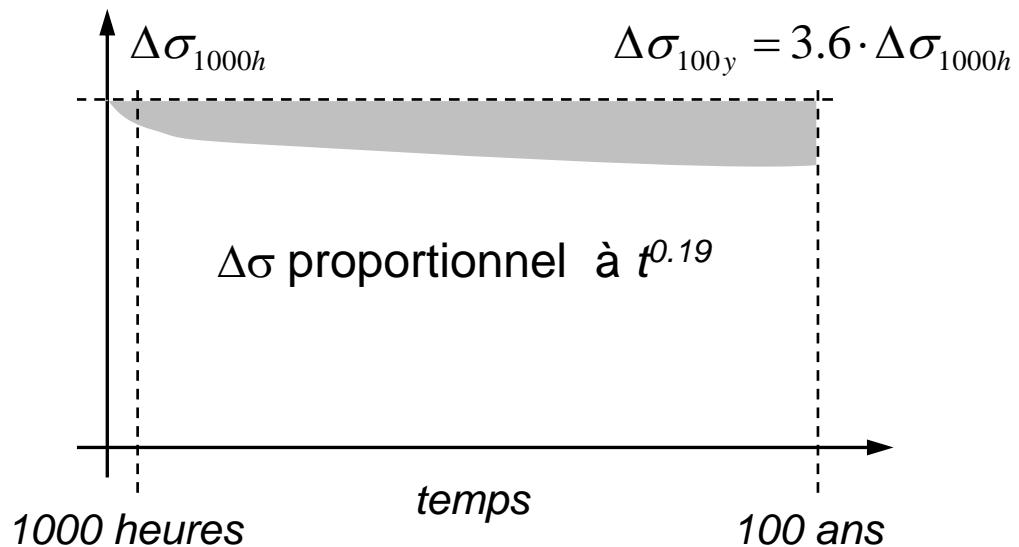
Time dependant losses of prestress

Losses of prestress due to

1. **relaxation** : reduction of stress at constant strain
2. **shrinkage** : concrete shortening over time
3. **creep** : concrete compressive stress in concrete causes elastic strain and an strain increment over time due to creep

Time dependant losses of prestress

Relaxation



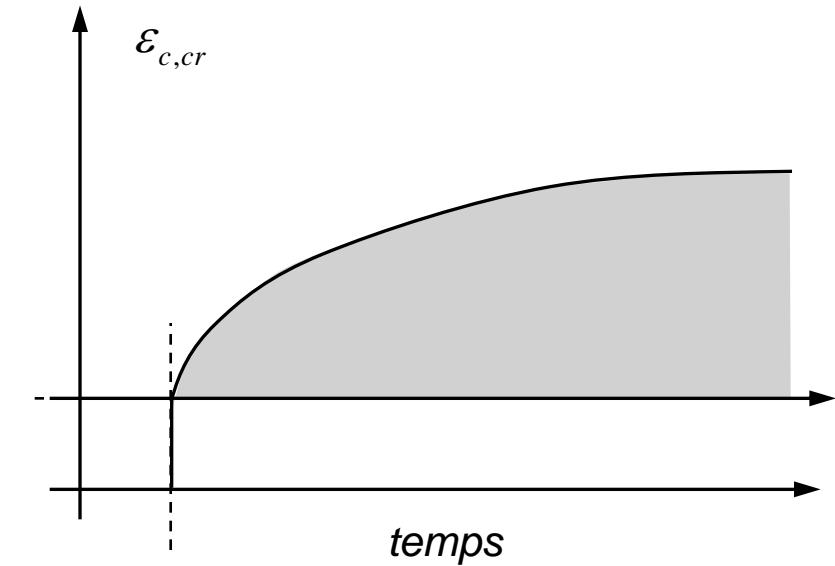
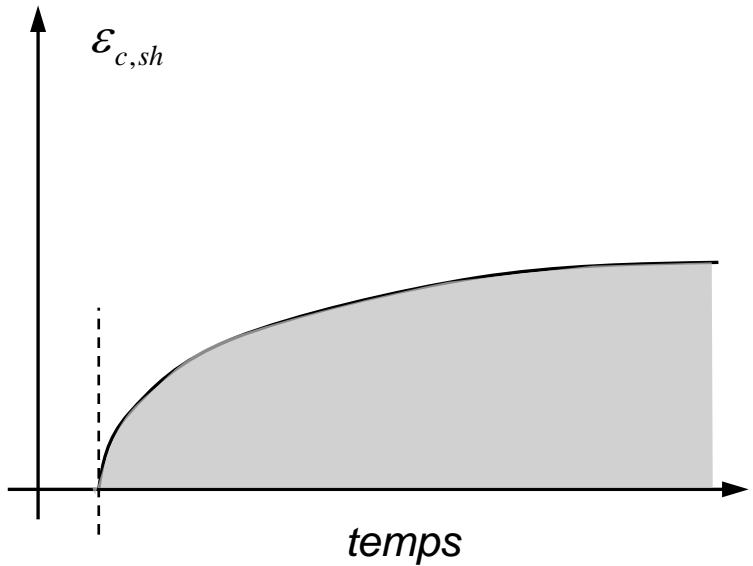
$\sigma_{p0} \leq 0.70 \cdot f_{pk}$ After the initial prestressing force

$\sigma_{p0} \leq 0.75 \cdot f_{pk}$ During the initial prestressing force

$\sigma_{p\infty} \geq 0.45 \cdot f_{pk}$ at $t = \infty$

Time dependant losses of prestress

Shrinkage and creep



$$\Delta P = -A_p \cdot E_p \cdot (\varepsilon_{c,sh} + \varepsilon_{c,cr})$$

Time dependant losses of prestress

Interaction between relaxation, shrinkage and creep

Without interaction

$$\begin{aligned}\Delta P &= -\rho(t, \sigma_{P0}) \cdot P_0 + A_p \cdot E_p \cdot (\varepsilon_{cs}(t) + \varepsilon_{cc}(t, t_0, \sigma_c)) \\ &= -\rho(t, \sigma_{P0}) \cdot P_0 + A_p \cdot E_p \cdot \left(\varepsilon_{cs}(t) + \frac{\sigma_c}{E_c} \cdot \varphi(t, t_0) \right)\end{aligned}$$

With interaction

Simplified

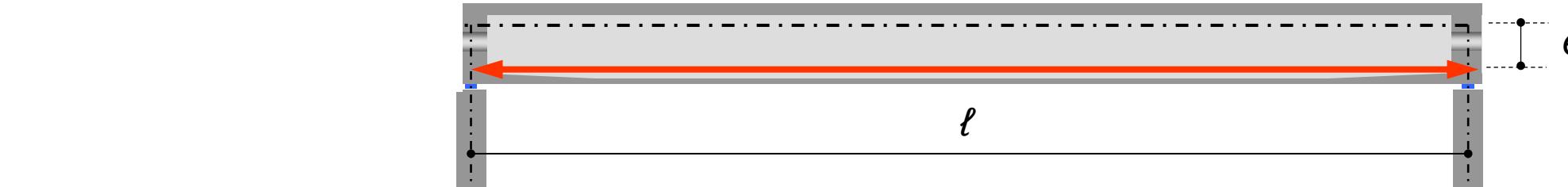
$$\Delta P = -0.8 \cdot \rho(t, \sigma_{P0}) \cdot P_0 + A_p \cdot E_p \cdot \left(\varepsilon_{cs}(t) + \frac{\sigma_c}{E_c} \cdot \phi(t, t_0) \right)$$

EC 2004 Approached

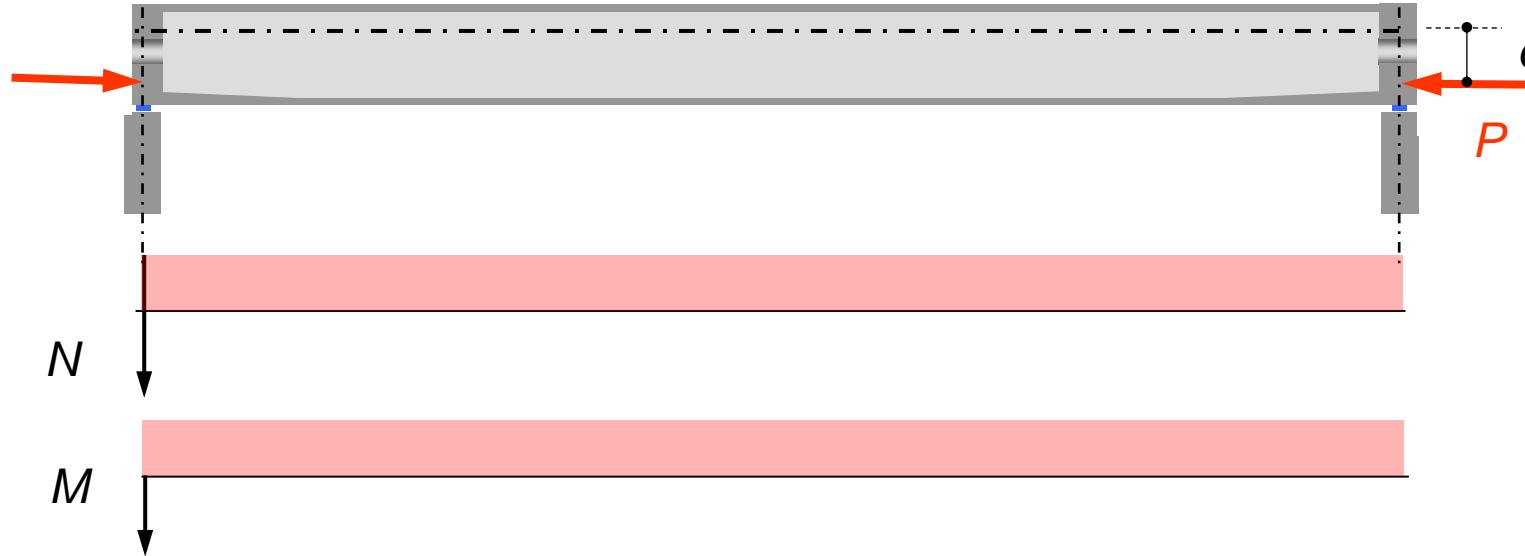
$$\Delta P = \frac{-0.8 \cdot \rho(t, \sigma_{P0}) \cdot P_0 + A_p \cdot E_p \cdot \left(\varepsilon_{cs}(t) + \frac{\sigma_c}{E_c} \cdot \phi(t, t_0) \right)}{1 + \frac{E_p}{E_c} \frac{A_p}{A_c} \left(1 + \left(\frac{e}{i_c} \right)^2 \right) \cdot (1 + 0.8 \cdot \phi(t, t_0))}$$

Isostatic example

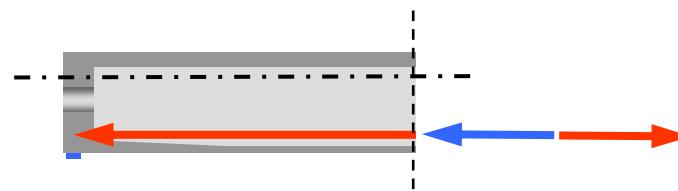
Simple supported beam with straight excentric tendon



Approach :
system of Forces



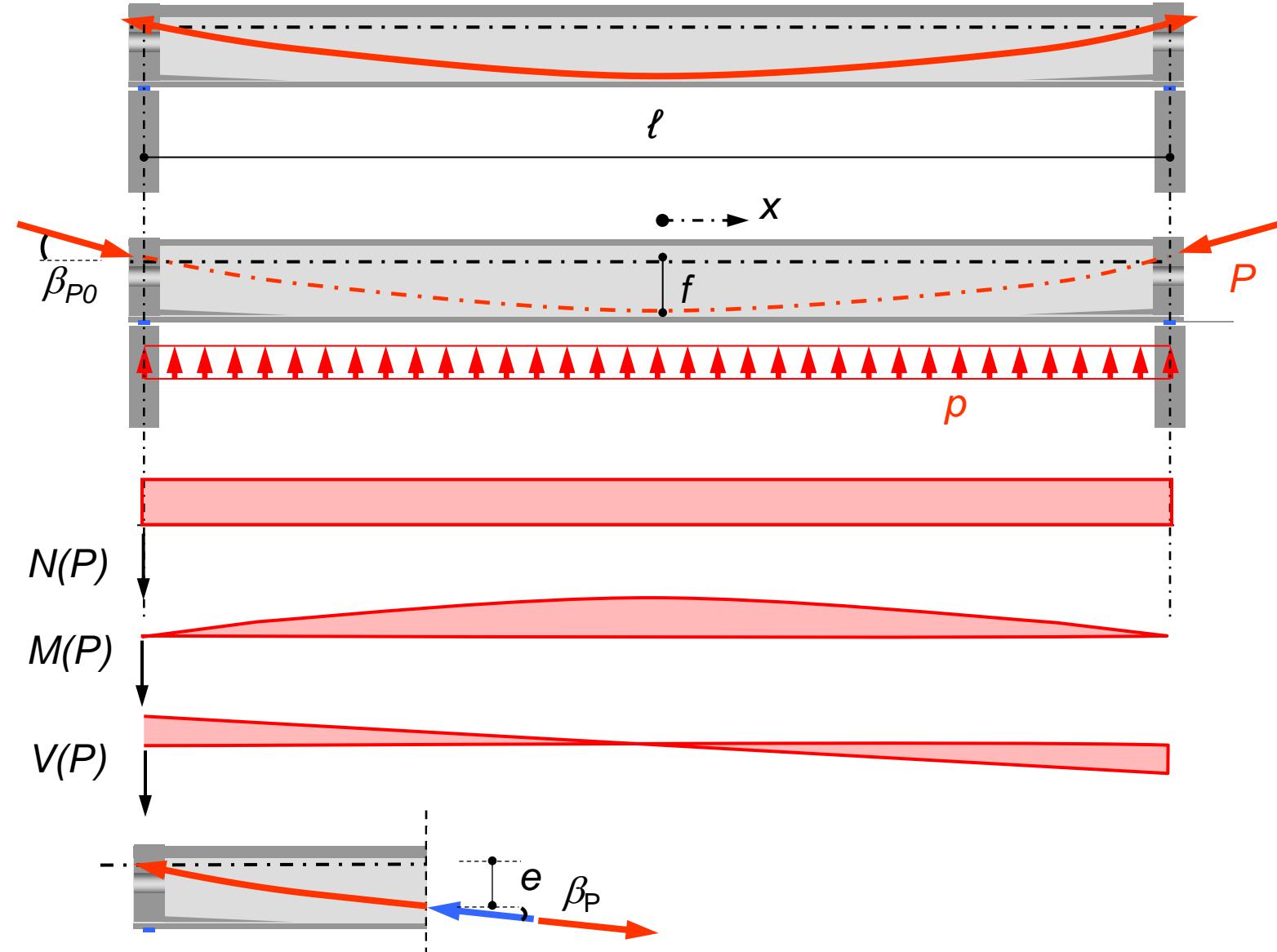
Approach :
state of stresses



Isostatic example

Simple supported beam with parabolic tendon

Approach :
system of Forces



Approach :
state of stresses