

# Prestressing 1      Conceptual design

Literatures :

- Polycopié *Structures en béton : Conception, dimensionnement et vérification* chap. 6
- *Prestressed Concrete Bridges*, C. Menn
- TGC 7, *Dimensionnement des structures en béton*
- TGC 8, *Dimensionnement des structures en béton*



# Introduction

Concrete → in compression during constructive stage

Bridges → Fundamental

Buildings → Large span or large loads

## Advantages

- Slenderness ↑
- Cracking ↓
- Stiffness ↑
- Use of high steel strength

Invention → XIX century - start of XXe

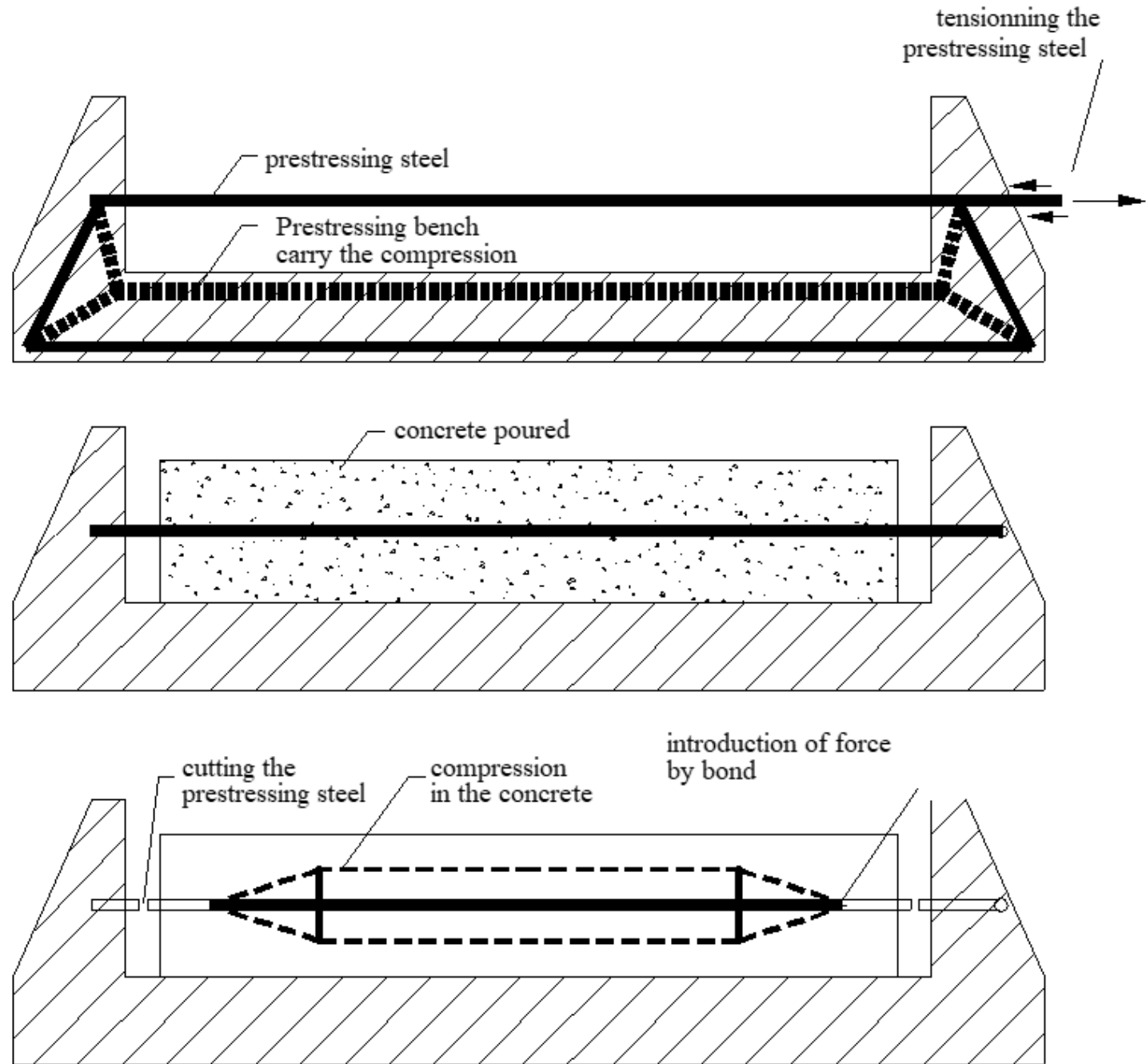
Main patent → 1928 (Eugène Freyssinet)

# Types of prestressing

## Pre-tensioning

### Prestressing Process

- Placing of the tendons
- Tensionning
- Concrete
- Curing and demoulding
- Detensioning (cutting)



# Types of prestressing

## Pre-tensioning





# Types of prestressing

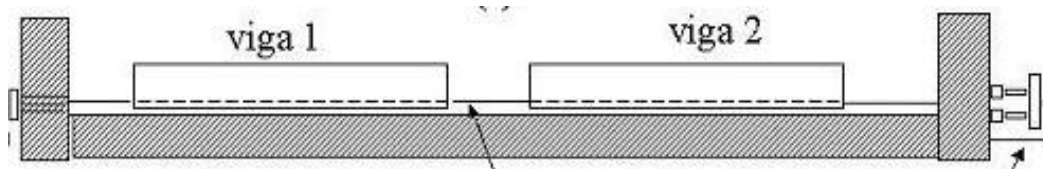
## Pre-tensioning



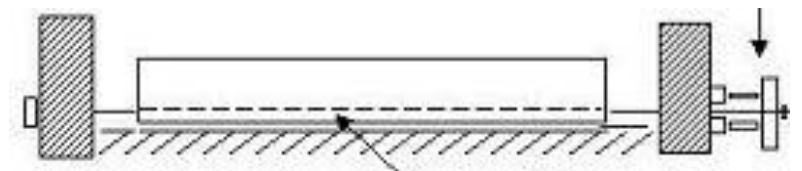
# Types of prestressing

## Pre-tensioning

Discontinuous



Continuous

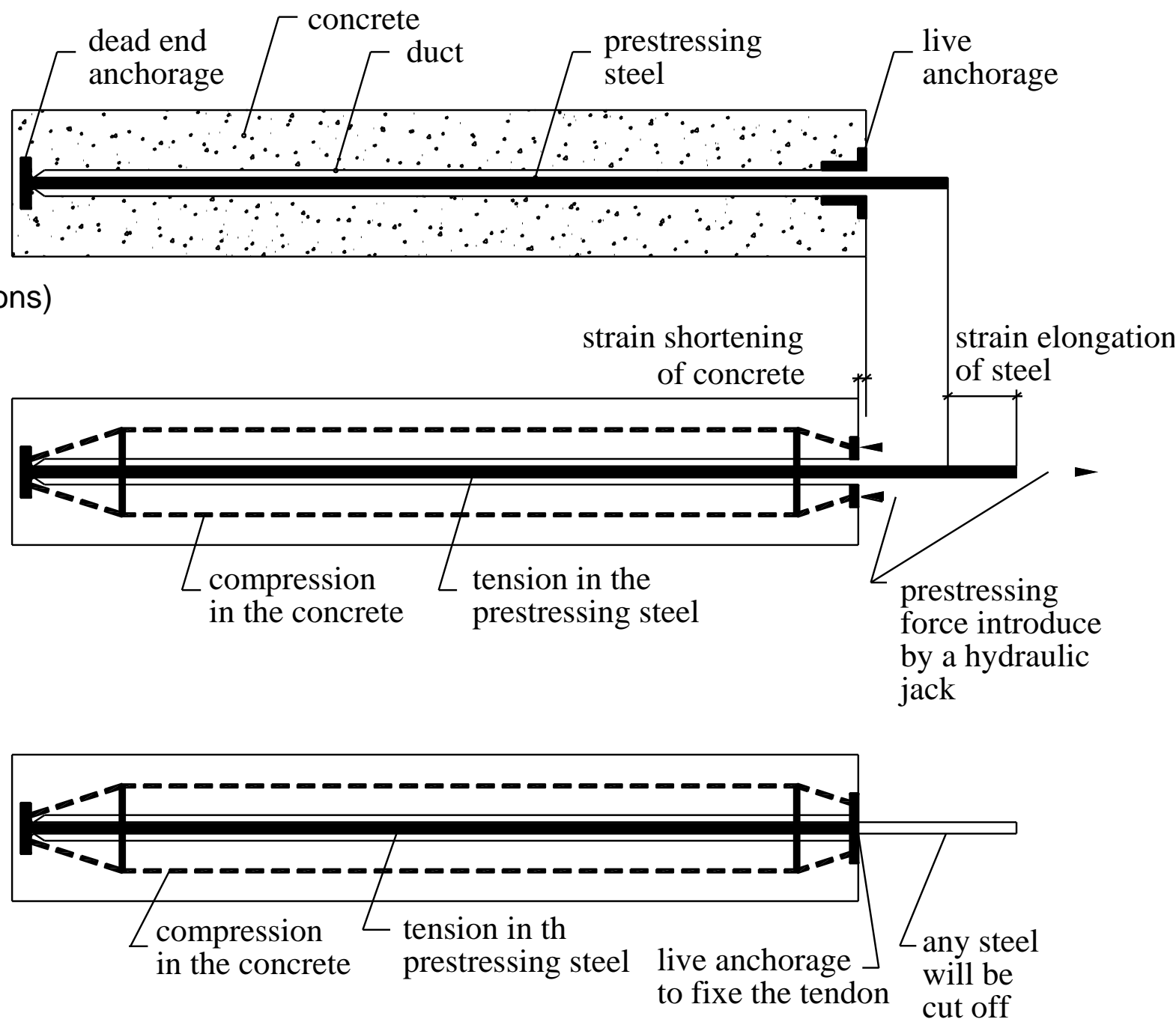


# Types of prestressing

## Post-tensioning

### Prestressing Process

- Concrete with the duct + anchorages (+ tendons)
- Curing and demoulding
- Tensioning





# Types of prestressing

## Post-tensioning

Tendon = prestressing steel (e.g. strands) + anchorages + duct + grout

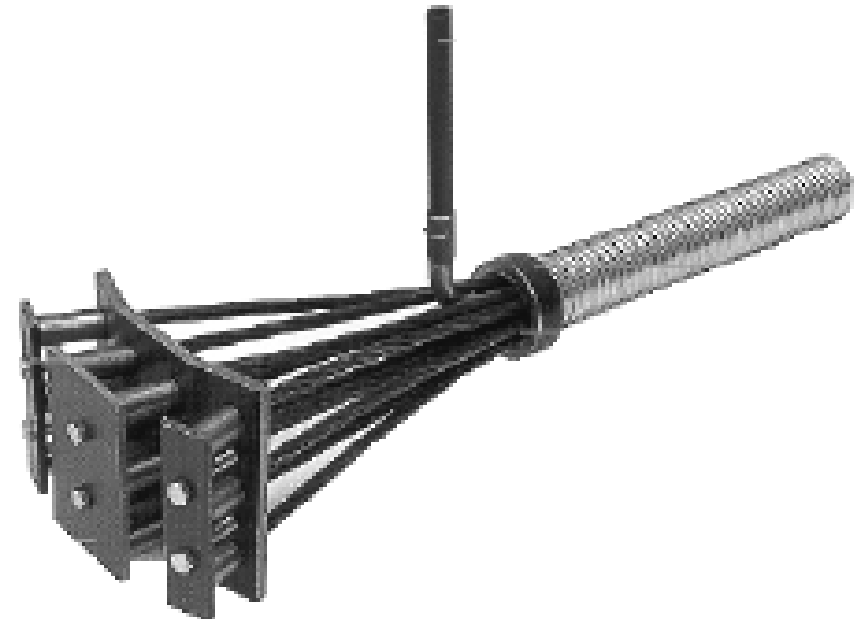
(câble = acier de précontrainte + têtes + gaine + coulis d'injection)



Live anchorage (tête mobile)



Dead end anchorage (tête fixe)

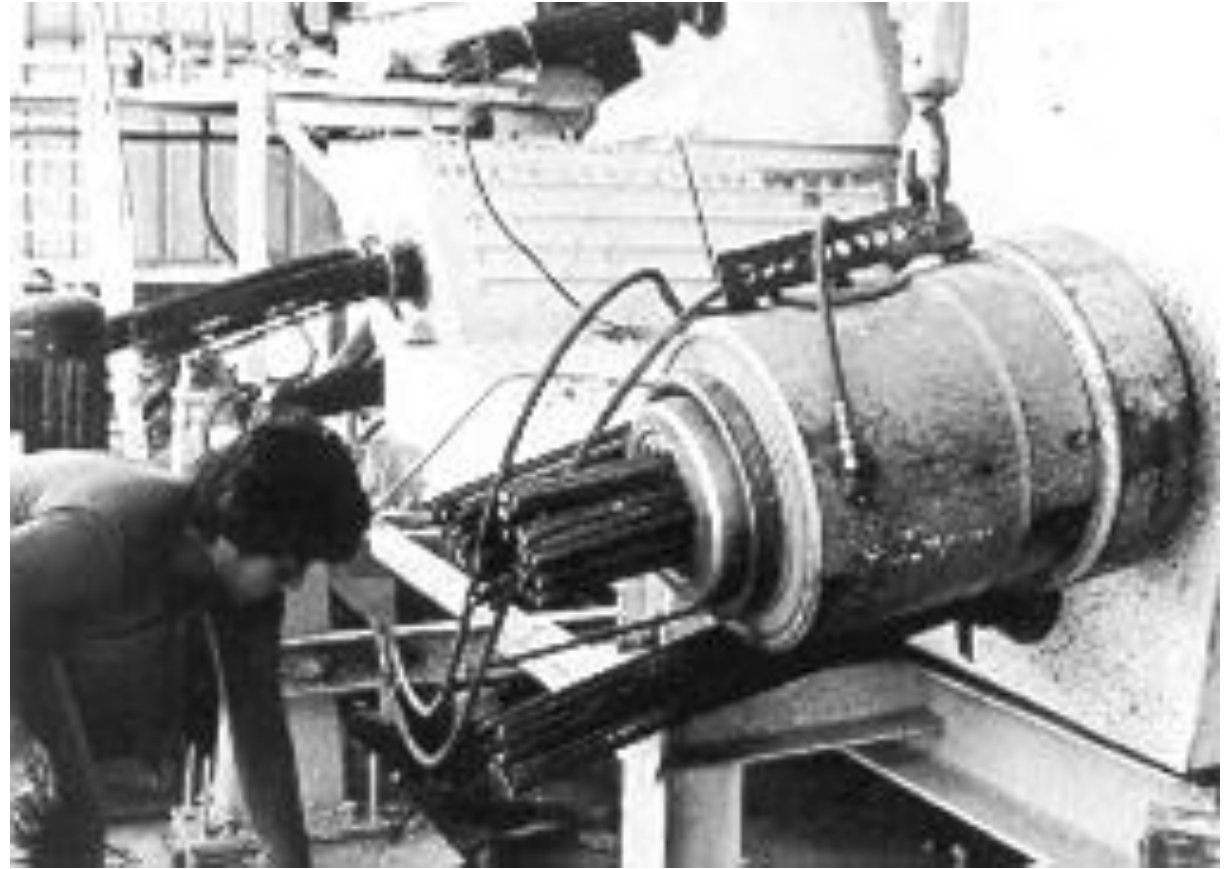




# Types of prestressing

## Post-tensioning

Jack



# Types of prestressing

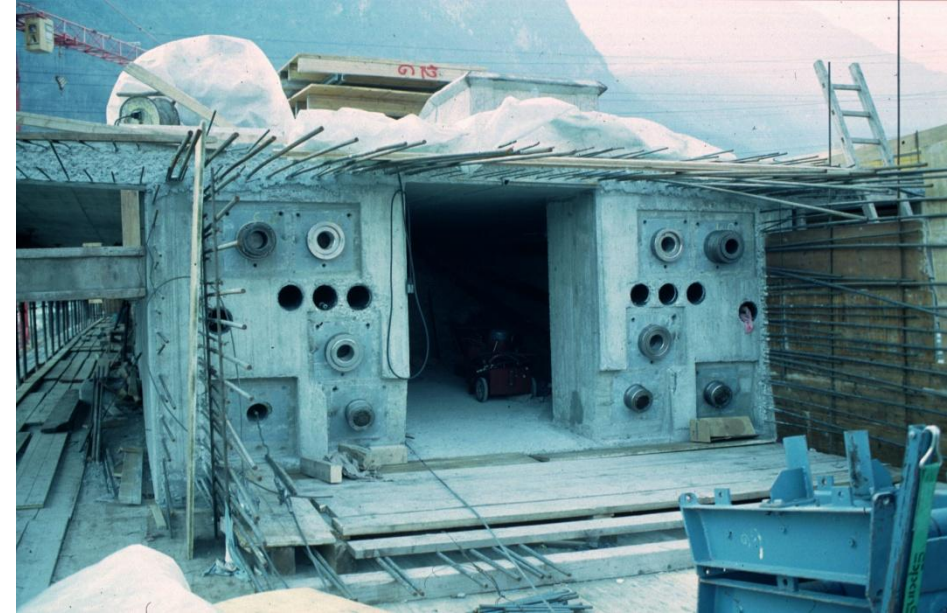
## Post-tensioning

Internal



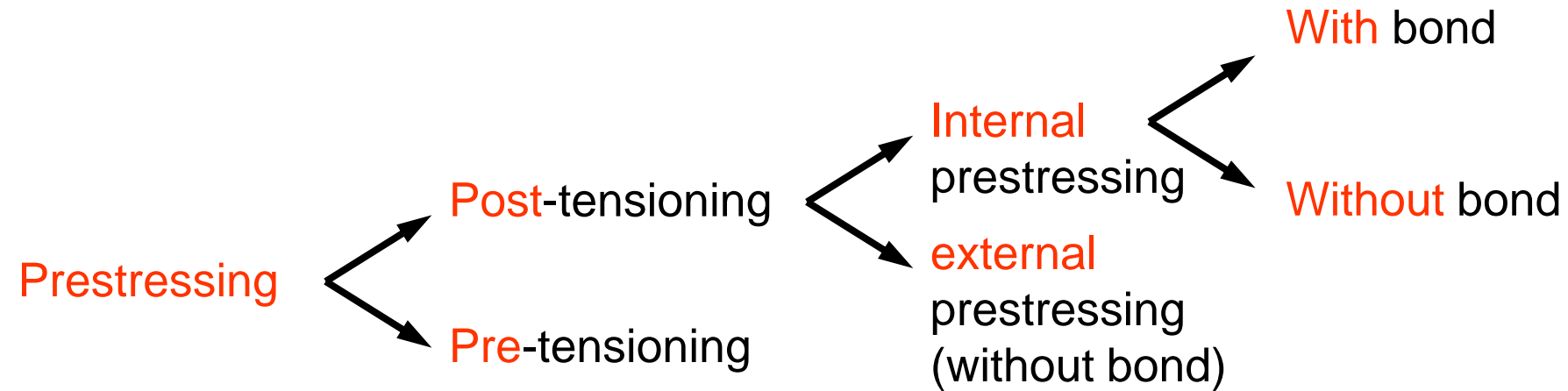
With or without bond

External



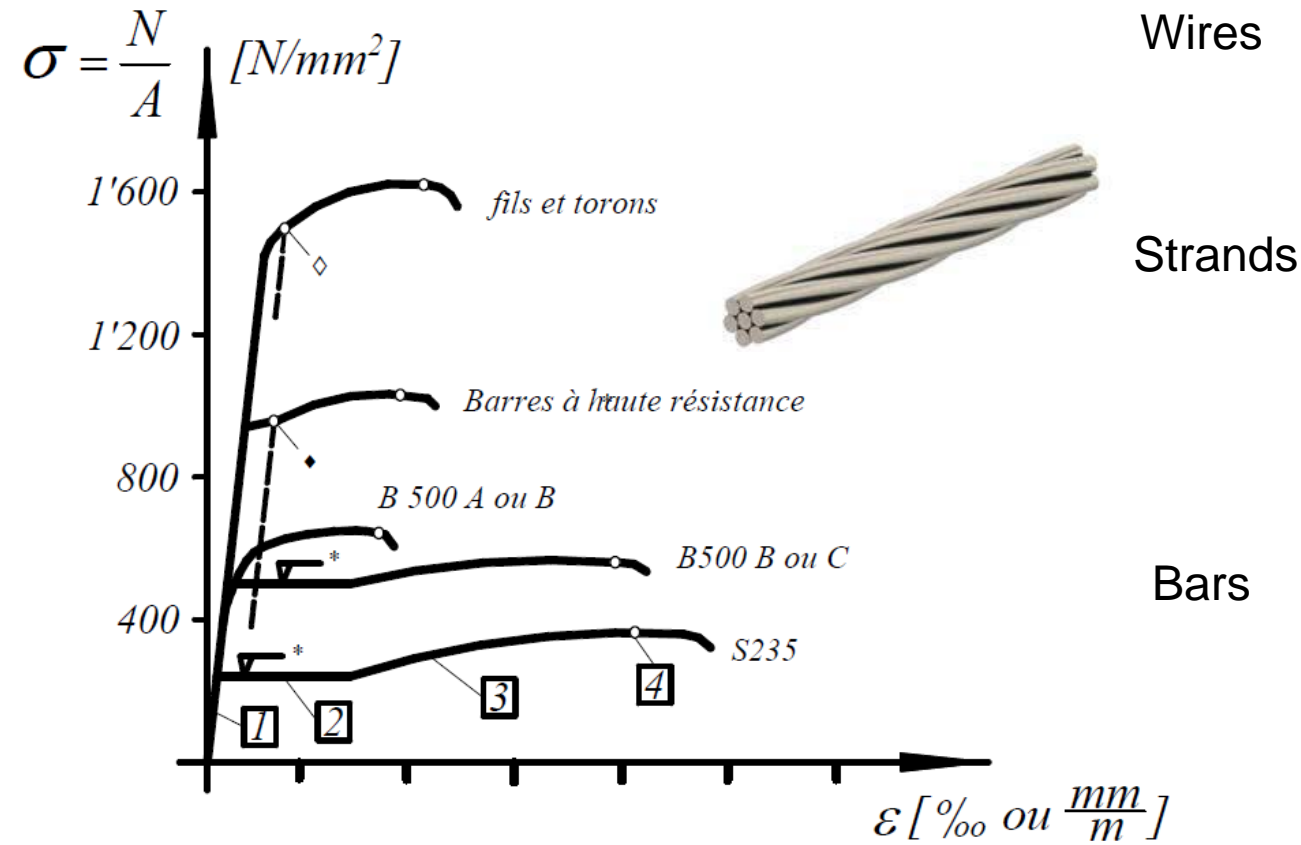
Without bond

# Types of prestressing





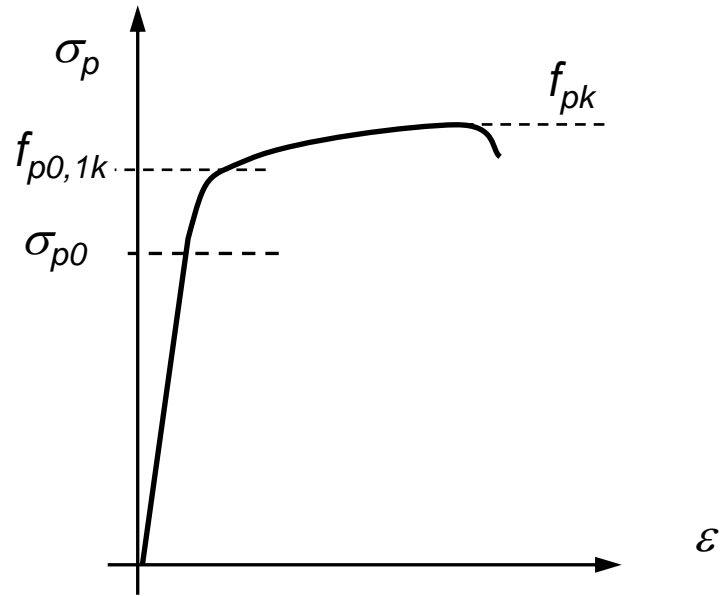
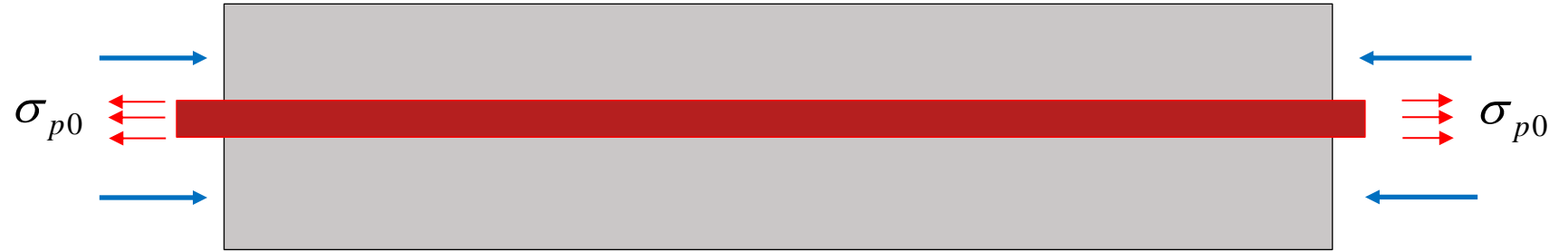
# Prestressing steel



Produit	Diamètre Ø [mm]	Section A <sub>p</sub> [mm <sup>2</sup> ]	Résistance à la traction f <sub>pk</sub> [N/mm <sup>2</sup> ]	Limite d'écoulement f <sub>p0,1k</sub> [N/mm <sup>2</sup> ]	Désignation
Fils	3,0	7,1	1860	1600	Y1860C-3,0
	4,0	12,6	1860	1600	Y1860C-4,0
	5,0	19,6	1860	1600	Y1860C-5,0
	6,0	28,3	1770	1520	Y1770C-6,0
	7,0	38,5	1670	1440	Y1670C-7,0
	8,0	50,3	1670	1440	Y1670C-8,0
	10,0	78,5	1570	1300	Y1570C-10,0
Torons	12,9	100	1860	1600	Y1860S7-12,9
	15,3	140	1770	1520	Y1770S7-15,3
	15,7	150	1770	1520	Y1770S7-15,7
			1860	1600	Y1860S7-15,7
Barres (lisses ou nervurées)	20,0	314	1100	900	Y1100H-20,0
	26,0	531	1030	830	Y1030H-26,0
			1050	950	Y1050H-26,0
			1230	1080	Y1230H-26,0
	26,5	552	1030	830	Y1030H-26,5
			1050	950	Y1050H-26,5
			1230	1080	Y1230H-26,5
	32,0	804	1030	830	Y1030H-32,0
			1050	950	Y1050H-32,0
			1230	1080	Y1230H-32,0
	36,0	1018	1030	830	Y1030H-36,0
			1050	950	Y1050H-36,0
			1230	1080	Y1230H-36,0

[SIA 262, 2013]

# Initial prestressing force



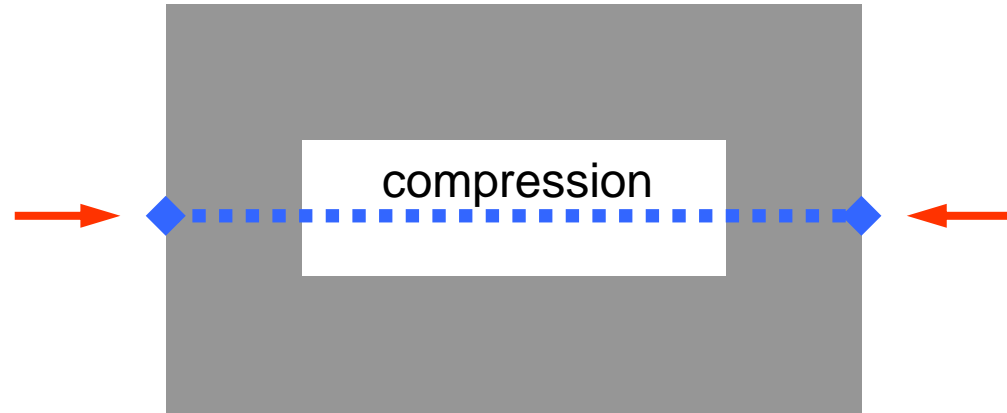
$$\sigma_{p0} \leq 0.70 \cdot f_{pk} \quad \text{After the initial prestressing force}$$

$$\sigma_{p0} \leq 0.75 \cdot f_{pk} \quad \text{During the initial prestressing force}$$

$$\sigma_{p\infty} \geq 0.45 \cdot f_{pk} \quad \text{at } t = \infty$$

# Approaches to considering prestressing

## Self-equilibrated **system** of **Forces** (prestressing considered as external action)



Forces exerted by the tendon on the concrete



Forces exerted by the concrete on the tendon

## Self-equilibrated **state** of **stresses** (prestressing considered on the side of the resistance)



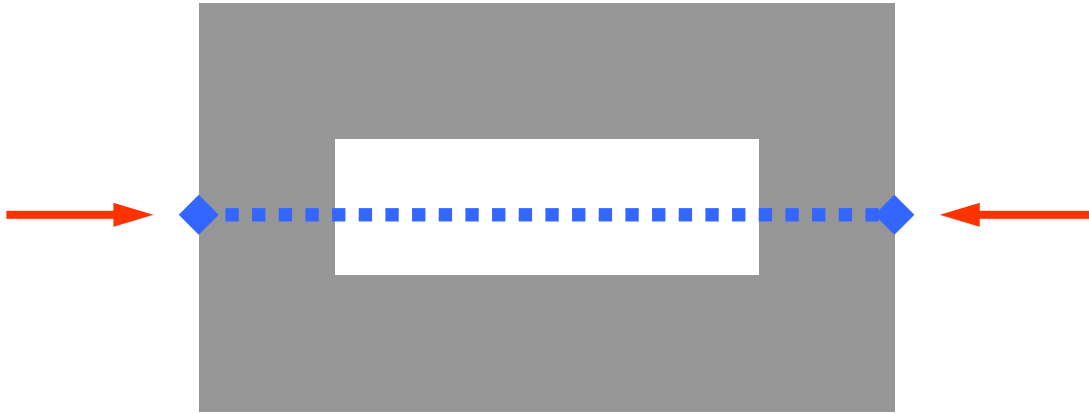
The system is composed by the concrete **with** the tendon. Prestressing induce internal forces et so deformation.



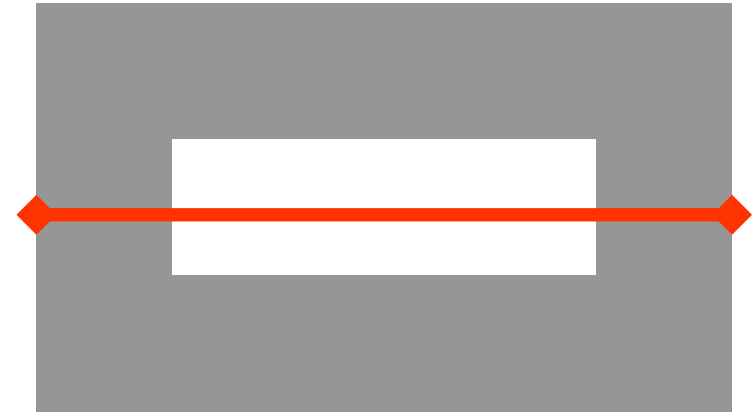
# Approaches to considering prestressing

## 1) Anchorage forces

Self-equilibrated **system** of **Forces**



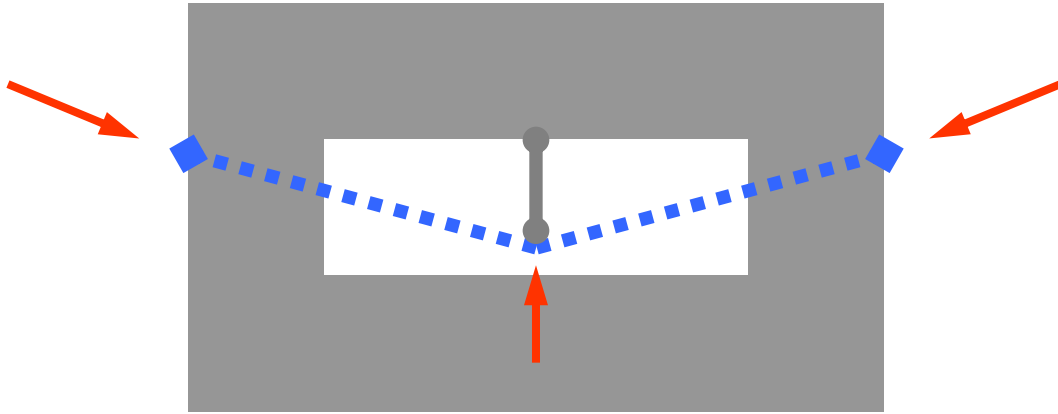
Self-equilibrated **state** of **stresses**



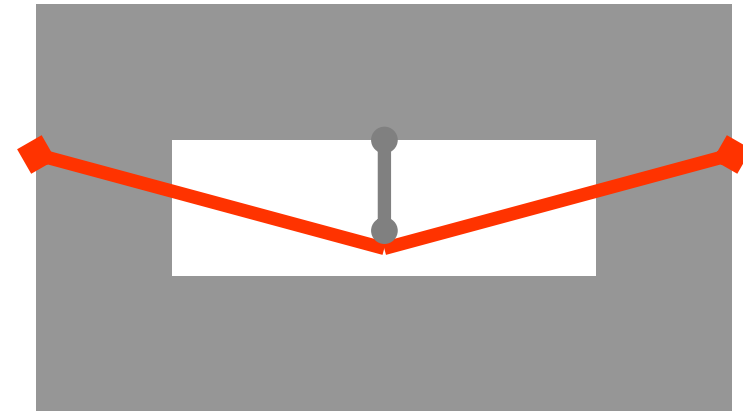
# Approaches to considering prestressing

## 2) Deviation forces

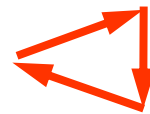
Self-equilibrated **system** of **Forces**



Self-equilibrated **state** of **stresses**



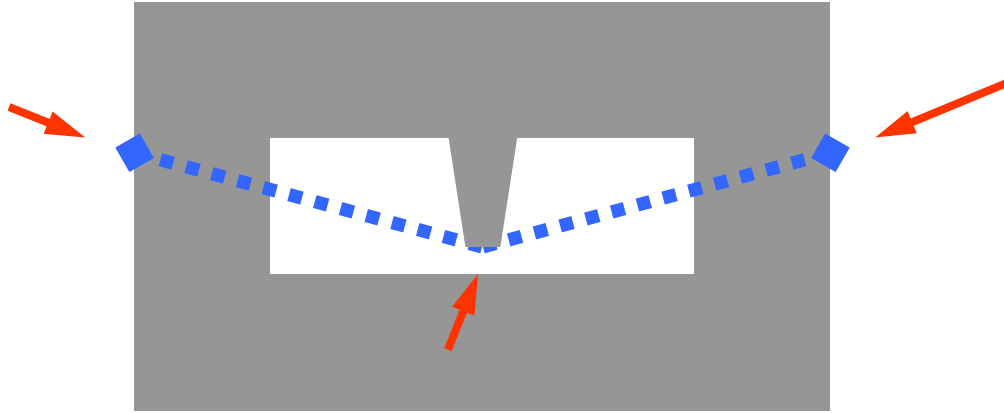
Deviation forces are in equilibrium with the anchorage forces



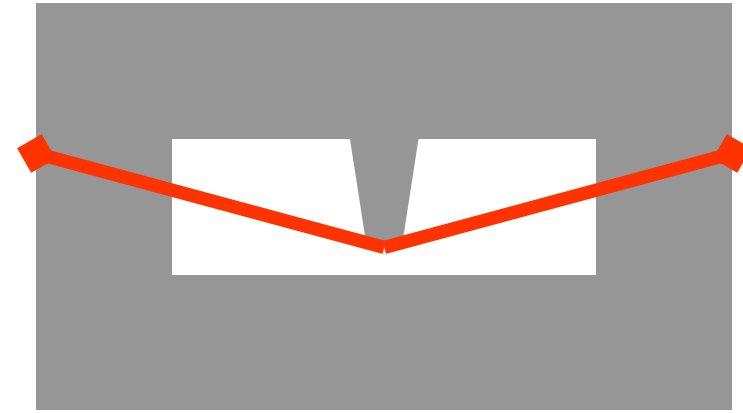
# Approaches to considering prestressing

## 3) Friction forces

Self-equilibrated **system** of **Forces**



Self-equilibrated **state** of **stresses**



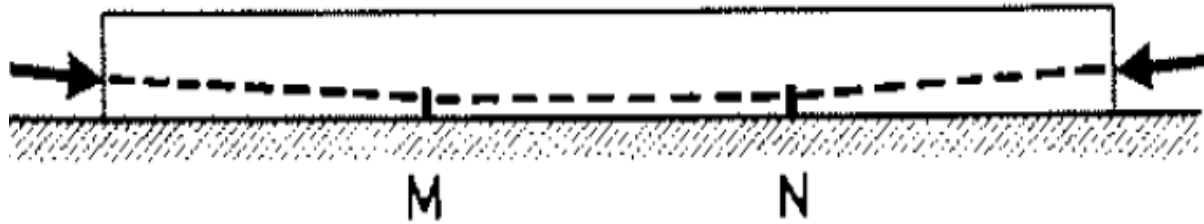
friction forces derive from a relative displacement between the tendon and the deviation element (when the tendon is tensioned for example)



# Prestressing tendon geometry

## Pre-tensioning

Deviators in intermediate cross sections (M y N) in the mould or the bench. They should resist vertical forces

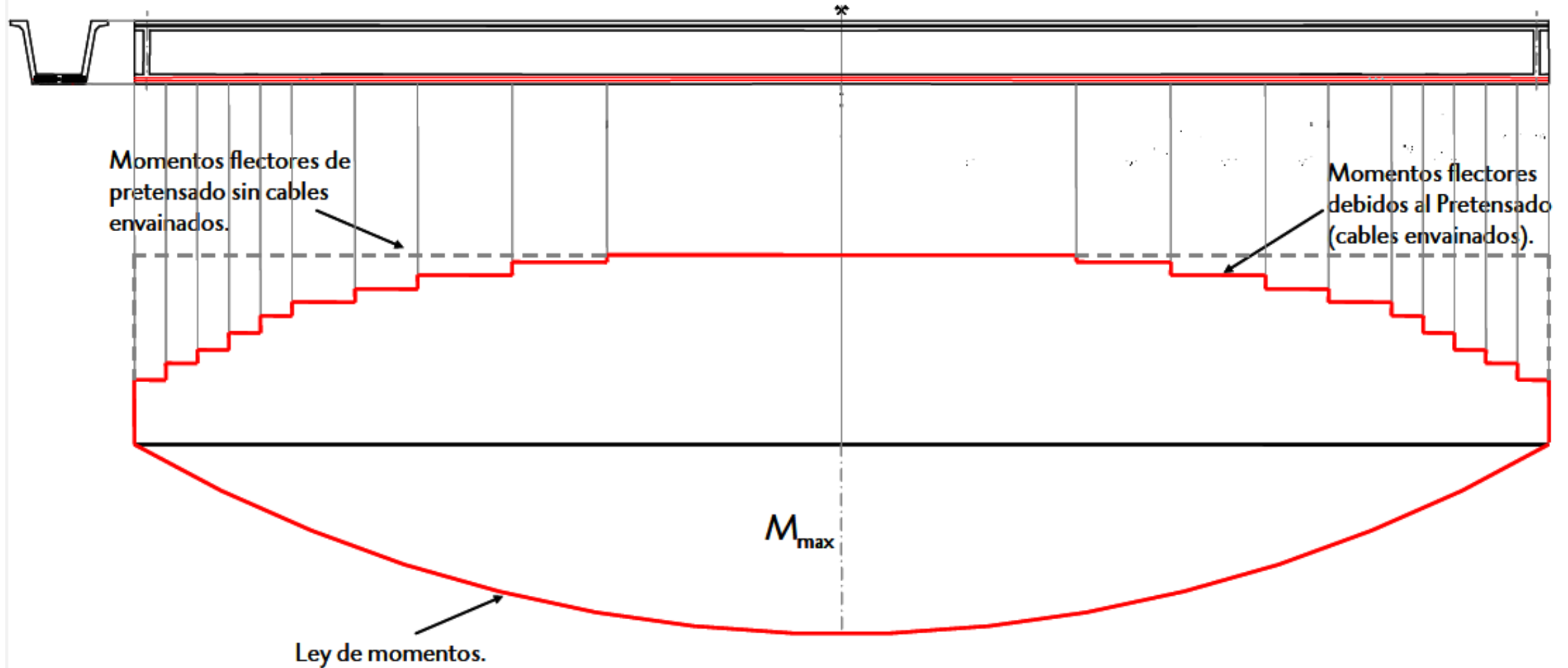


With several layers of **debonding** of strands



# Prestressing tendon geometry

## Pre-tensioning - Debonding



# Prestressing tendon geometry

## Pre-tensioning – Debonding : anchorage length

EN 1992-1-1:2004 (E)

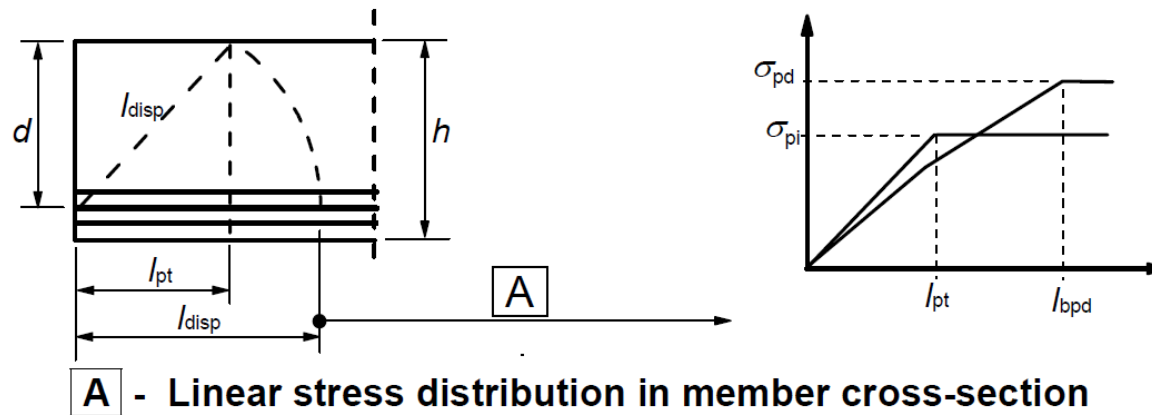
**Eurocode 2: Design of concrete structures -  
Part 1-1: General rules and rules for buildings**

### 8.10.2 Anchorage of pre-tensioned tendons

#### 8.10.2.1 General

(1) In anchorage regions for pre-tensioned tendons, the following length parameters should be considered, see Figure 8.16:

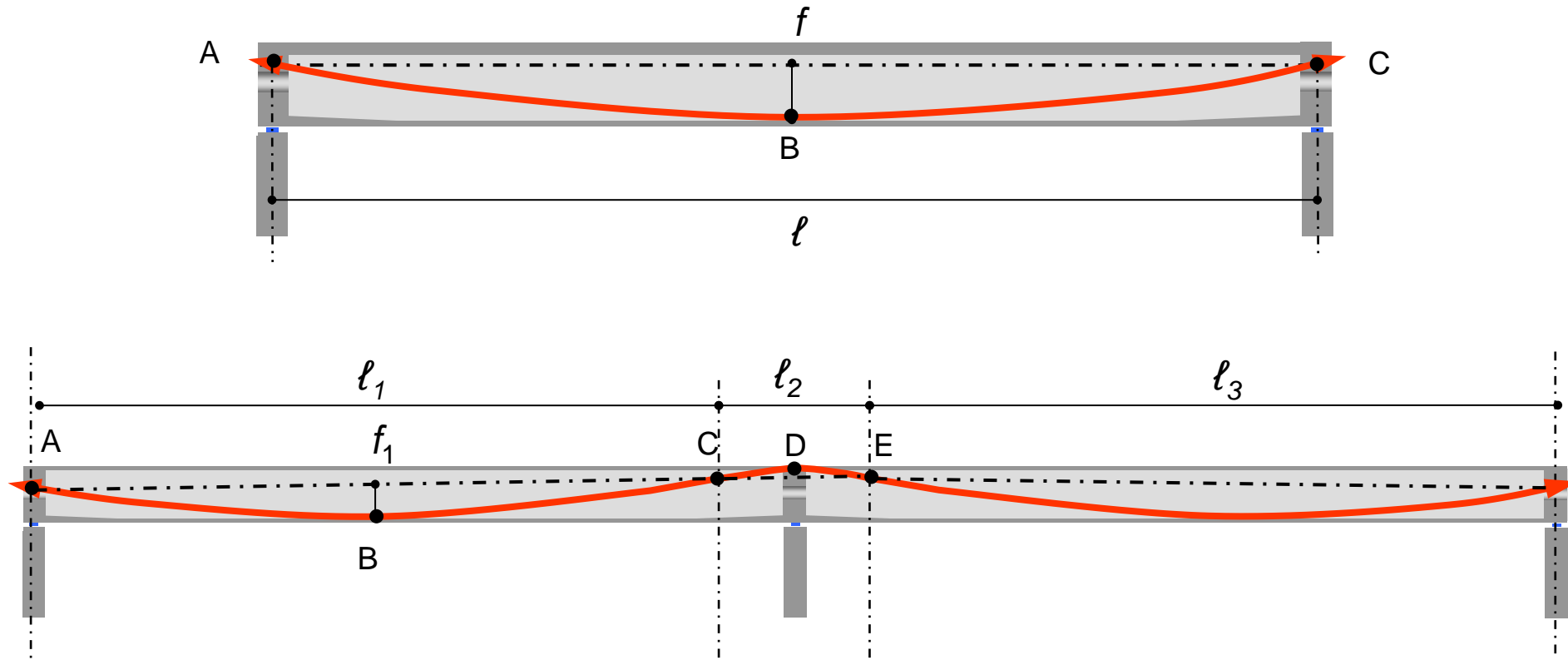
- Transmission length,  $l_{pt}$ , over which the prestressing force ( $P_0$ ) is fully transmitted to the concrete; see 8.10.2.2 (2),
- Dispersion length,  $l_{disp}$  over which the concrete stresses gradually disperse to a linear distribution across the concrete section; see 8.10.2.2 (4),
- Anchorage length,  $l_{bpd}$ , over which the tendon force  $F_{pd}$  in the ultimate limit state is fully anchored in the concrete; see 8.10.2.3 (4) and (5).



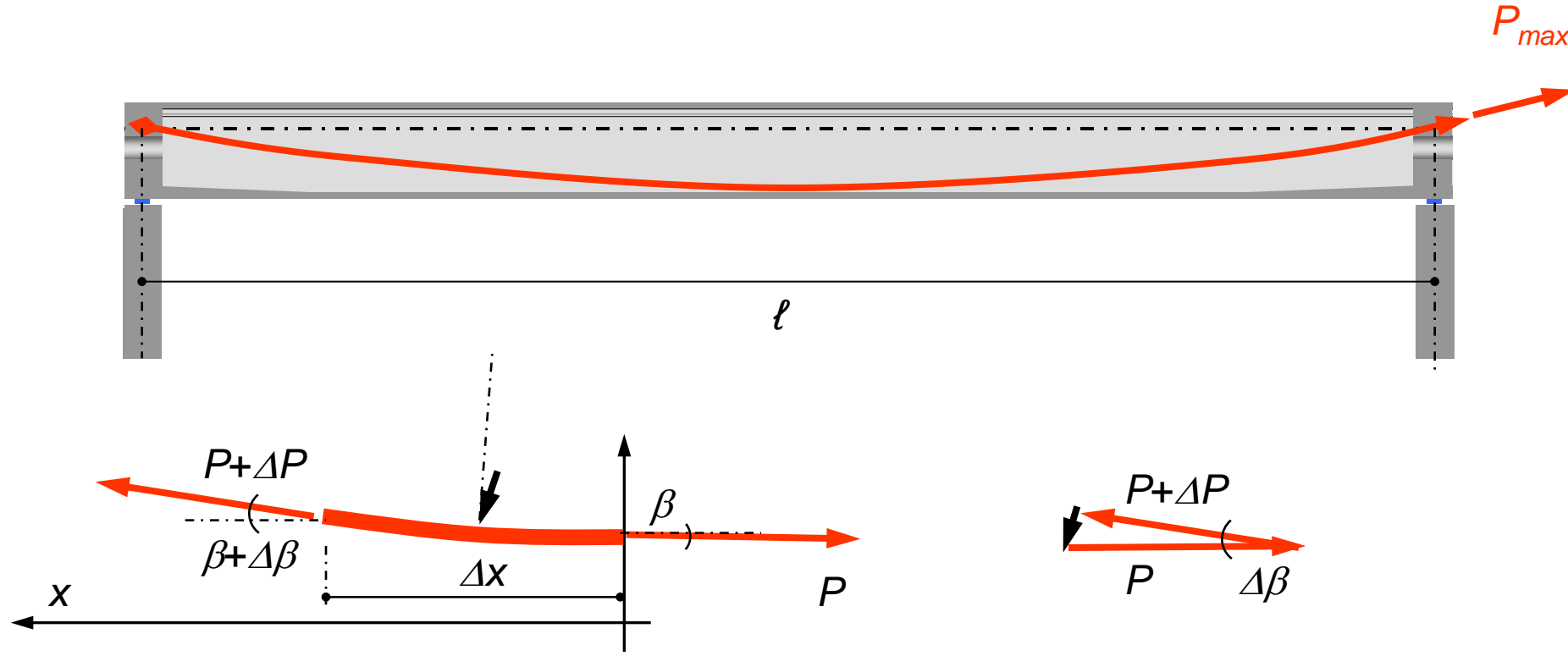
**Figure 8.16: Transfer of prestress in pretensioned elements; length parameters**

# Prestressing tendon geometry

## Post-tensioning



# Immediate losses of prestress : due to friction



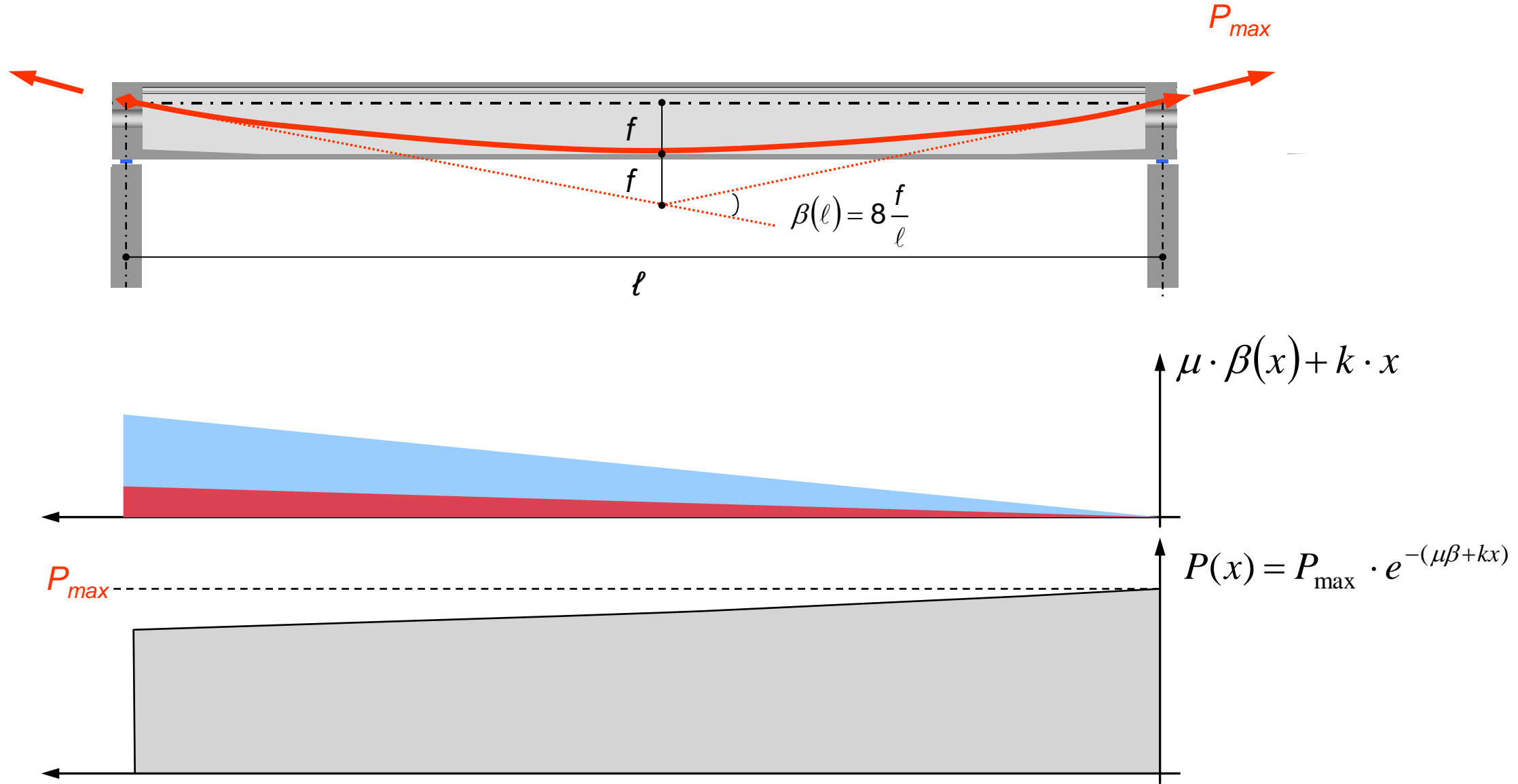
For example for strands

Duct type		
Metal	$\mu \approx 0.20$	$k \approx 0.0008 \text{ m}^{-1}$
Polymer (plastic)	$\mu \approx 0.14$	$k \approx 0.0010 \text{ m}^{-1}$

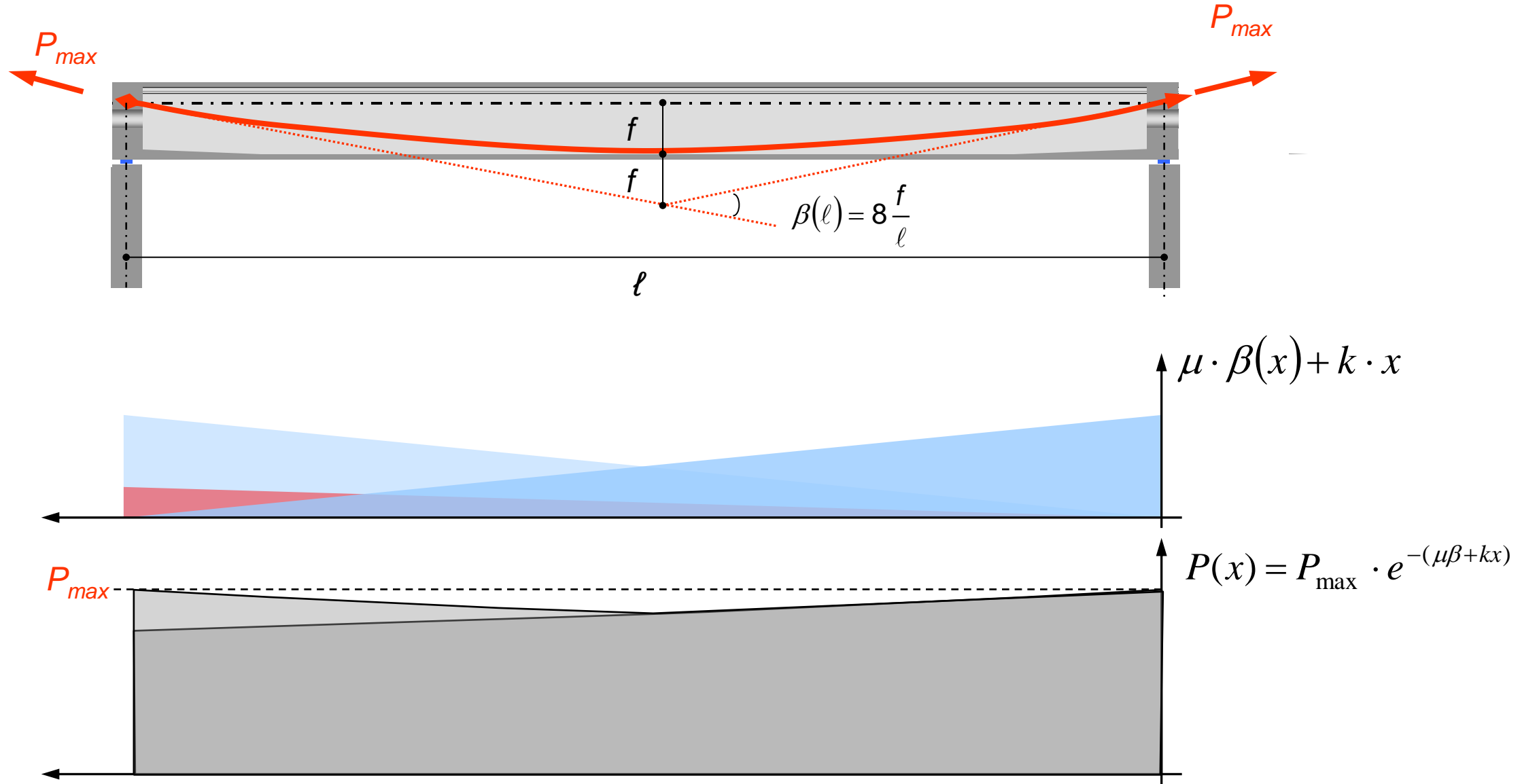
$$\Delta P = -P \cdot (\mu \cdot \Delta\beta + k \cdot \Delta x) \quad \longrightarrow \quad P(x) = P_{\max} \cdot e^{-(\mu\beta + kx)}$$



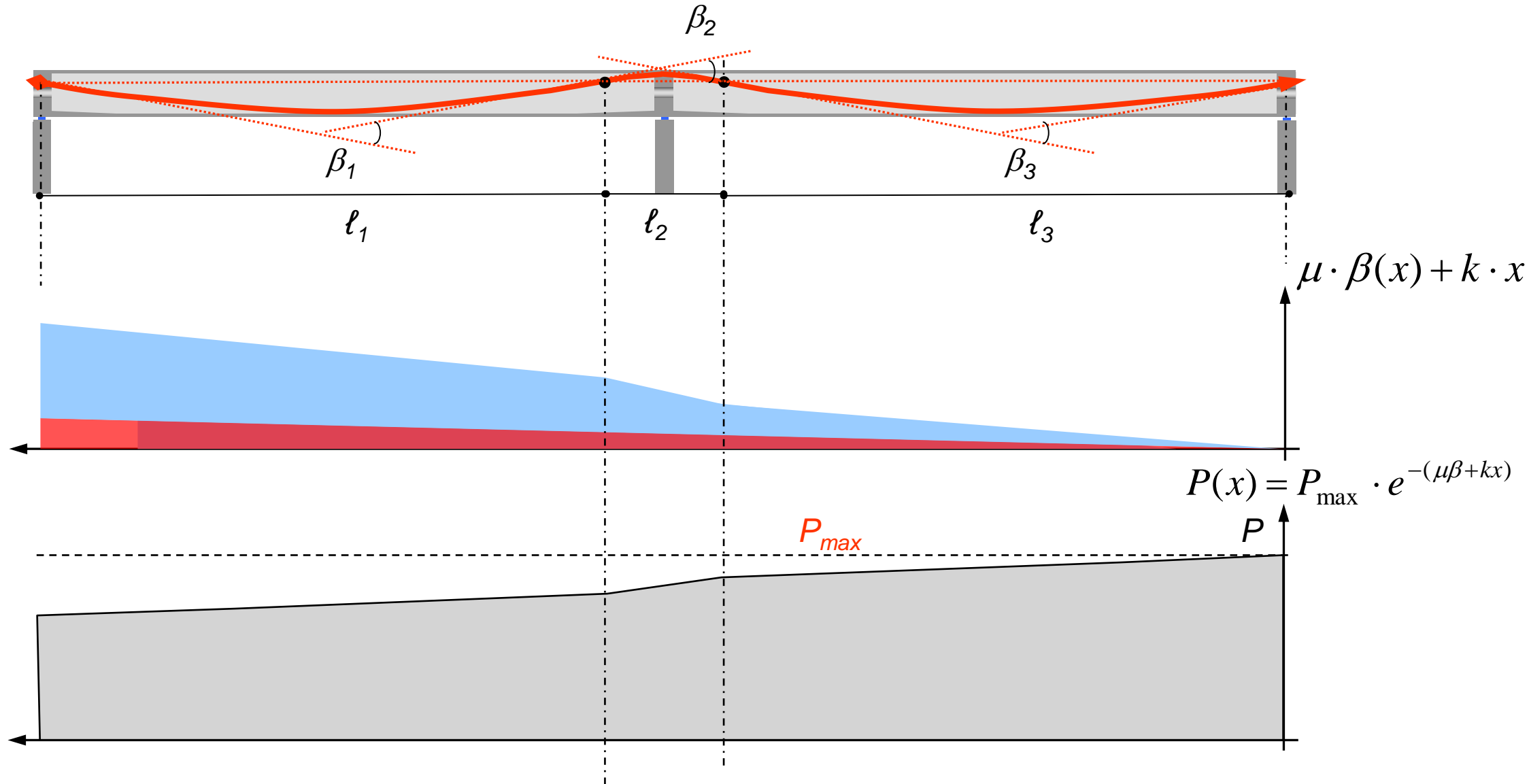
# Immediate losses of prestress : due to friction



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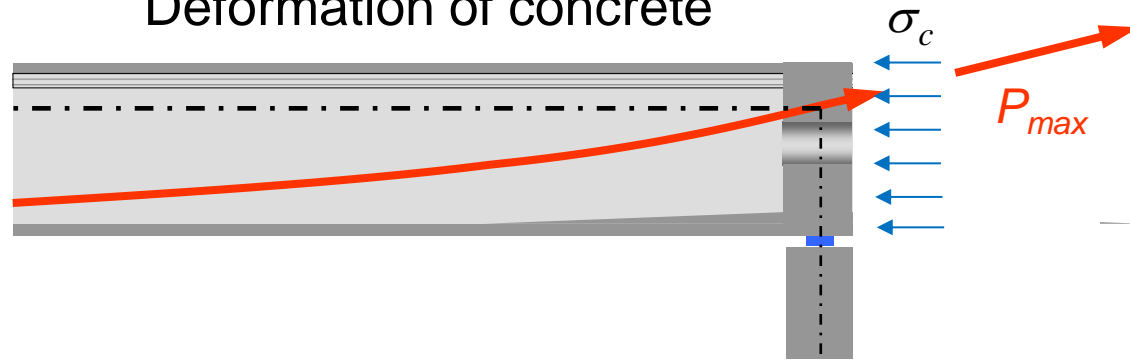


# Immediate losses of prestress : due to friction

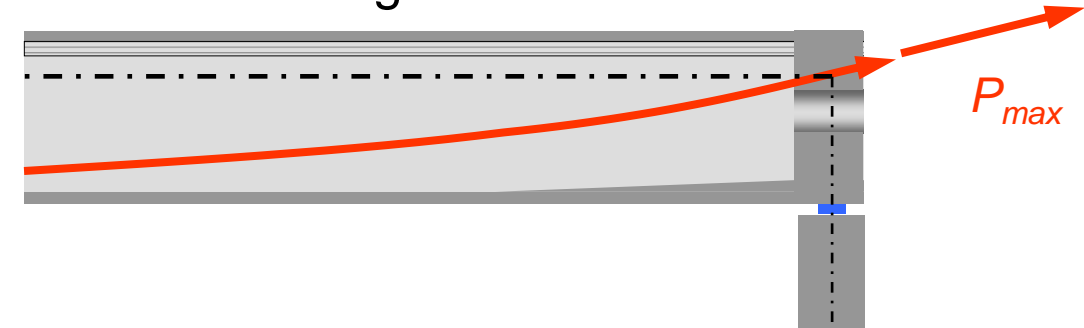


# Immediate losses of prestress : others

Deformation of concrete



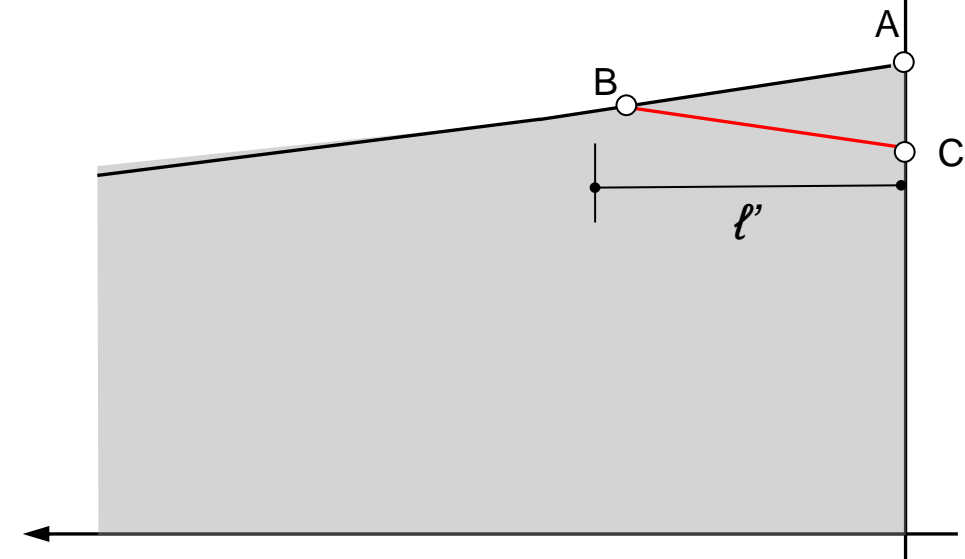
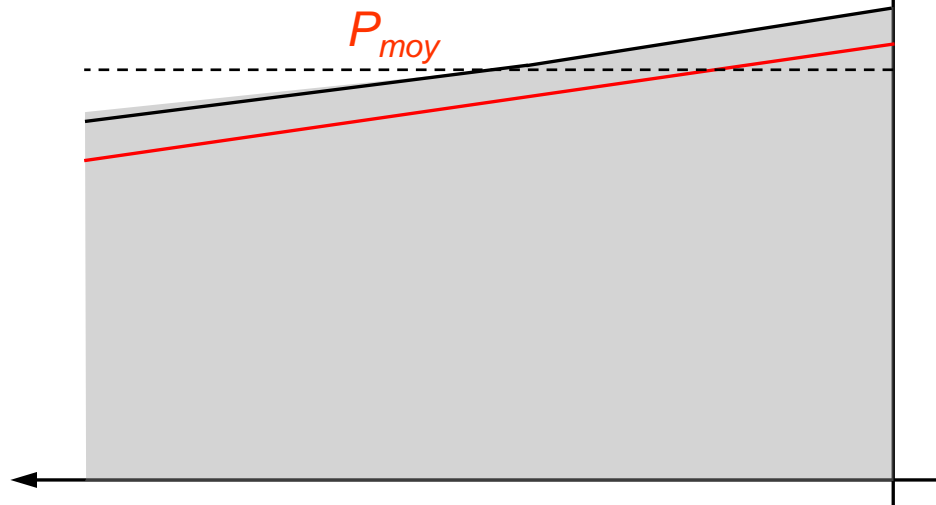
Wedge draw-in



$$\Delta\sigma_{p,el} = \varepsilon_{moy} \cdot E_p = \frac{\sigma_{cp}}{E_c} \cdot E_p = \frac{P_{moy}}{A_c \cdot E_{cm}} \cdot E_p$$

$$P(x) = P_{max} \cdot e^{-(\mu\beta + kx)}$$

$$\Delta\sigma_{p,el}$$



This loss can be neglected by

- Sequence of prestressing
- Larger prestressing stresses

$A_c$  : Cross sectional area of concrete

$E_c$  : modulus of elasticity of concrete

# Time dependant losses of prestress

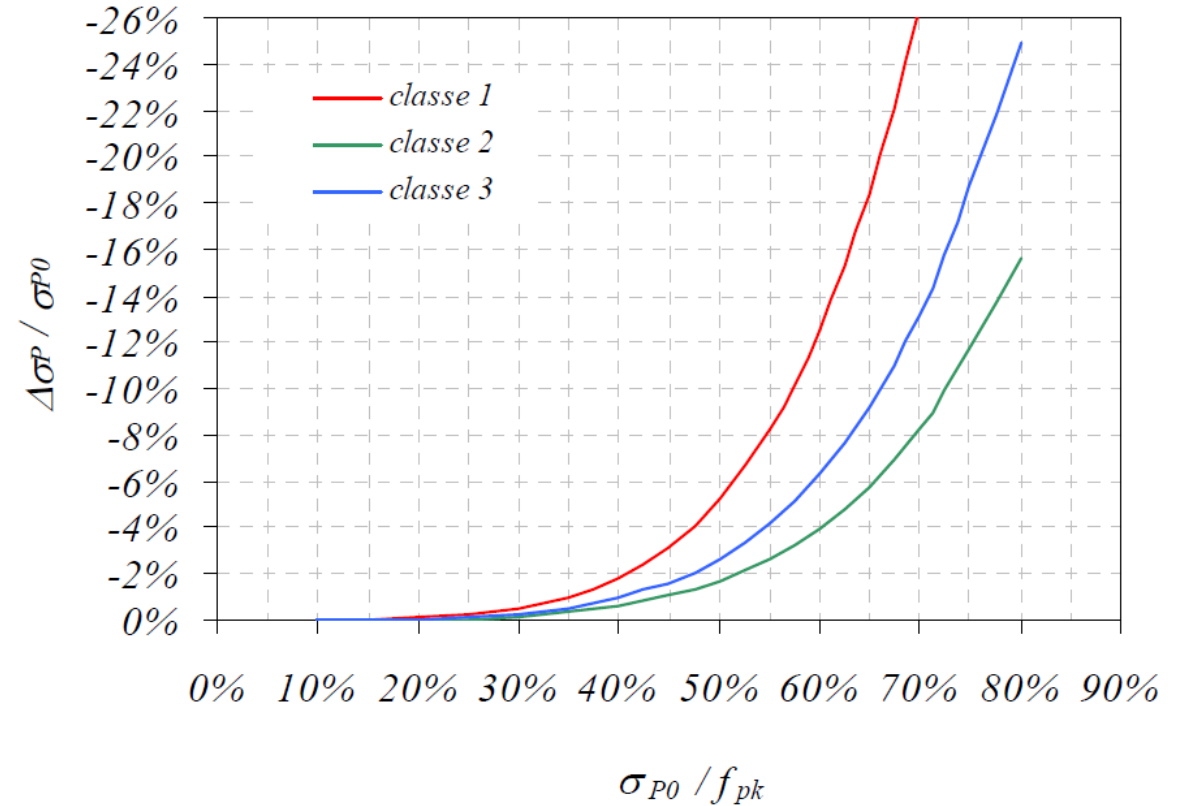
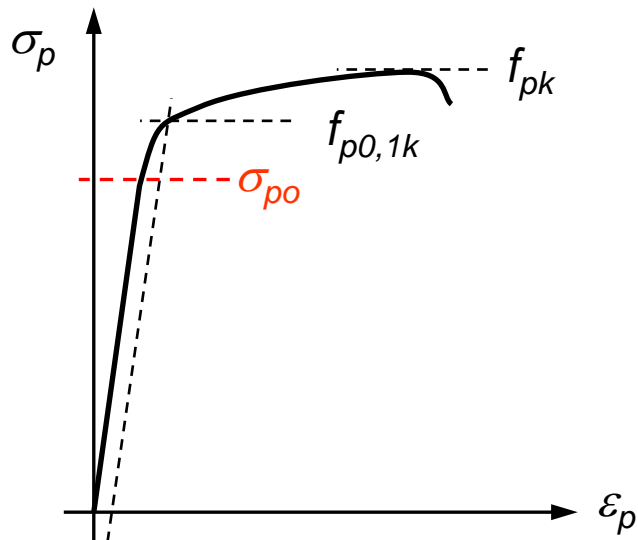
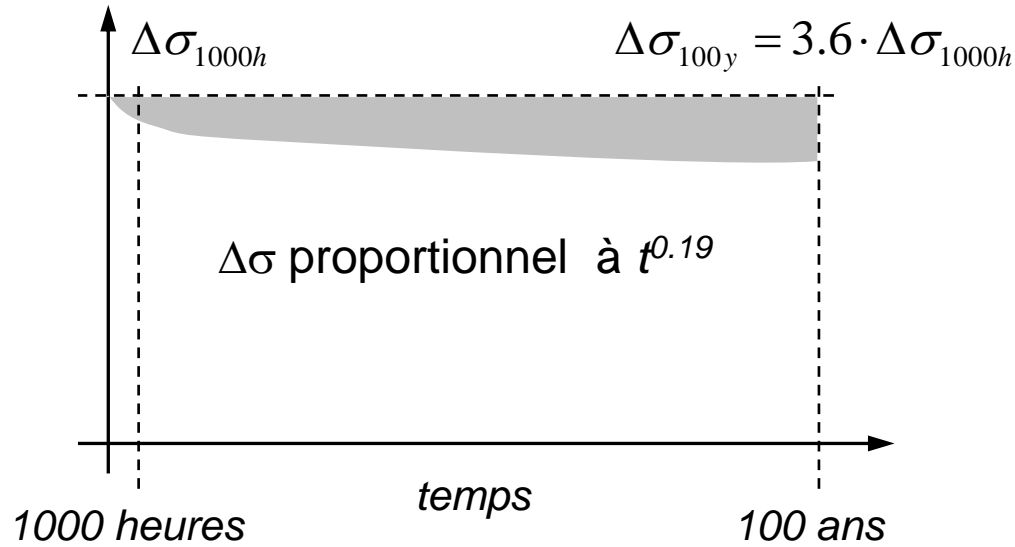
Losses of prestress due to

1. **relaxation** : reduction of stress at constant strain
2. **shrinkage** : concrete shortening over time
3. **creep** : concrete compressive stress in concrete causes elastic strain and an strain increment over time due to creep



# Time dependant losses of prestress

## Relaxation



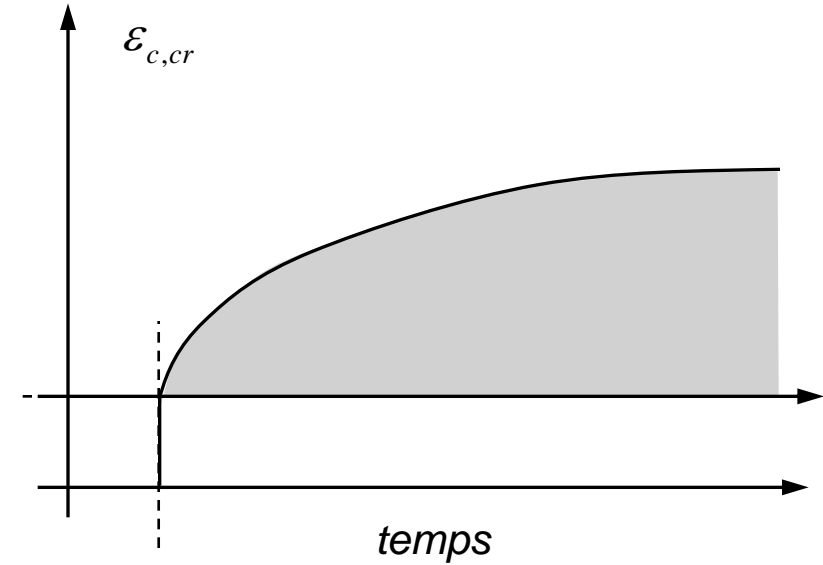
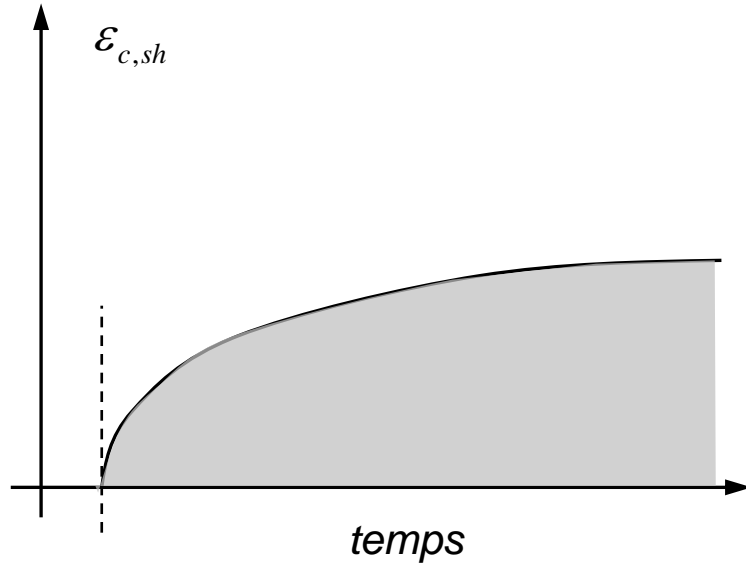
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# Time dependant losses of prestress

## Shrinkage and creep



$$\Delta P = -A_p \cdot E_p \cdot (\epsilon_{c,sh} + \epsilon_{c,cr})$$

# Time dependant losses of prestress

## Interaction between relaxation, shrinkage and creep

Without interaction

With interaction

*Simplified*

$$\begin{aligned}\Delta P &= -\rho(t, \sigma_{P0}) \cdot P_0 + A_p \cdot E_p \cdot (\varepsilon_{cs}(t) + \varepsilon_{cc}(t, t_0, \sigma_c)) \\ &= -\rho(t, \sigma_{P0}) \cdot P_0 + A_p \cdot E_p \cdot \left( \varepsilon_{cs}(t) + \frac{\sigma_c}{E_c} \cdot \phi(t, t_0) \right)\end{aligned}$$

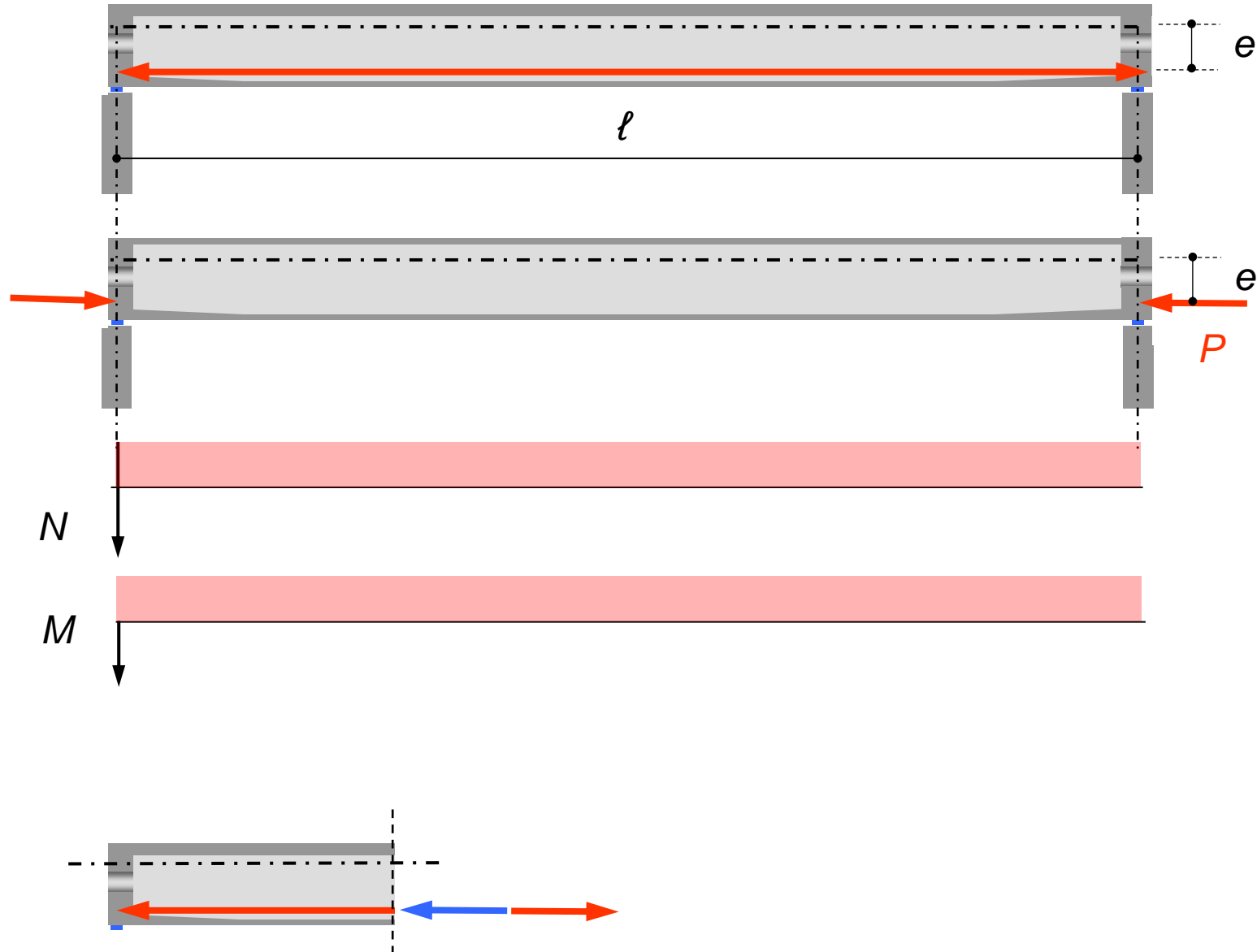
$$\Delta P = -0.8 \cdot \rho(t, \sigma_{P0}) \cdot P_0 + A_p \cdot E_p \cdot \left( \varepsilon_{cs}(t) + \frac{\sigma_c}{E_c} \cdot \phi(t, t_0) \right)$$

*EC 2004 Approached*

$$\Delta P = \frac{-0.8 \cdot \rho(t, \sigma_{P0}) \cdot P_0 + A_p \cdot E_p \cdot \left( \varepsilon_{cs}(t) + \frac{\sigma_c}{E_c} \cdot \phi(t, t_0) \right)}{1 + \frac{E_p}{E_c} \frac{A_p}{A_c} \left( 1 + \left( \frac{e}{i_c} \right)^2 \right) \cdot (1 + 0.8 \cdot \phi(t, t_0))}$$

# Isostatic example

## Simple supported beam with straight excentric tendon



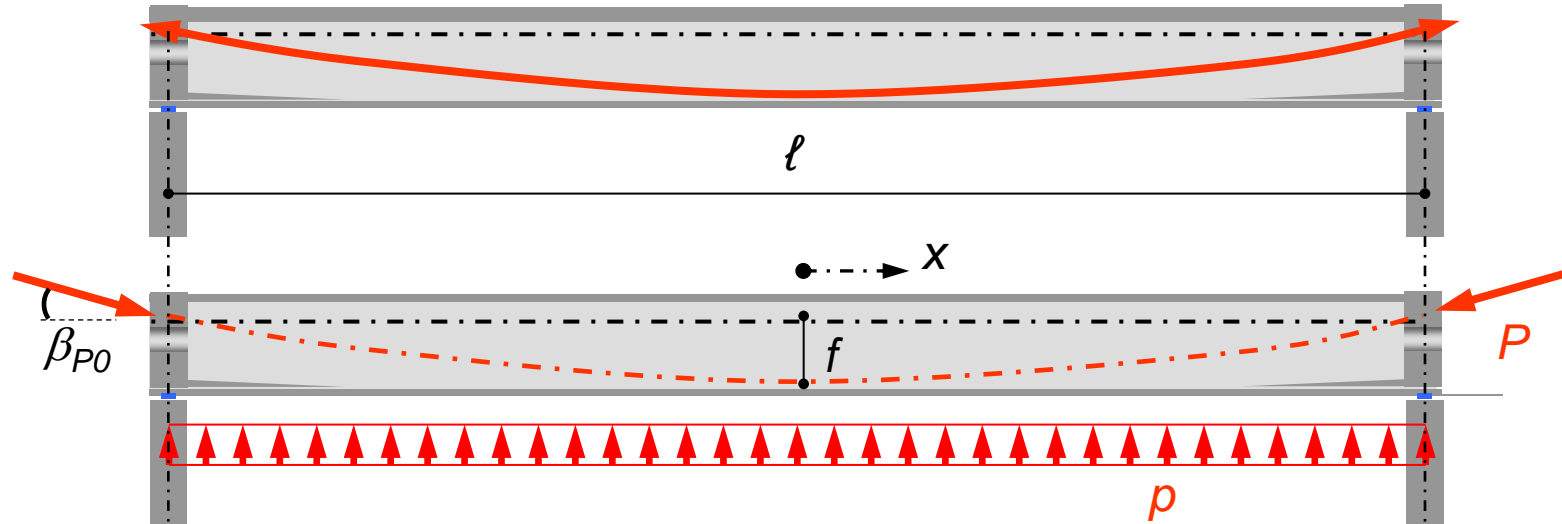
Approach :  
system of Forces

Approach :  
state of stresses

# Isostatic example

## Simple supported beam with parabolic tendon

Approach :  
system of Forces



Approach :  
state of stresses

