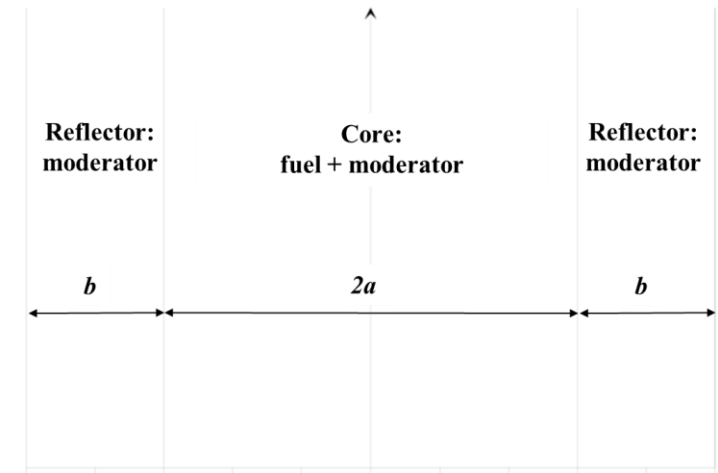


- Skip exercise
- #1 Two general questions: Maël
 1. Role of delayed neutrons during normal reactor operation and accidents. Comments on reactivity feedbacks during accidents
 2. Design of a PWR and its components
- #2 Two general questions: Filip
 1. Design of a Sodium Fast Reactor and its components
 2. Neutron slowing down via elastic scattering and implications for LWR reactors
- #3 Two general questions: Solène
 1. Breeding and transmutation in nuclear reactors
 2. Neutron balance equation and diffusion approximation

- Grading of the numerical exercises:
 - The instructor can run the scripts independently (3/6)
 - The quality of the script documentation (what each part/function is supposed to do) (2/6)
 - The script produces accurate results (answers to questions) (1/6)
- Open door policy for solving syntax issues (PH D3 465) until 23.1.2026
 - **No email!** Pass by...
 - Don't show up at 15h on the 23rd
- Final submission date for the script portfolio is 25/01/2026 at 23h59
 - **One** single zip file with naming convention #LastName_FinalAssignement.zip
 - 1 folder per exercise with **one** standalone script producing/saving only the requested output/plot
 - Script documentation should be provided within the script
 - **One** report including the 5 templates

- Using the 1D reactor model of a three batch core approach (Problem #4)
- Each assembly is 20cm wide, there are 4 fresh (ID 1), 4 once burned (ID 2) and 4 twice burned (ID 3) fuel assemblies
- The reflector assembly has the ID 4
- The loading pattern over a half space is [2 1 2 1 3 3 4]
 - $a = 120\text{ cm}$
 - $b = 10\text{ cm}$
- The reactor produces a constant power of 240 MW
- The homogenized fuel assembly has the following characteristics:
 - 264 fuel rods per assembly
 - Fuel rod is 400cm high
 - Outer pellet radius is 0.4cm
 - Fuel density (UO_2) is 10.4 gcm^{-3}
- The concentrations of Pu-239, U-235, U-238 and Y are tracked in every region of the core.
 - All isotopes are stable
 - All fissionable isotopes produce only Y with a FY of 2
 - The decay of U-239 into Pu-239 happens instantaneously



Initial Fuel Composition

| State | U-238 | U-235 | Pu-239 | Y |
|-----------------|----------|----------|----------|----------|
| Fresh (1) | 8.47E-03 | 2.62E-04 | 0.00E+00 | 0.00E+00 |
| Once Burnt (2) | 8.38E-03 | 1.39E-04 | 3.31E-05 | 3.31E-04 |
| Twice Burnt (3) | 8.28E-03 | 6.76E-05 | 4.15E-05 | 4.15E-04 |

- The microscopic XS are not affected by the change of composition in the medium
- The sets of 2G macroscopic XS are build from microscopic cross sections
 - The macroscopic scattering matrix are assumed fixed irrespective of the fuel composition.

| Macro XS Grp. ID | Reflector | |
|---------------------|-------------|-------------|
| | 1 | 2 |
| D | 1.20000E+00 | 4.00000E-01 |
| Σ_a | 1.00000E-03 | 2.00000E-02 |
| $\nu\Sigma_f$ | 0.00000E+00 | 0.00000E+00 |
| $\kappa\Sigma_f$ | 0.00000E+00 | 0.00000E+00 |
| Scattering Matrix | | |
| to grp | 1 | 2 |
| from 1 | 2.51780E-01 | 2.50000E-02 |
| from 2 | 0.00000E+00 | 8.13330E-01 |

Microscopic Cross Sections

| Isotope Grp. ID | U-238 | | U-235 | | Pu-239 | | Y | |
|--------------------|------------|------------|------------|------------|------------|------------|------------|------------|
| | 1 | 2 | 1 | 2 | 1 | 2 | 1 | 2 |
| Kappa | 3.3169E-11 | 3.3169E-11 | 3.2407E-11 | 3.2407E-11 | 3.3305E-11 | 3.3305E-11 | 0.0000E+00 | 0.0000E+00 |
| Nu | 2.8156E+00 | 2.4921E+00 | 2.4511E+00 | 2.4367E+00 | 2.8962E+00 | 2.8665E+00 | 0.0000E+00 | 0.0000E+00 |
| sig_f | 1.2620E-01 | 8.8950E-06 | 8.1513E+00 | 2.7936E+02 | 9.0170E+00 | 7.8388E+02 | 0.0000E+00 | 0.0000E+00 |
| sig_c | 7.2612E-01 | 1.4287E+00 | 3.8226E+00 | 4.9061E+01 | 5.2792E+00 | 4.3977E+02 | 0.0000E+00 | 7.0000E+01 |

Macroscopic Scattering Cross Sections

| to grp | 1 | 2 |
|--------|-----|------|
| from 1 | 0.4 | 0.02 |
| from 2 | 0.0 | 1.0 |

Algorithm:

- For each time step do:
 - Compute macroscopic cross sections for each mesh of the problem
 - Determine the matrix A , F
 - Determine k_{eff} and ϕ using power iterations
 - Normalize the flux level to the reactor power
 - For each spatial mesh
 - ✓ Setup the Bateman matrix A
 - ✓ Determine the isotopic composition for the next time step using the Matrix Exponential method
 - Go to the next time step

- Express the total macroscopic XS for a group g of a given spatial mesh i considering:

- Microscopic capture and fission XS
- Isotopic compositions
- Fixed macroscopic scattering matrix

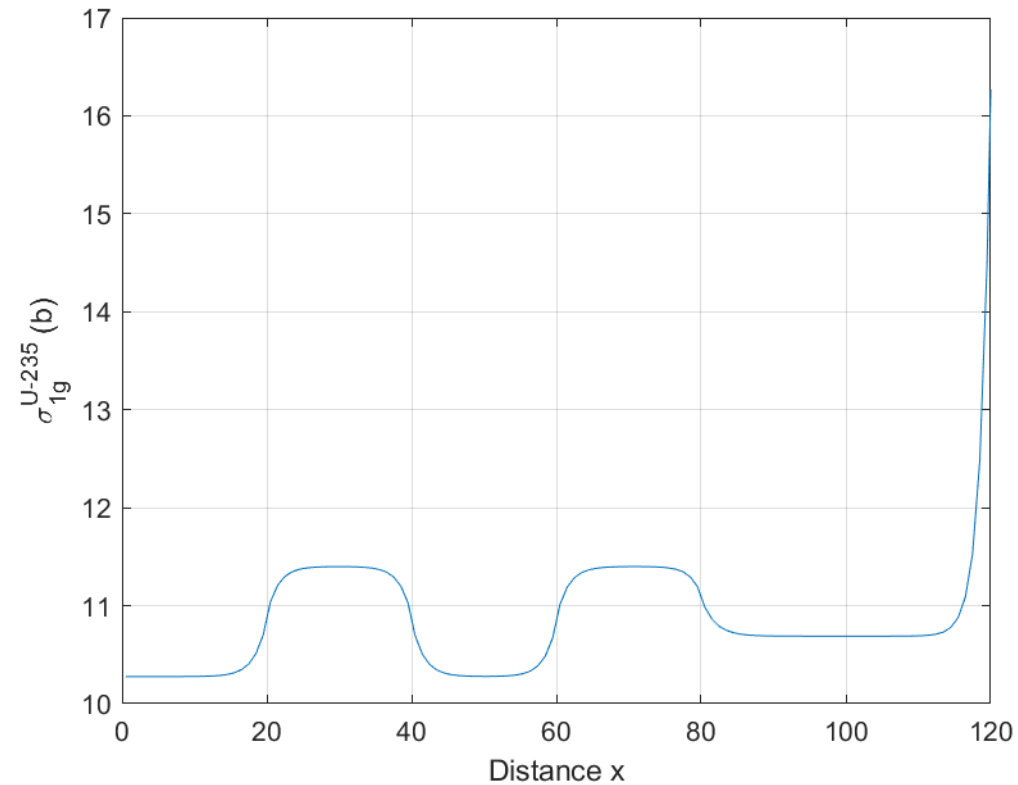
$$\Sigma_{t,i}^g = \sum_j \left(\sigma_{c,i}^g + \sigma_{f,i}^g \right) N_i^j + \sum_{g'} \Sigma_{s,i}^{gg'}$$

- Produce a table of 2G macroscopic XS for each assembly at the Beginning of Cycle

- Report D, sig_t, sig_a, sig_f, kappa sig_f, nu sig_f and the scattering matrix

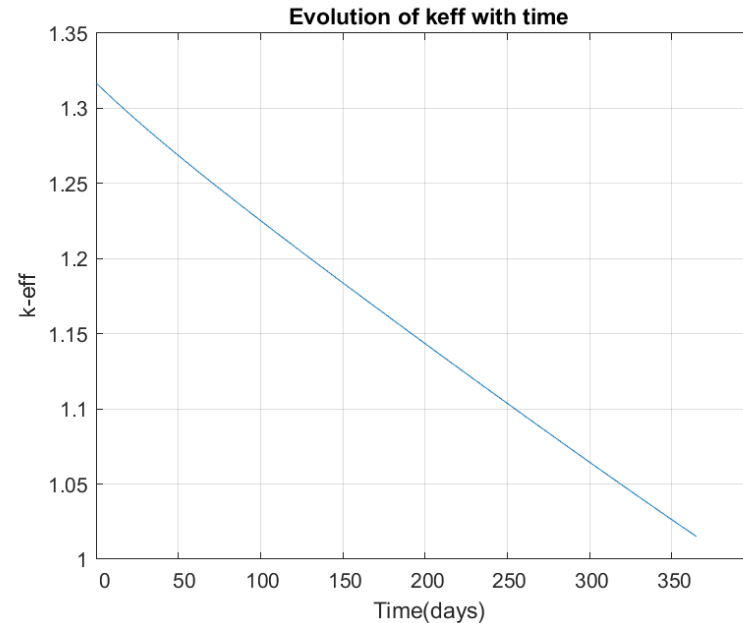
| Ass. ID | 1 | | 2 | | 3 | | 4 | |
|----------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Grp. ID | 1 | 2 | 1 | 2 | 1 | 2 | 1 | 2 |
| D | 7.74550E-01 | 3.03540E-01 | 7.76490E-01 | 2.97280E-01 | 7.77980E-01 | 2.99260E-01 | 1.20000E+00 | 4.00000E-01 |
| sig_t | 4.30360E-01 | 1.09810E+00 | 4.29280E-01 | 1.12130E+00 | 4.28460E-01 | 1.11390E+00 | 2.77780E-01 | 8.33330E-01 |
| sig_a | 1.03560E-02 | 9.81480E-02 | 9.28000E-03 | 1.21300E-01 | 8.46000E-03 | 1.13860E-01 | 1.00000E-03 | 2.00000E-02 |
| nusig_f | 8.24440E-03 | 1.78350E-01 | 6.61930E-03 | 1.69000E-01 | 5.37650E-03 | 1.39270E-01 | 0.00000E+00 | 0.00000E+00 |
| ksig_f | 1.04670E-13 | 2.37200E-12 | 8.17370E-14 | 2.12260E-12 | 6.49800E-14 | 1.69550E-12 | 0.00000E+00 | 0.00000E+00 |
| scat mat | | | | | | | | |
| to grp | 1 | 2 | 1 | 2 | 1 | 2 | 1 | 2 |
| from 1 | 4.00000E-01 | 2.00000E-02 | 4.00000E-01 | 2.00000E-02 | 4.00000E-01 | 2.00000E-02 | 2.51780E-01 | 2.50000E-02 |
| from 2 | 0.00000E+00 | 1.00000E+00 | 0.00000E+00 | 1.00000E+00 | 0.00000E+00 | 1.00000E+00 | 0.00000E+00 | 8.13330E-01 |

- Report the flux normalization factor at BOC (4 sig digs)
 - $4.3612e+13$
- Plot the 1group microscopic capture XS of U-235 vs position at BOC in the fuel assemblies



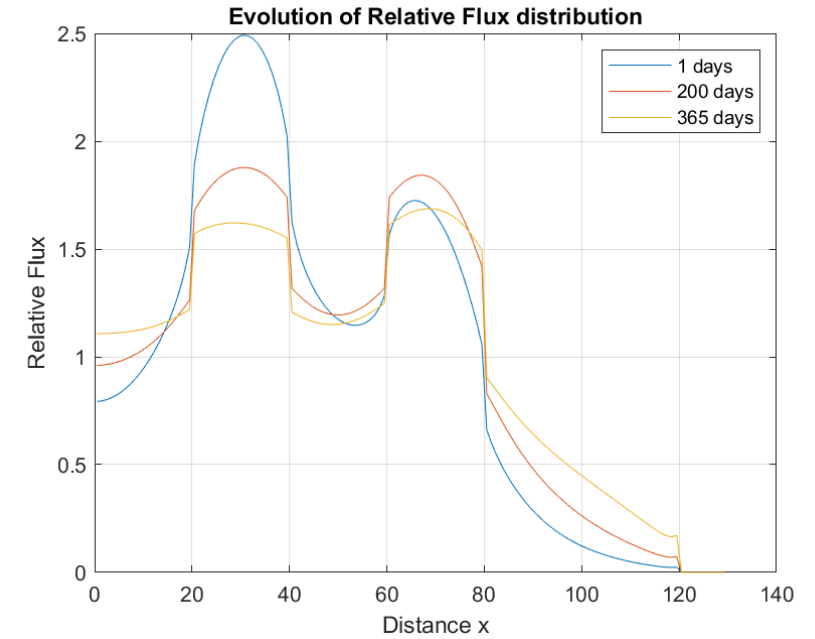
Solve the problem numerical using the matrix exponential method, a time step of 1 day. The spatial resolution for the core is 1cm. The cycle length is 365 days. The convergence criteria for k_{eff} is set to 10^{-6} . Predictor-corrector algorithm is not used initially.

- Plot k_{eff} as a function of time;



- Report the core exposure at EOC in MWd/kgU (initial heavy metal mass) as well as the initial U mass (in kg, 4 sig digs)
 - Initial U mass 3.3128×10^3 kg
 - Burnup at EOC 13.2213 MWd/kgU

- Plot the spatial distribution of the relative power after 1day, 200 days and 365 days.



- Plot the spatial distribution of U-235, Pu-239 and Y after 1day, 200 days and 365 days.

