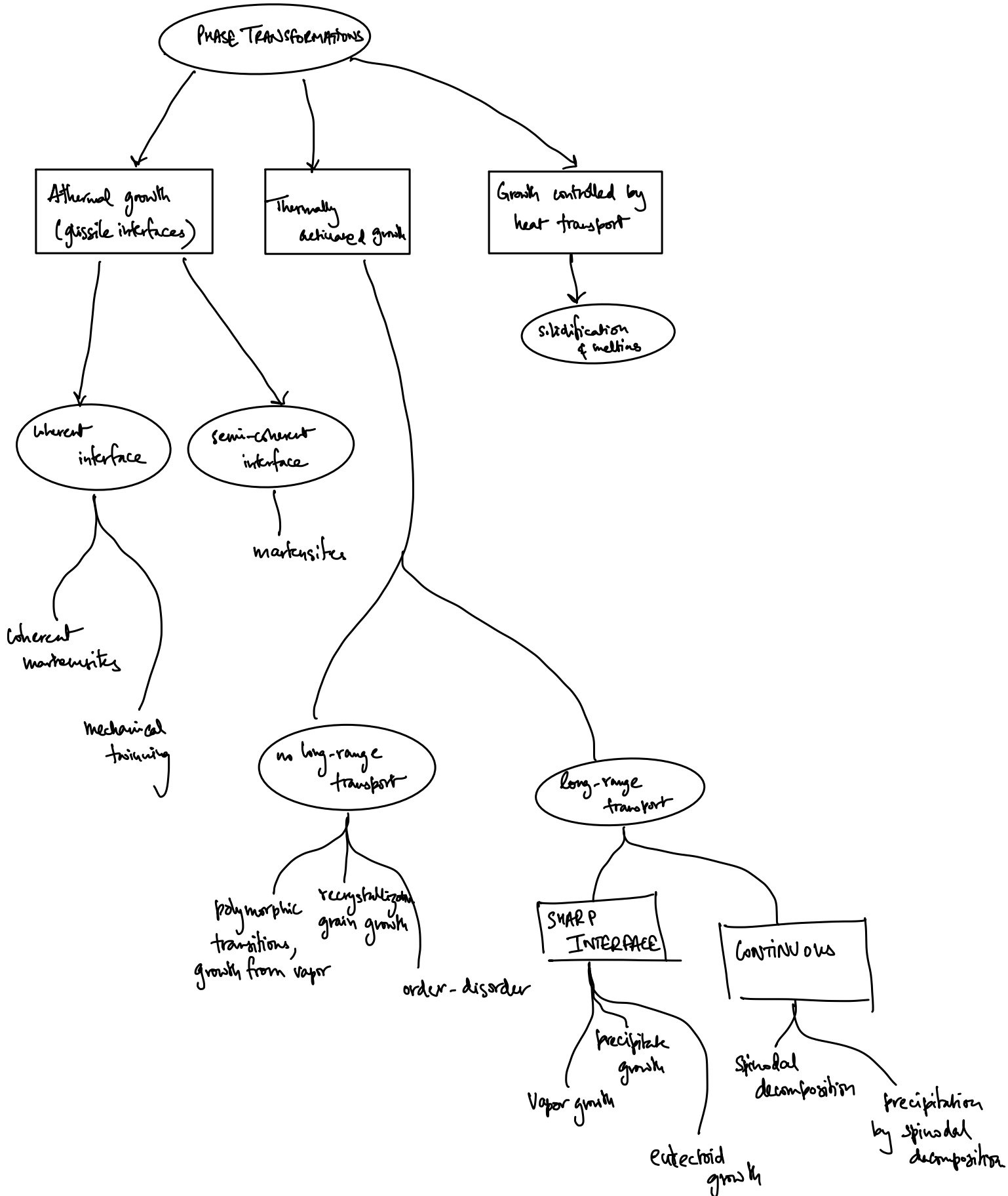


PHASE TRANSFORMATIONS:

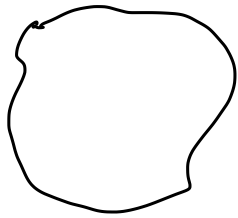
- phase transformations in the solid state (involving crystalline solids)
 - * metals (alloys)
 - * ceramics, oxides, battery materials
 - * compound semiconductors, thermoelectrics, memory devices.

- An attempt @ classification



* Consider the following experiments:

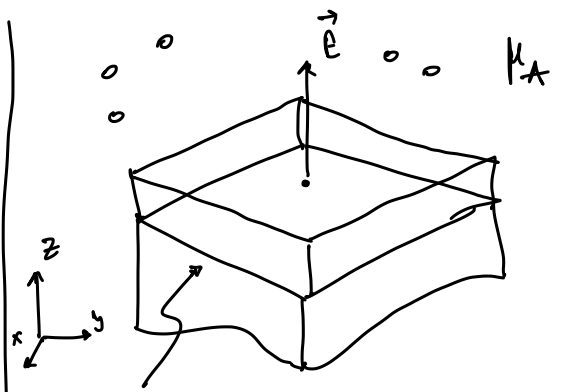
$T, p = \text{constant}$



how do we determine which phase is stable?

→ minimize Gibbs free energy wrt internal degrees of freedom (i.e. various possible crystal structures/phases)

$$G = U - TS + pV$$



epitaxially constrained.

experimentally you are controlling

$$\underline{T, \vec{E}, \epsilon_{xx}, \epsilon_{yy}, \epsilon_{xy}, \sigma_{zz}, \mu_A}$$

→ how do we determine which phase is stable?

→ minimize what?

$G?$ $F?$...

→ if the epitaxial film undergoes a phase transformation, how much heat is exchanged with the environment?

* FIRST PART OF THE COURSE:

Develop the thermodynamic tools to analyze arbitrarily complex boundary conditions.

THERMODYNAMICS:

What is thermodynamics?

Macroscopic framework of energy flows, and how they affect the properties of the system

— Macroscopic theory → no atomic scale information

— deals only with macroscopic variables

(eg) Volume (V)
pressure (P)

— temperature (T) ...

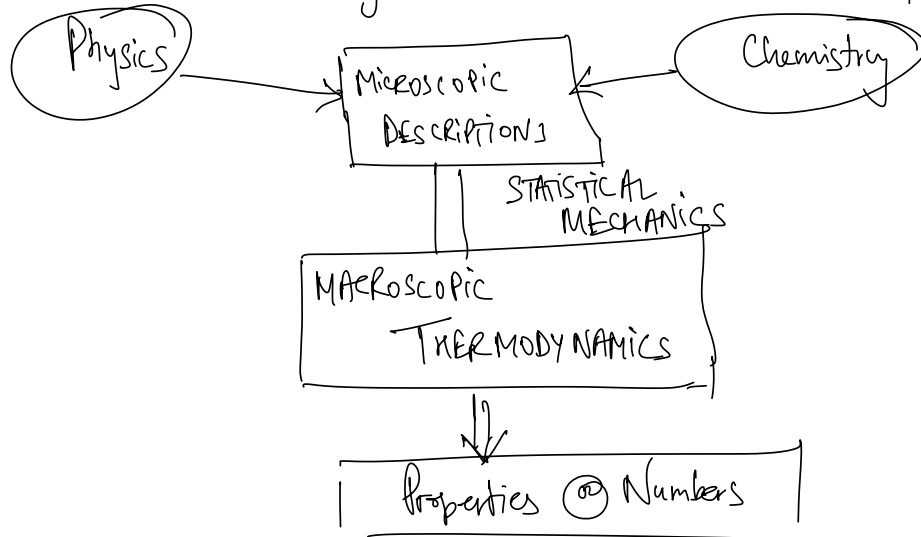
— Completely general framework that does not rely on atomic details.

— Thermodynamics is a "processor" @ "accountant"

⇒ You have to put some information / physics into the framework to get other properties out

RELATION TO OTHER FIELDS:

can derive thermodynamic relations from atomic / electronic



THERMO: determines the equilibrium states and free energy landscape between phases

KINETICS: determines the mechanisms and rates.

DEFINITIONS:

* SYSTEM: Any collection of matter that can be uniquely specified (and over which macroscopic averages can be specified)

* SURROUNDING / ENVIRONMENT: Universe - System

* VARIABLES:

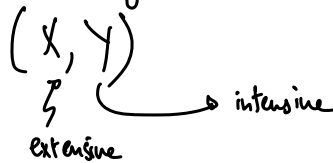
- extensive: scale with the size of the system

$$(S, V, \vec{M}, N_i, V_0 \epsilon_{ij}) \Rightarrow \text{normalized extensive variables: } \frac{N_i}{V} = \rho_i$$

- intensive: do not scale with the size of the system

$$(T, p, \vec{H}, \mu_i, \sigma_{ij})$$

extensive and intensive variables always come in conjugate pairs

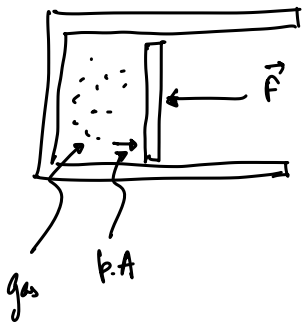


* CHANGE OF STATE → by exchanging heat or work between the system and the environment

* TYPES OF PATHS:

- reversible → mathematical idealisation where the system and the environment are always in eq^m with each other
- irreversible → all real and spontaneous changes of state

EXAMPLE: piston work (work is $\delta W = \vec{f} \cdot d\vec{r}$)



- real compression $F > p \cdot A$
 - real expansion $F < p \cdot A$] ⇒ real changes of state need an imbalance between the system and the environment

REVERSIBLE WORK

$$F = pA$$

$$\delta W = \vec{F} \cdot d\vec{r} = \underbrace{pA}_{-dV} dl = -pdV$$

Reversible p-V work
 $\delta W = -pdV$

Expressed in terms of STATE VARIABLES of the system.

In general: REVERSIBLE work is "force" applied by the environment on the system times "displacement"

$$\delta W_{\text{reversible}} = Y dX$$

$\begin{matrix} \nearrow & \text{extensive} \\ & \text{(displacement)} \\ \searrow & \text{intensive} \\ & \text{(force)} \end{matrix}$

HEAT: exchange of energy between system and the environment due to a temperature difference

REVERSIBLE: $\Rightarrow \Delta T \rightarrow 0$

LAWS OF THERMODYNAMICS:

1st law: $\Delta U = Q + W$ $U \rightarrow$ internal energy

$$dU = \underbrace{\delta q}_{\substack{\nearrow \\ \text{NEW STATE} \\ \text{VARIABLE}}} + \underbrace{\delta W}_{\substack{\searrow \\ \text{both variables.}}}$$

2nd law: $\Delta S \geq \frac{Q}{T}$ $S =$ entropy $>$ for irreversible
 $\qquad \qquad \qquad =$ for reversible.

$$dS \geq \frac{\delta Q}{T}$$

$$\frac{\delta Q_{\text{reversible}}}{T} = dS \Rightarrow \boxed{\delta Q_{\text{reversible}} = T dS}$$

COMBINED 1st AND 2nd LAW:

$$\boxed{dU = \underbrace{T dS}_{\delta Q_{\text{rev}}} + \sum_i \underbrace{Y_i dX_i}_{\delta W_{\text{reversible}}}}$$

ASIDE:

for macroscopic systems

$$\left. \begin{matrix} N \rightarrow 2N & \Rightarrow & U \rightarrow 2U \\ & & U \rightarrow 2U \\ & & S \rightarrow 2S \end{matrix} \right\} \text{EXTENSIVITY}$$

* REVERSIBLE WORK

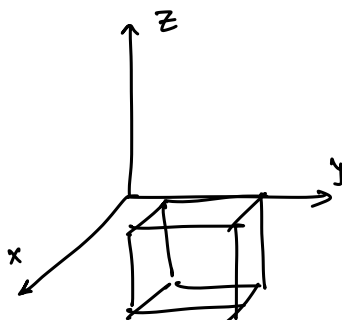
$$\delta W = Y \cdot dx$$

intensive force extensive displacement

Y & X are state variables of the system.

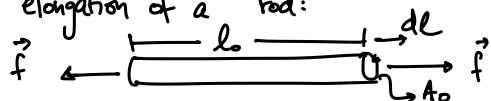
① STRAIN WORK:

$$\delta W = V_0 \sum_i \sum_j \sigma_{ij} d\epsilon_{ij}$$



Special cases

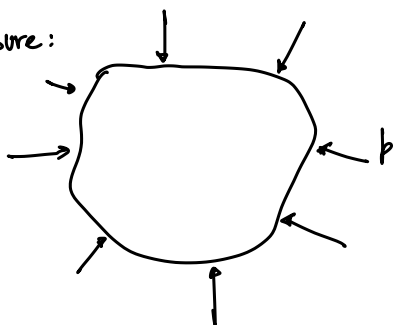
* elongation of a rod:



$A_0 \rightarrow$ area of the rod cross-section

$$\delta W = f \cdot dl = f \cdot l_0 \frac{\delta l}{l_0} = \underbrace{\left(\frac{f}{A_0}\right)}_{\sigma_{xx}} \underbrace{(A_0 l_0)}_{V_0} \underbrace{\left(\frac{\delta l}{l_0}\right)}_{d\epsilon_{xx}} = V_0 \sigma_{xx} d\epsilon_{xx}$$

* hydrostatic pressure:



$$\sigma_{xx} = \sigma_{yy} = \sigma_{zz} = -p \quad \text{sign convention}$$

$$\sigma_{xy} = \sigma_{xz} = \sigma_{yz} = 0$$

reference volume

$$V = V_0 (1 + \epsilon_{xx} + \epsilon_{yy} + \epsilon_{zz})$$

↑ hydrostatic stress/strain

$$dV = V_0 d(\epsilon_{xx} + \epsilon_{yy} + \epsilon_{zz})$$

$$\delta W = V_0 \sum_i \sum_j \sigma_{ij} d\epsilon_{ij} = V_0 (\sigma_{xx} d\epsilon_{xx} + \sigma_{yy} d\epsilon_{yy} + \sigma_{zz} d\epsilon_{zz})$$

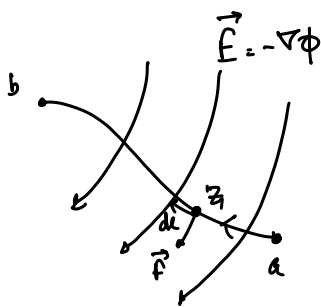
$$= V_0 (-p) d(\epsilon_{xx} + \epsilon_{yy} + \epsilon_{zz}) = -p dV$$

$$\boxed{\delta W = -p dV}$$

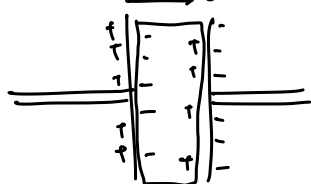
* Electrical Work:

- moving charge from one potential to another

$$\delta W = \Delta \phi dQ$$

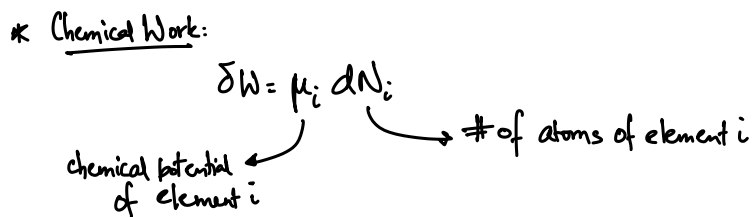
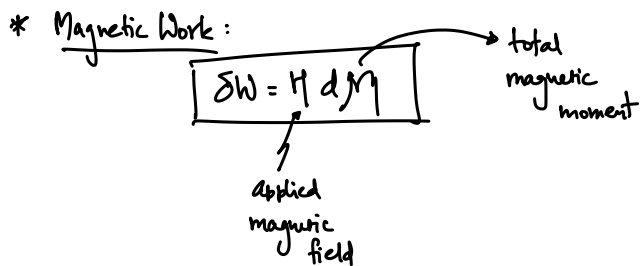


- work to polarize a material



$$\delta W = \vec{E} \cdot d\vec{P}$$

total dipole moment of the material



SUMMARY:

<u>form of work</u>	δW	<u>state variables</u>	
- lengthen rod	$\vec{f} \cdot d\vec{l}$	f	l
- hydrostatic pressure	$-p \cdot dV$	p	V
- general strain work	$V_0 \sum_{ij} \sigma_{ij} d\epsilon_{ij}$	σ_{ij}	$V_0 \epsilon_{ij}$
- moving charge through a potential	$\phi d'z_1$	ϕ	z_1
- electric polarization	$\vec{E} \cdot d\vec{P}$	\vec{E}	\vec{P}
- magnetization	$\vec{H} \cdot d\vec{M}$	\vec{H}	\vec{M}
- chemical	$\mu_i dN_i$	μ_i	N_i
		INTENSIVE VARIABLES	EXTENSIVE VARIABLES

CONJUGATE PAIRS

GENERAL: $\delta W = \int \gamma dx$ → reversible work expressed in terms of state variables of the system.

\int → intensive
 dx → extensive

FUNDAMENTAL RELATION IN THERMO:

$$\boxed{du = Tds + \sum_i \gamma_i dx_i} \rightarrow \text{connects all state variables of a system.}$$

↑
differentials are all extensive

$$\Rightarrow U(S, X_1, X_2, \dots)$$

"natural variables" of internal energy.

$$\Rightarrow \boxed{du = \left(\frac{\partial u}{\partial s}\right)_{X_1, X_2, \dots} ds + \sum_i \left(\frac{\partial u}{\partial x_i}\right)_{X_{j \neq i}, s} dx_i} \quad \text{--- ②}$$

Comparing eqns. ① & ②

→ EQUATIONS OF STATE

$$\left. \begin{aligned} T &= \left(\frac{\partial u}{\partial s}\right)_{X_1, X_2, \dots} \\ \gamma_i &= \left(\frac{\partial u}{\partial x_i}\right)_{s, X_{j \neq i}} \end{aligned} \right\}$$

All intensive variables are partial derivatives w/ respect to the conjugate extensive variable.

- if U is known in terms of S and $X_i \Rightarrow$ all thermodynamic properties can be extracted from U .
- if all EOS are known $\Rightarrow U$ can be determined through integration.

* EULER RELATION: $\boxed{U = TS + \sum_i \gamma_i X_i}$

extensivity: $U(\lambda S, \lambda X_i) = \lambda U(S, X_i)$

take derivative w/rt to λ

$$\left(\frac{\partial U}{\partial(\lambda S)}\right)_{X_i} \left(\frac{d(\lambda S)}{d\lambda}\right) + \sum_i \left(\frac{\partial U}{\partial(\lambda X_i)}\right)_{\lambda S, X_{j \neq i}} \left(\frac{\partial(\lambda X_i)}{\partial \lambda}\right) = U(S, X_i)$$

evaluate for $\lambda=1$

$$\underbrace{\left(\frac{\partial U}{\partial s}\right)_{X_i}}_T \cdot S + \sum_i \underbrace{\left(\frac{\partial U}{\partial x_i}\right)_{s, X_{j \neq i}}}_{\gamma_i} X_i = U(S, X_i)$$

★ GIBBS-DUHEM :

Start with Euler: $U = TS + \sum_i \gamma_i X_i$

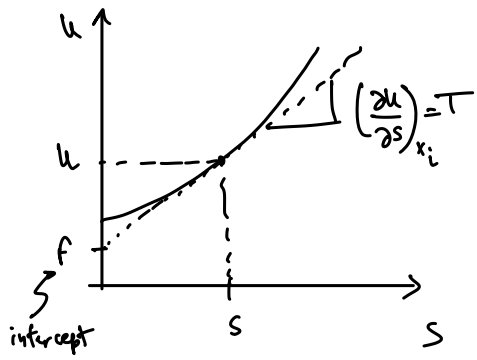
Take differential: $dU = TdS + SdT + \sum_i (\gamma_i dX_i + X_i d\gamma_i)$
 Fundamental eqn of thermo $\Rightarrow dU = TdS + \sum_i \gamma_i dX_i$ \Rightarrow $SdT + \sum_i X_i d\gamma_i = 0$
all intensive

LEGENDRE TRANSFORM: \rightarrow gives us the "characteristic potential".

$U(S, X_i) \rightarrow U$ is the characteristic potential when we control (S, X_i) i.e. extensive quantities.

Controlling extensive quantities in experiment may be difficult.
 (eg) Controlling S is difficult.

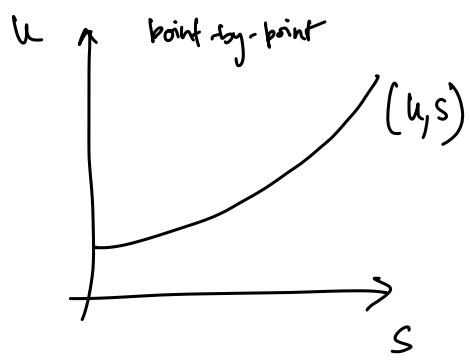
Say I want to run an experiment where we control (T, X_i) instead of (S, X_i)
 \Rightarrow I would like a ^{state} function that has (T, X_i) as natural variables \Rightarrow How do we obtain this from U ?



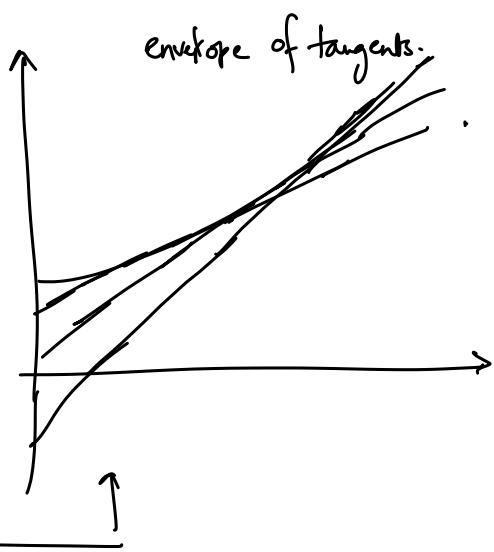
$$\frac{U - F}{S} = \left(\frac{\partial U}{\partial S}\right)_{X_i} = T$$

$$\Rightarrow \boxed{F = U - TS}$$

Two ways to represent a curve



OR



Specify slope (T) and intercept (F)
 $F = U - TS$

The two curves have the same information content.

Whenever an INTENSIVE variable is experimentally controlled, we have to perform a LEGENDRE TRANSFORM

In general: $\phi = U - Y_i X_i$ $\left\{ \begin{array}{l} X_i = \text{extensive} \\ Y_i = \text{intensive} \end{array} \right.$

char. potential under the experimental conditions.

EXAMPLES:

* Constant T, V:



* start with fundamental equation:

$$dU = Tds - pdV \rightarrow U(S, V) \begin{array}{l} \text{need to replace} \\ \text{this with conjugate } T \\ \text{good} \end{array}$$

Legendre transform:

$$F = U - TS$$

Legendre transform.

$$dF = dU - Tds - SdT$$

$$= Tds - pdV - Tds - SdT$$

$$\boxed{dF = -SdT - pdV} \rightarrow F(T, V)$$

$$dF = \left(\frac{\partial F}{\partial T}\right)_V dT + \left(\frac{\partial F}{\partial V}\right)_T dV \Rightarrow \boxed{\begin{array}{l} \left(\frac{\partial F}{\partial T}\right)_V = -S \quad \left(\frac{\partial F}{\partial V}\right)_T = -p \\ \text{EQUATIONS OF STATE} \end{array}}$$

(eg) IDEAL GAS: from statistical mechanics.

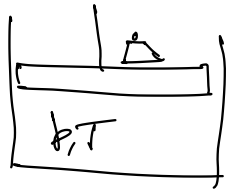
$$F(T, V) = -nRT \left[\log V - \frac{3}{2} \log T + \frac{3}{2} \log \left(\frac{m}{2\pi k_B T} \right) \right]$$

$$p = - \left(\frac{\partial F}{\partial V}\right)_T = \frac{nRT}{V}$$

$$S = - \left(\frac{\partial F}{\partial T}\right)_V = nR \left[\log V - \frac{3}{2} \log T + \frac{3}{2} \log \left(\frac{m}{2\pi k_B T} \right) \right] - \frac{3}{2} nR$$

$$U = pV + TS = \frac{3}{2} nRT = U(T)$$

2. constant T, p



fundamental equation: $dU = TdS - pdV$

$U(S, V) \rightarrow$ replace both variables with their conjugates

$$G = U - TS + pV$$

\hookrightarrow sign because $Y_i = -p$

$$dG = -SdT + Vdp$$

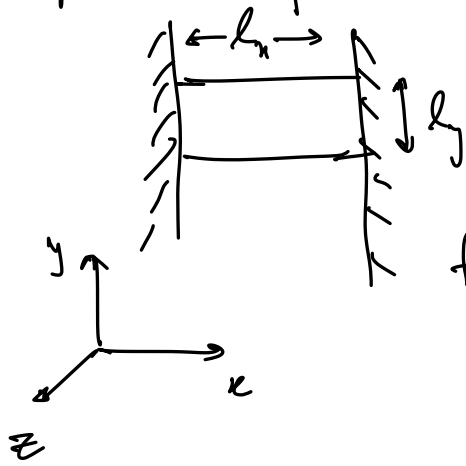
$G(T, p) \rightarrow$ GIBBS FREE ENERGY

$$dG = \left(\frac{\partial G}{\partial T}\right)_p dT + \left(\frac{\partial G}{\partial p}\right)_T dp$$

EQUATIONS OF STATE:

$$S = -\left(\frac{\partial G}{\partial T}\right)_p \quad V = \left(\frac{\partial G}{\partial p}\right)_T$$

③ Clamped block of material @ constant T, p



generalized stress/strain work

$$\sum_i \sum_j V_0 \sigma_{ij} d\epsilon_{ij}$$

for simplicity, assume no shear stress/strain

$$\delta W = V_0 (\sigma_{xx} d\epsilon_{xx} + \sigma_{yy} d\epsilon_{yy} + \sigma_{zz} d\epsilon_{zz})$$

fundamental equation:

$$dU = T dS + V \sigma_{xx} d\epsilon_{xx} + V \sigma_{zz} d\epsilon_{zz} + V \sigma_{yy} d\epsilon_{yy}$$

$$U(S, V\epsilon_{xx}, V\epsilon_{zz}, V\epsilon_{yy})$$

we control:

$$\left(T, \underbrace{V\epsilon_{xx}}_{\text{extensive}}, \underbrace{V\epsilon_{zz}, V\epsilon_{yy}}_{-p} \right)$$

$$\Delta = U - TS - V\sigma_{yy}\epsilon_{yy} - V\sigma_{zz}\epsilon_{zz} = U - TS + pV(\epsilon_{yy} + \epsilon_{zz})$$

$$d\Delta = -SdT + \sigma_{xx} V d\epsilon_{xx} - V(\epsilon_{yy} + \epsilon_{zz}) dp$$

EQUATIONS OF STATE:

$$S = - \left(\frac{\partial \Delta}{\partial T} \right)_{V\epsilon_{xx}, p}$$

$$\sigma_{xx} = \left(\frac{\partial \Delta}{\partial \epsilon_{xx}} \right)_{T, p} \frac{1}{V}$$

$$V(\epsilon_{xx} + \epsilon_{yy}) = - \left(\frac{\partial \Delta}{\partial p} \right)_{T, V\epsilon_{xx}}$$