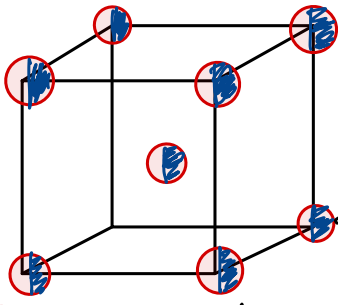


ORDER-DISORDER REACTIONS:

example: ①

bcc



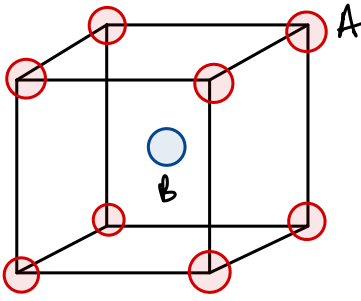
disordered phase on the bcc structure

A & B atoms are randomly distributed across the entire structure

⇒ NO LONG-RANGE BCC ORDER

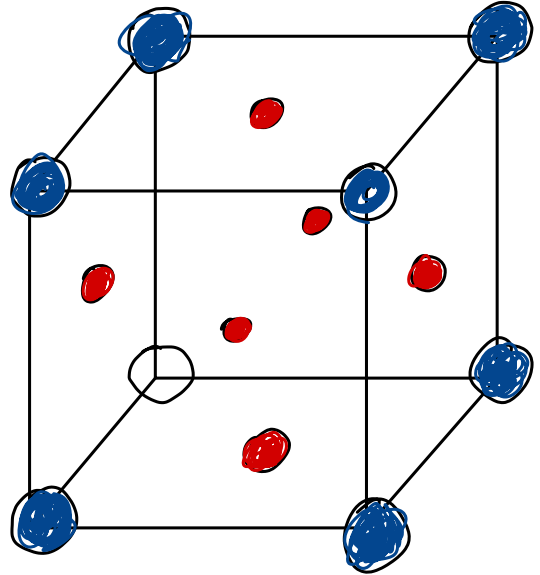
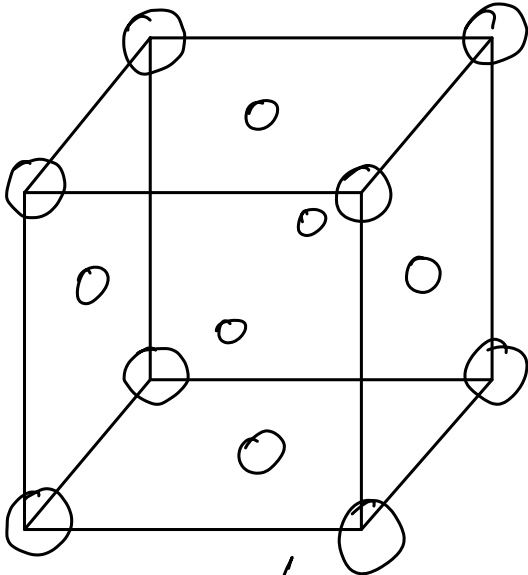
A atoms occupy one set of sites,
B atoms occupy the other.

B2

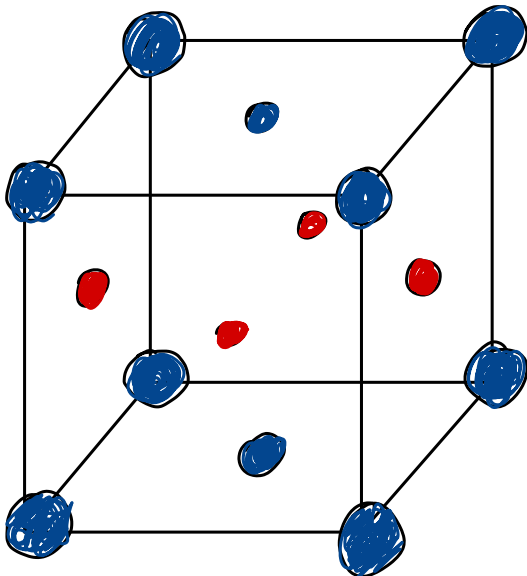


Strukturbericht notation.

② FCC:

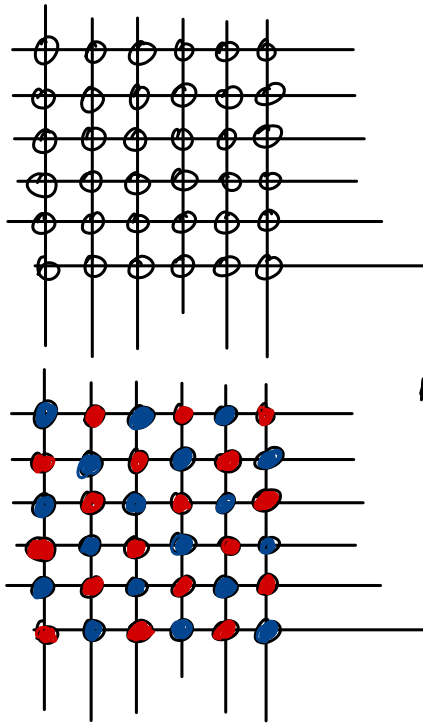


L₁₂
(A₂B)



L₁₀
(AB)

2-Dimensional examples:

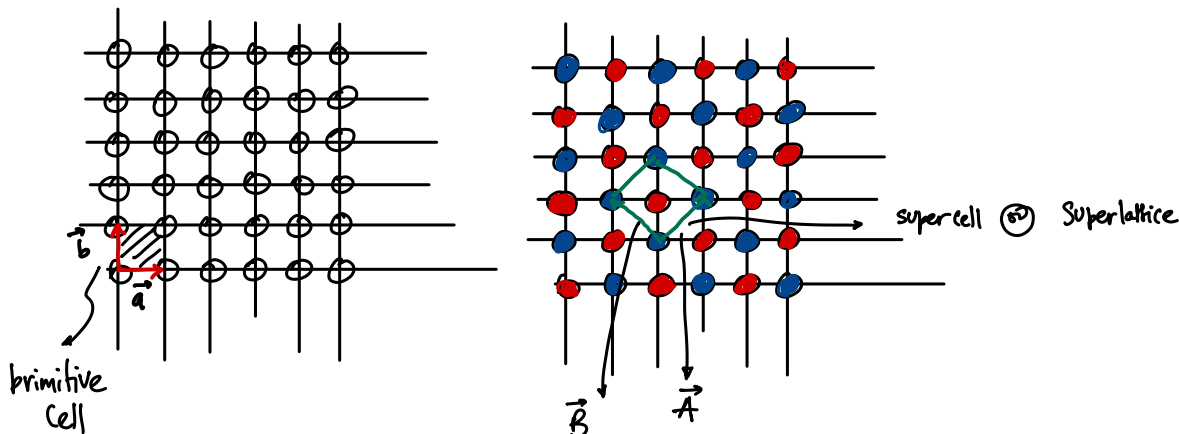


Consider a material system where A-B bonds are preferred.

To describe these phase transitions we need descriptors that can uniquely identify each phase of interest.

DESCRIPTORS OF ORDERING:

- We would like to find "order parameters" that can distinguish the disordered phase from the ordered phase.
- In experiment you could use characterization techniques like XRD, TEM etc. to quantify the degree of ordering \Rightarrow what about in theory?
- * Orderings are typically formed on lattices that have a larger periodicity than the disordered phase:

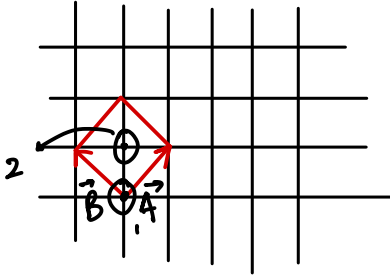


$$\begin{cases} \vec{A} = \vec{a} + \vec{b} \\ \vec{B} = -\vec{a} + \vec{b} \end{cases}$$

\Rightarrow Supercell vectors can be written as linear combinations of primitive cell vectors.

To compute order parameters for a particular ordering:

① Identify the supercell that defines the periodicity of the ordering:



② Each site in the supercell corresponds to a "sublattice".

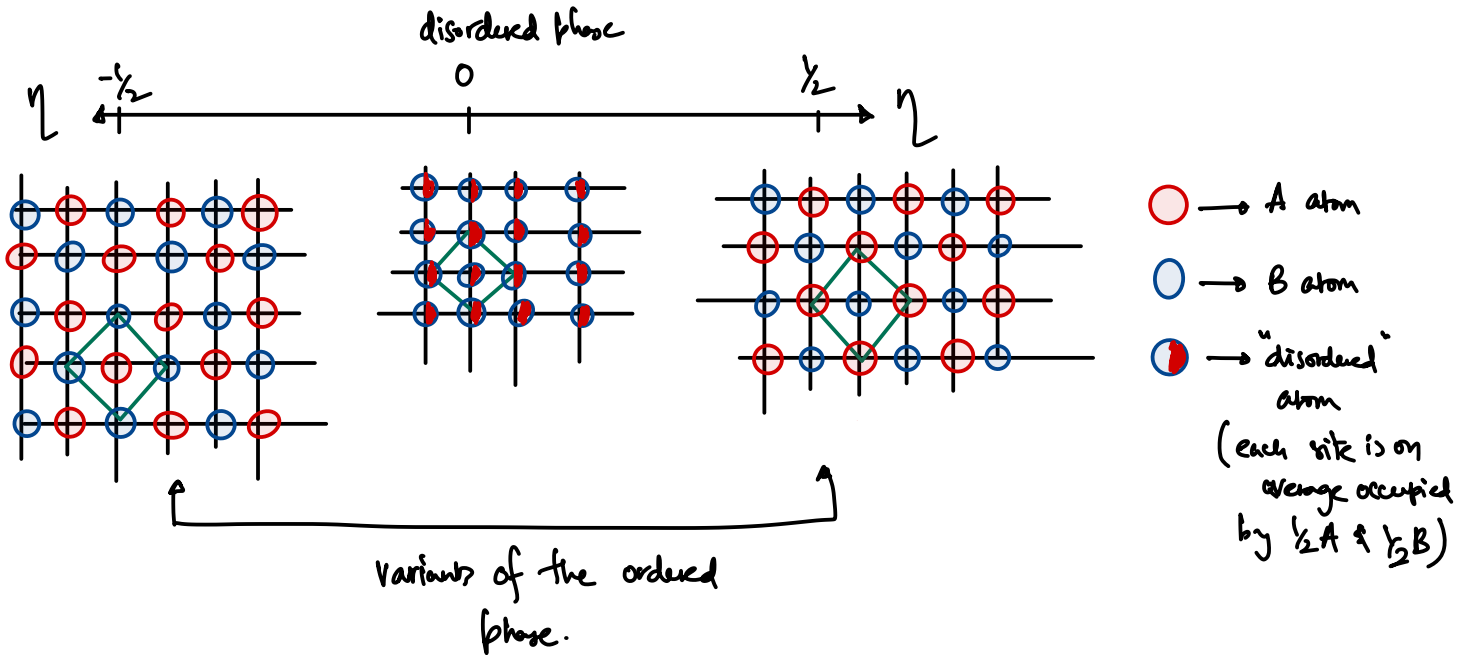
We have 2 sublattices in the above supercell.

Let the concentration of element A on sublattice 1 be X_1
and concn. in sublattice 2 be X_2

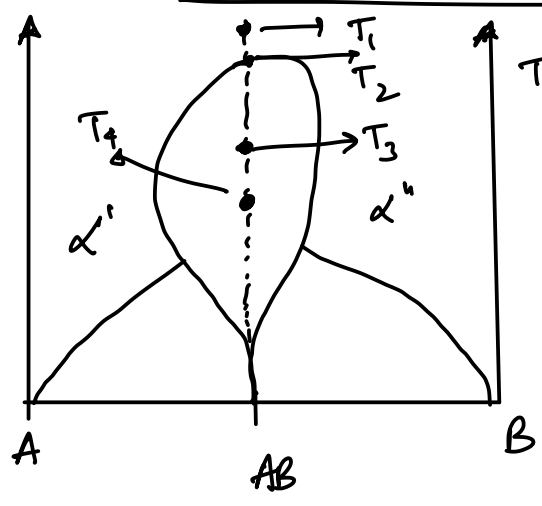
③ Order parameters can be derived as linear combinations of sublattice composition:

$$X = \frac{X_1 + X_2}{2} = \text{Average composition of the alloy.}$$

$$\eta = \frac{X_1 - X_2}{2} = \text{order parameter to distinguish the ordered phase from the disordered phase}$$



* PHASE DIAGRAMS, ORDER PARAMETERS & FREE ENERGIES:



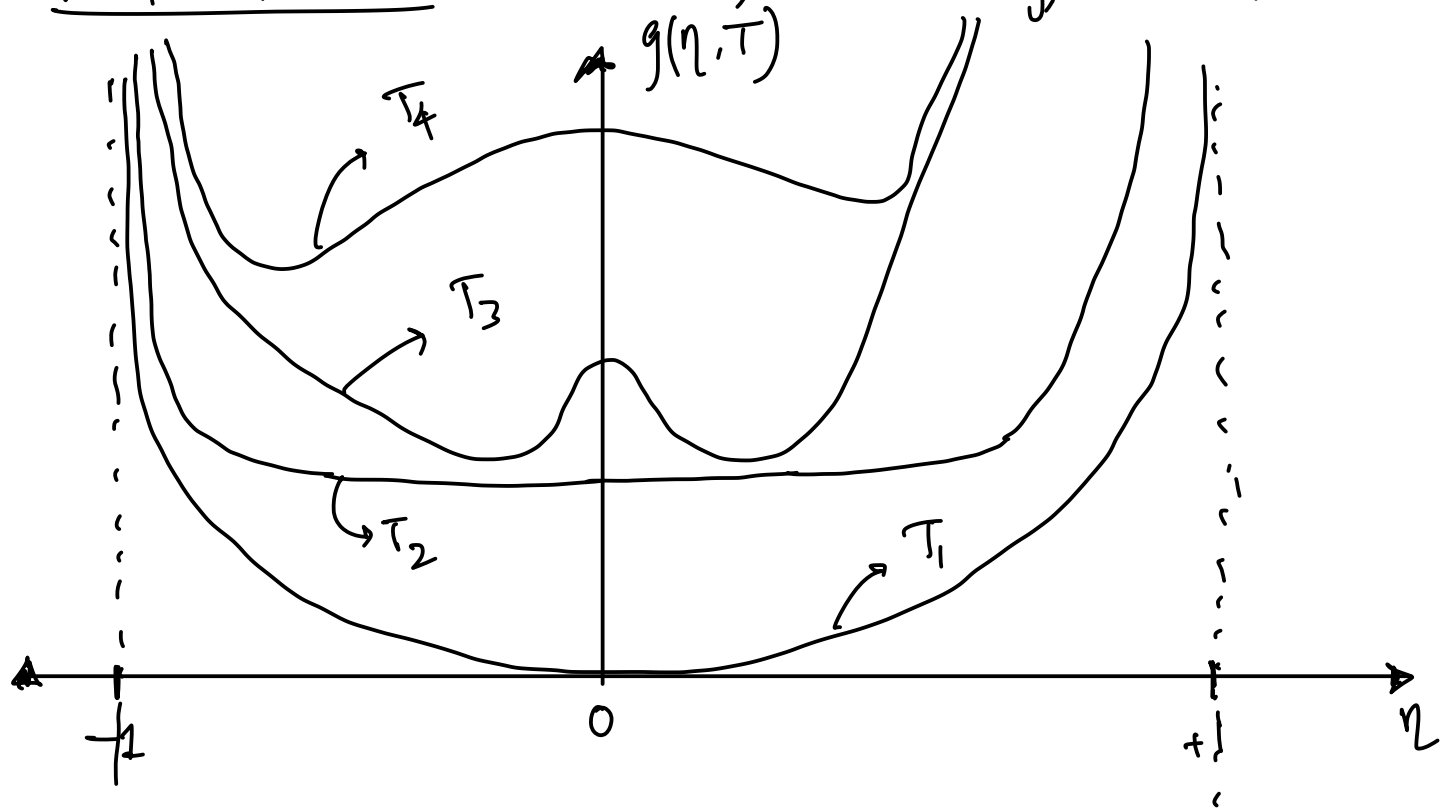
Consider the phase diagram

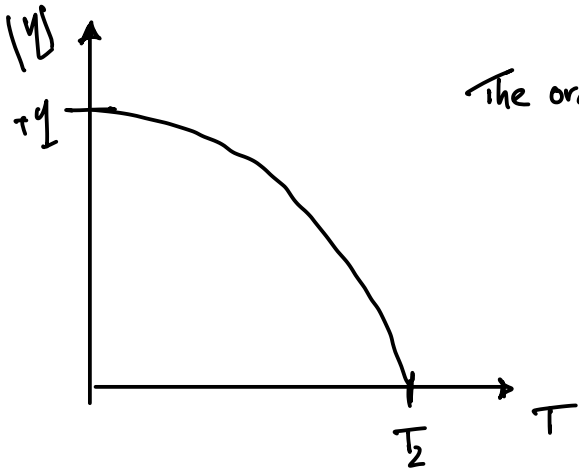
The ordered AB phase undergoes a 2nd order phase transition to the disordered phase at elevated temperatures.

For simplicity: say a single order parameter (η) can distinguish the ordered phase from the disordered phase. $\Rightarrow \eta$

$$\eta = \begin{cases} 0, & \text{disordered phase} \\ \pm 1, & \text{ordered phase.} \end{cases}$$

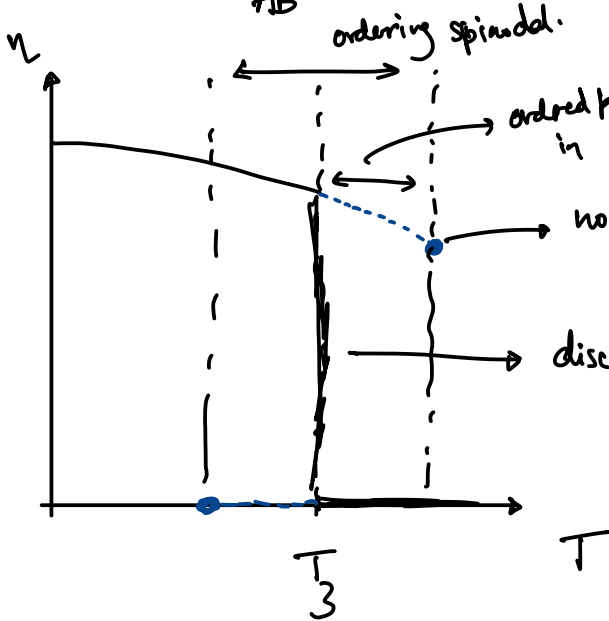
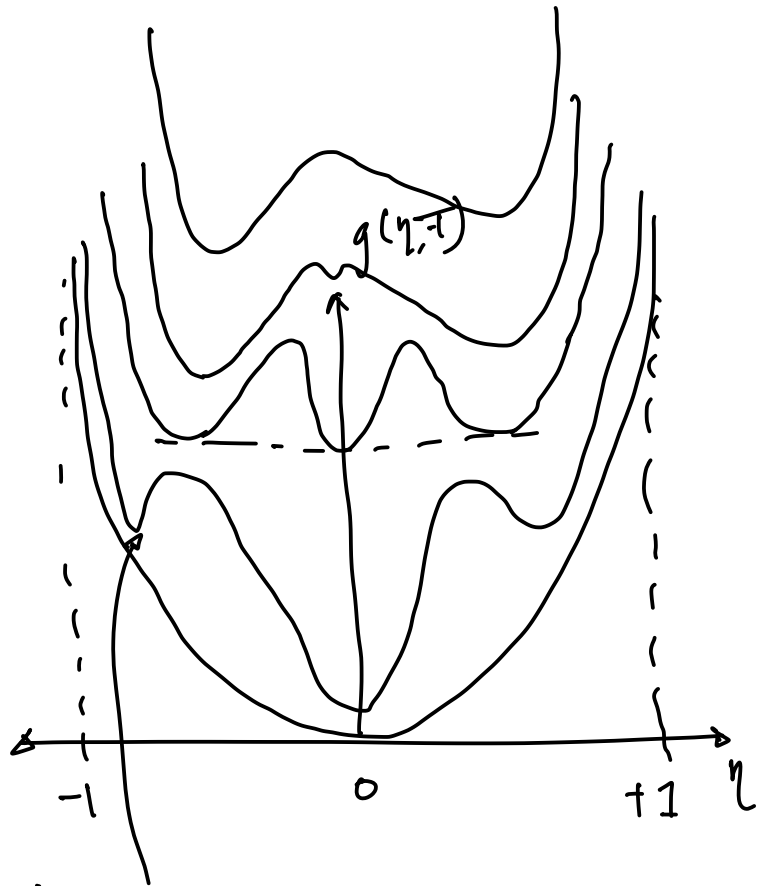
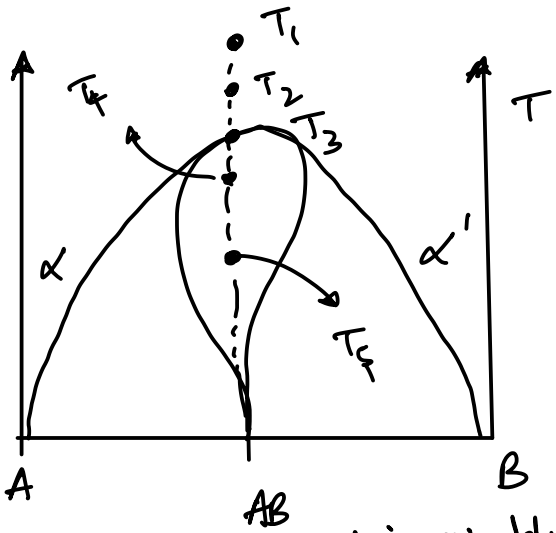
examples of such phase transitions: $B2 \leftrightarrow \text{bcc}$, checkerboard ordering, $L1_0 \leftrightarrow \text{fcc}$, ...





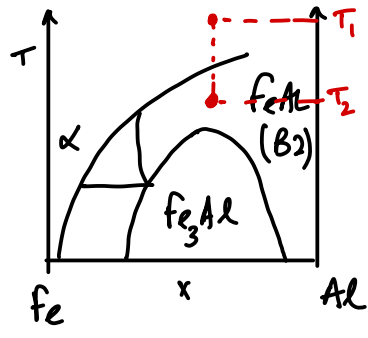
The order parameter smoothly transitions from 1 to 0

* 1st order phase transition:

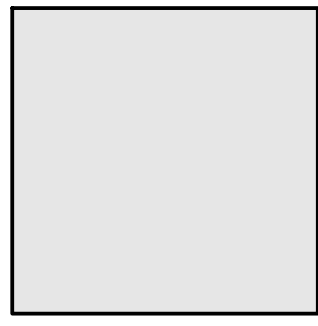


At temperatures below the order-disorder transition temperature (for 2nd order phase transition) and below the ordering spinodal for 1st order we will have a negative curvature of the free energy w/respect to $\eta \Rightarrow$ Similar mechanism and kinetics to Spinodal decomposition.

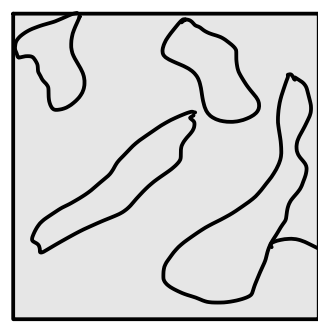
* PHENOMENOLOGICAL THEORY OF ALLEN-CAHN:



Allen-Cahn: studying the binary $Fe-Al$ ^{alloy} with a composition $\sim 25\% Al$



microstructure @ T_1

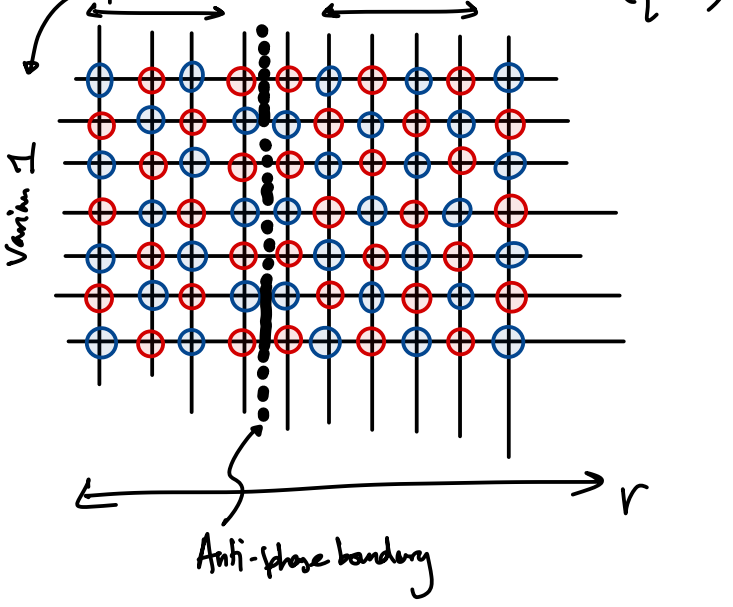


microstructure @ T_2

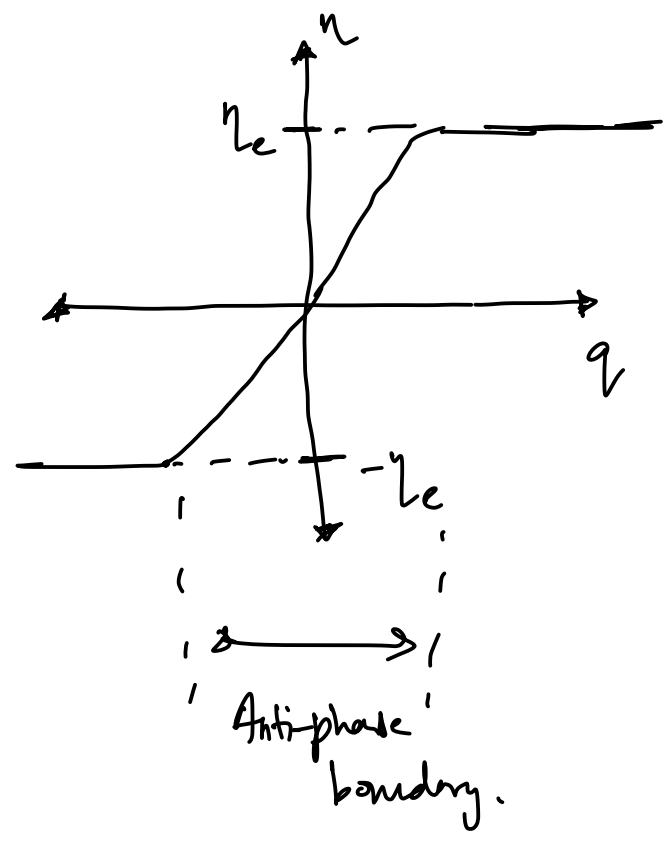
B2 phase everywhere but 2 different variants are formed.

Anti-phase boundary.

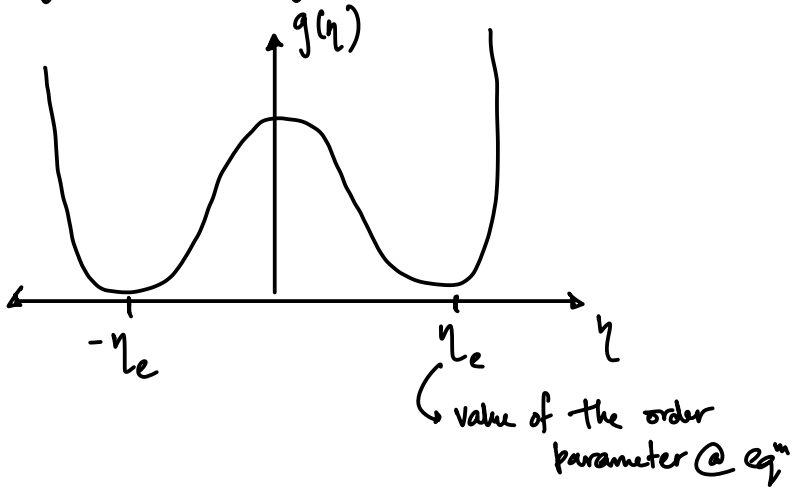
Anti-phase boundary:



At the APB \Rightarrow A-A and B-B bonds are energetically unfavorable.
APB's cost the system energy.



System can minimize its energy by getting rid of APB



Similar to the case of spinodal decomposition:

$$G[\eta(\vec{r})] = \int_V [g(\eta(\vec{r})) + k(\nabla\eta)^2] d\vec{r}$$

functional \int_V

gradient energy.

* EVOLUTION EQUATION:

- for Cahn-Hilliard \rightarrow we obtained an evolution equation from Fick's first and 2nd laws
- we need an evolution equation for the order parameter field.

$\eta \rightarrow$ non-conserved. \Rightarrow no conservation equation.

- The evolution equation must result in an overall decrease in the total free energy with time.

$$\frac{\partial \eta}{\partial t} = -\alpha \frac{\delta \Delta G}{\delta \eta}$$

Allen-Cahn Mobility \rightarrow related to how quickly APB's move.

taking the variational derivative of $\Delta G = \int \left\{ \Delta g + k \nabla^2 \eta \right\} dr \Rightarrow \frac{\delta \Delta G}{\delta \eta} = \frac{\partial \Delta g}{\partial \eta} - 2k(\nabla^2 \eta)$

$$\boxed{\frac{\partial \eta}{\partial t} = -\alpha \left(\frac{\partial \Delta g}{\partial \eta} \right) + M \nabla^2 \eta}$$