

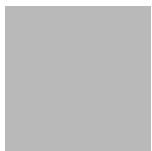
PAUL SCHERRER INSTITUT



WIR SCHAFFEN WISSEN – HEUTE FÜR MORGEN

# Materials Science at Large Scale Facilities

Neutron imaging

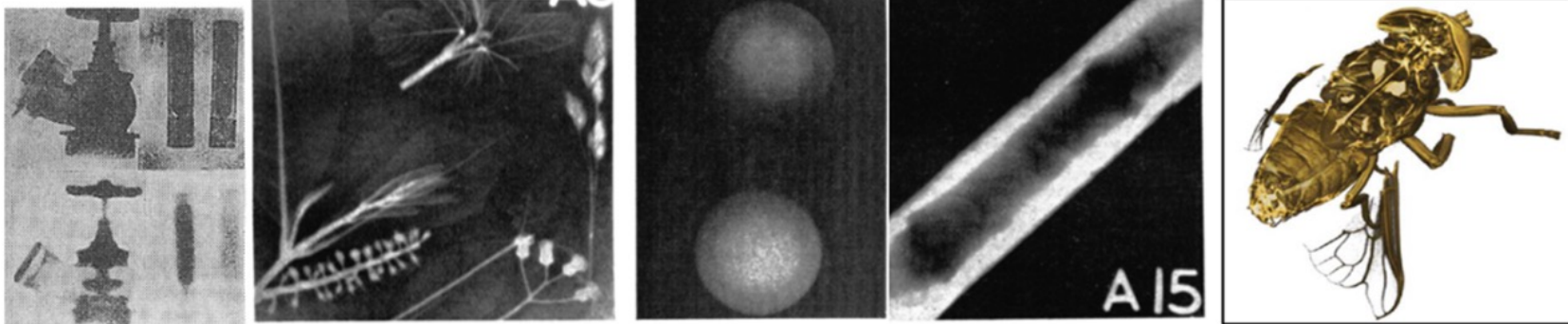


**Early neutron imaging (1935–1938)**

- Kallmann & Kuhn in Berlin produced the first neutron images using Ra–Be sources and D–D generator.
- First converter–film system and vacuum cassette, similar to later film-based radiography setups.
- Their work was patented in 1940 (*Photographic Detection of Slowly Moving Neutrons*)

**First widely recognized neutron radiographs (Peter, 1946)**

- Used a high-voltage neutron generator with reduced x-ray background → clearer neutron images.
- Demonstrated two defining neutron imaging strengths:
  - High penetration through dense metals (e.g., faucet).
  - Isotope sensitivity (strong contrast between H<sub>2</sub>O and D<sub>2</sub>O).





### Reactor era begins (mid-1950s)

- Nuclear reactors (e.g., BEPO) provided orders-of-magnitude higher flux, enabling practical and industrial neutron imaging.
- Technique adopted for non-destructive testing (NDT), especially in nuclear and aerospace sectors.

### Field organization and milestones (1960s–1980s)

- First newsletters (1964–1977), first dedicated conference (1973).
- ASTM E545 (1975) → first neutron imaging standard.
- WCNR-1 (1981): major expansion of the community.
- Development of time-resolved imaging and first 3D tomographies (film & TV detectors).

### Modern neutron imaging starts (1990s)

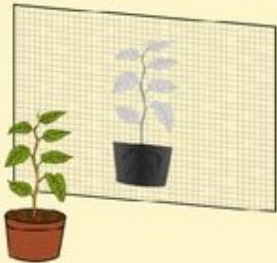
Introduction of digital detectors enabled:

- True 3D tomography
- Quantitative image analysis
- High-quality time-resolved imaging

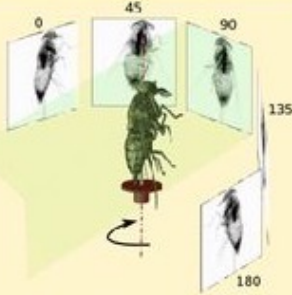
# Imaging modalities

## Classic neutron imaging methods

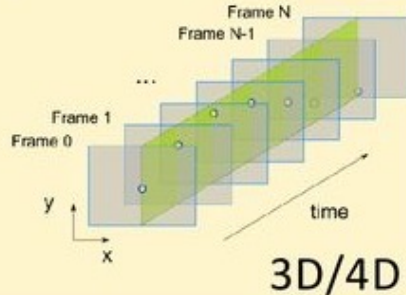
Radiography



Tomography

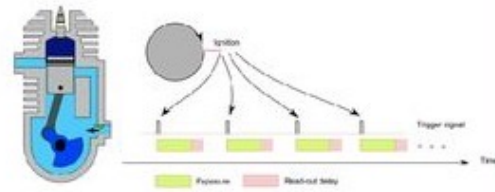


Real-time imaging



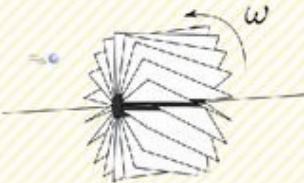
3D/4D

Stroboscopic imaging

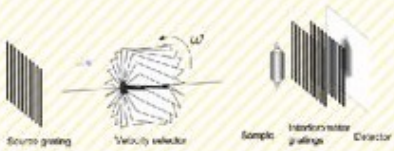


## Advanced neutron imaging methods

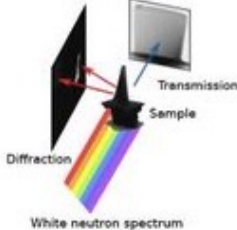
Energy selective imaging



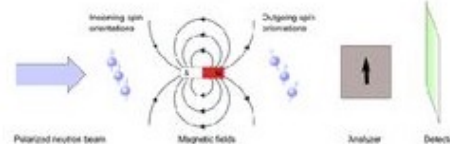
Neutron grating interferometry



Diffraction imaging



Polarized neutron imaging



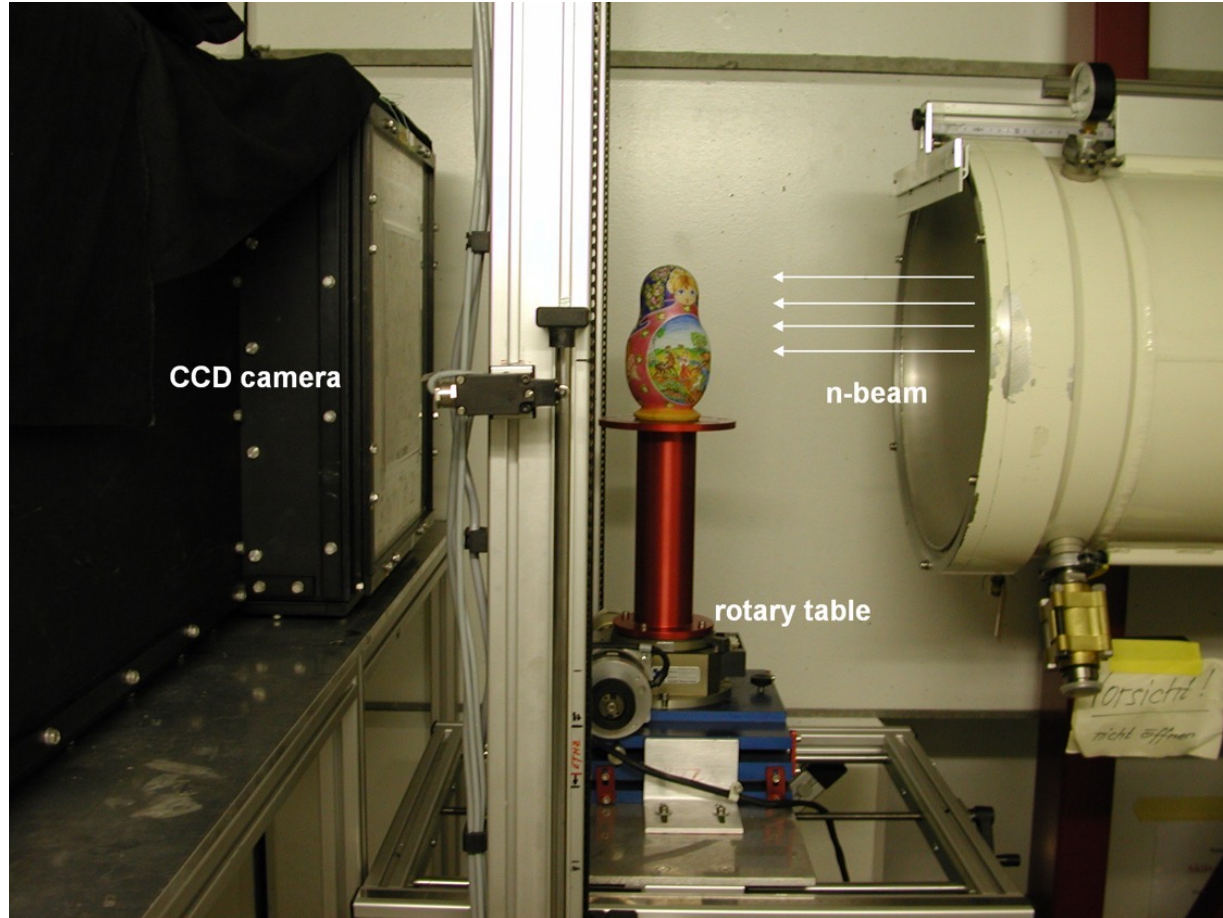
# Overview some techniques

Technique	Use When...	Best For	Limitations / Notes
<b>Absorption Contrast Imaging</b> (incl. radiography, tomography)	You want a <b>direct attenuation-based image</b> of the sample; you need fast, intuitive visualization; or need 3D structure via tomography.	<ul style="list-style-type: none"> <li>Hydrogen-rich materials (water, polymers, oils, adhesives)</li> <li>Metals that are opaque to X-rays (Al, Ti, Pb)</li> <li>Multi-material systems (e.g., water in metal)</li> </ul>	<ul style="list-style-type: none"> <li>Limited by detector efficiency &amp; neutron flux</li> <li>Spatial resolution typically lower than X-ray imaging</li> <li>Requires high-quality beam collimation</li> </ul>
<b>Neutron Microscope</b> (optical focusing using MLLs or Wolter optics)	You need <b>micron-scale spatial resolution</b> , beyond conventional pinhole geometry.	<ul style="list-style-type: none"> <li>High-resolution imaging of microstructures in metals or energy materials</li> <li>Situations requiring both penetration &amp; resolution (e.g., cracks in dense alloys)</li> </ul>	<ul style="list-style-type: none"> <li>Still developing; lower flux and small field of view</li> <li>Optics are difficult to fabricate; alignment sensitive</li> </ul>
<b>Stroboscopic Neutron Imaging</b>	When you need to study <b>periodic or cyclic processes</b> with high temporal precision but low average flux.	<ul style="list-style-type: none"> <li>Rotating machinery</li> <li>Periodic motion in engines, pumps, valves</li> <li>Repetitive fluid flow or cavitation studies</li> </ul>	<ul style="list-style-type: none"> <li>Requires strictly periodic motion</li> <li>Low duty cycle → only suitable for repeatable processes</li> <li>Synchronization hardware needed</li> </ul>

# Overview some techniques

Technique	Use When...	Best For	Limitations / Notes
<b>Bragg Edge Imaging</b>	You want to obtain <b>crystallographic information</b> in real space — strain, texture, phase distribution — using energy-dependent transmission.	<ul style="list-style-type: none"> <li>• Mapping strain fields in welded or additively manufactured metals</li> <li>• Distinguishing crystalline phases</li> <li>• Texture gradients in rolled or forged components</li> </ul>	<ul style="list-style-type: none"> <li>• Needs time-of-flight or monochromatic beams</li> <li>• Requires good energy resolution</li> <li>• Interpretation requires modeling (cross-sections, crystallography)</li> </ul>
<b>Neutron Grating Interferometry (Talbot–Lau)</b>	You need sensitivity to <b>microstructure below spatial resolution</b> , such as micrometer-scale porosity, grain boundaries, or magnetic domain structures (if using polarized neutrons).	<ul style="list-style-type: none"> <li>• Quantifying microcracks, porosity, voids</li> <li>• Anisotropic microstructure (dark-field contrast)</li> <li>• Fiber orientation in composites</li> <li>• Phase-contrast on soft matter</li> </ul>	<ul style="list-style-type: none"> <li>• Long exposure times</li> <li>• Sensitive to vibrations and sample motion</li> <li>• Modulated intensity limits dynamic imaging</li> </ul>
<b>Polarization-Contrast Neutron Imaging</b>	When you want to image <b>magnetic fields or magnetic microstructure</b> inside bulk materials, nondestructively.	<ul style="list-style-type: none"> <li>• Mapping internal magnetic fields in superconductors or permanent magnets</li> <li>• Magnetic domain structures in thick samples</li> <li>• Magnetic shielding quality</li> <li>• Lorentz-force imaging of currents</li> </ul>	<ul style="list-style-type: none"> <li>• Requires polarized beam + spin analyzers</li> <li>• Reduced flux due to polarization optics</li> <li>• Interpretation of magnetic contrast can be non-unique without modeling</li> </ul>

# Neutron radiography / tomography

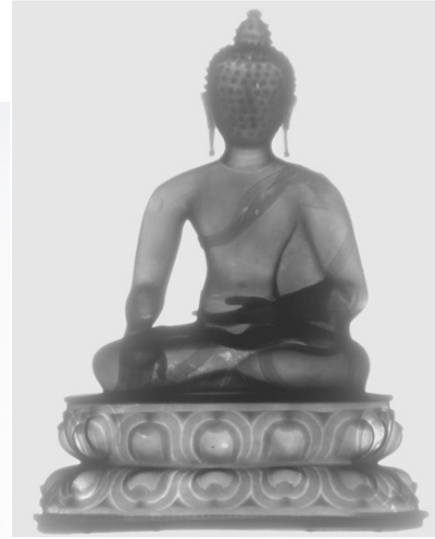


# Contrast

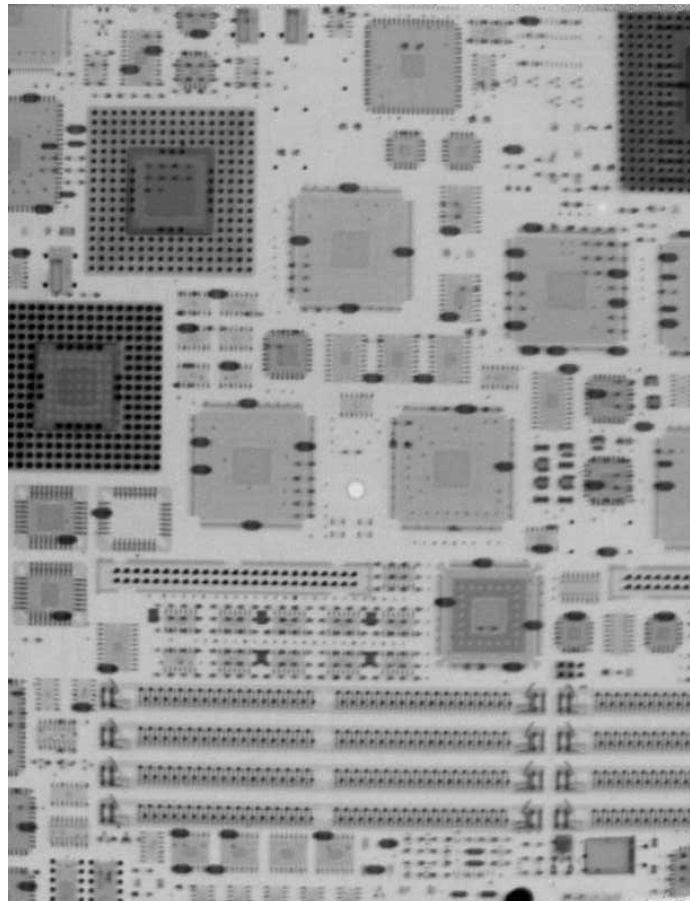
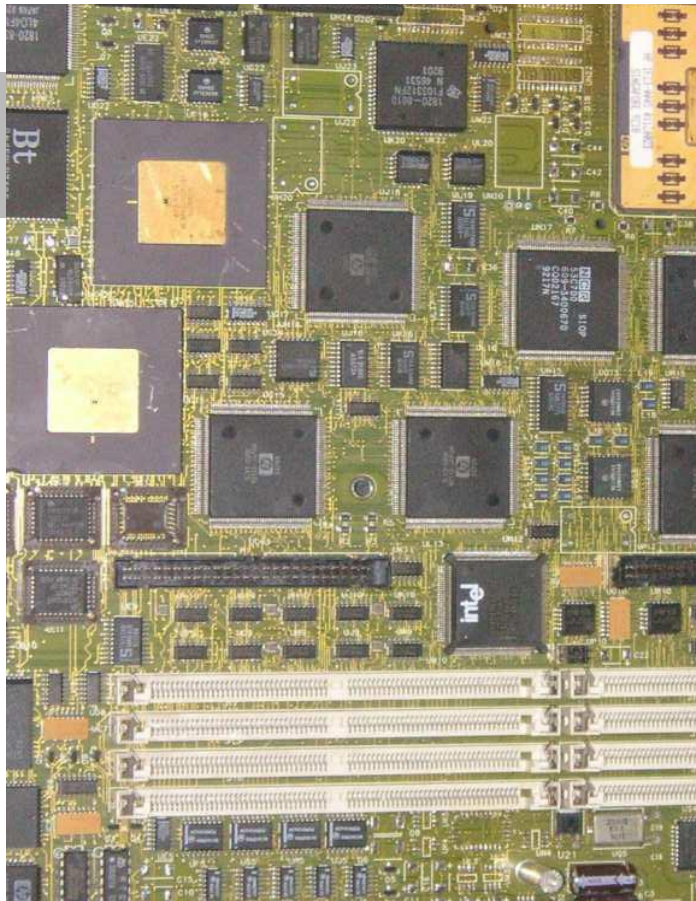
Neutron radiography



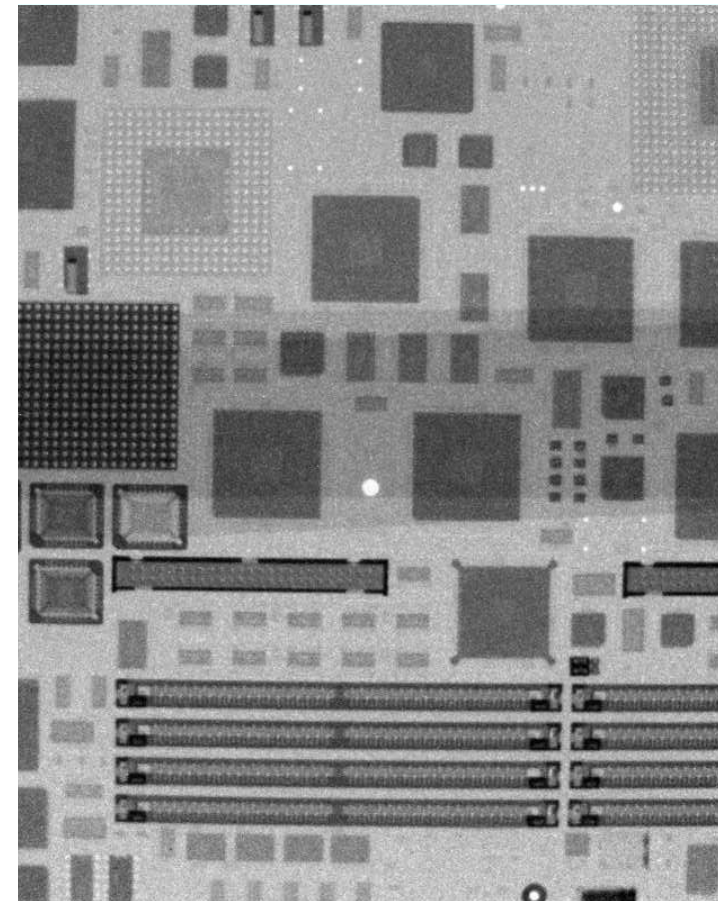
X-ray radiography



# Printed circuit board

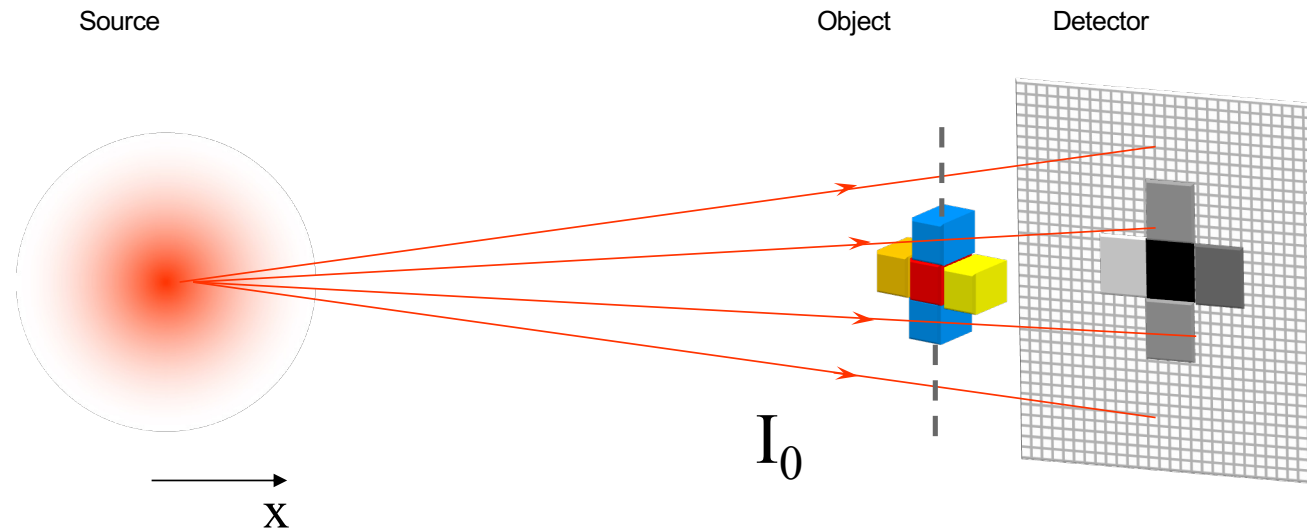


X-ray



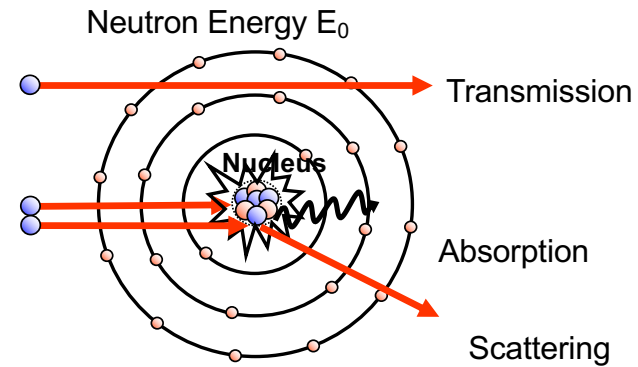
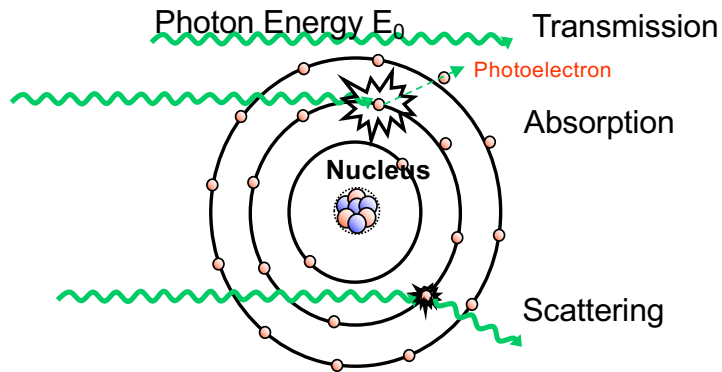
Neutron

## Contrast



$$I_0 e^{-\int \Sigma(x) dx}$$

$I_0$  - primary beam  
 $\Sigma(x)$  - attenuation coefficient  
 $x$  - propagation direction



$$I_0 e^{-\int \Sigma(x) dx}$$

$$\Sigma = N \cdot \sigma$$

$N$  = number of nuclei per  $\text{cm}^3$ .

Unit of  $\Sigma$  is  $[\text{cm}^{-1}]$

$$\sigma = \sigma_a + \sigma_s$$

Unit of  $\sigma$  is [barn] =  $[10^{-24} \text{cm}^2]$

## X-ray attenuation

Attenuation coefficients with X-ray [ $\text{cm}^{-1}$ ]																	
1a	2a	3b	4b	5b	6b	7b	8			1b	2b	3a	4a	5a	6a	7a	0
H 0.02																	He 0.02
Li 0.06	Be 0.22											B 0.28	C 0.27	N 0.11	O 0.16	F 0.14	Ne 0.17
Na 0.13	Mg 0.24											Al 0.38	Si 0.33	P 0.25	S 0.30	Cl 0.23	Ar 0.20
K 0.14	Ca 0.26	Sc 0.48	Ti 0.73	V 1.04	Cr 1.29	Mn 1.32	Fe 1.57	Co 1.78	Ni 1.96	Cu 1.97	Zn 1.64	Ga 1.42	Ge 1.33	As 1.50	Se 1.23	Br 0.90	Kr 0.73
Rb 0.47	Sr 0.86	Y 1.61	Zr 2.47	Nb 3.43	Mo 4.29	Tc 5.06	Ru 5.71	Rh 6.08	Pd 6.13	Ag 5.67	Cd 4.84	In 4.31	Sn 3.98	Sb 4.28	Te 4.06	I 3.45	Xe 2.53
Cs 1.42	Ba 2.73	La 5.04	Hf 19.70	Ta 25.47	W 30.49	Re 34.47	Os 37.92	Ir 39.01	Pt 38.61	Au 35.94	Hg 25.88	Tl 23.23	Pb 22.81	Bi 20.28	Po 20.22	At	Rn 9.77
Fr	Ra 11.80	Ac 24.47	Rf	Ha													
Lanthanides	Ce 5.79	Pr 6.23	Nd 6.46	Pm 7.33	Sm 7.68	Eu 5.66	Gd 8.69	Tb 9.46	Dy 10.17	Ho 10.91	Er 11.70	Tm 12.49	Yb 9.32	Lu 14.07			
*Actinides	Th 28.95	Pa 39.65	U 49.08	Np	Pu	Am	Cm	Bk	Vf	Es	Fm	Md	No	Lr x-ray			

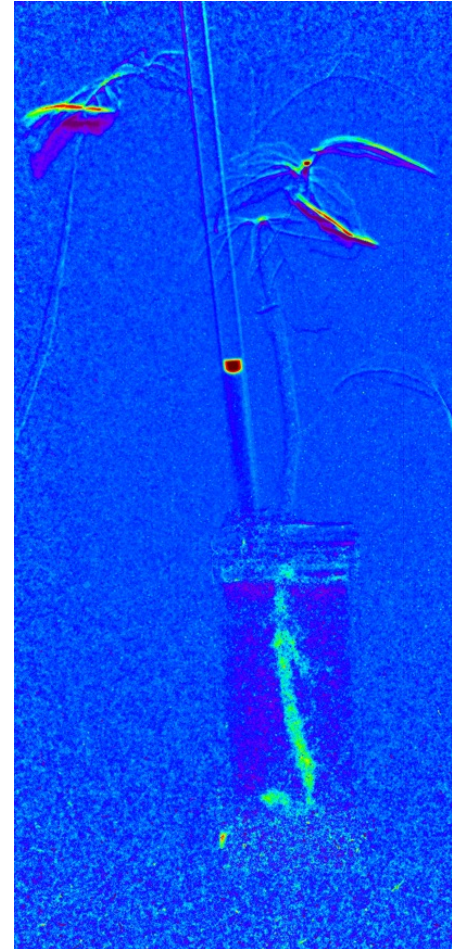
## Neutron attenuation

Attenuation coefficients with neutrons [ $\text{cm}^{-1}$ ]

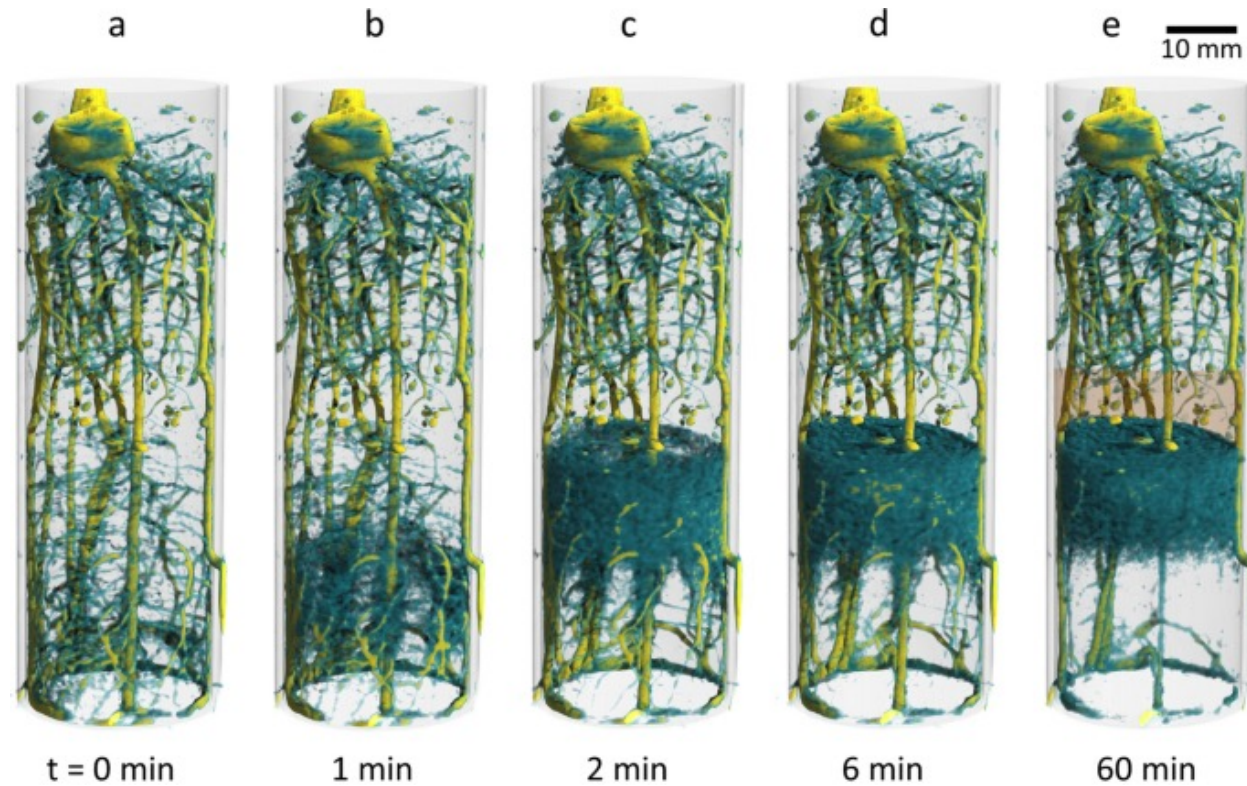
1a	2a	3b	4b	5b	6b	7b	8					1b	2b	3a	4a	5a	6a	7a	0
H 3.44																			He 0.02
Li 3.30	Be 0.79													B 101.60	C 0.56	N 0.43	O 0.17	F 0.20	Ne 0.10
Na 0.09	Mg 0.15													Al 0.10	Si 0.11	P 0.12	S 0.06	Cl 1.33	Ar 0.03
K 0.06	Ca 0.08	Sc 2.00	Ti 0.60	V 0.72	Cr 0.54	Mn 1.21	Fe 1.19	Co 3.92	Ni 2.05	Cu 1.07	Zn 0.35	Ga 0.49	Ge 0.47	As 0.67	Se 0.73	Br 0.24	Kr 0.61		
Rb 0.08	Sr 0.14	Y 0.27	Zr 0.29	Nb 0.40	Mo 0.52	Tc 1.76	Ru 0.58	Rh 10.88	Pd 0.78	Ag 4.04	Cd 115.11	In 7.58	Sn 0.21	Sb 0.30	Te 0.25	I 0.23	Xe 0.43		
Cs 0.29	Ba 0.07	La 0.52	Hf 4.99	Ta 1.49	W 1.47	Re 6.85	Os 2.24	Ir 30.46	Pt 1.46	Au 6.23	Hg 16.21	Tl 0.47	Pb 0.38	Bi 0.27	Po	At	Rn		
Fr	Ra 0.34	Ac	Rf	Ha															
*Lanthanides	Ce 0.14	Pr 0.41	Nd 1.87	Pm 5.72	Sm 171.47	Eu 94.58	Gd 1479.04	Tb 0.93	Dy 32.42	Ho 2.25	Er 5.48	Tm 3.53	Yb 1.40	Lu 2.75					
**Actinides	Th 0.59	Pa 8.46	U 0.82	Np 9.80	Pu 50.20	Am 2.86	Cm	Bk	Cf	Es	Fm	Md	No	Lr neut.					

# Water uptake in plants

- D<sub>2</sub>O as contrast agent



# Water uptake in plants in 3D



Time-resolved neutron tomography of a 13-days-old maize root system after infiltration of 4 ml deuterated water

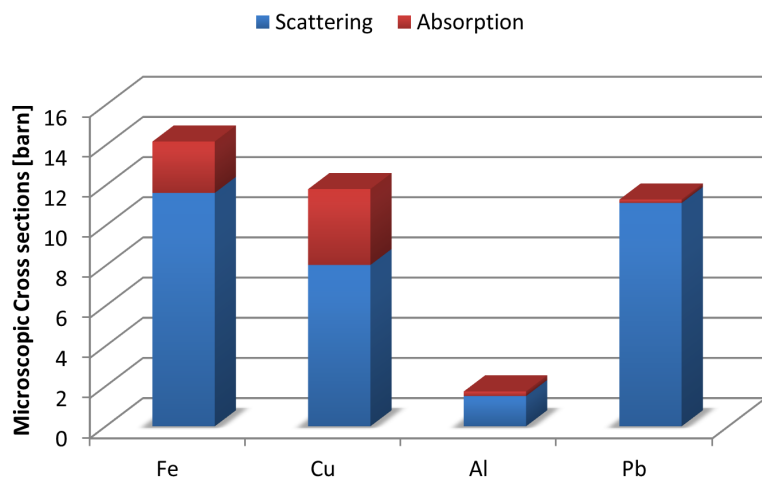
# Combining X-ray and neutron imaging

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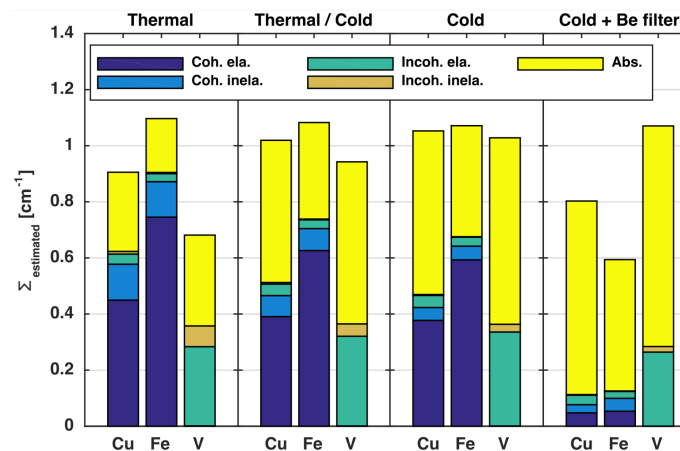
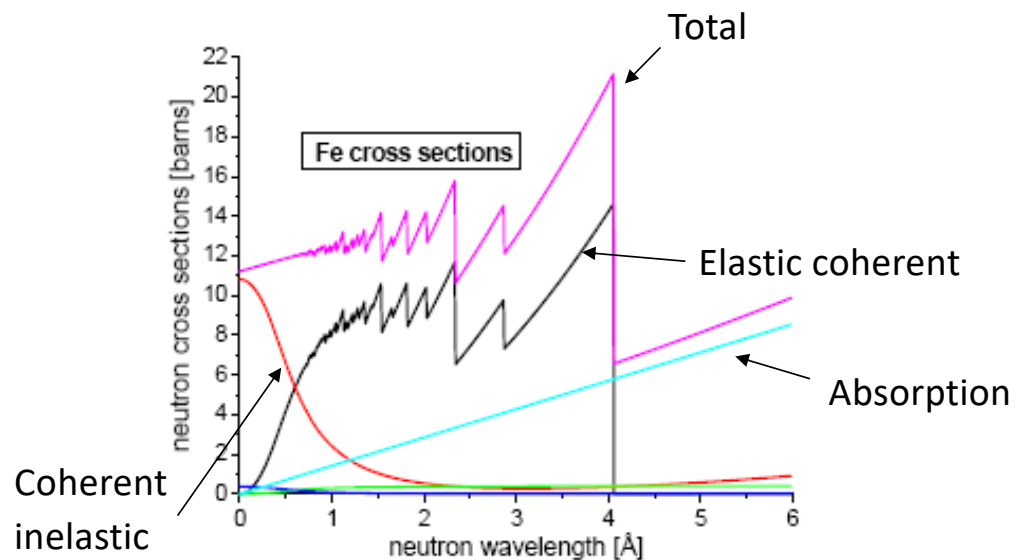


# Cross-sections

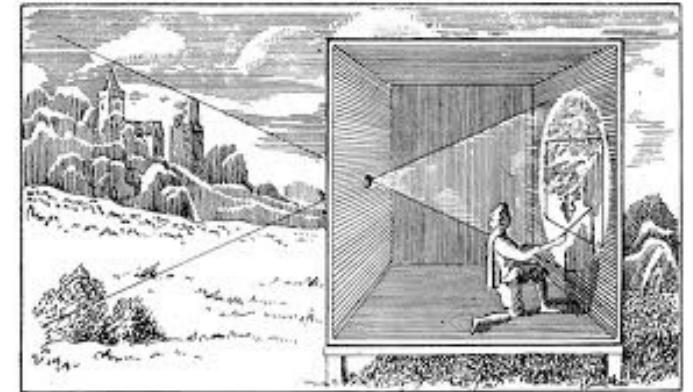
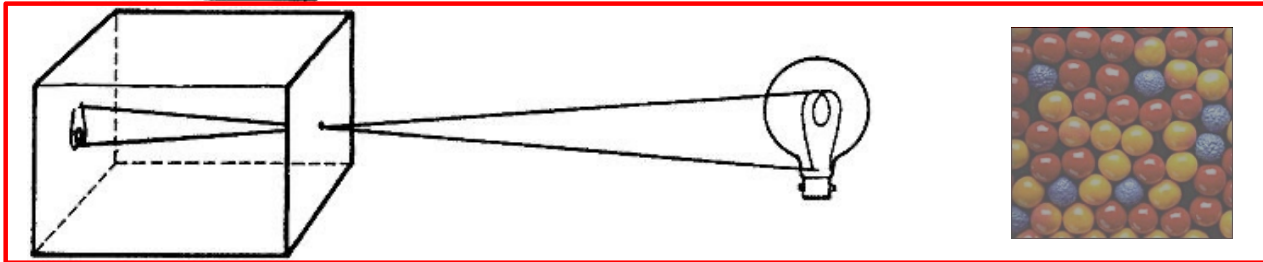
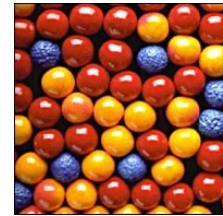
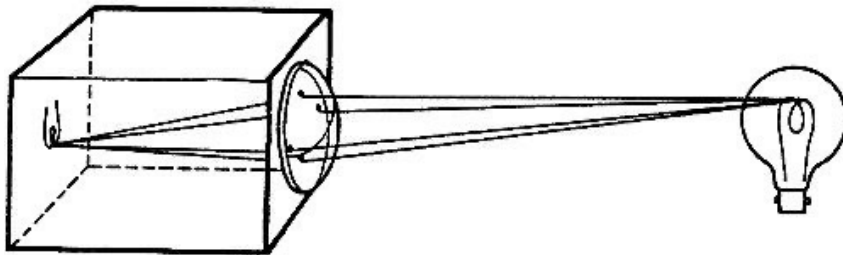
## Total neutron cross section



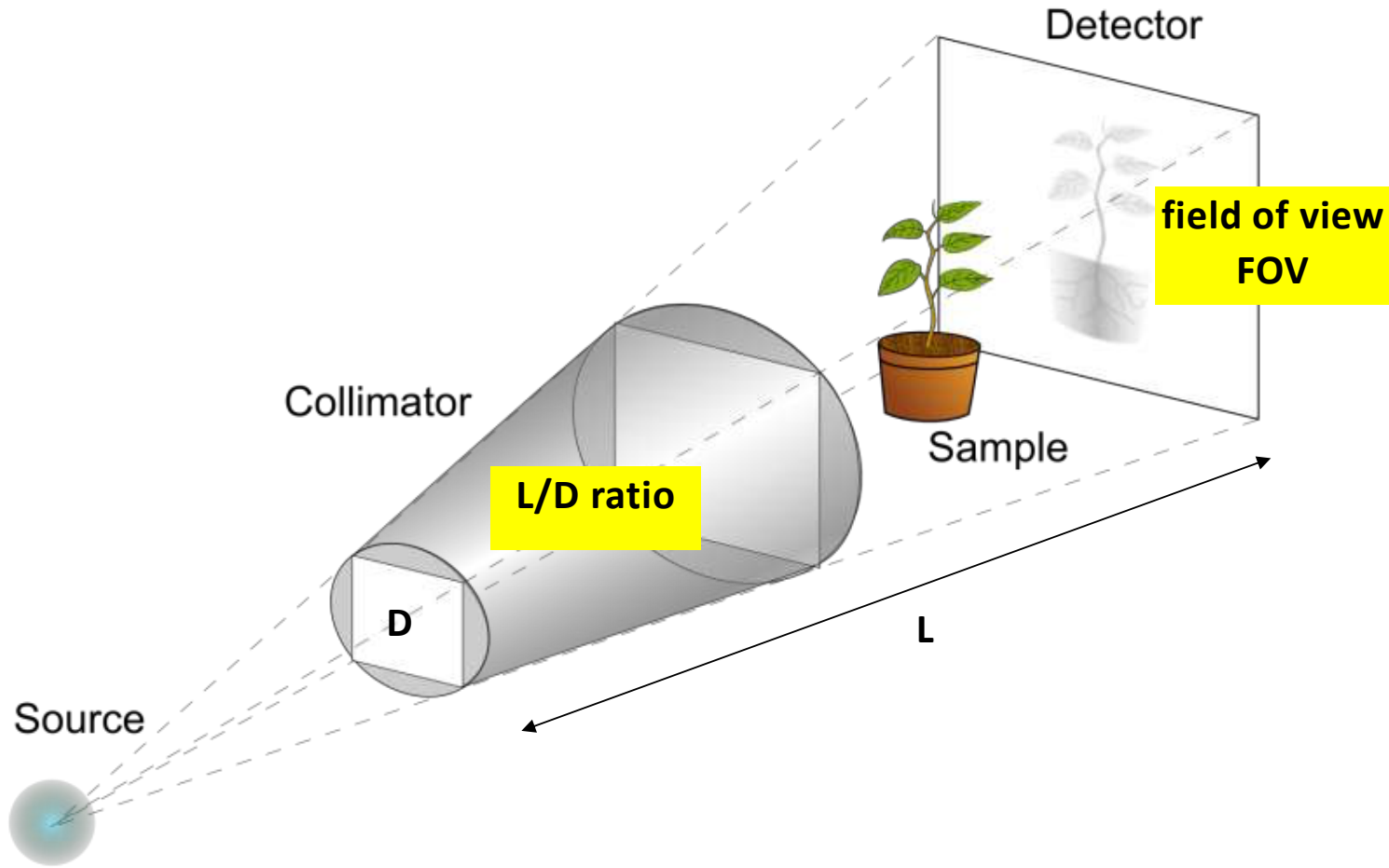
$$\sigma = \sigma_a + \sigma_s$$



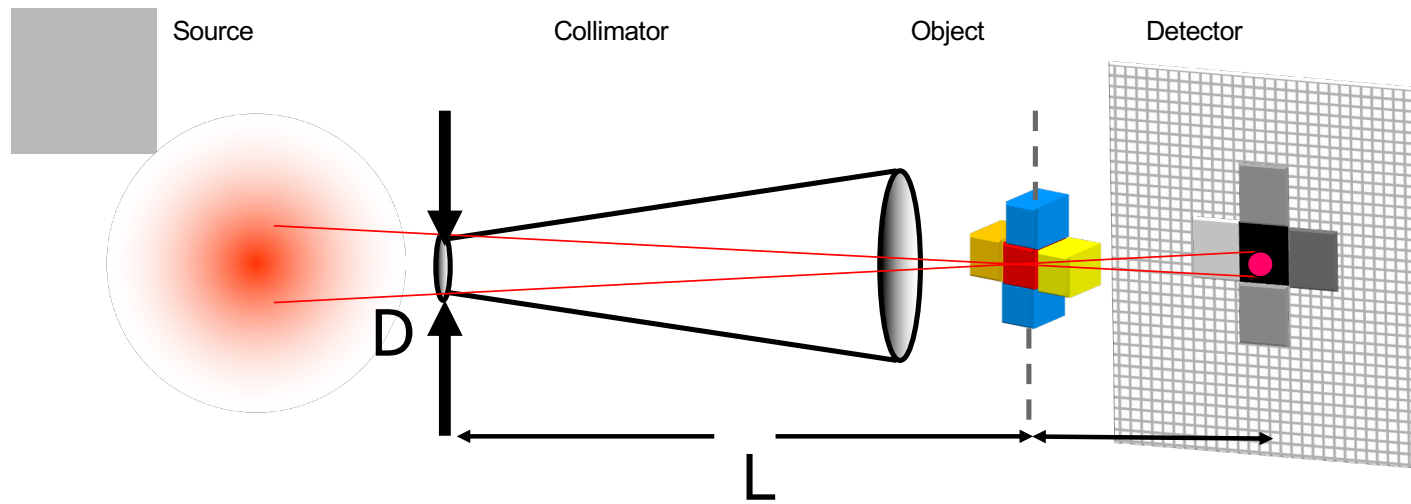
# Resolution



# Simplified setup

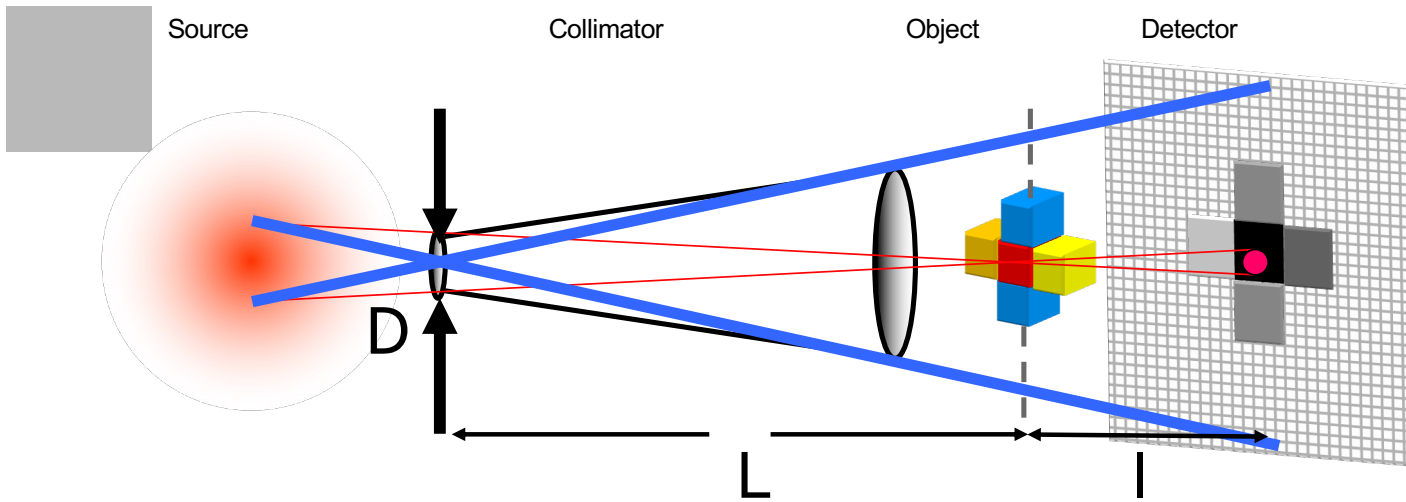


# Influence geometry



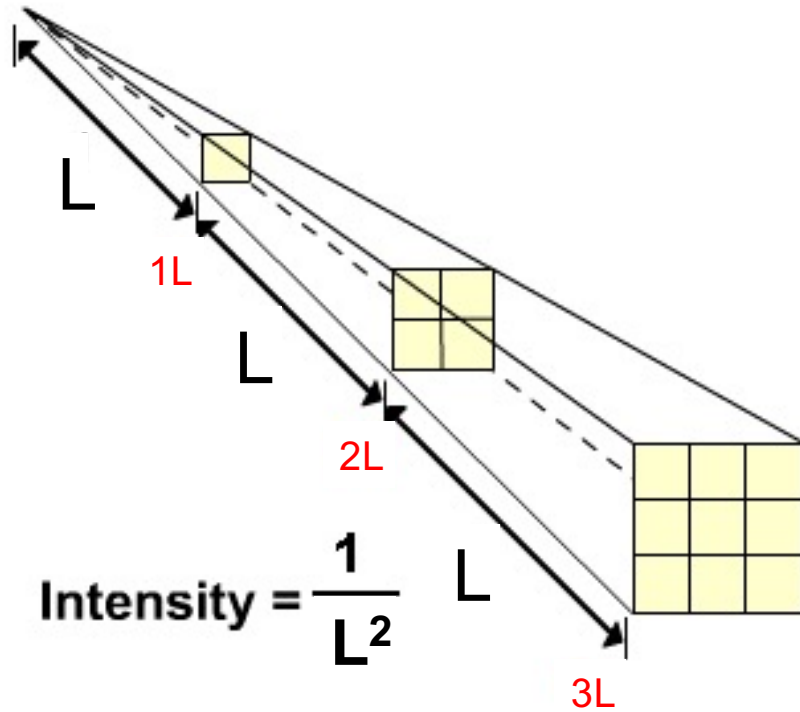
collimation ratio  $L/D$  typical: several 100

## Influence geometry



blur  $d = \frac{I}{L/D}$

## Influence geometry

flux limitations  $10^9 \text{ cm}^{-2}\text{s}^{-1}$ 

$$I=1 \quad D=1$$

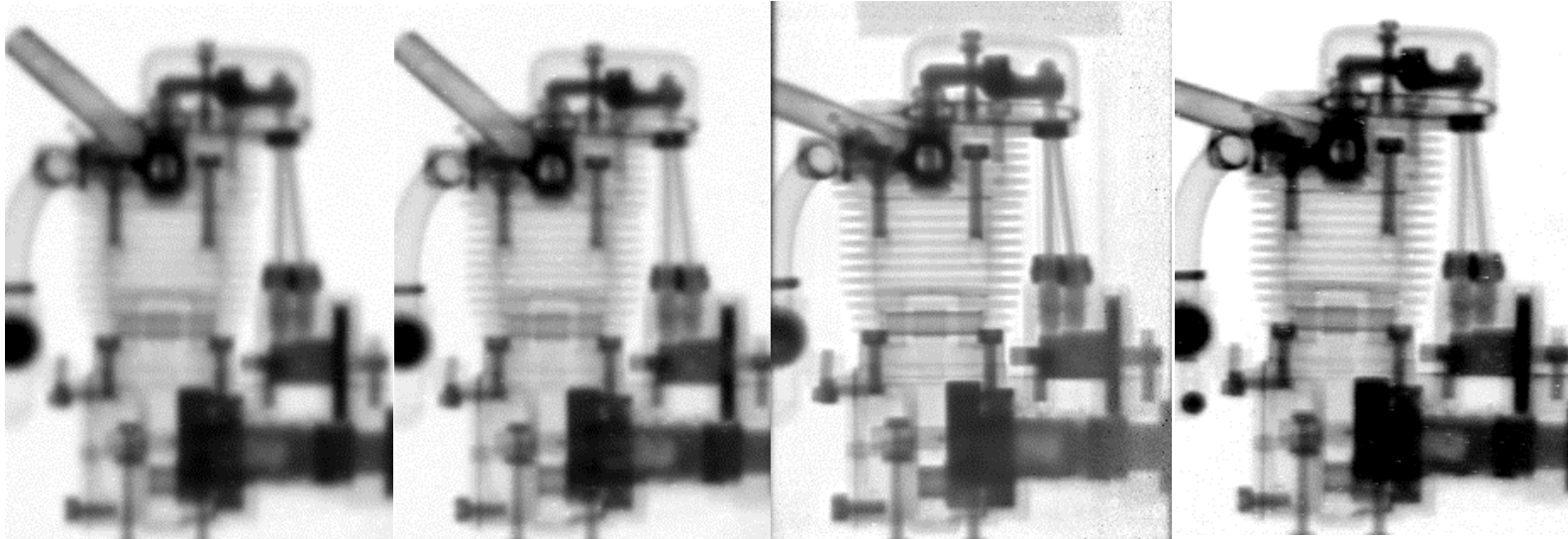
$$I=1/4 \quad D=1/2$$

$$I=1/16 \quad D=1/4$$

$$\text{Intensity} = D^2$$

blur  $d = \frac{L}{D}$

# Influence geometry



L/D=71

L/D=115

L/D=320

L/D>500.

Radiographs of a small motor taken at different beam positions  
with different L/D ratios.

# Time resolved neutron radiography

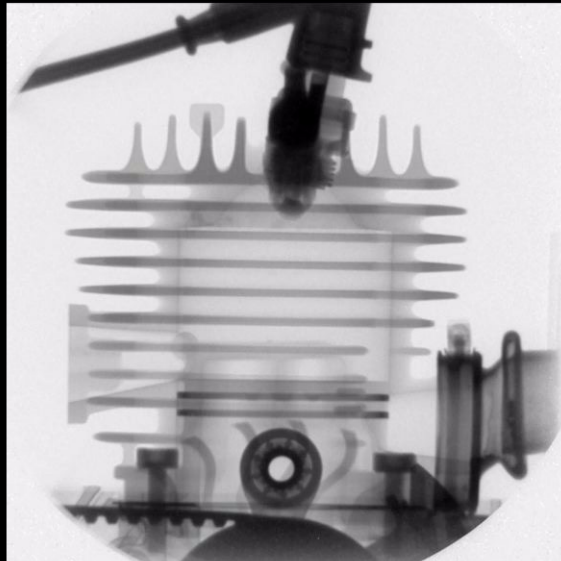


# Fast neutron imaging

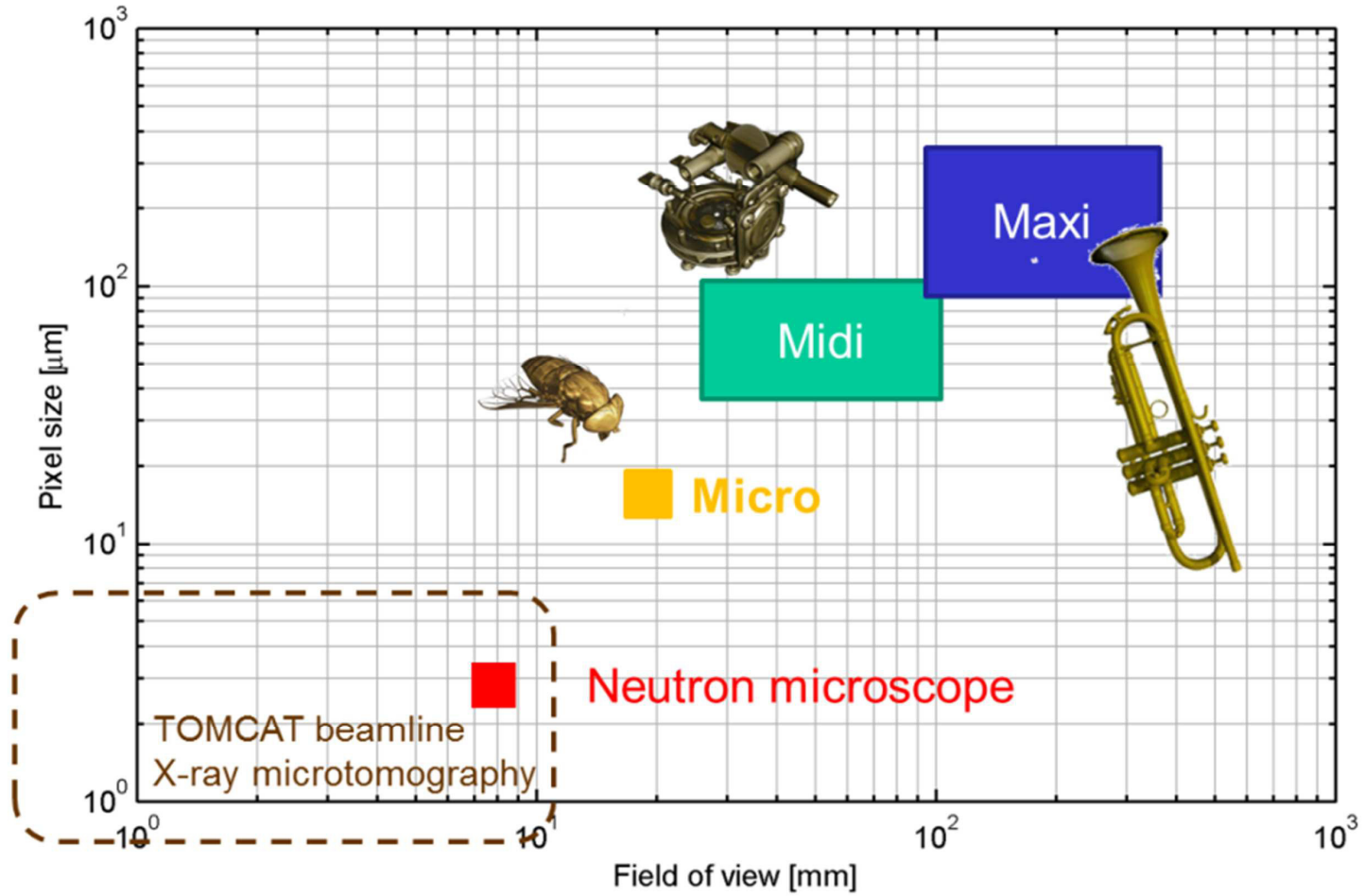
- Neutron flux is relatively low as compared to synchrotron x-ray flux. Difficult to perform fast in situ measurements.
- Except for periodical processes, here one can work in stroboscopic mode
- Advantage:
  - the number of neutrons/photons in one time window is still very low, but many exposures of the same time window of the periodic process may be accumulated on the detector before read-out, thus increasing the available intensity
- Disadvantage:
  - Only one time window of the periodic process can be recorded in one sequence, the periodic process has to be recorded in a sequence of many consecutive time window accumulations, sacrificing most neutrons.

## Dynamic Neutron Radiography

fired 64ccm two-stroke engine @ 8'000rpm  
STIHL TS 400

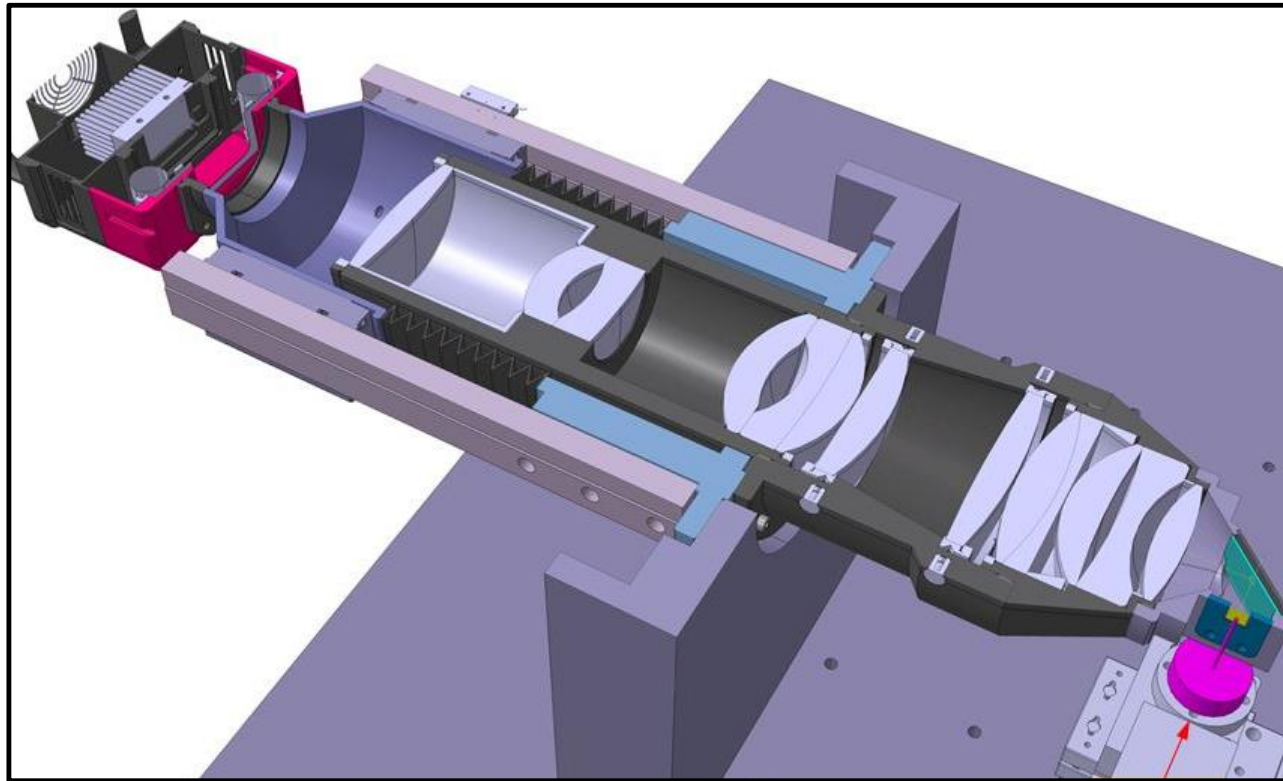


# Neutron microscope



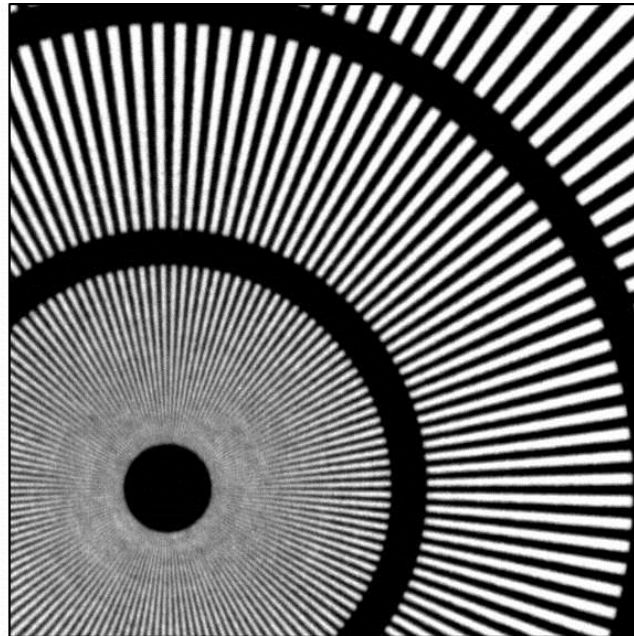
# Neutron microscope

The dedicated objective is designed for a field of view of 10 mm x 10 mm and the object distance is 60 mm. It is composed of thirteen individual lenses. The scintillator screen is based on isotopically-enriched  $^{157}\text{Gd}_2\text{O}_3$ .

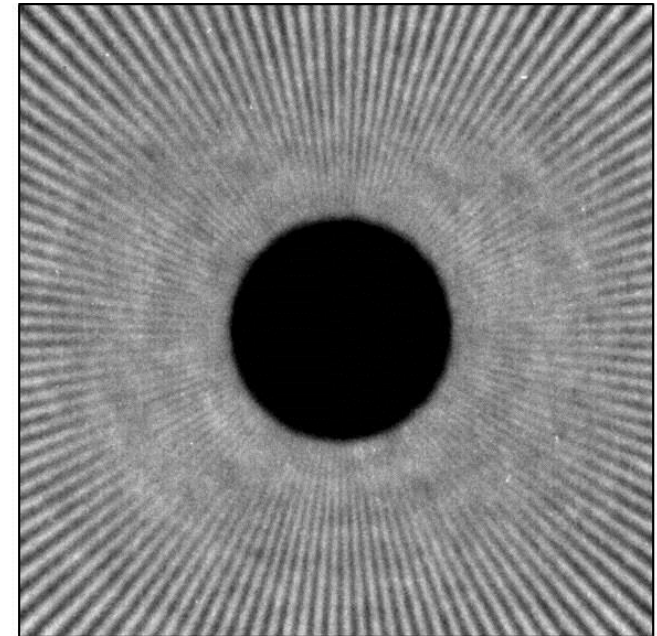


## Neutron microscope

- Siemens star
- Resolution =  $5.4\mu\text{m}$


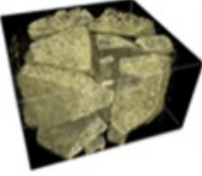
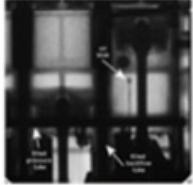

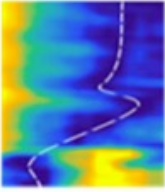
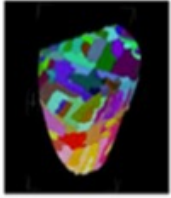
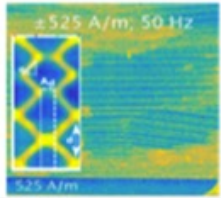

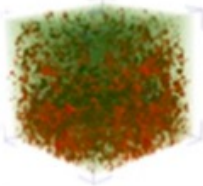
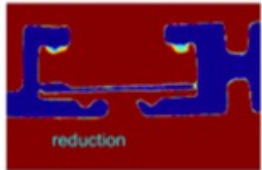

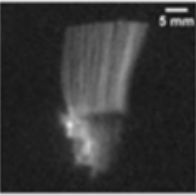
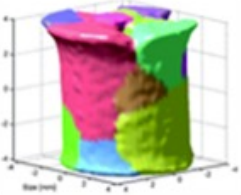
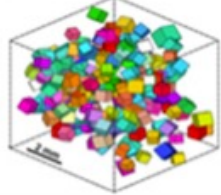


2.65 mm



1.05 mm

# Beyond attenuation contrast

	2D	3D		4D +
	spatial	spatial	spatiotemporal	spatiotemporal/ +
attenuation contrast				
dark-field contrast				
diffraction contrast				
diffractive contrast				

# Beyond attenuation contrast

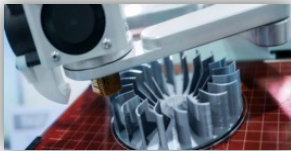
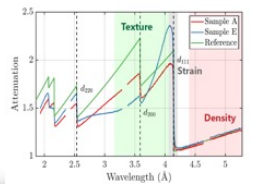
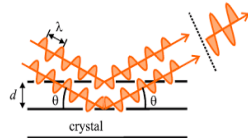
	2D	3D		4D +
	spatial	spatial	spatiotemporal	spatiotemporal/ +
diffractive contrast				
polarisation contrast				
resonance contrast				
bi-modal XN contrast				

# Imaging modalities

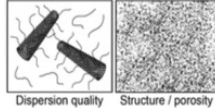
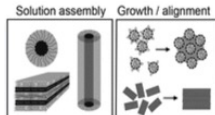
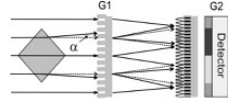
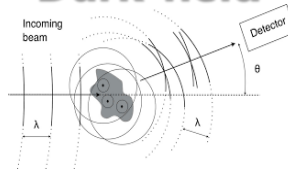
## Attenuation contrast



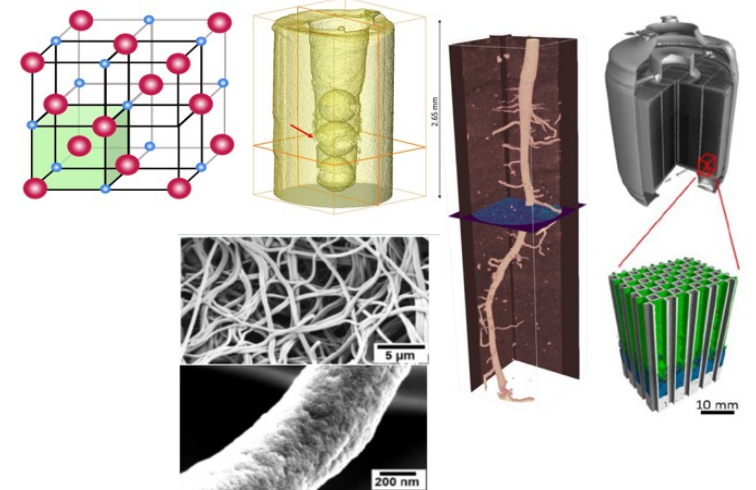
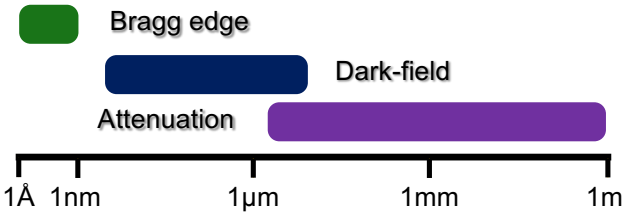
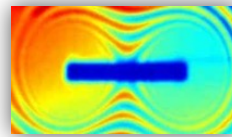
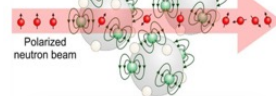
## Bragg edge



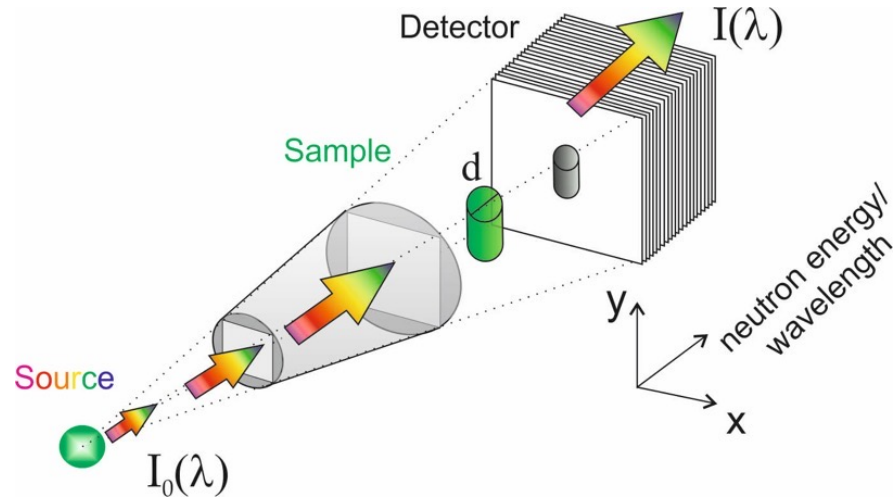
## Dark-field



## Polarized

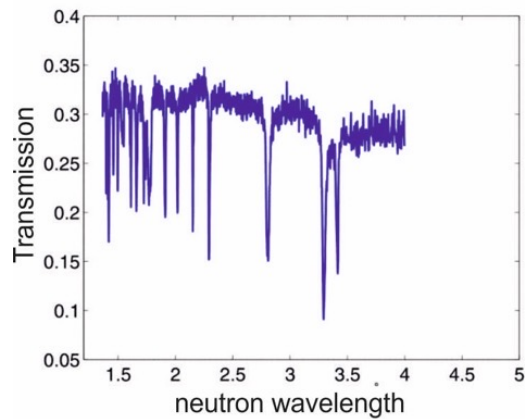


## Neutron Bragg edge imaging

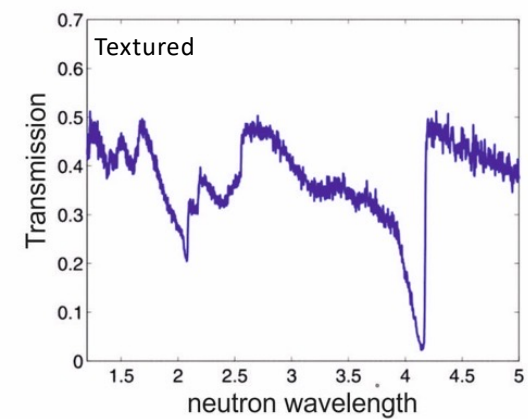
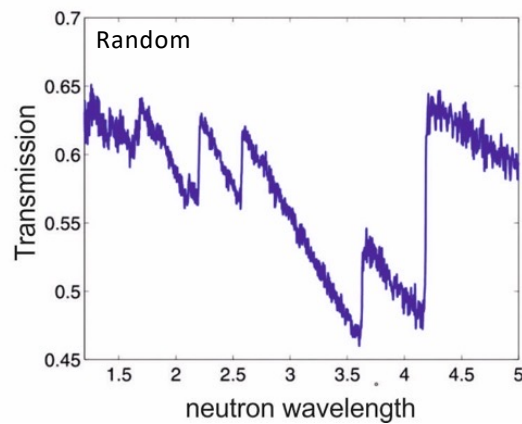


$$T(x, y, \lambda) = \frac{I(x, y, \lambda)}{I_0(x, y, \lambda)}$$

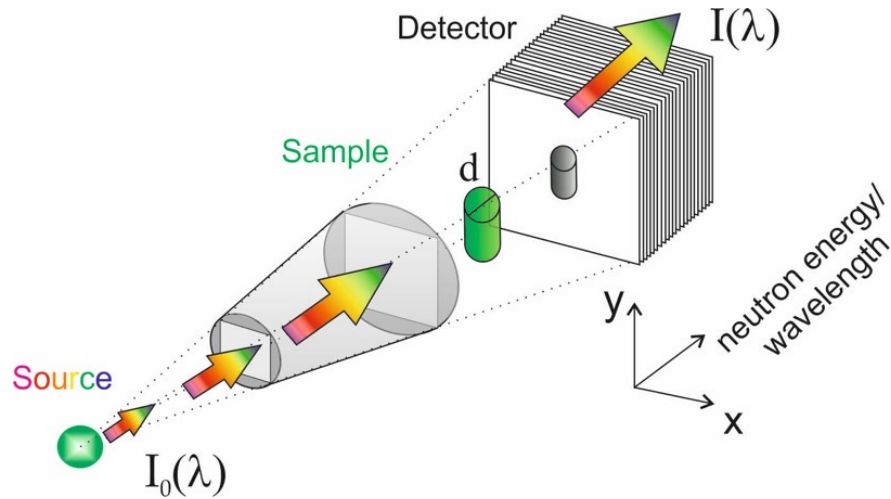
Single crystal



Polycrystalline materials



# Neutron Bragg edge imaging



$$T(x, y, \lambda) = \frac{I(x, y, \lambda)}{I_0(x, y, \lambda)}$$

The transmission spectra contain information on the neutrons that didn't interact with the sample



All processes that remove neutrons from the incident beam

Bragg reflections



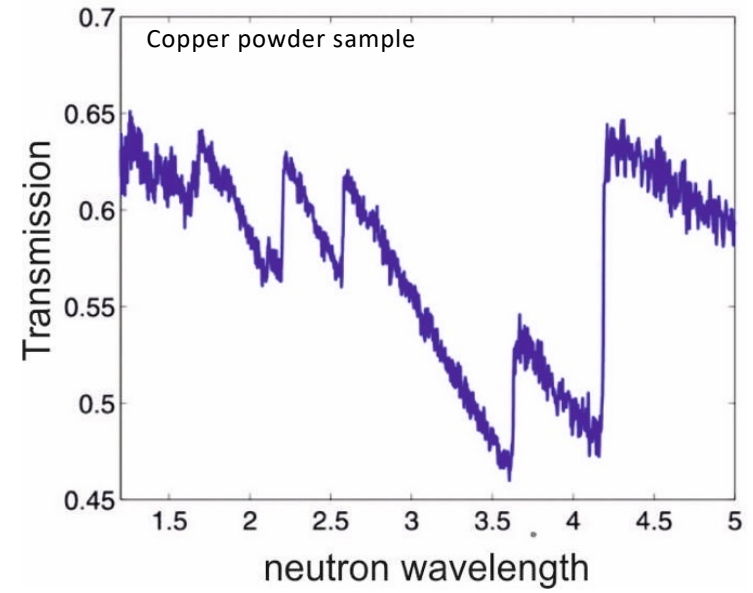
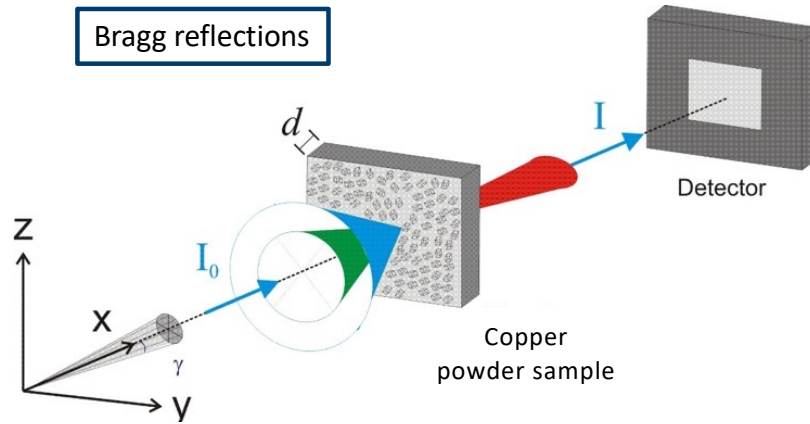
Neutrons reflected on the crystal planes

Thermal diffuse scattering

Absorption

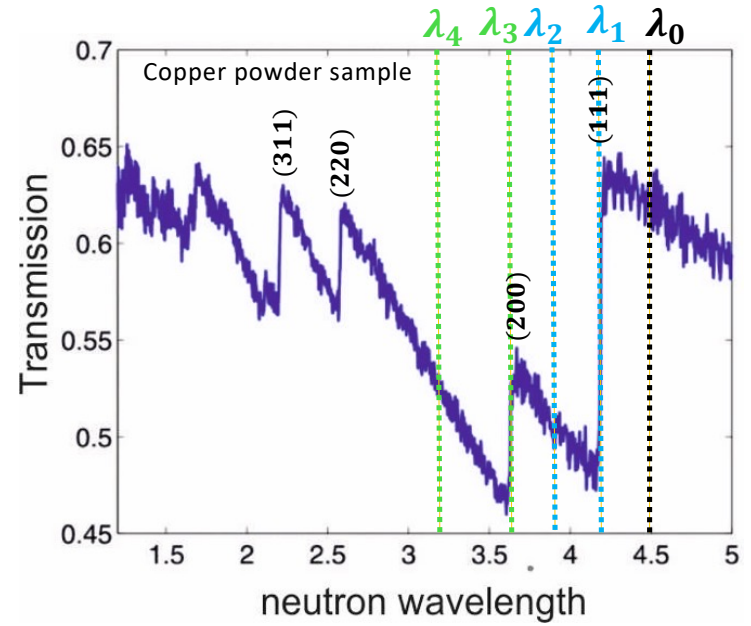
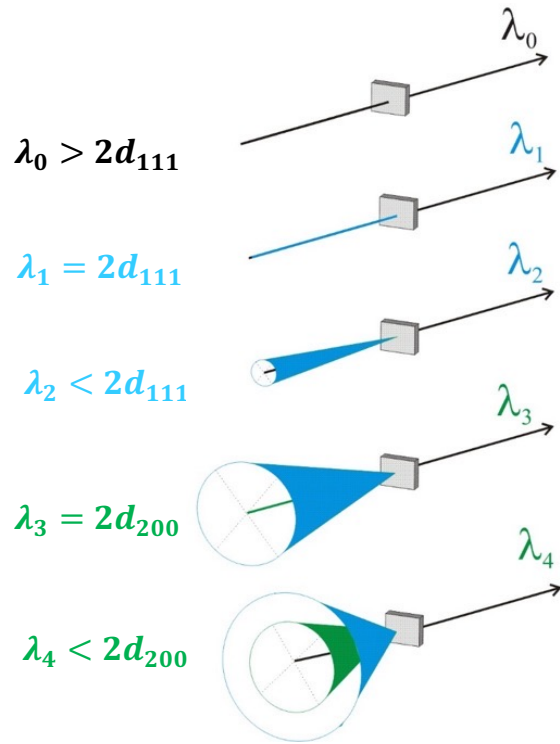
smooth dependences on neutron wavelength

## Neutron Bragg edge imaging



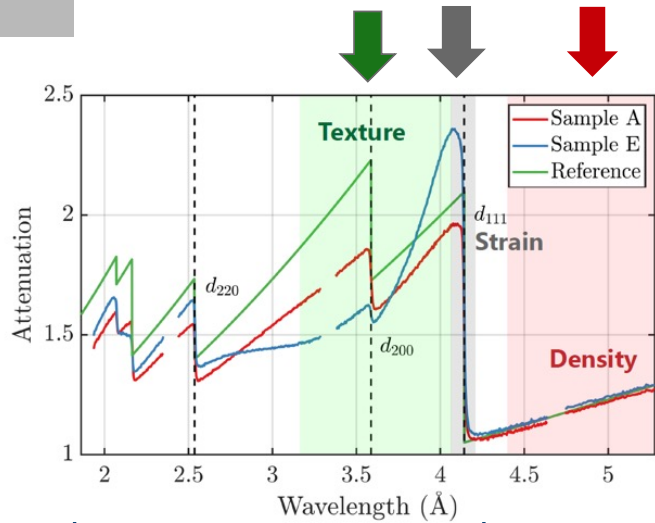
# Neutron Bragg edge imaging

Bragg reflections

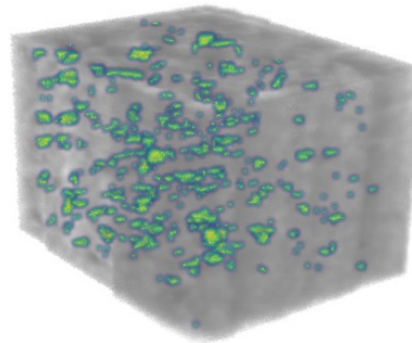


# Neutron Bragg edge imaging

$$\mu(x, y, \lambda) = -\frac{1}{l} \log \left( \frac{I(x, y, \lambda)}{I_0(x, y, \lambda)} \right)$$

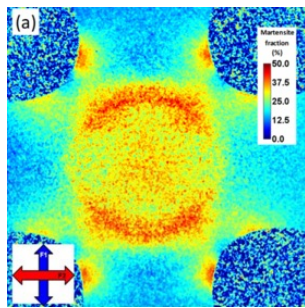


Bulk density

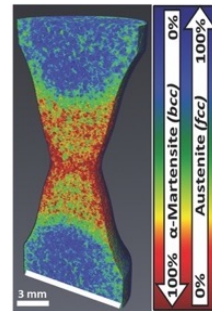


Busi, M., et al. *Ph. Rev. Mat.* (2022)

Crystallographic Phase Transformations

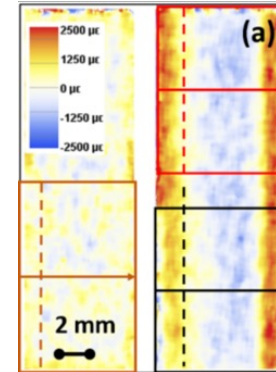


Poladitis, E., et al. *Materials* (2020)



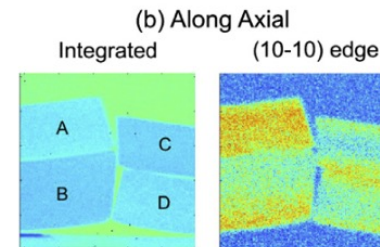
Woracek, R., et al. *Advanced Materials* (2014)

Residual Strain



M. Morgano et al., *Add. Man.* (2020)

Crystallographic Texture

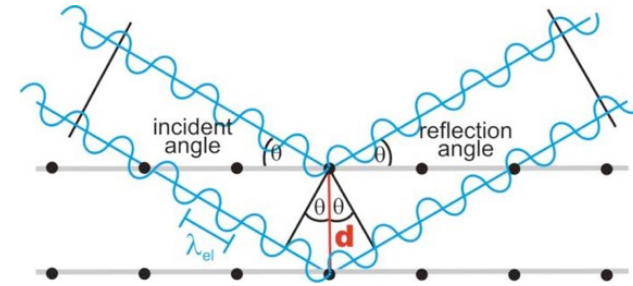


Santisteban., et al. *Journal of Nuclear Materials* (2012)

# Lattice strain mapping

- Bragg's law:**

$$\lambda_{hkl} = 2d_{hkl} \sin(\theta)$$



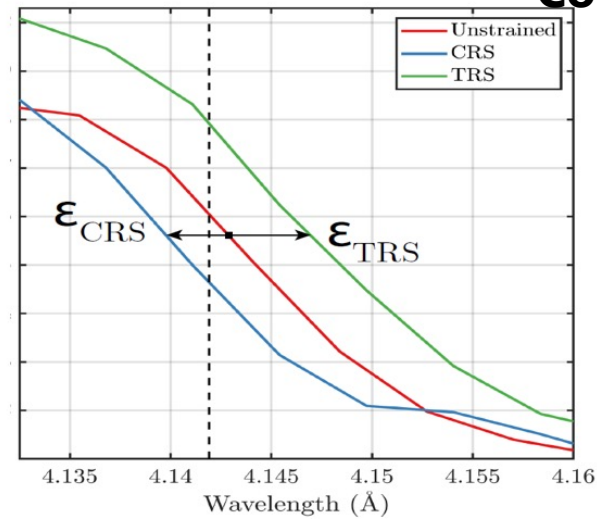
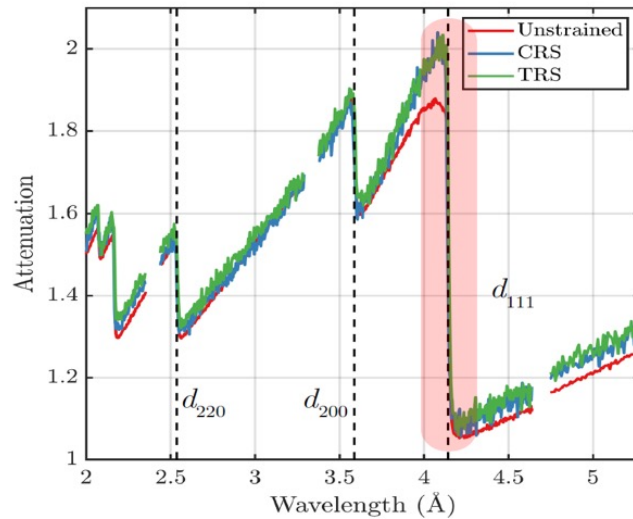
Relates Bragg edge wavelength to lattice spacing

- Lattice strain:**

$$\epsilon_{hkl} = \frac{d_{hkl} - d_{hkl}^0}{d_{hkl}^0}$$

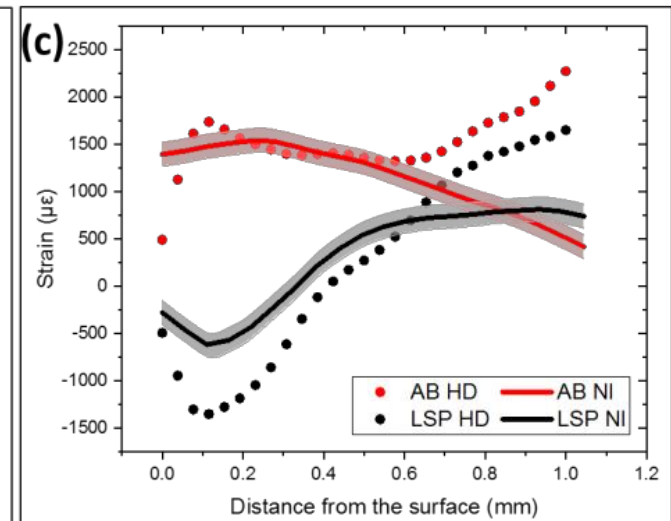
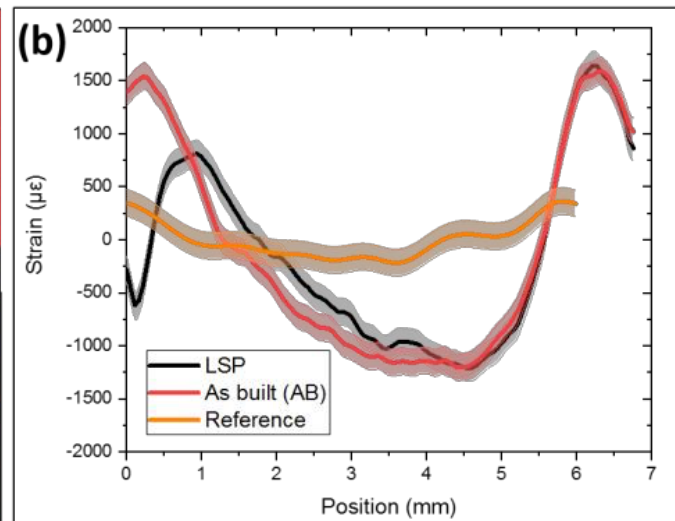
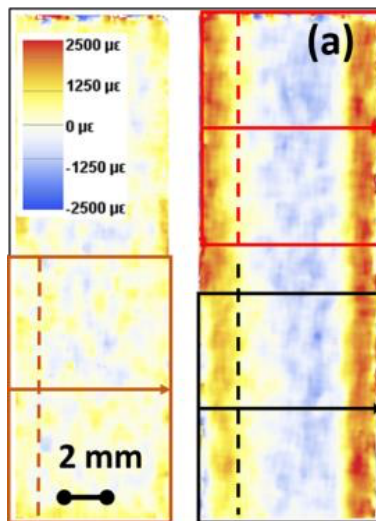
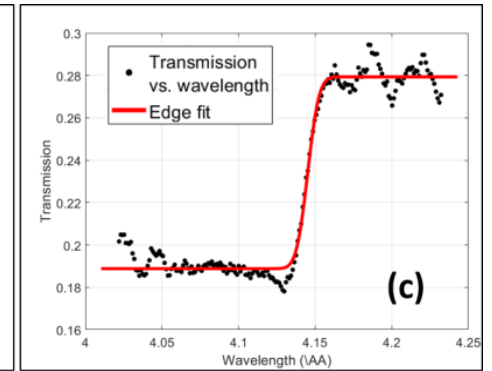
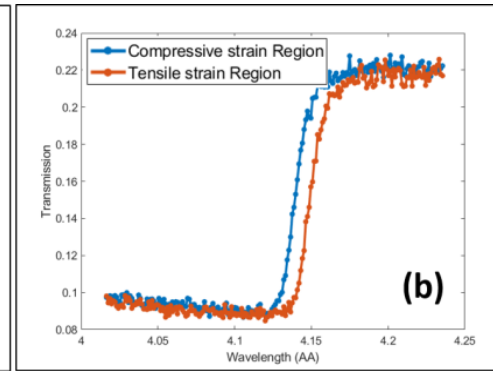
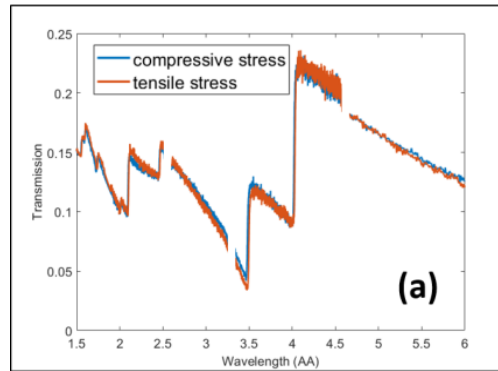
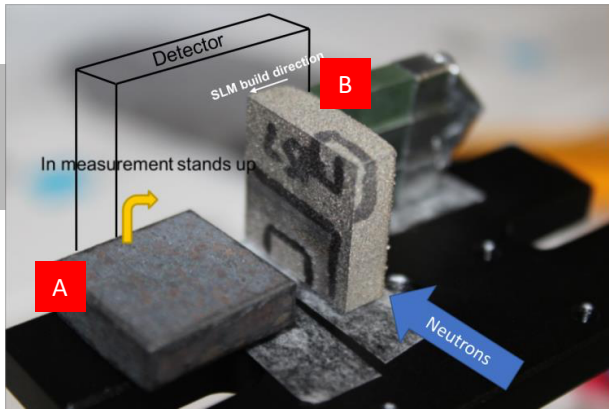
- Tensile (+)**

- Compressive (-)**



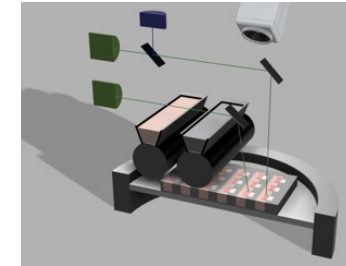
Busi, M., et al. *Scientific Reports* (2021)

# Strain imaging in AM 316L

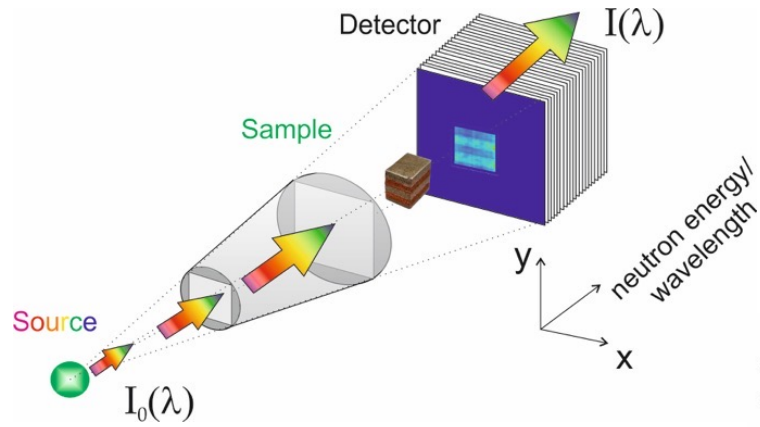


# Multi-material LPBF

CuCrZr-316L layered specimens



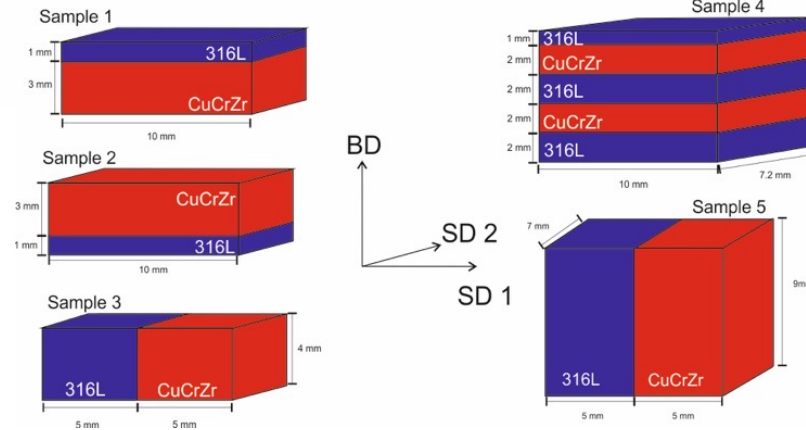
ETH zürich



Interface

Crystallographic texture

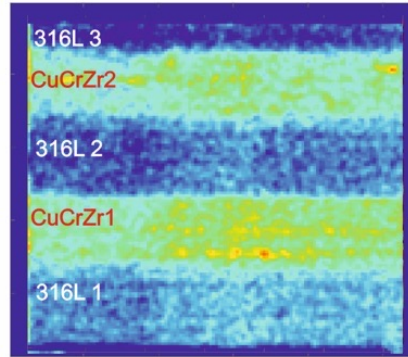
Residual stresses



# Texture characterization

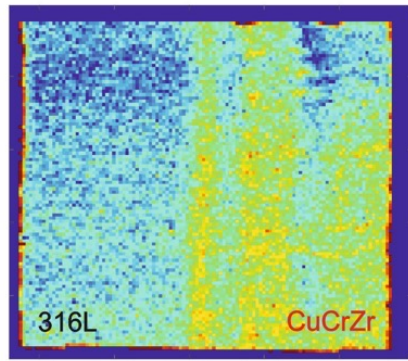
Bragg Edge Imaging at BOA

Sample 4



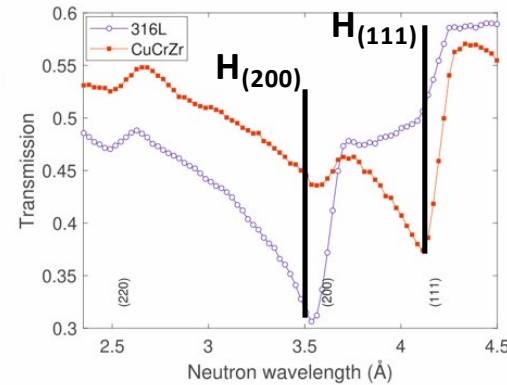
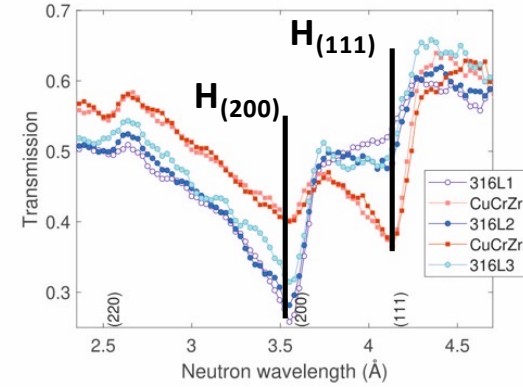
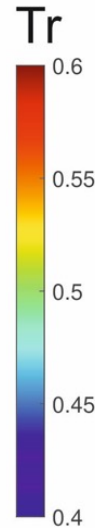
BD

Sample 5



SD

1 2 3 4 5 6 7 8 9 10  
mm



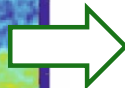
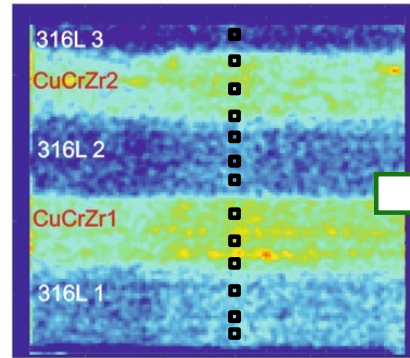
316L ⇒ Strong (200) texture along TD

Cu ⇒ Random texture along TD

# Texture characterization

Bragg Edge Imaging  
at BOA

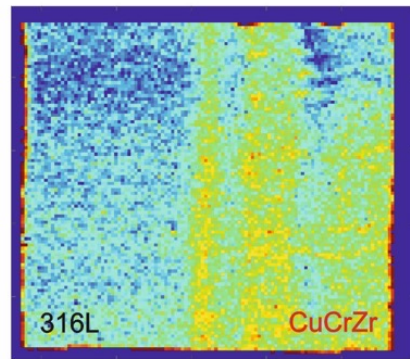
Sample 4



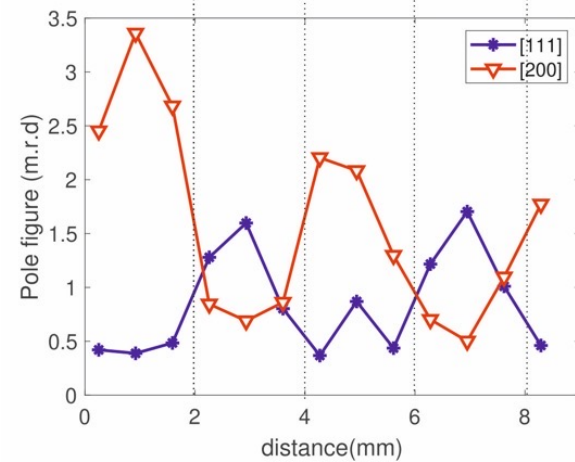
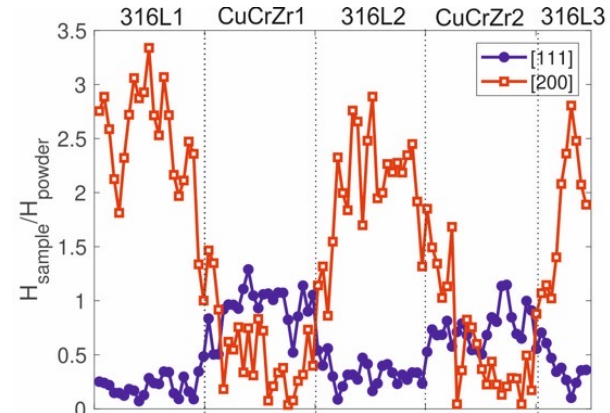
BD



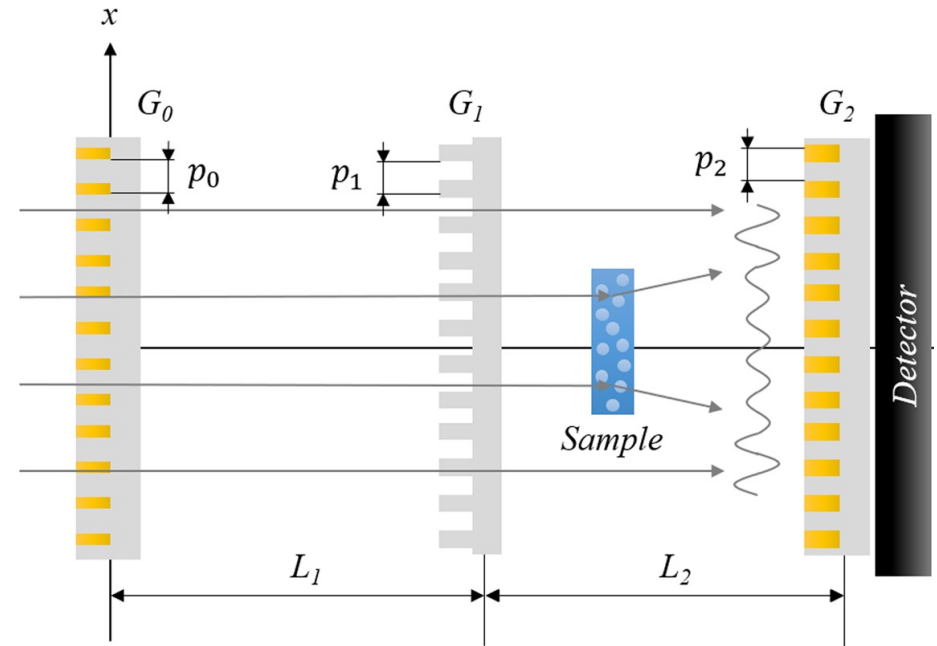
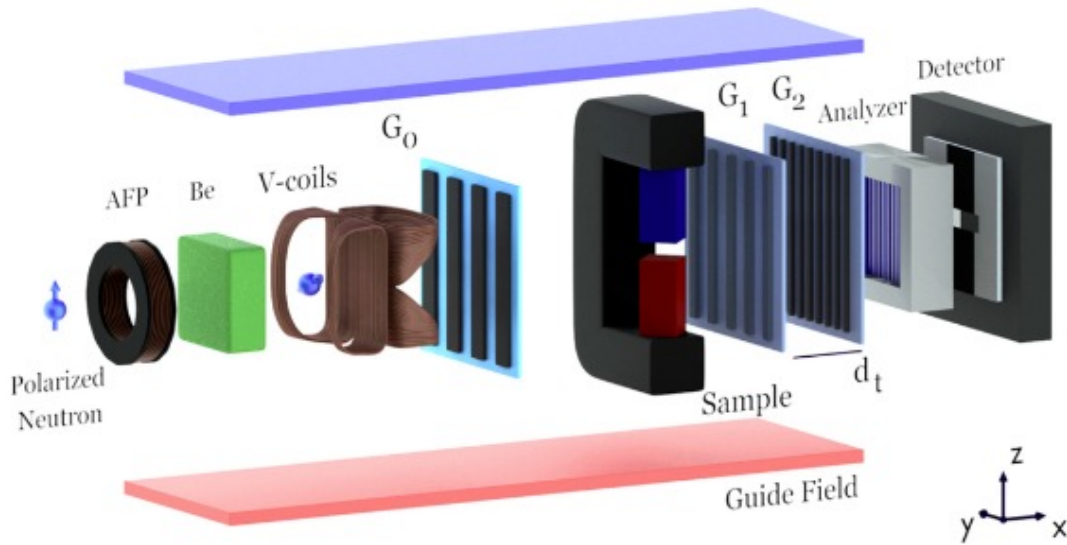
Sample 5



SD



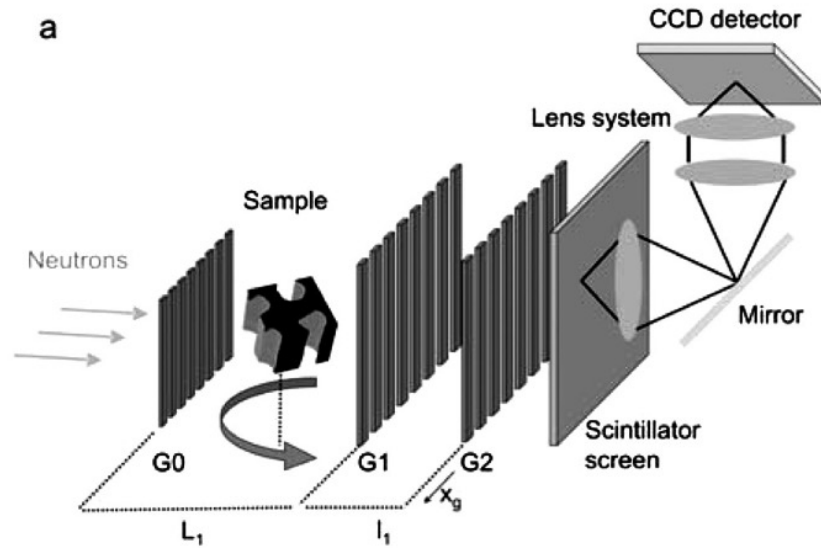
# Neutron Grating Interferometry (NGI)



- G0: source grating
- G1: phase grating
- G2: analyser absorption grating

# Neutron Grating Interferometry (NGI)

Strobl, M., et al. *P.R.L.* (2008)



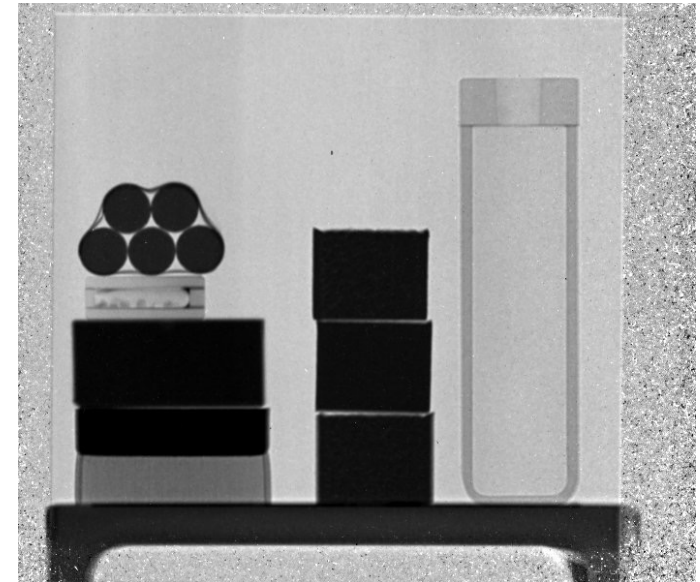
Refractive index:

$$n = \delta + i\beta$$

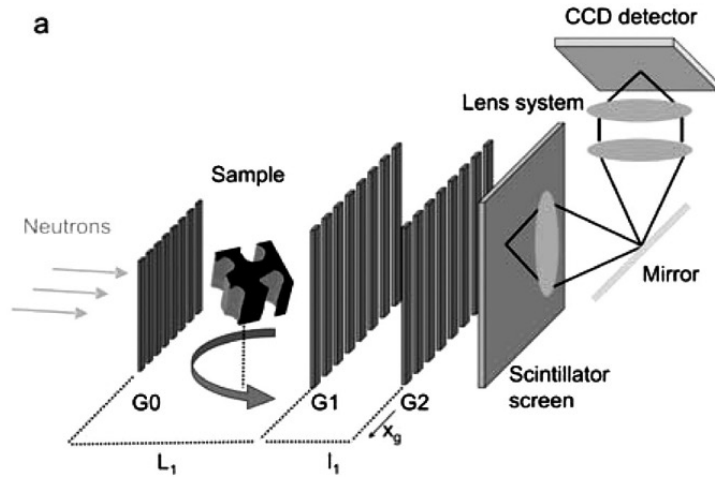
Measure simultaneously:

- Transmission (T)  $\propto$  attenuation  $\beta$

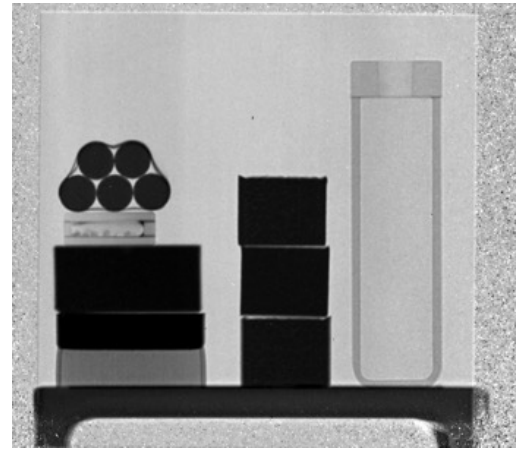
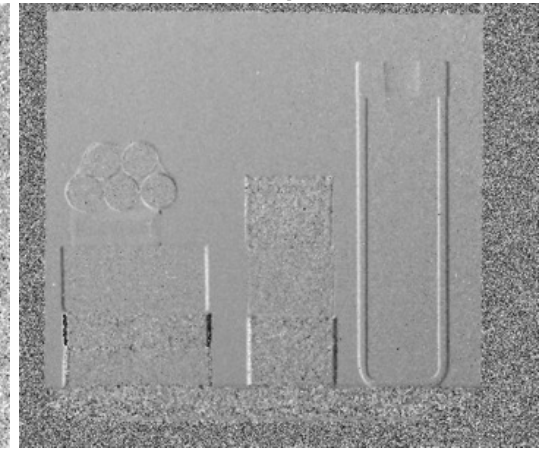
Transmission



## Neutron Grating Interferometry (NGI)



Transmission

Differential phase ( $\delta_x$ )

Refractive index:

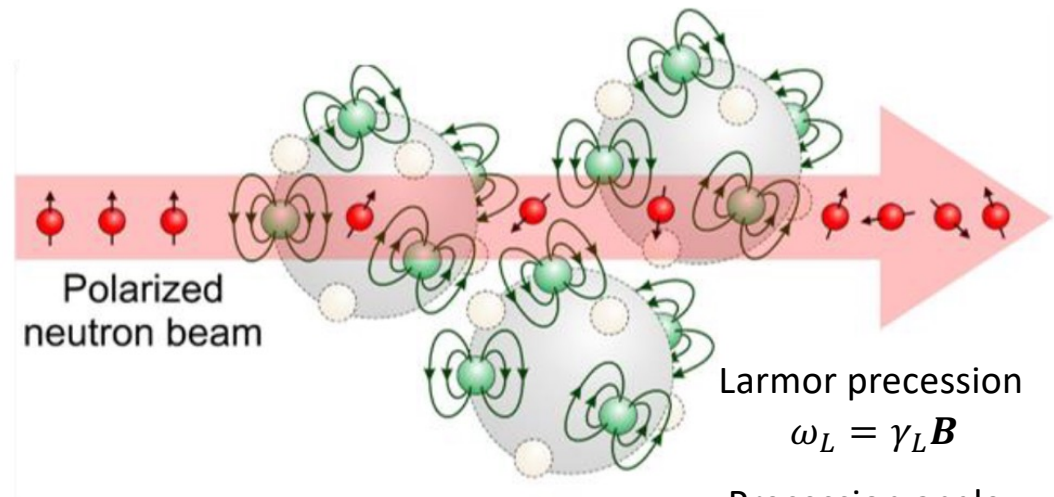
$$n = \delta + i\beta$$

Measure simultaneously:

- Transmission (T)  $\propto$  attenuation  $\beta$
- Differential phase (DP)  $\propto$  phase  $\delta$

# Imaging with polarized neutrons

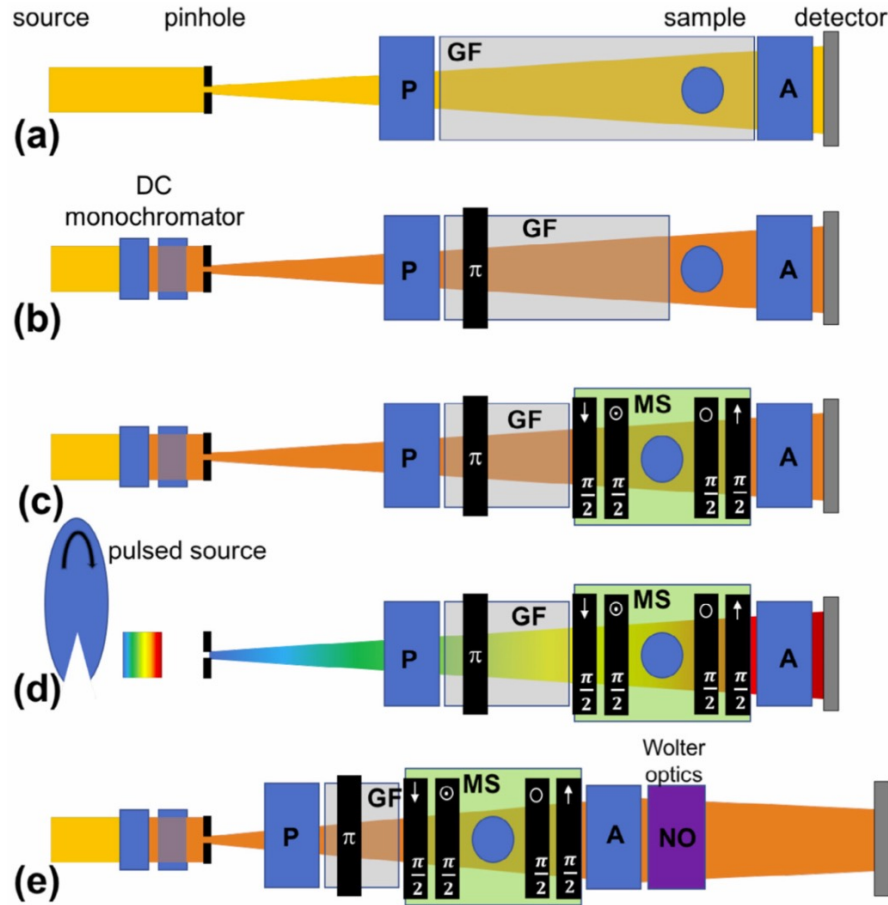
- **Neutron:**
  - Spin  $1/2$
  - Magnetic moment  $\mu$



Precession angle:

$$\phi = \frac{\gamma_L}{v} \int_{path} B ds$$

# Imaging with polarized neutrons



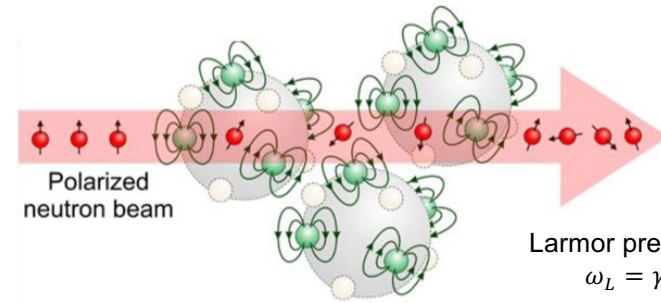
Depolarization imaging with white beam

Depolarization imaging with monochromatic beam

polarimetric neutron imaging  
probing the full depolarization matrix

# Imaging with polarized neutrons

- **Neutron:**
  - Spin  $1/2$
  - Magnetic moment  $\mu$

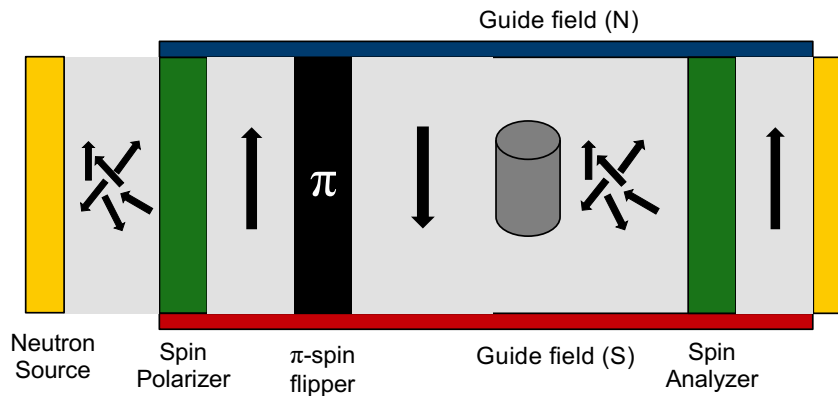


Larmor precession  
 $\omega_L = \gamma_L \mathbf{B}$

Precession angle:

$$\phi = \frac{\gamma_L}{v} \int_{path} B ds$$

- **Instrumentation:**



2D  
Imaging  
Detector

$$I = I_{\uparrow} + I_{\downarrow}$$

$$P = \frac{I_{\uparrow} - I_{\downarrow}}{I_{\uparrow} + I_{\downarrow}}$$

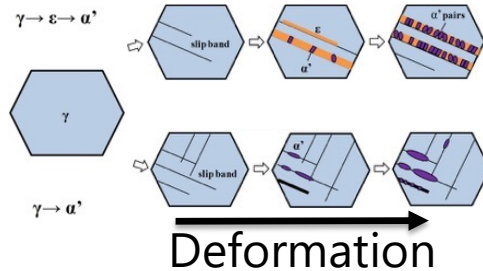
$$T = \frac{I}{I_0}$$

$$D = \frac{P}{P_0}$$

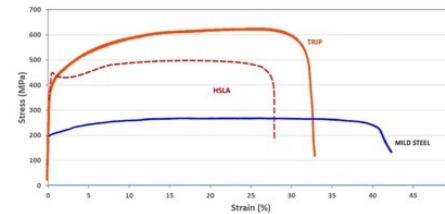
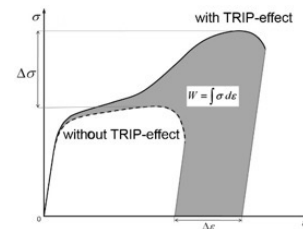
ToF-chopper and additional spin-flippers can be added

# TRIP effect: martensitic phase transformation

TRIP effect: martensite transformation upon deformation



Martensite: **ferromagnetic**



TRIP effect leads to work hardening increasing alloy's:

- **strength**
- **ductility**

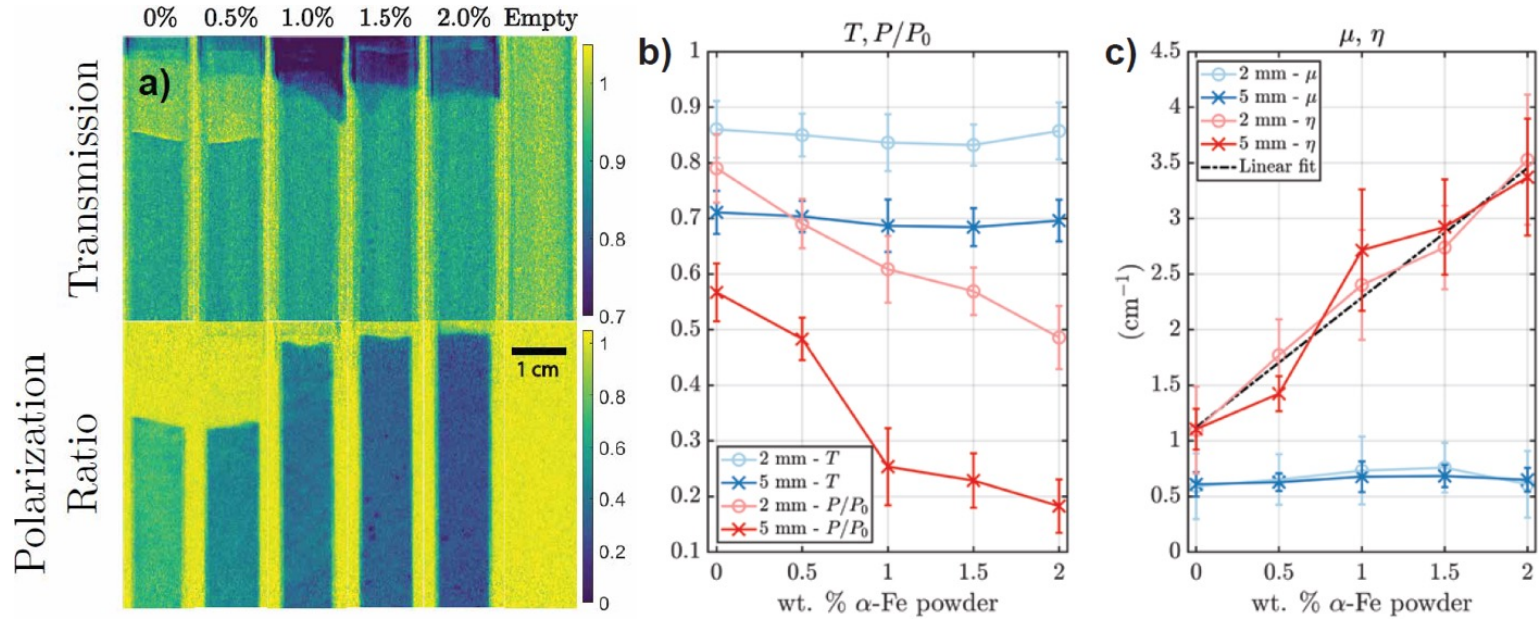
Locally tailor the crystallographic **texture**, in order to **enhance** or **suppress** local transformations according to the requirements of a component.

Build complex samples with local varying material properties and thus **superior performance**

# Method validation with BCC/FCC powder mixtures

$$\mu = -\frac{1}{t} \log\left(\frac{I}{I_0}\right)$$

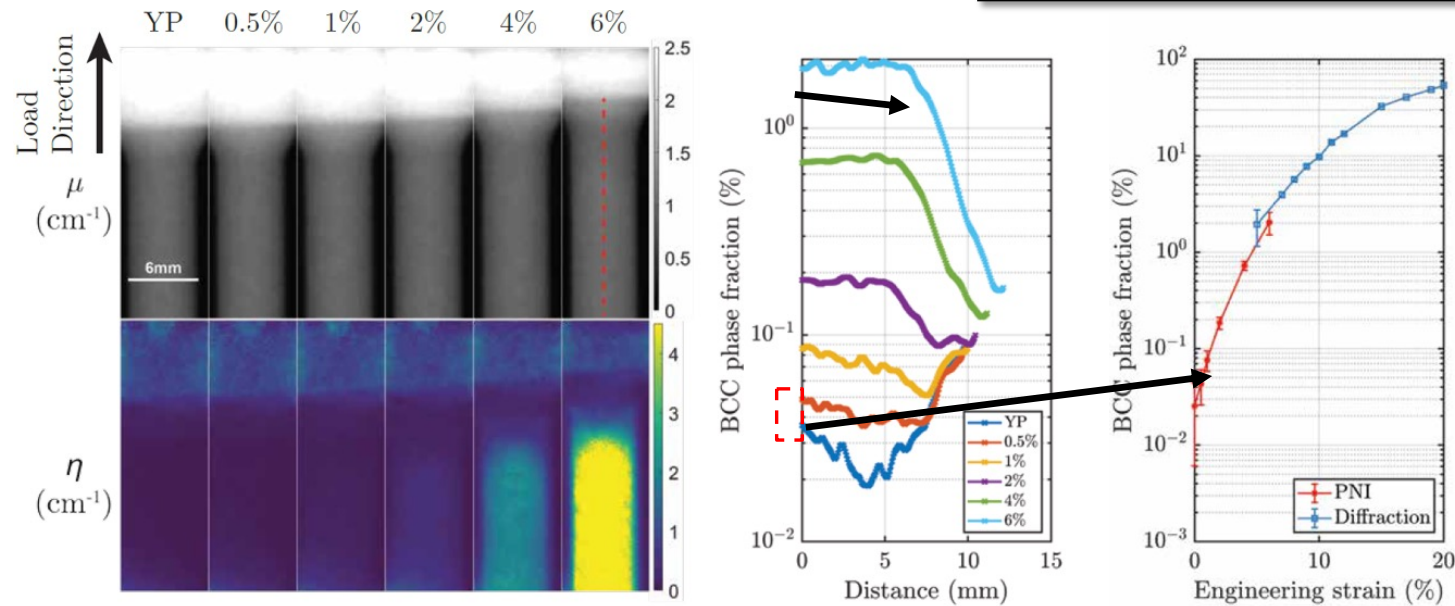
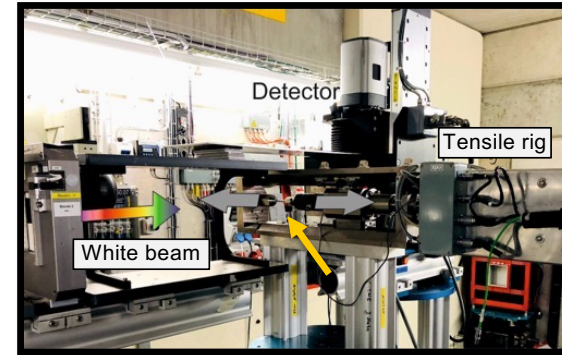
$$\eta = -\frac{1}{t} \log\left(\frac{P}{P_0}\right)$$



Validation of linear attenuation and depolarization coefficient for **quantitative martensite phase fraction determination**

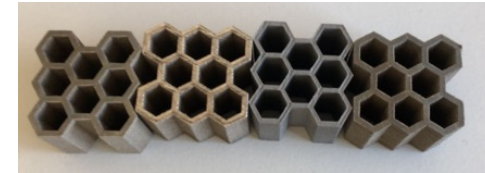
# In-situ tensile test

**Short exposures** made it possible to carry out **in-situ** measurements with a uniaxial **tensile rig**

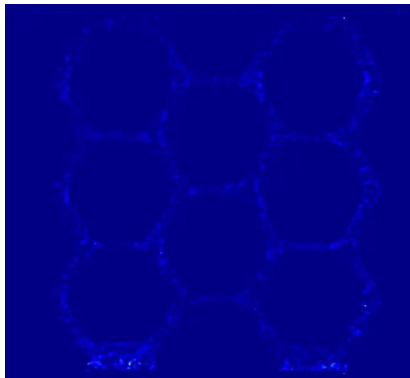


# Shape Memory Alloys

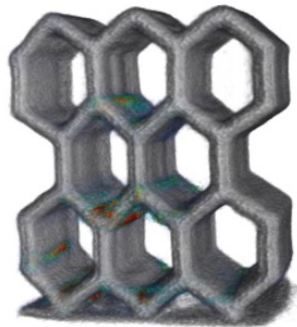
- FeMnSi SMAs for compression energy absorption
  - Upon compression the lattice deforms
  - Heat treatment is applied for shape recovery
  - Formation of martensite is detrimental to shape recovery



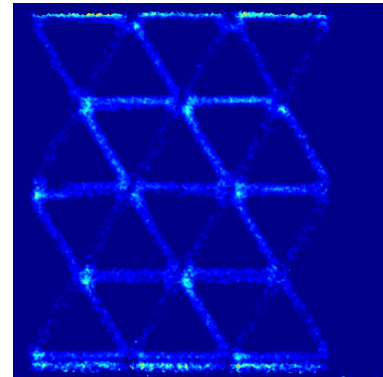
Time-resolved\*  
Radiography



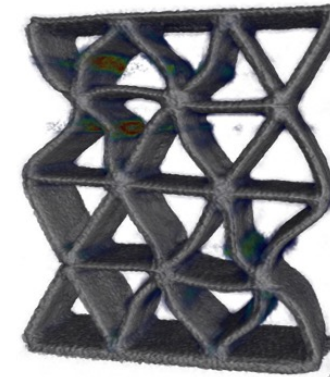
Tomography



Time-resolved\*  
Radiography



\*20 seconds per  
frame  
Tomography



Results match well finite element analysis (FEA) simulations

- Advances in neutron imaging, Materials Today 21, 6252 (2018)
- Detailed talk on neutron tomography: [https://www.youtube.com/watch?v=s95mKjIKm\\_c](https://www.youtube.com/watch?v=s95mKjIKm_c)
- Introduction talk: <https://www.youtube.com/watch?v=tyWTzrnRH9U>