

# Legged Robots: Practice Sessions

Week 2

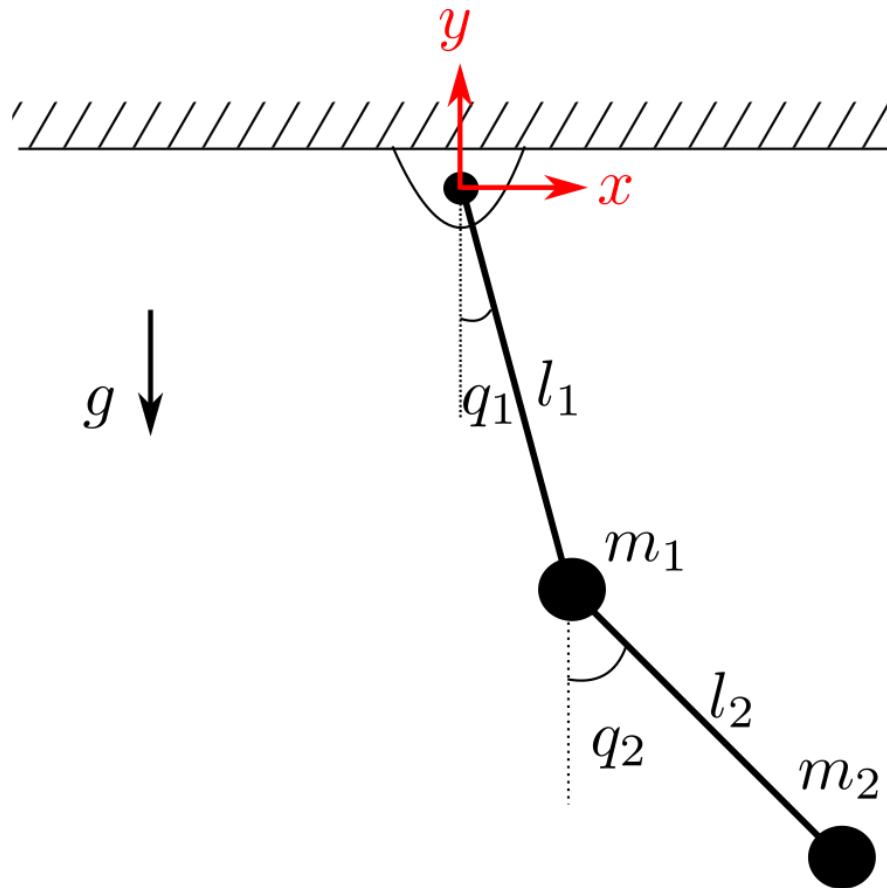
# Updates

- Instructions for virtual environment installation and tutorials have been added on Gitlab: <https://gitlab.epfl.ch/lgevers/lr-practicals>
- Solutions for the practicals will be released by the end of **Week 3**

# W1-3 Fundamentals

- Part 1: Double pendulum kinematics and dynamics
- **Part 2: Jacobian (Cartesian PD + Force Control)**
- Part 3: Inverse Kinematics (compare with force control)
- Part 4: Single-leg hopping

# Recall: Double Pendulum Forward Kinematics



## Position

$$x_1(q_1) = l_1 \sin(q_1(t))$$

$$y_1(q_1) = -l_1 \cos(q_1(t))$$

$$x_2(q_1, q_2) = l_1 \sin(q_1(t)) + l_2 \sin(q_2(t))$$

$$y_2(q_1, q_2) = -l_1 \cos(q_1(t)) - l_2 \cos(q_2(t))$$

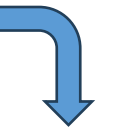
## Velocity

$$\dot{x}_1(q_1, \dot{q}_1) = l_1 \cos(q_1(t)) \dot{q}_1(t)$$

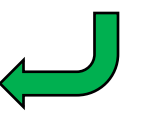
$$\dot{y}_1(q_1, \dot{q}_1) = l_1 \sin(q_1(t)) \dot{q}_1(t)$$

$$\dot{x}_2(\dots) = l_1 \cos(q_1(t)) \dot{q}_1(t) + l_2 \cos(q_2(t)) \dot{q}_2(t)$$

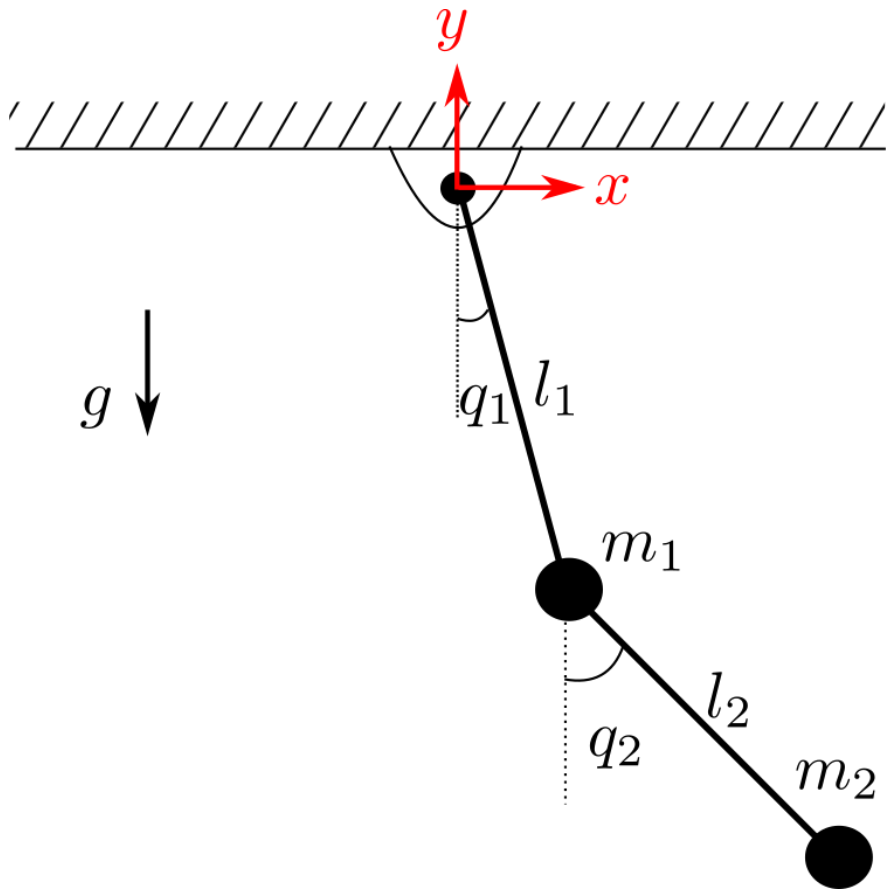
$$\dot{y}_2(\dots) = l_1 \sin(q_1(t)) \dot{q}_1(t) + l_2 \sin(q_2(t)) \dot{q}_2(t)$$



$$\dot{x} = \frac{dx}{dt}$$



Rewrite



### Position

$$x_1(q_1) = l_1 \sin(q_1(t))$$

$$y_1(q_1) = -l_1 \cos(q_1(t))$$

$$x_2(q_1, q_2) = l_1 \sin(q_1(t)) + l_2 \sin(q_2(t))$$

$$y_2(q_1, q_2) = -l_1 \cos(q_1(t)) - l_2 \cos(q_2(t))$$



$$\dot{x} = \frac{dx}{dt}$$

### Velocity

$$\dot{x}_1(q_1, \dot{q}_1) = l_1 \cos(q_1(t)) \dot{q}_1(t)$$

$$\dot{y}_1(q_1, \dot{q}_1) = l_1 \sin(q_1(t)) \dot{q}_1(t)$$

$$\dot{x}_2(\dots) = l_1 \cos(q_1(t)) \dot{q}_1(t) + l_2 \cos(q_2(t)) \dot{q}_2(t)$$

$$\dot{y}_2(\dots) = l_1 \sin(q_1(t)) \dot{q}_1(t) + l_2 \sin(q_2(t)) \dot{q}_2(t)$$

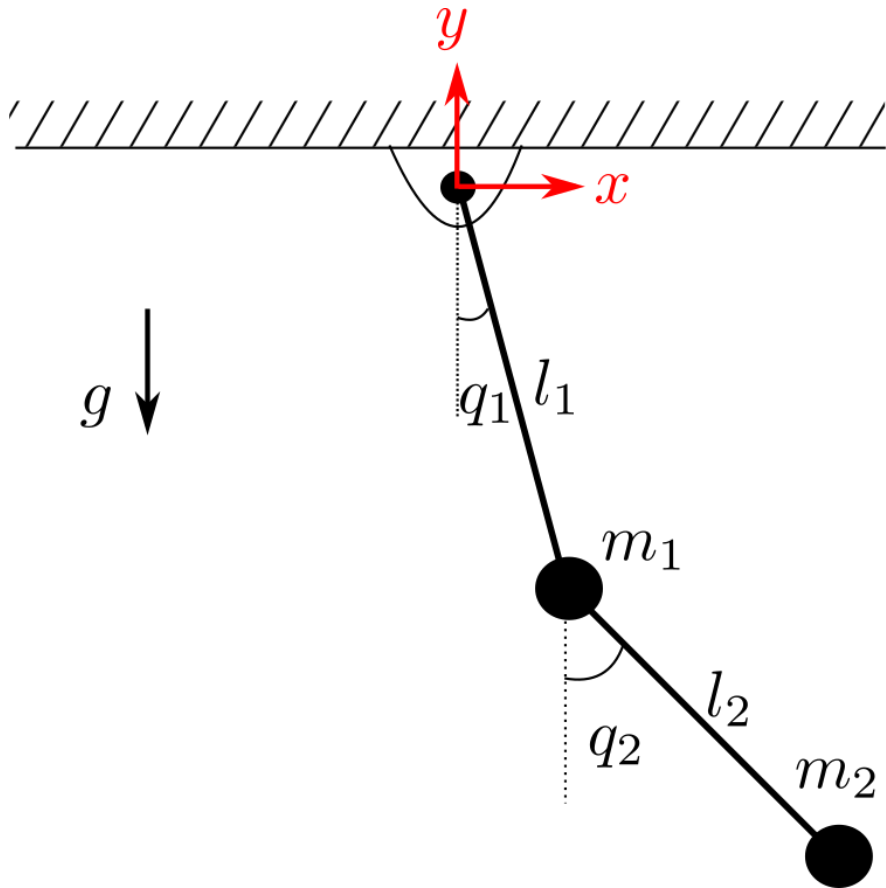


### Velocity matrix form

$$\begin{bmatrix} \dot{x}_2 \\ \dot{y}_2 \end{bmatrix} = \begin{bmatrix} l_1 \cos(q_1) & l_2 \cos(q_2) \\ l_1 \sin(q_1) & l_2 \sin(q_2) \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix}$$



# Jacobian



Velocity matrix form

$$\begin{bmatrix} \dot{x}_2 \\ \dot{y}_2 \end{bmatrix} = \begin{bmatrix} l_1 \cos(q_1) & l_2 \cos(q_2) \\ l_1 \sin(q_1) & l_2 \sin(q_2) \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix}$$

Jacobian

$$J(q) = \begin{bmatrix} l_1 \cos(q_1) & l_2 \cos(q_2) \\ l_1 \sin(q_1) & l_2 \sin(q_2) \end{bmatrix}$$

Velocity matrix form

$$\begin{bmatrix} \dot{x}_2 \\ \dot{y}_2 \end{bmatrix} = \begin{bmatrix} l_1 \cos(q_1) & l_2 \cos(q_2) \\ l_1 \sin(q_1) & l_2 \sin(q_2) \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix}$$

$$v = J(q)\dot{q}$$

# Jacobian

- Helps to connect **Joint** space (**joints**) and **Task** space (**end-effector**).
- Matrix equivalent of the derivative
- The derivative of a **vector**-valued function with respect to a **vector**

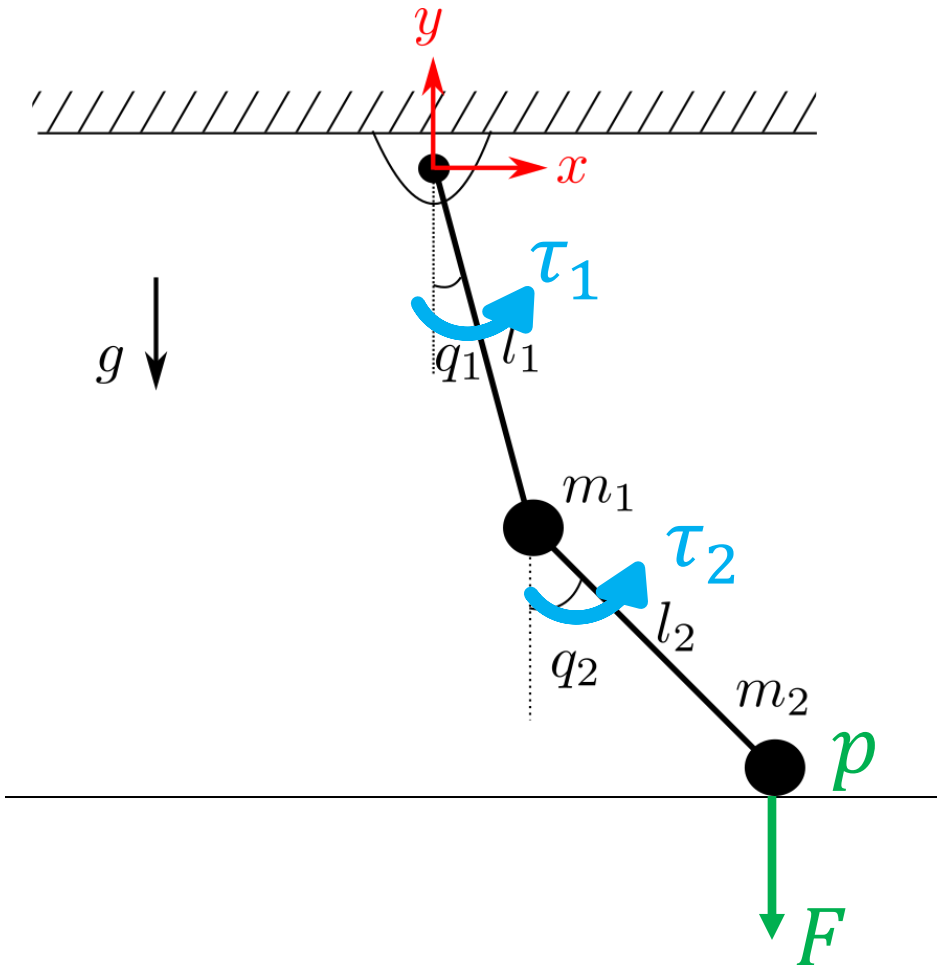
$$\mathbf{y} = F(\mathbf{x}) \quad \mathbf{x} \in \mathbb{R}^n, \mathbf{y} \in \mathbb{R}^m$$

- Linear map **between differentials**
- The Jacobian is an  $m \times n$  matrix

$$J = \frac{\partial \mathbf{F}}{\partial \mathbf{x}} = \begin{matrix} \begin{matrix} \uparrow \\ m \\ \downarrow \end{matrix} & \begin{matrix} \leftarrow n \rightarrow \\ \left[ \begin{array}{ccc} \frac{\partial y_1}{\partial x_1} & \dots & \frac{\partial y_1}{\partial x_n} \\ \frac{\partial y_2}{\partial x_1} & \dots & \frac{\partial y_2}{\partial x_n} \\ \vdots & \ddots & \vdots \\ \frac{\partial y_m}{\partial x_1} & \dots & \frac{\partial y_m}{\partial x_n} \end{array} \right] \end{matrix} \end{matrix}$$

# How can we use the Jacobian to control our system?

$$\mathbf{v} = \mathbf{J}(\mathbf{q})\dot{\mathbf{q}}$$



- If we want to apply a force  $\mathbf{F}$  at the end effector, we can compute the corresponding desired joint torques  $\boldsymbol{\tau}$  with:

$$\boldsymbol{\tau} = \mathbf{J}^T(\mathbf{q})\mathbf{F}$$

- Why? Principle of Virtual Work

Virtual = Small/imagined

- For a virtual displacement  $\delta\mathbf{q}$  at the joints, the virtual displacement  $\delta\mathbf{p}$  at the end effector is:

$$\delta\mathbf{p} = \mathbf{J}(\mathbf{q})\delta\mathbf{q}$$

- Work done by  $\mathbf{F}$ :

$$\mathbf{F}^T \delta\mathbf{p} = \mathbf{F}^T \mathbf{J}(\mathbf{q})\delta\mathbf{q}$$

- Work done by joint torques  $\boldsymbol{\tau}$ :

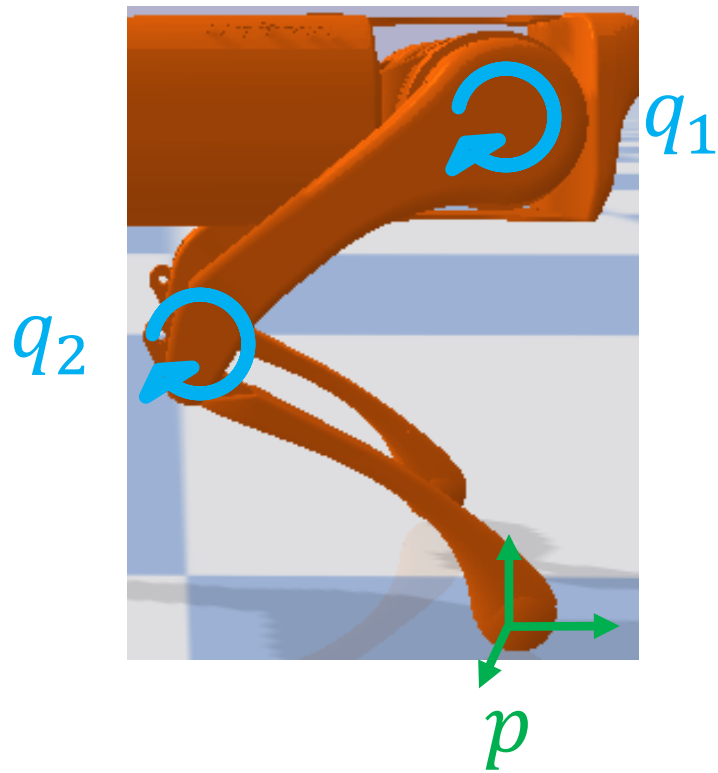
$$\boldsymbol{\tau}^T \delta\mathbf{q}$$



- Work done must be equal

$$\boldsymbol{\tau}^T \delta\mathbf{q} = \mathbf{F}^T \mathbf{J}(\mathbf{q})\delta\mathbf{q} = (\mathbf{J}^T(\mathbf{q})\mathbf{F})^T \delta\mathbf{q}$$

Summary: Joint angles  $\leftrightarrow$  Cartesian space



$$p = f(q)$$

Forward kinematics

$$q = f^{-1}(p)$$

Inverse kinematics

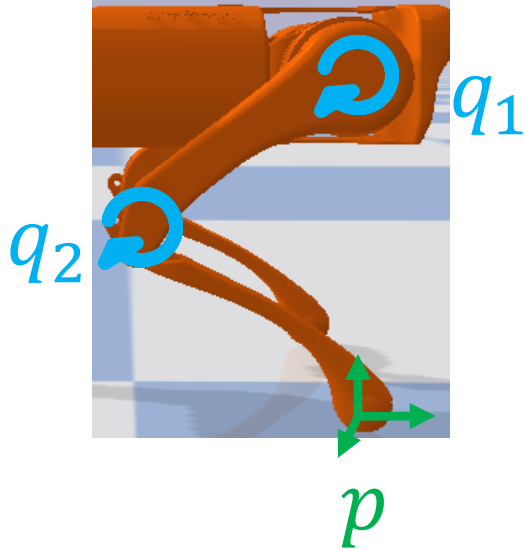
$$\dot{p} = v = J(q)\dot{q}$$

Foot linear velocity

$$\tau = J^T(q)F$$

Map desired end effector force to torques

# Leg Control



$$p = f(q)$$

$$q = f^{-1}(p)$$

$$\dot{p} = v = J(q)\dot{q}$$

$$\tau = J^T(q)F$$

Goal: How much torque do I apply?

Forward kinematics

Inverse kinematics

Foot linear velocity

Map desired end effector force to torques

"I want to move my joint to a certain angle"

"I want my end effector to go to a certain position"

"I want to apply an extra force at the foot"

**Joint PD**

**Cartesian PD**

**Extra applied torque**

# Leg Control

Goal: How much torque do I apply?

## Joint PD

$$\tau_{joint} = K_{p,joint}(q_d - q) + K_{d,joint}(\dot{q}_d - \dot{q})$$

## Cartesian PD

$$\tau_{Cartesian} = J^T(q) [K_{p,Cartesian}(p_d - p) + K_{d,Cartesian}(v_d - v)]$$

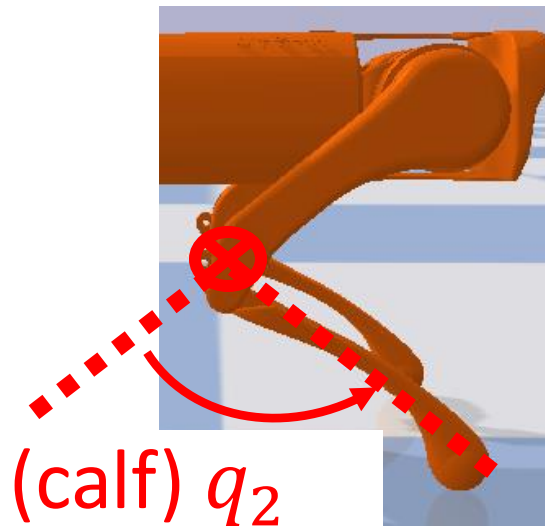
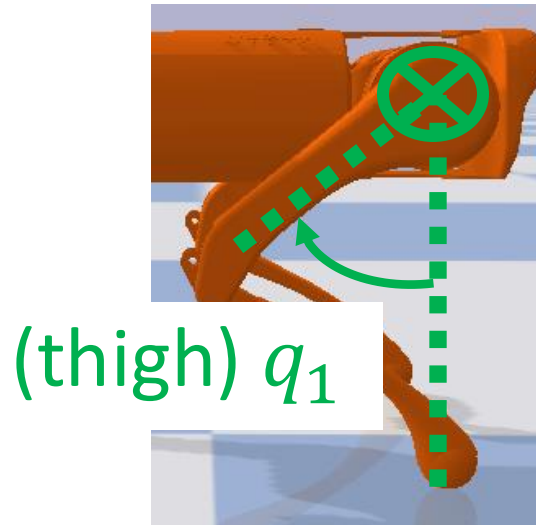
## Extra applied torque

$$\tau = J^T(q)F$$

## Total required torque

$$\tau_{final} = \tau_{joint} + \tau_{Cartesian} + J^T(q)F$$

# Pybullet Quadruped Leg Joint References



- Careful: what is the axis?
- In figure,  $q_1$  is  $\pi/4$  (axis into page)
- In figure,  $q_2$  is  $-\pi/2$  (axis into page)

$$x_2(q_1, q_2) = l_1 \sin(q_1(t)) + l_2 \sin(q_2(t))$$

$$y_2(q_1, q_2) = -l_1 \cos(q_1(t)) - l_2 \cos(q_2(t))$$

**Your turn: derive the Jacobian!**

$$J = \frac{\partial F}{\partial x} \quad \text{Hint}$$
$$= \begin{bmatrix} \frac{\partial y_1}{\partial x_1} & \dots & \frac{\partial y_1}{\partial x_n} \\ \vdots & \ddots & \vdots \\ \frac{\partial y_m}{\partial x_1} & \dots & \frac{\partial y_m}{\partial x_n} \end{bmatrix}$$

# W1-3 Fundamentals

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- **Part 3: Inverse Kinematics (compare with force control)**
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# Inverse Kinematics Today

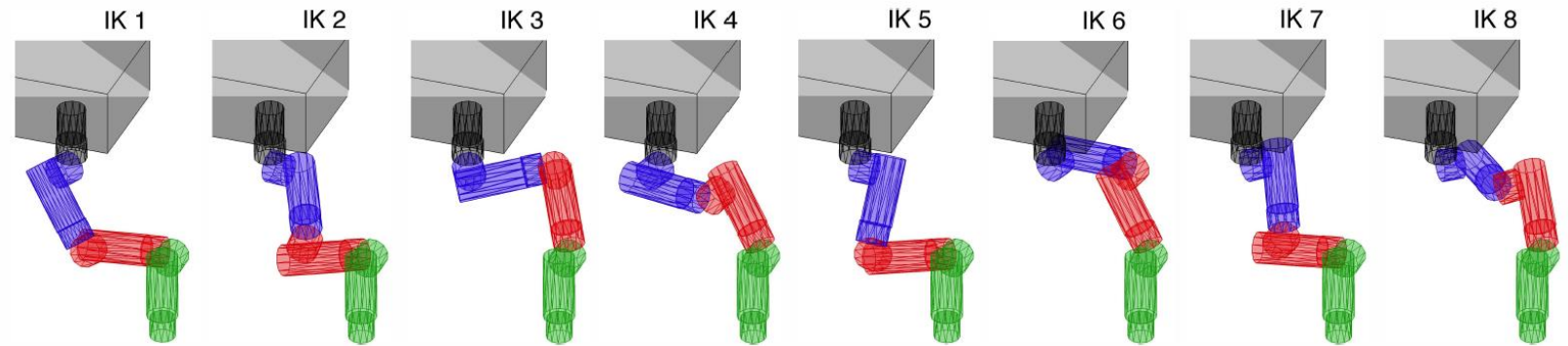
## 1. Analytical

- Very fast
- Exact solutions
- Impossible for complex robots
- Complicated equations

## 2. Iterative (numerical)

- Can handle complex tasks
- Can include constraints
- Works for almost any robot geometry
- Slow
- Convergence depends on good initial guess

# JPL's RoboSimian: Inverse Kinematics

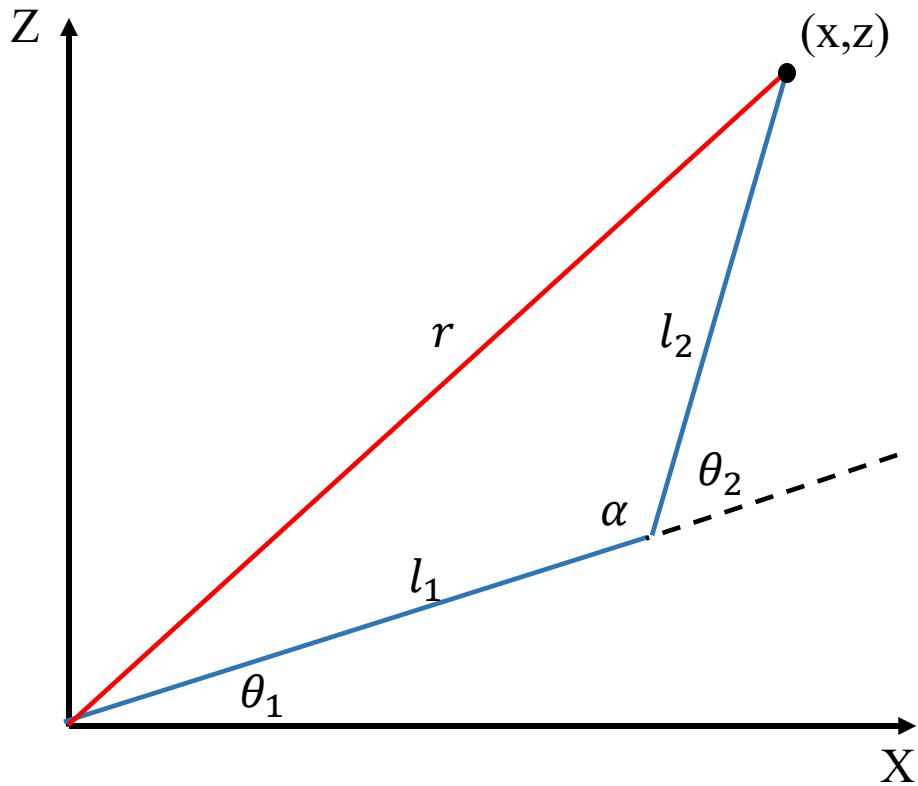


- Four identical limbs, each with 7 degrees of freedom (DOFs)
- 8 Inverse Kinematics “Families”
  - 3 “elbows”  $\rightarrow 2^3$  choices
- How should we choose between these?



# Analytical Inverse Kinematic

Goal: Make  $\theta_2$  as primary variable



- Recall the cosine rule:

$$r^2 = l_1^2 + l_2^2 - 2l_1l_2 \cos \alpha$$

- Therefore:

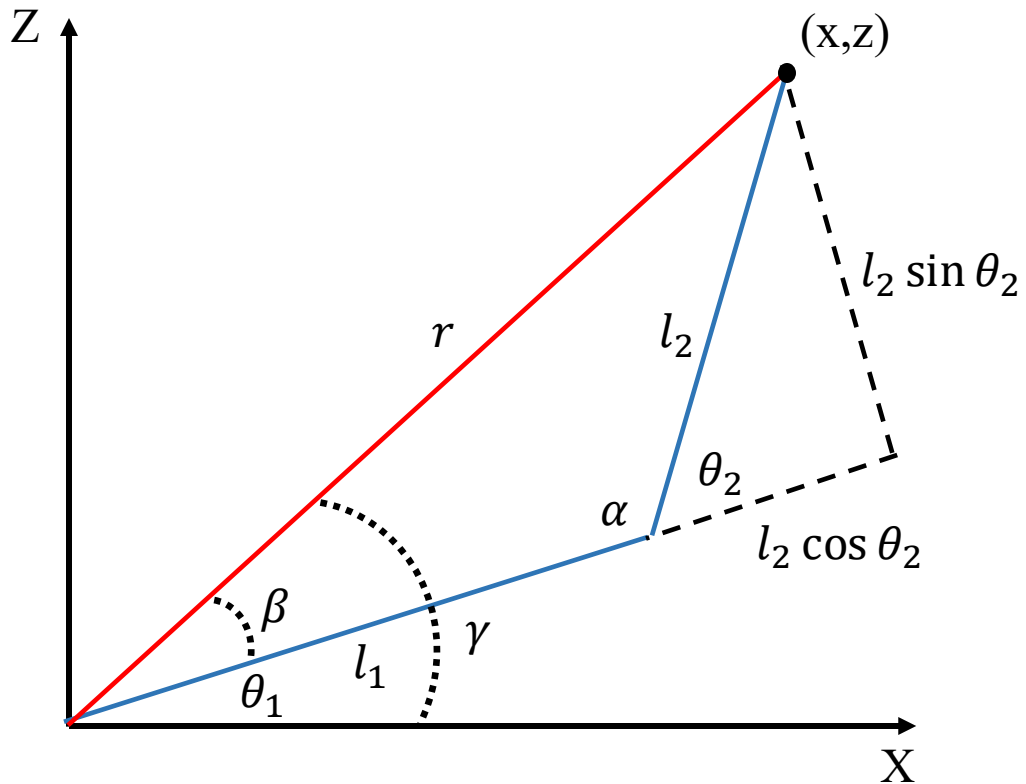
$$\cos \alpha = \frac{l_1^2 + l_2^2 - r^2}{2l_1l_2} = \frac{l_1^2 + l_2^2 - x^2 - z^2}{2l_1l_2}$$

- Since  $\theta_2 = \pi - \alpha$ ,

$$\cos \theta_2 = -\cos \alpha = \frac{r^2 - l_1^2 - l_2^2}{2l_1l_2} = \frac{x^2 + z^2 - l_1^2 - l_2^2}{2l_1l_2}$$

# Analytical Inverse Kinematics

Goal: Make  $\theta_1$  as primary variable



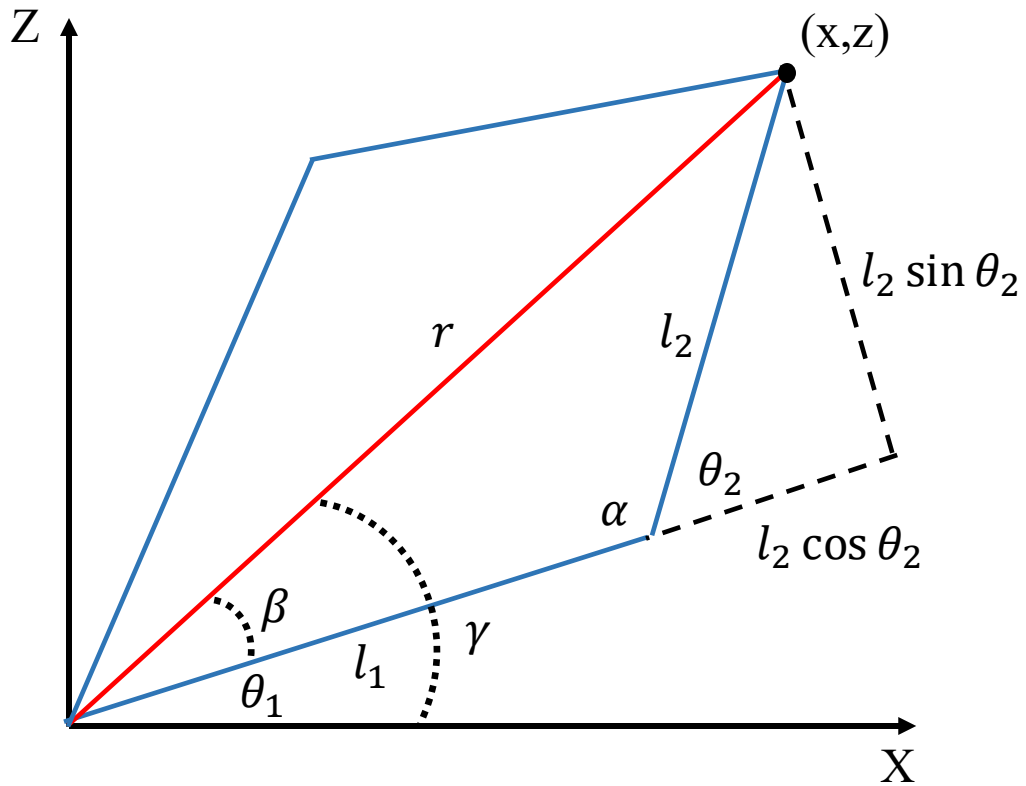
- New variables:  $\gamma, \beta$

$$\gamma = \tan^{-1} \left( \frac{z}{x} \right), \quad \theta_1 = \gamma - \beta$$

- Therefore:

$$\theta_1 = \tan^{-1} \left( \frac{z}{x} \right) - \tan^{-1} \left( \frac{l_2 \sin \theta_2}{l_1 + l_2 \cos \theta_2} \right)$$

# Analytical Inverse Kinematics

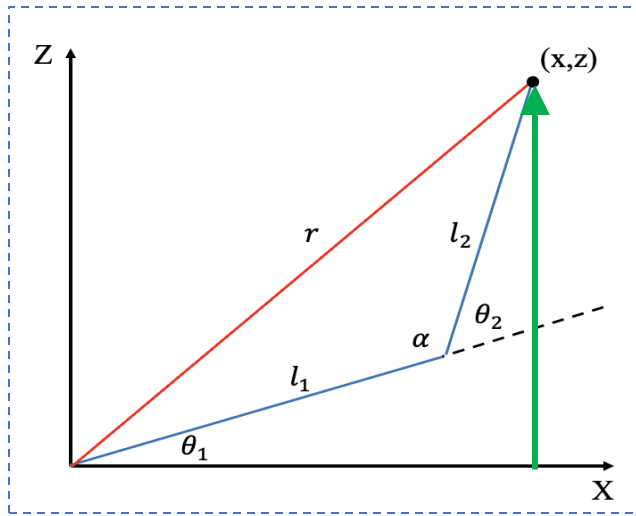


- Summary (both solutions):

$$\theta_2 = \pm \cos^{-1} \left( \frac{x^2 + z^2 - l_1^2 - l_2^2}{2l_1 l_2} \right)$$

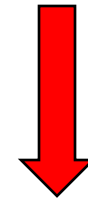
$$\theta_1 = \tan^{-1} \left( \frac{z}{x} \right) \mp \tan^{-1} \left( \frac{l_2 \sin \theta_2}{l_1 + l_2 \cos \theta_2} \right)$$

# Careful: Pybullet Reference Frame



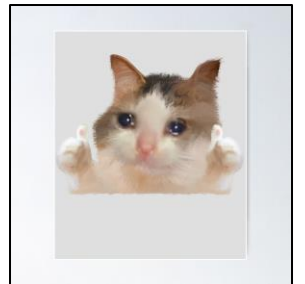
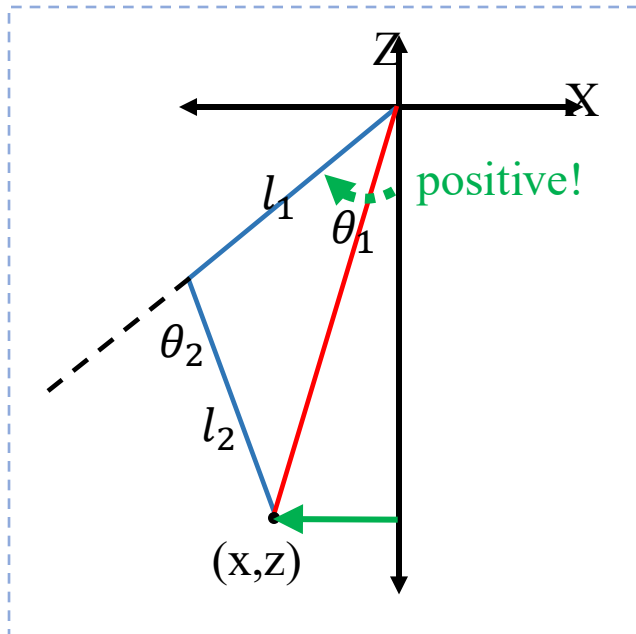
$$\theta_2 = \pm \cos^{-1} \left( \frac{x^2 + z^2 - l_1^2 - l_2^2}{2l_1l_2} \right)$$

$$\theta_1 = \tan^{-1} \left( \frac{z}{x} \right) \mp \tan^{-1} \left( \frac{l_2 \sin \theta_2}{l_1 + l_2 \cos \theta_2} \right)$$



$$\theta_2 = \mp \cos^{-1} \left( \frac{x^2 + z^2 - l_1^2 - l_2^2}{2l_1l_2} \right)$$

$$\theta_1 = np.arctan2(-x, -z) - \tan^{-1} \left( \frac{l_2 \sin \theta_2}{l_1 + l_2 \cos \theta_2} \right)$$



# How is this useful?

$$\theta_2 = \mp \cos^{-1} \left( \frac{x^2 + z^2 - l_1^2 - l_2^2}{2l_1l_2} \right)$$

$$\theta_1 = np.arctan2(-x, -z) - \tan^{-1} \left( \frac{l_2 \sin \theta_2}{l_1 + l_2 \cos \theta_2} \right)$$



**Joint PD**

$$\tau_{joint} = K_{p,joint}(q_d - q) + K_{d,joint}(\dot{q}_d - \dot{q})$$


# Iterative Inverse Kinematics

Degrees of Freedom (DOF) = How many independent ways the mechanism can move

Actuation = How many joints you can control

- What if our system is more complex?
  - **Jacobian is not square**
    - Underactuated (**Fewer** actuations than DOF of task)
      - 3 DOF leg (**3** joints (hip, thigh, calf) but only **1** is actuated/controlled, 2 are passive)
    - Overactuated/Redundant (**More** actuations than DOF of task)
      - **7** DOF arm controlling 3D end-effector position and orientation (**6**)
  - **Jacobian near singularity ( $\det(J) \sim 0$ )**
    - Robot "loses ability to exert force in some directions"
    - Instability, leads to **extremely large joint velocities**

# Iterative Inverse Kinematics

$$v = J(q)\dot{q}$$

$$\dot{q} = J^{-1}(q)v$$

**Exists?**

Goal: Is there any way to get a 'safe inverse'?

# Moore-Penrose Pseudo-Inverse

Note:  $A = J$

- Generalization of the matrix inversion operation for non-square matrices
- Consider a general matrix  $A \in \mathbb{R}^{m \times n}$ . When  $m \geq n$  and  $\text{rank}(A) = n$ , define the *left pseudo-inverse*  $A_l^+$ , with  $A_l^+ A = \mathbb{I}^{n \times n}$

$$A_l^+ := (A^T A)^{-1} A^T$$

(Fewer joints than task dimensions)

- If  $m \leq n$  and  $\text{rank}(A) = m$ , define the *right pseudo-inverse*  $A_r^+$ , with  $A A_r^+ = \mathbb{I}^{m \times m}$

$$A_r^+ := A^T (A A^T)^{-1}$$

(More joints than task dimensions)

- To handle singularities, define the *damped pseudo-inverses* with damping factor  $\lambda$  as:

Higher  $\lambda$  = Stable

Lower  $\lambda$  = Closer to true Pseudo-Inverse but less stable near singularities

$$A_l^+ := (A^T A + \lambda^2 \mathbf{I}_{n \times n})^{-1} A^T$$

Near singularity

$$A_r^+ := A^T (A A^T + \lambda^2 \mathbf{I}_{m \times m})^{-1}$$

# Iterative Inverse Kinematics

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## Algorithm 1: Iterative inverse kinematics

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```
Data:  $p_{des}, q^0$  ; /* Desired foot position, initial joint angle guess */
Result:  $q$  ; /* Joint angles satisfying  $p=f(q)$  */
 $q \leftarrow q^0$ ;
 $p \leftarrow f(q^0)$ ;
④ while  $\|p - p_{des}\| > tol$  do
    |  $J \leftarrow J(q)$  ; /* Evaluate Jacobian for current q */
    |  $J^+ \leftarrow (J)^+$  ; /* Update the pseudoinverse */
    | ①  $\Delta p \leftarrow p_{des} - p$  ; /* find the end-effector error */
    | ②  $q \leftarrow q + \alpha J^+ \Delta p$  ; /* update the joint angles (step size  $\alpha$ ) */
    | ③
end
```

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- ① Check what Pseudo-Inverse should be used
- ② Compute current error in end effector
- ③ Compute joint angle  $\alpha = \text{Scalar gain (Control step size)}$
- ④ Repeat iteratively until convergence

# Assignment

- Gitlab link: <https://gitlab.epfl.ch/lgevers/lr-practicals>
- Instructions are on Moodle
- This week: Part 2 only
- The assignment for weeks 1-3 are **not graded**

