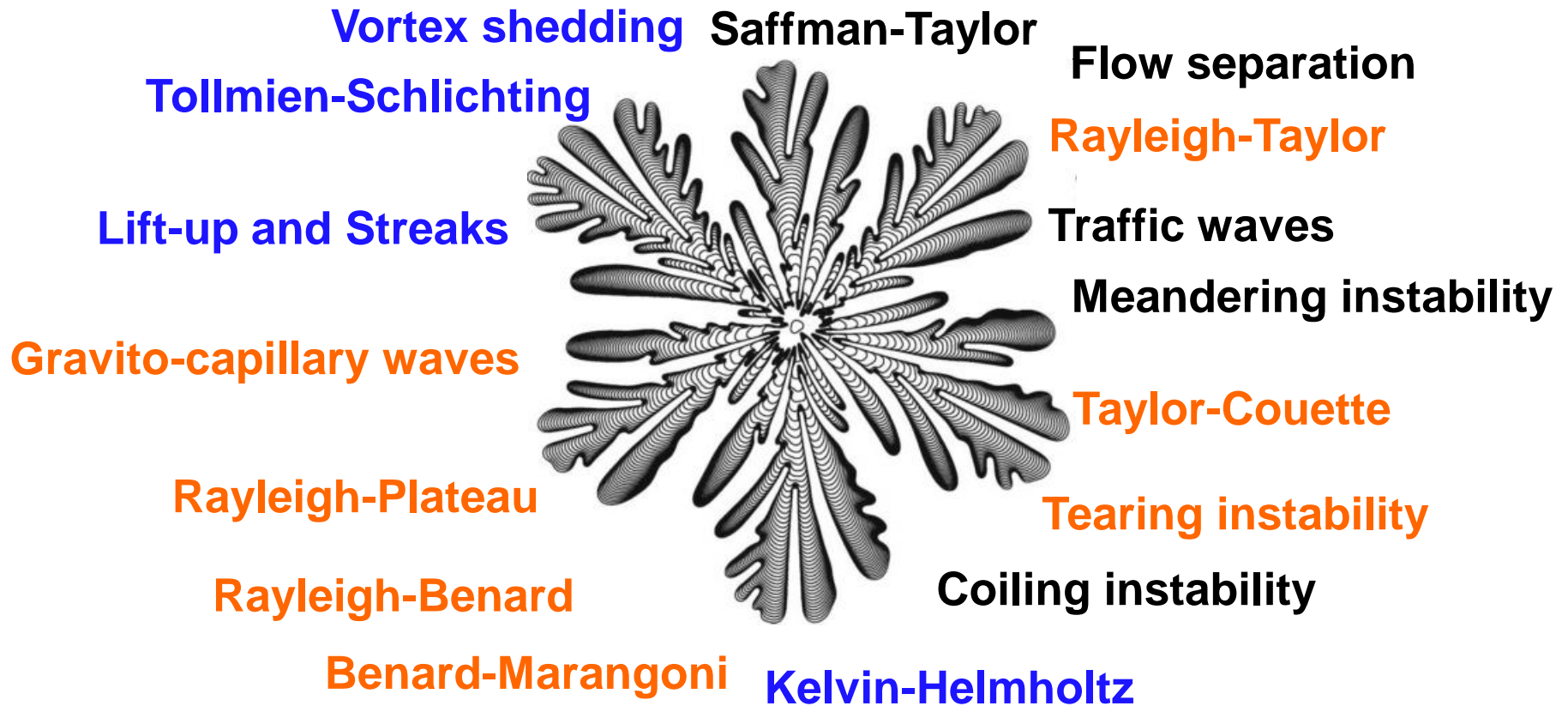
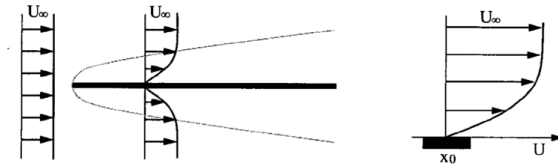


Most flows are unstable...

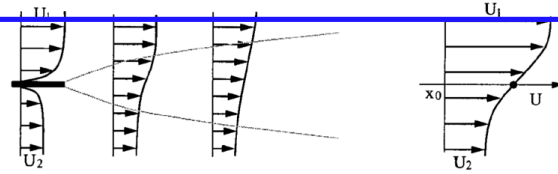


SPATIALLY DEVELOPING SHEAR FLOWS

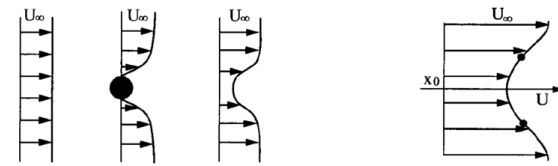
Flat plate boundary layer



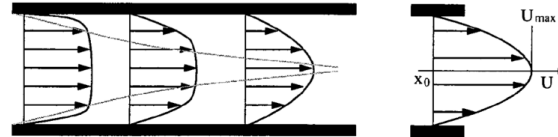
Mixing layer



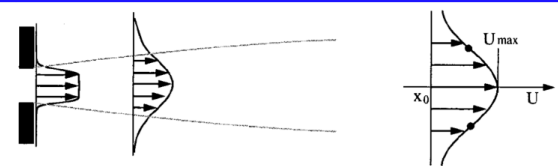
Cylinder wake



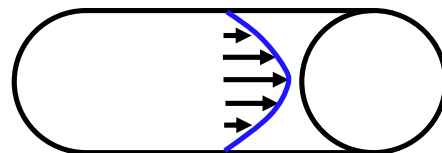
Plane channel flow



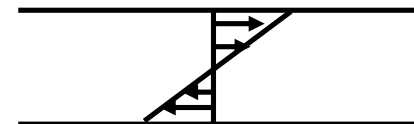
2D jet



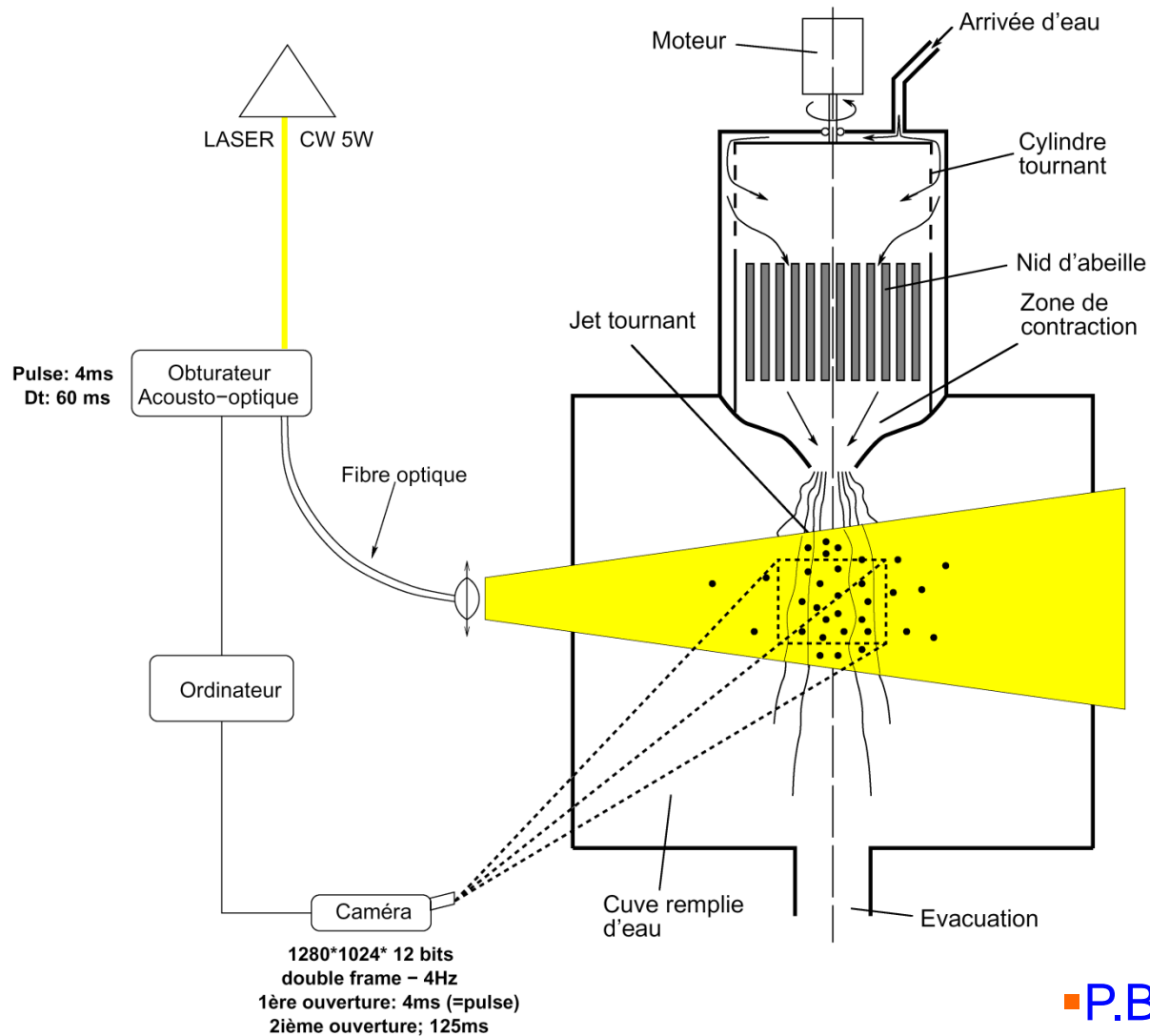
Hagen Poiseuille



Couette



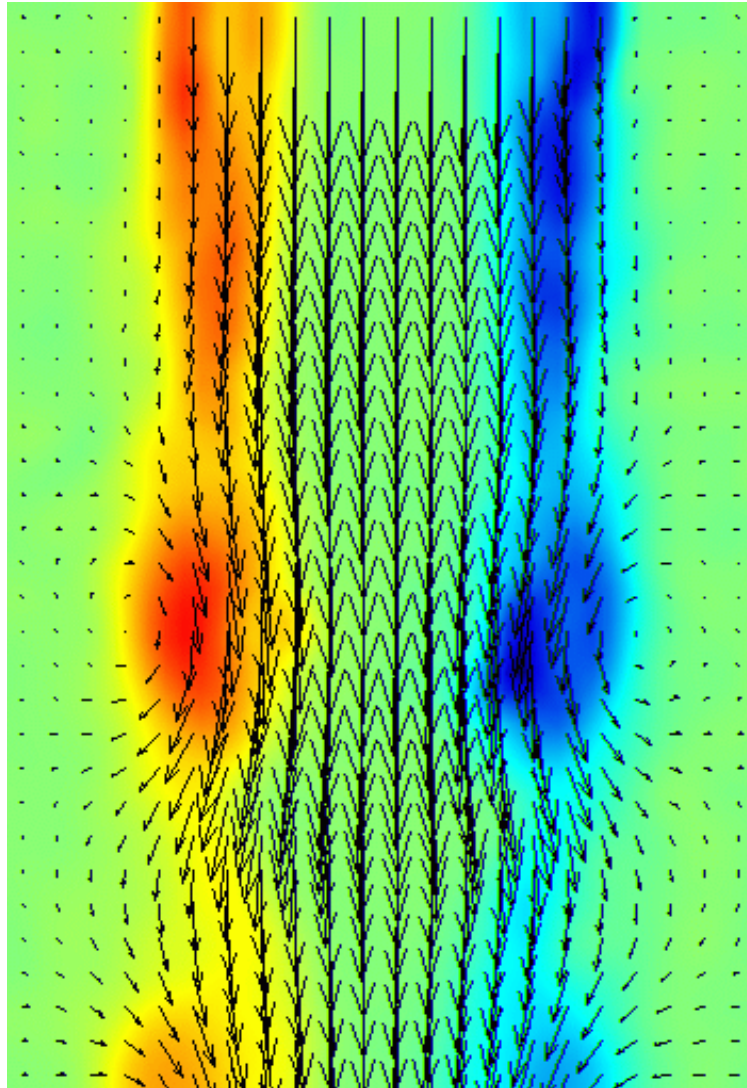
Round jet



Toroidal vortices – vortex rings



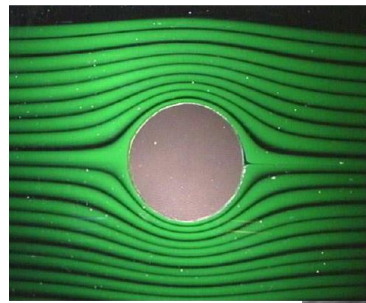
Vorticity field measured by PIV



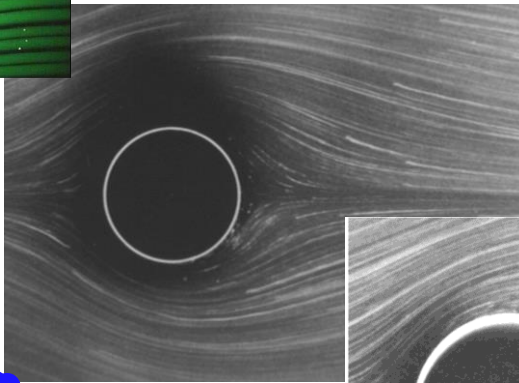
1 point de vitesse sur 4 est représenté

Sinusous mode

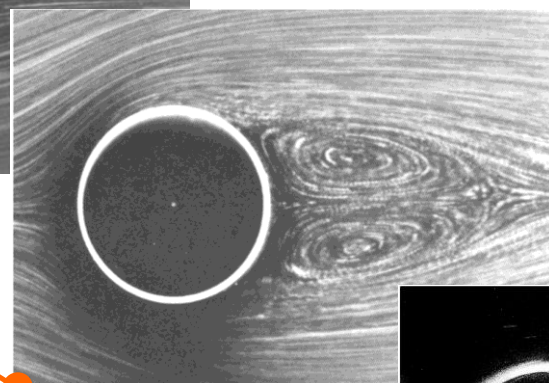
Cylinder wake



Re=0
Eclt symétrique

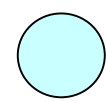


Re=1.5
Eclt attaché



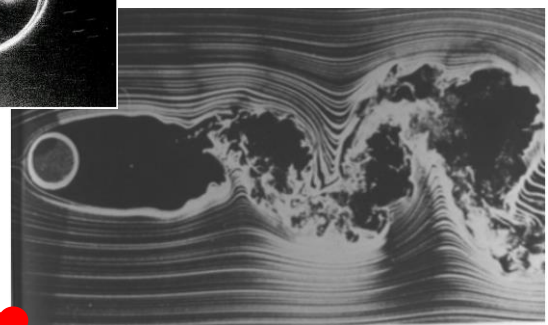
Allée de von Karman

Re=26
Eclt décollé



Re=100
Eclt périodique

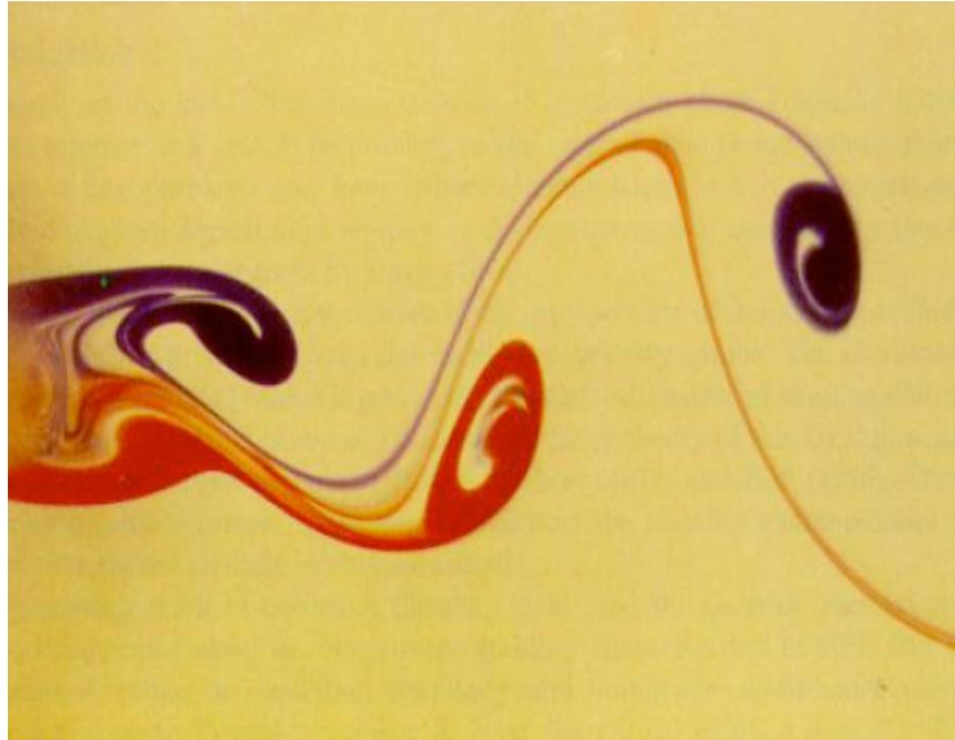
chaos



Re=10000
Eclt turbulent

Couche limite turbulente
C. L. turb. décollé

Allée de von Karman



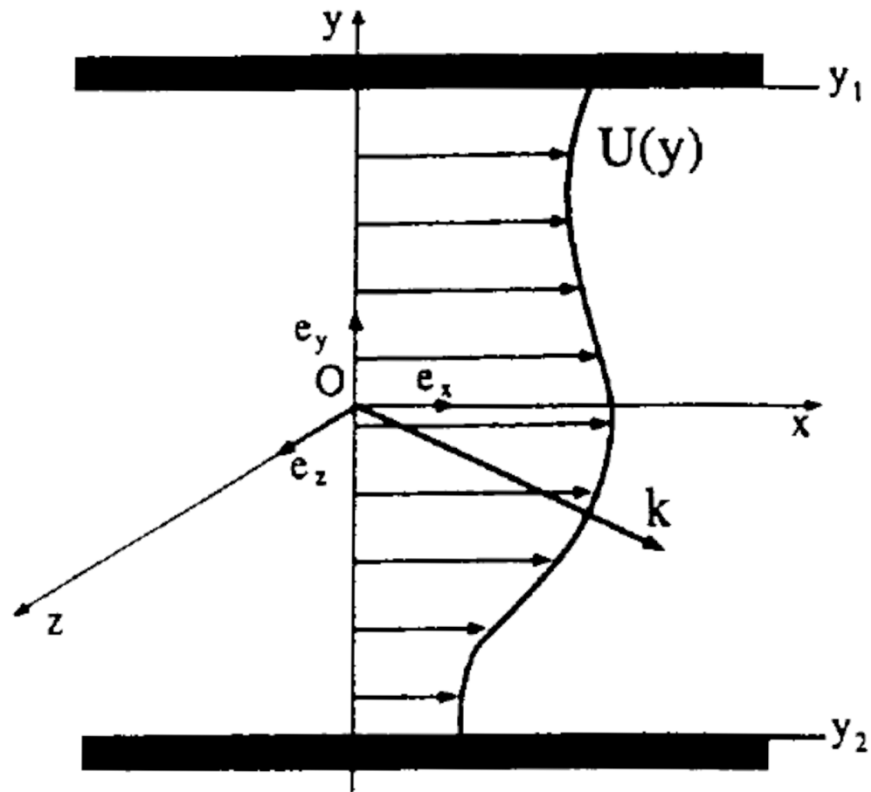
(Perry, Chong & Lim (1982))

Sinuuous mode

PARALLEL FLOW CONCEPTS

Inviscid 3D instabilities

Basic flow



PARALLEL FLOW CONCEPTS

Inviscid 3D instabilities

3D Euler equations

$$\nabla \cdot \mathbf{U} = 0$$
$$\frac{\partial \mathbf{U}}{\partial t} + (\mathbf{U} \cdot \nabla) \mathbf{U} = -\nabla P$$

Basic flow + perturbation

$$\mathbf{U}(\mathbf{x}, t) = U(y) \mathbf{e}_x + \mathbf{u}(\mathbf{x}, t)$$

$$P(\mathbf{x}, t) = P_0 + p(\mathbf{x}, t)$$

Linear Euler equations

$$\nabla \cdot \mathbf{u} = 0 \quad \left(\frac{\partial}{\partial t} + U(y) \frac{\partial}{\partial x} \right) \mathbf{u} + U'(y) v \mathbf{e}_x = -\nabla p$$

PARALLEL FLOW CONCEPTS

Inviscid 3D instabilities

Normal mode decomposition

$$\mathbf{u}(\mathbf{x}, t) = \mathcal{R}e \{ \hat{\mathbf{u}}(y) \exp[i(k_x x + k_z z - \omega t)] \}$$

$$p(\mathbf{x}, t) = \mathcal{R}e \{ \hat{p}(y) \exp[i(k_x x + k_z z - \omega t)] \}$$

$$\mathbf{k} = k_x \mathbf{e}_x + k_z \mathbf{e}_z$$

$$c = \omega / k_x$$

Linear o.d.e.'s

$$ik_x \hat{u} + ik_z \hat{w} + \frac{d\hat{v}}{dy} = 0$$

$$ik_x [U(y) - c] \hat{u} + U'(y) \hat{v} = -ik_x \hat{p}$$

$$ik_x [U(y) - c] \hat{v} = -\frac{d\hat{p}}{dy},$$

$$ik_x [U(y) - c] \hat{w} = -ik_z \hat{p}$$

$$\hat{v}(y_1) = \hat{v}(y_2) = 0$$

3D dispersion relation

$$D(\mathbf{k}, \omega) = 0$$

PARALLEL FLOW CONCEPTS

Inviscid 3D instabilities

Squire's transformation

$$\bar{k}^2 = k_x^2 + k_z^2, \quad \bar{c} = c,$$

$$\bar{k}\bar{u} = k_x\hat{u} + k_z\hat{w}, \quad \bar{v} = \hat{v}, \quad \bar{p}/\bar{k} = \hat{p}/k_x.$$

Linear o.d.e.'s

$$i\bar{k}\bar{u} + \frac{d\bar{v}}{dy} = 0,$$

$$i\bar{k}[U(y) - \bar{c}]\bar{u} + U'(y)\bar{v} = -i\bar{k}\bar{p},$$

$$i\bar{k}[U(y) - \bar{c}]\bar{v} = -\frac{d\bar{p}}{dy},$$

$$\bar{v}(y_1) = \bar{v}(y_2) = 0,$$

2D dispersion relation

$$\bar{D}(\bar{k}, \bar{\omega}) = 0$$

PARALLEL FLOW CONCEPTS

Inviscid 3D instabilities

Squire's transformation

$$D(\mathbf{k}, \omega) \equiv \tilde{D} \left[\left(k_x^2 + k_z^2 \right)^{1/2}, \left(\left(k_x^2 + k_z^2 \right)^{1/2} / k_x \right) \omega \right] = 0$$

to each oblique mode (\mathbf{k}, ω) of temporal growth rate ω_i is associated a two-dimensional mode $(\tilde{\mathbf{k}}, \tilde{\omega})$ of larger temporal growth rate $\tilde{\omega}_i = \sqrt{k_x^2 + k_z^2} \omega_i / k_x > \omega_i$. *The wave of maximum growth rate is therefore two-dimensional*

2D PARALLEL FLOW CONCEPTS

Dispersion relation

2D vorticity equation

$$\left(\frac{\partial}{\partial t} + \frac{\partial \Psi}{\partial y} \frac{\partial}{\partial x} - \frac{\partial \Psi}{\partial x} \frac{\partial}{\partial y} \right) \nabla^2 \Psi = 0$$

Basic flow + perturbation

$$\Psi(x, t) = \int U(y) dy + \psi(x, y, t)$$

$$u = \partial_y \psi \text{ et } v = -\partial_x \psi$$

Linear vorticity equation

$$\left(\frac{\partial}{\partial t} + U(y) \frac{\partial}{\partial x} \right) \nabla^2 \psi - U''(y) \frac{\partial \psi}{\partial x} = 0$$

Rayleigh equation

Dispersion relation

Normal mode decomposition

$$\psi(x, y, t) = \mathcal{R}e \left\{ \phi(y) e^{i(kx - \omega t)} \right\}$$

$$[U(y) - c] [\phi'' - k^2 \phi] - U''(y) \phi = 0$$

$$\phi(y) \Rightarrow 0 \quad \text{at } y = \pm\infty$$

Dispersion relation

$$D(k, \omega) = 0$$

PARALLEL FLOW CONCEPTS

Inviscid instabilities

Rayleigh's inflection point criterion

In order for the basic flow $U(y)$ to be unstable, it should have an inflection point, say at $y = y_s$, such that $U''(y_s) = 0$

or, in other words $\Omega(y)$ has an extremum

Rayleigh theorem (1916)

$$(U - c) \left(\frac{d^2 \psi}{dy^2} - k^2 \psi \right) - U''(y) \psi = 0$$

$$\int_{y_1}^{y_2} \left(\left(\frac{d^2 \psi}{dy^2} - k^2 \psi \right) \psi^* - \frac{U''(y) \psi \psi^*}{U - c} \right) dy = 0$$

$$\int_{y_1}^{y_2} \left(\left(\frac{d^2 \psi}{dy^2} - k^2 \psi \right) \psi^* - \frac{U''(y) \psi \psi^*}{|U - c|^2} (U - c^*) \right) dy = 0$$

$$\left[\frac{d\psi}{dy} \psi^* \right]_{y_1}^{y_2} + \int_{y_1}^{y_2} \left(-\frac{d\psi}{dy} \frac{d\psi^*}{dy} - k^2 \psi \psi^* - \frac{U''(y) \psi \psi^*}{|U - c|^2} (U - c^*) \right) dy = 0$$

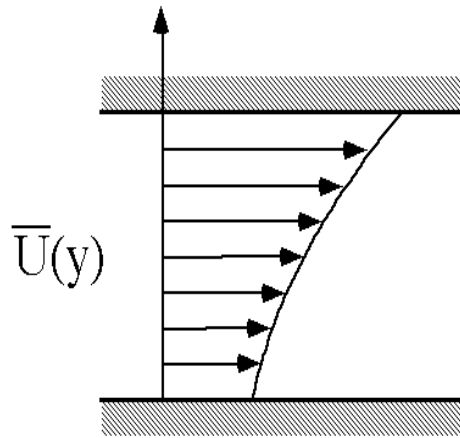
Rayleigh theorem

$$\cancel{\left[\frac{d\psi}{dy} \psi^* \right]_{y_1}^{y_2}} + \int_{y_1}^{y_2} \left(\underbrace{-\frac{d\psi}{dy} \frac{d\psi^*}{dy}}_{\text{real}} - \underbrace{k^2 \psi \psi^*}_{\text{real}} - \underbrace{\frac{U''(y) \psi \psi^*}{|U - c|^2}}_{\text{real}} (U - c^*) \right) dy = 0$$

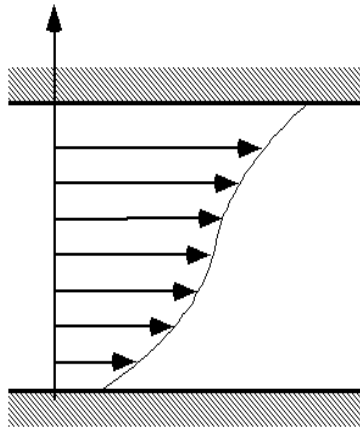
take the imaginary part

$$\int_{y_1}^{y_2} \frac{U''(y) |\psi|^2}{|U - c|^2} c_i dy = 0$$

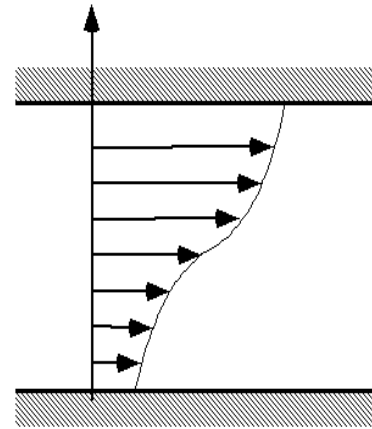
Quiz



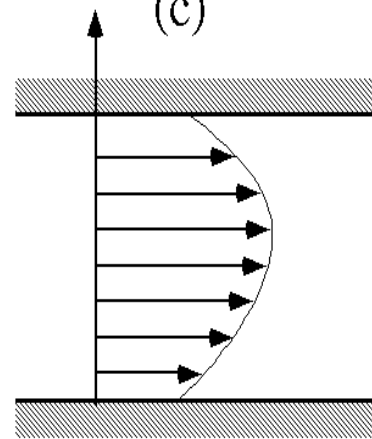
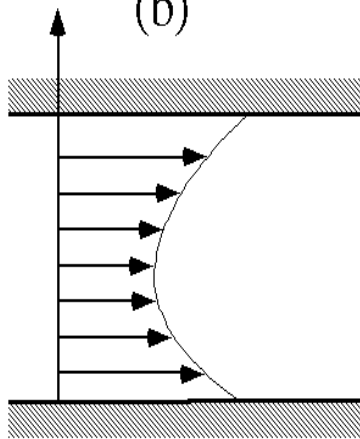
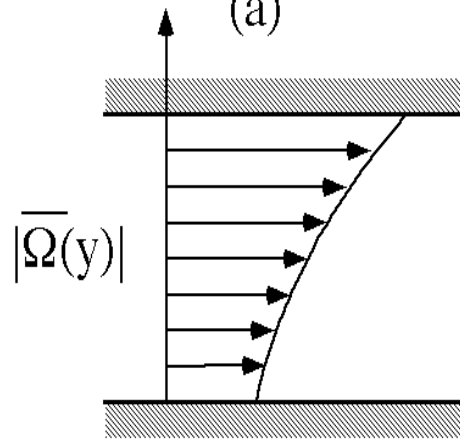
(a)



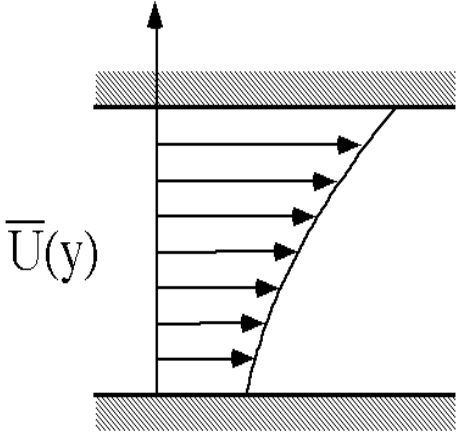
(b)



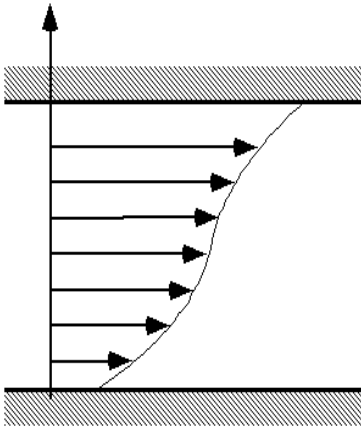
(c)



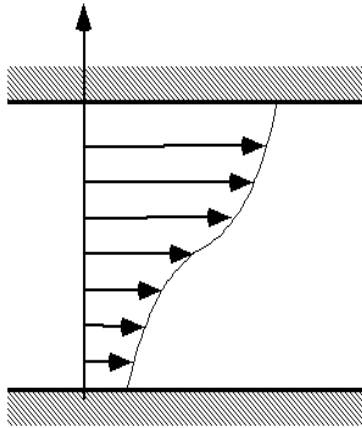
Quiz



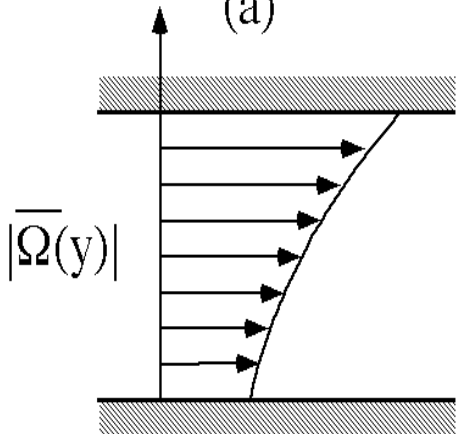
(a)



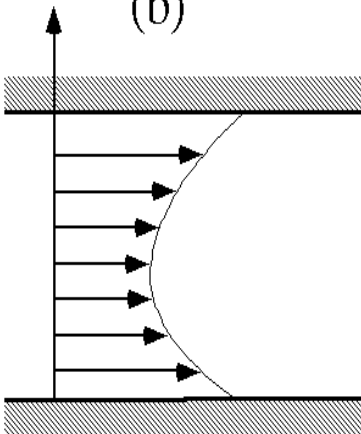
(b)



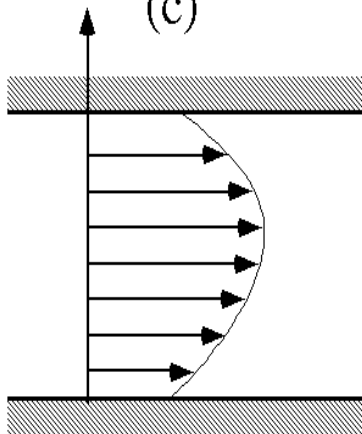
(c)



stable



Unstable?

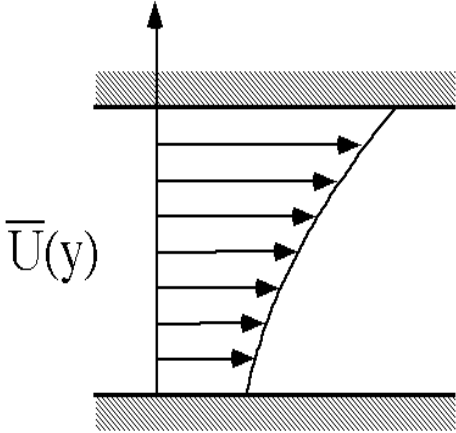


Unstable?

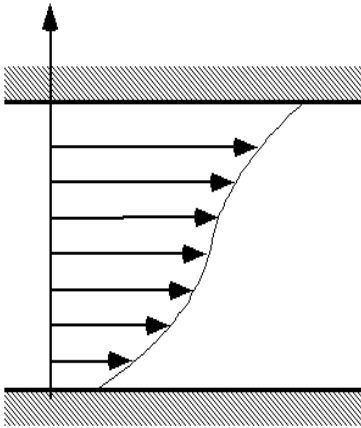
Fjorthoft criterion (1950)

For monotonous velocity profiles with only one inflection point, $|\Omega(y)|$ should have a maximum for instability to be possible

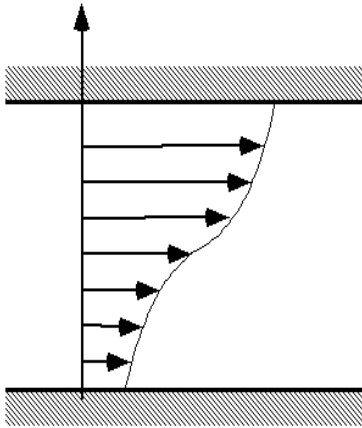
Quiz



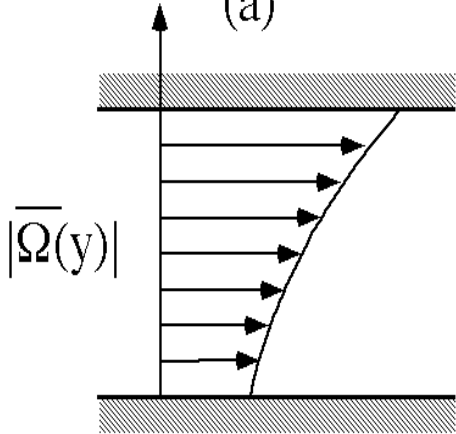
(a)



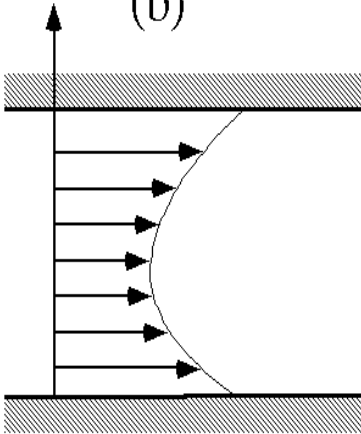
(b)



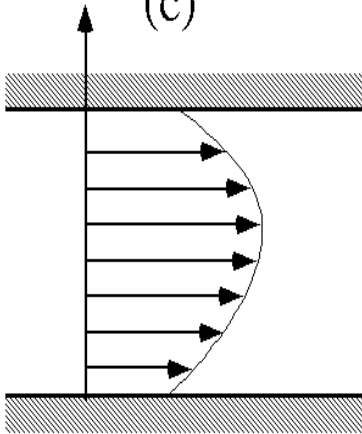
(c)



stable

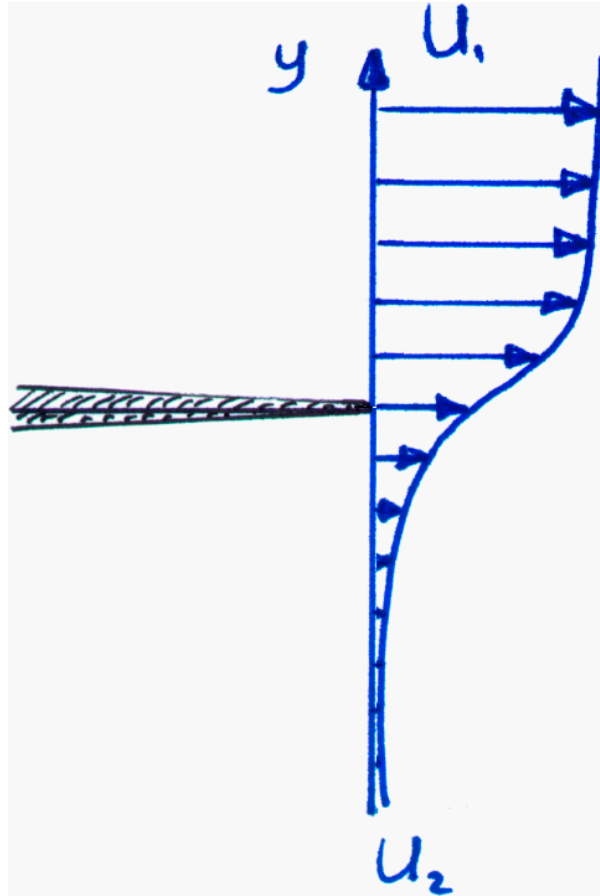


Stable

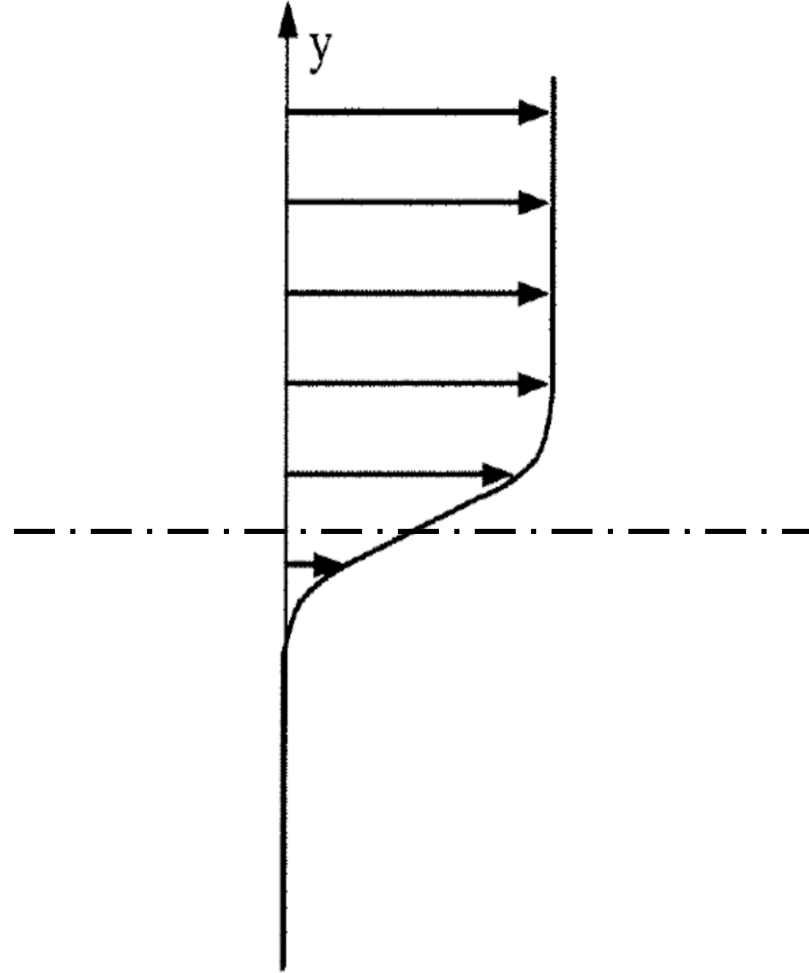


Unstable?

Tangent hyperbolic mixing layer

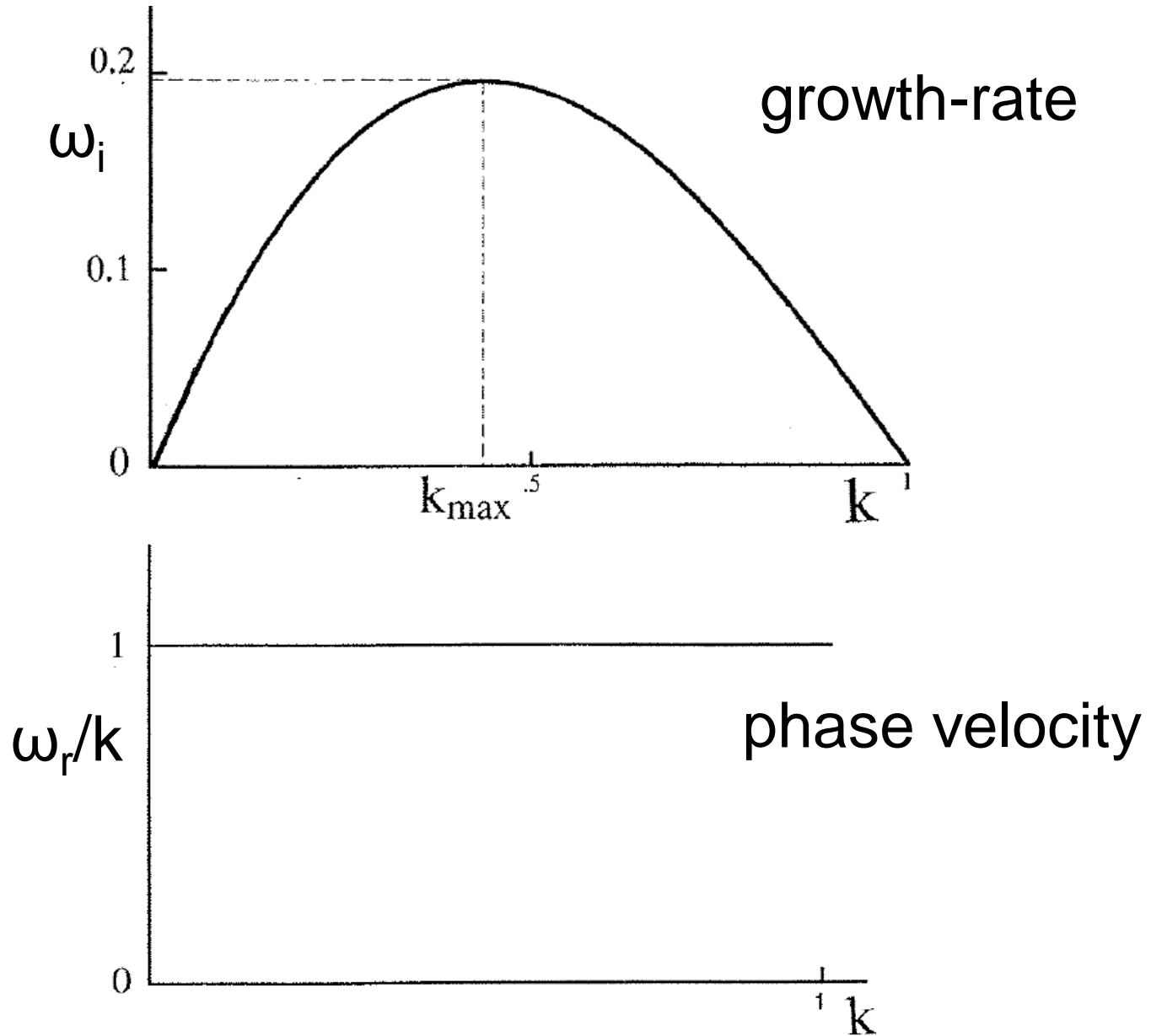


Tangent hyperbolic shear layer



$$U_B(y) = \tanh y$$

Tangent hyperbolic shear layer

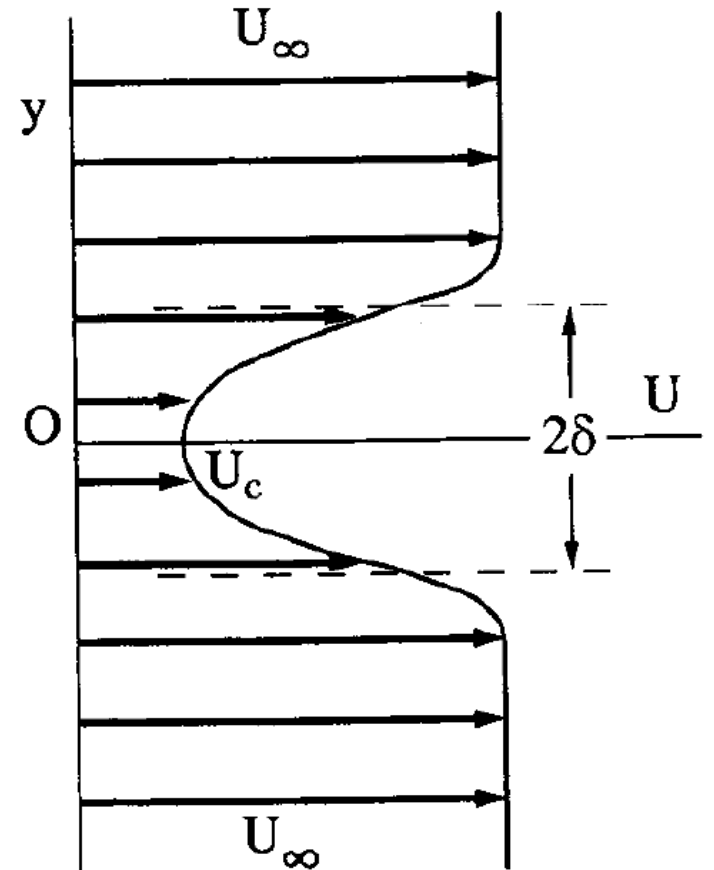


Wake instability

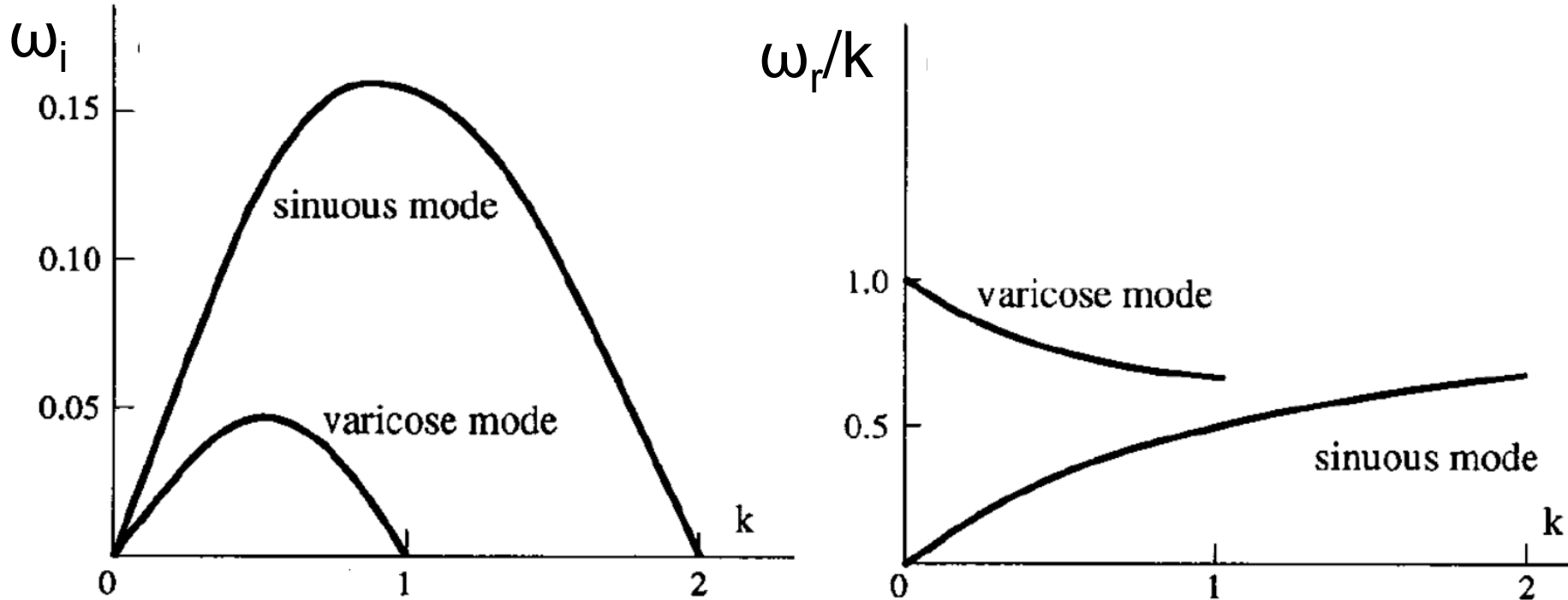
$$U(y) = U_{\infty} + (U_c - U_{\infty}) \operatorname{sech}^2 \frac{y}{\delta}$$

Velocity ratio

$$R \equiv (U_c - U_{\infty}) / (U_c + U_{infty})$$



Wake instability



Betchov & Criminale (1966)

How to solve Rayleigh equation?

We fix k , we need to find all c and ψ such that

$$\left(U \left(\frac{d^2}{dy^2} - k^2 \right) - U''(y) \right) \psi = c \left(\frac{d^2}{dy^2} - k^2 \right) \psi$$
$$\psi(-L) = \psi(L) = 0$$

Formally,

$$\mathcal{A}\psi = c\mathcal{E}\psi$$

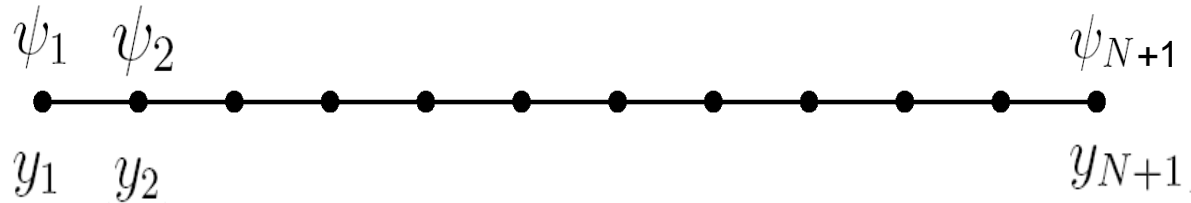
Discretize

$$\mathbf{A}\Psi = c\mathbf{E}\Psi$$

Generalized eigenvalue problem

How to solve Rayleigh equation?

Method 1: Finite differences of order 1.



$$\Psi = \begin{pmatrix} \psi(y_1) \\ \psi(y_2) \\ \vdots \\ \psi(y_N) \\ \psi(y_{N+1}) \end{pmatrix} = \begin{pmatrix} \psi_1 \\ \psi_2 \\ \vdots \\ \psi_N \\ \psi_{N+1} \end{pmatrix} \quad \Psi'' = \begin{pmatrix} \psi''(y_1) \\ \psi''(y_2) \\ \vdots \\ \psi''(y_N) \\ \psi''(y_{N+1}) \end{pmatrix}$$

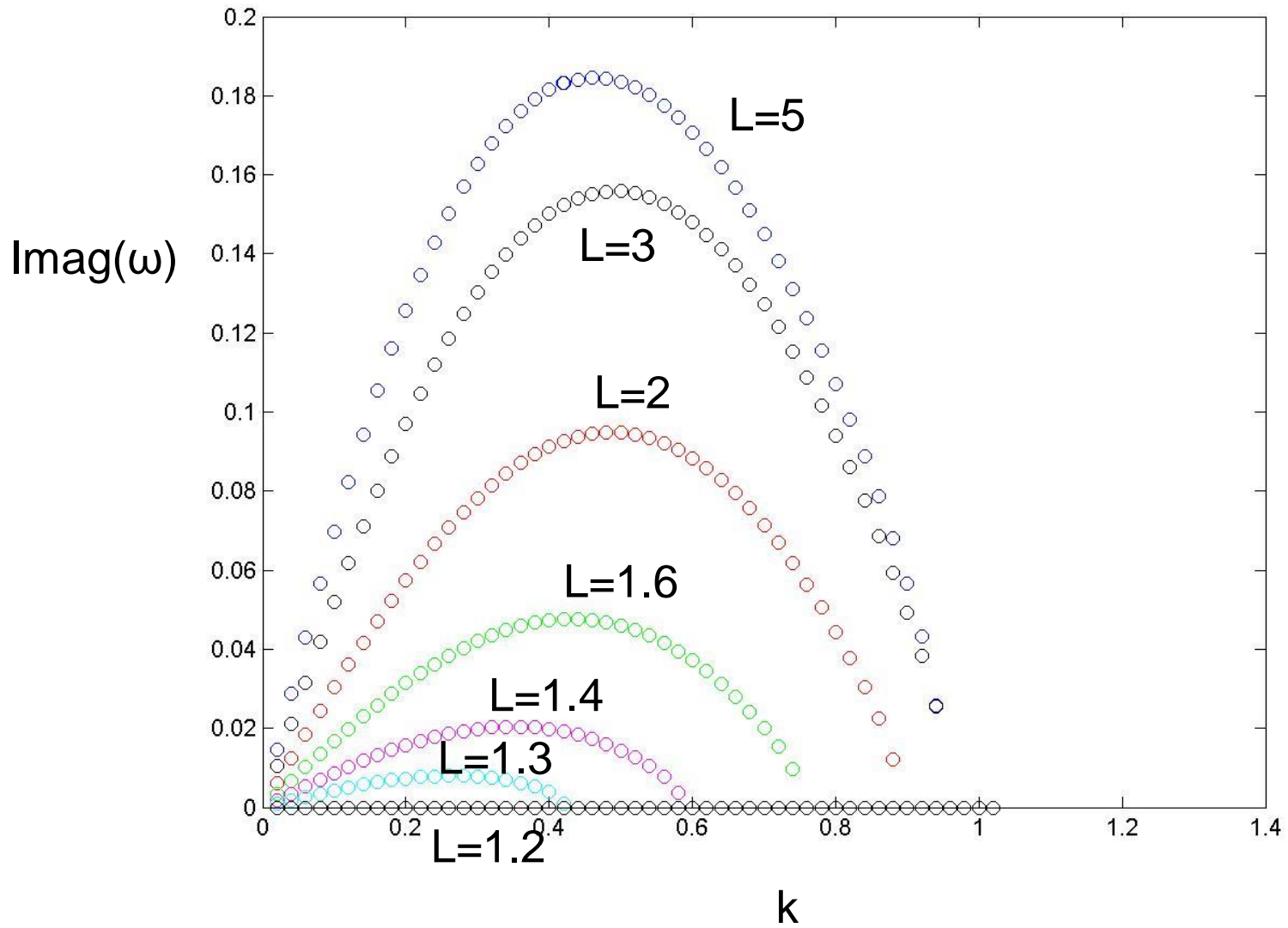
How to solve Rayleigh equation?

Method 1: Finite differences

$$\begin{pmatrix} \psi_2'' \\ \psi_3'' \\ \psi_4'' \\ \vdots \\ \psi_{N-3}'' \\ \psi_{N-2}'' \\ \psi_{N-1}'' \end{pmatrix} = \begin{pmatrix} -2 & 1 & 0 & \dots & \dots & \dots & 0 \\ 1 & -2 & 1 & 0 & \dots & \dots & 0 \\ 0 & 1 & -2 & 1 & 0 & \dots & 0 \\ \dots & \dots & \dots & \dots & \dots & \dots & \dots \\ 0 & \dots & 0 & 1 & -2 & 1 & 0 \\ 0 & \dots & \dots & 0 & 1 & -2 & 1 \\ 0 & \dots & \dots & \dots & 0 & 1 & -2 \end{pmatrix} \begin{pmatrix} \psi_2 \\ \psi_3 \\ \psi_4 \\ \vdots \\ \psi_{N-3} \\ \psi_{N-2} \\ \psi_{N-1} \end{pmatrix}$$

Sparse matrix but low order!

Influence of confinement



PARALLEL FLOW CONCEPTS

Viscous 3D instabilities

3D Navier - Stokes equations

$$\nabla \cdot \mathbf{U} = 0,$$

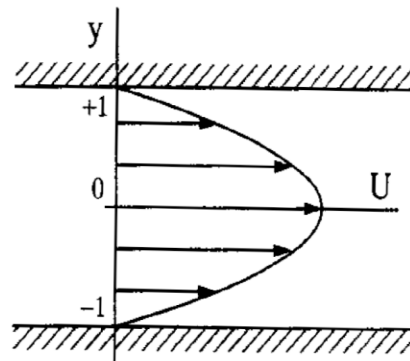
$$\frac{\partial \mathbf{U}}{\partial t} + (\mathbf{U} \cdot \nabla) \mathbf{U} = -\nabla P + \frac{1}{\text{Re}} \nabla^2 \mathbf{U}$$

Basic flow + perturbation

$$\mathbf{U}(\mathbf{x}, t) = U(y) \mathbf{e}_x + \mathbf{u}(\mathbf{x}, t)$$

$$P(\mathbf{x}, t) = P_0(x) + p(\mathbf{x}, t)$$

Basic flow



PARALLEL FLOW CONCEPTS

Viscous 3D instabilities

Squire's transformation

$$\begin{aligned}\bar{k}^2 &= k_x^2 + k_z^2, & \bar{c} &= c, \\ \bar{k}\bar{u} &= k_x\hat{u} + k_z\hat{w}, & \bar{v} &= \hat{v}, & \bar{p}/\bar{k} &= \hat{p}/k_x. \\ \bar{k}\bar{Re} &= k_x Re\end{aligned}$$

3D dispersion relation

$$D(\mathbf{k}, \omega; Re) \equiv \tilde{D} \left[(k_x^2 + k_z^2)^{1/2}, \frac{(k_x^2 + k_z^2)^{1/2}}{k_x} \omega; \frac{k_x}{(k_x^2 + k_z^2)^{1/2}} Re \right] = 0$$

To each oblique mode (\mathbf{k}, ω) of temporal growth rate ω_i , at Reynolds number Re , corresponds a two-dimensional mode $(\bar{k}, \bar{\omega})$ of larger growth rate $\bar{\omega}_i = \omega_i \sqrt{k_x^2 + k_z^2} / k_x$, at a *lower* Reynolds number $\bar{Re} = Re k_x / \sqrt{k_x^2 + k_z^2}$.

2D PARALLEL FLOW CONCEPTS

Dispersion relation

2D vorticity equation

$$\left(\frac{\partial}{\partial t} + \frac{\partial \Psi}{\partial y} \frac{\partial}{\partial x} - \frac{\partial \Psi}{\partial x} \frac{\partial}{\partial y} \right) \nabla^2 \Psi = \frac{1}{Re} \nabla^4 \Psi$$

Basic flow + perturbation

$$\Psi(x, t) = \int U(y) dy + \psi(x, y, t)$$

Linear vorticity equation

$$\left(\frac{\partial}{\partial t} + U(y) \frac{\partial}{\partial x} \right) \nabla^2 \psi - U''(y) \frac{\partial \psi}{\partial x} = \frac{1}{Re} \nabla^4 \psi$$

2D PARALLEL FLOW CONCEPTS

Dispersion relation

Normal mode decomposition

$$\psi(x, y, t) = \mathcal{R}e \left\{ \phi(y) e^{i(kx - \omega t)} \right\}$$

Orr-Sommerfeld equation

$$[U(y) - c][\phi'' - k^2\phi] - U''(y)\phi = \frac{1}{i k Re} \left(\frac{d^2}{dy^2} - k^2 \right)^2 \phi$$

$$\phi(y) \Rightarrow 0 \quad \text{at } y = \pm\infty$$

Dispersion relation

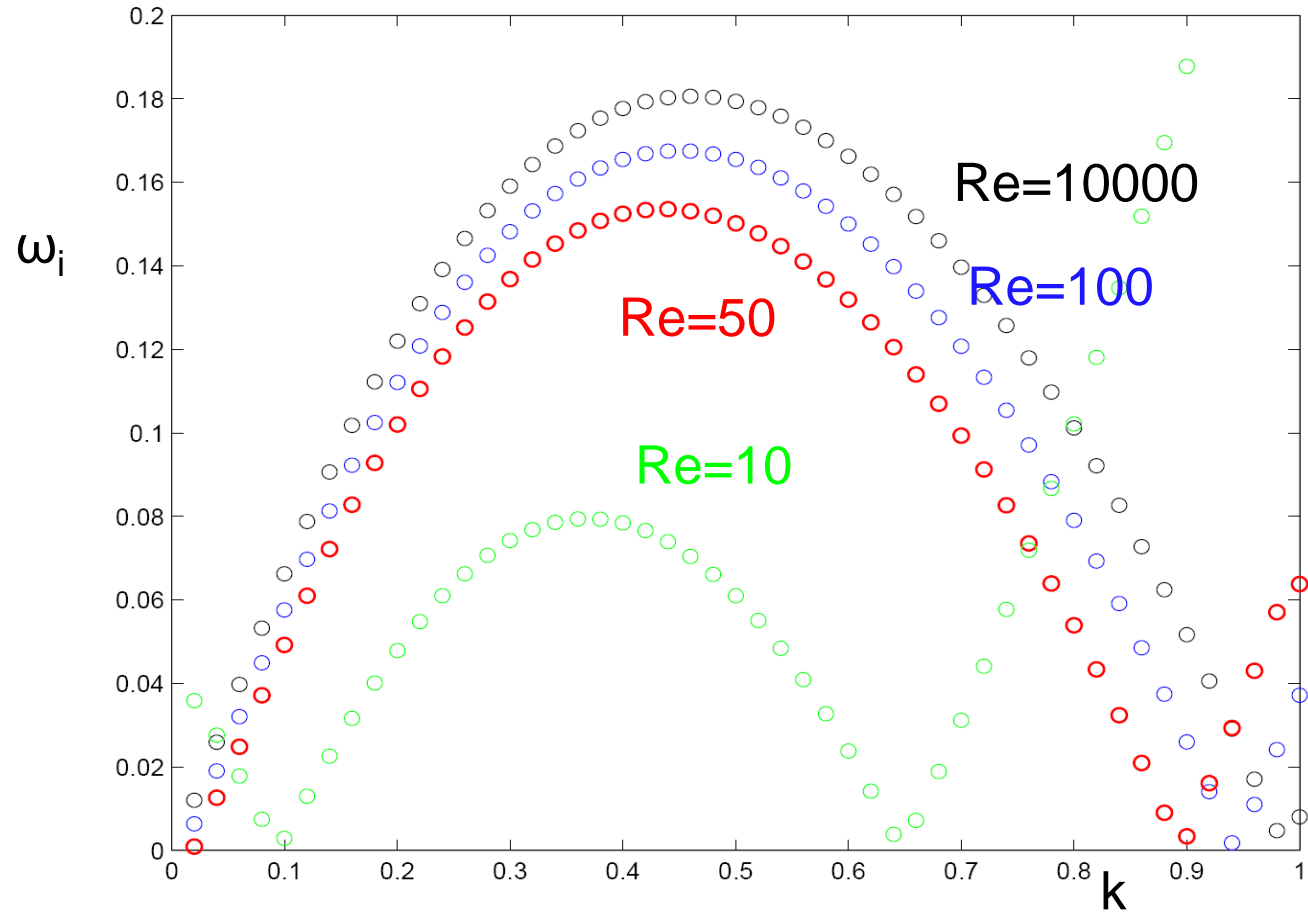
$$D(k, \omega; Re) = 0$$

Viscosity has limited stabilizing influence on K-H instability

$$Re := \Delta U \delta / \nu$$

$$\omega_{i,max} \frac{\delta}{\Delta U} \approx \sqrt{\frac{0,2}{1 + \text{constant} / 0,2 Re}}$$

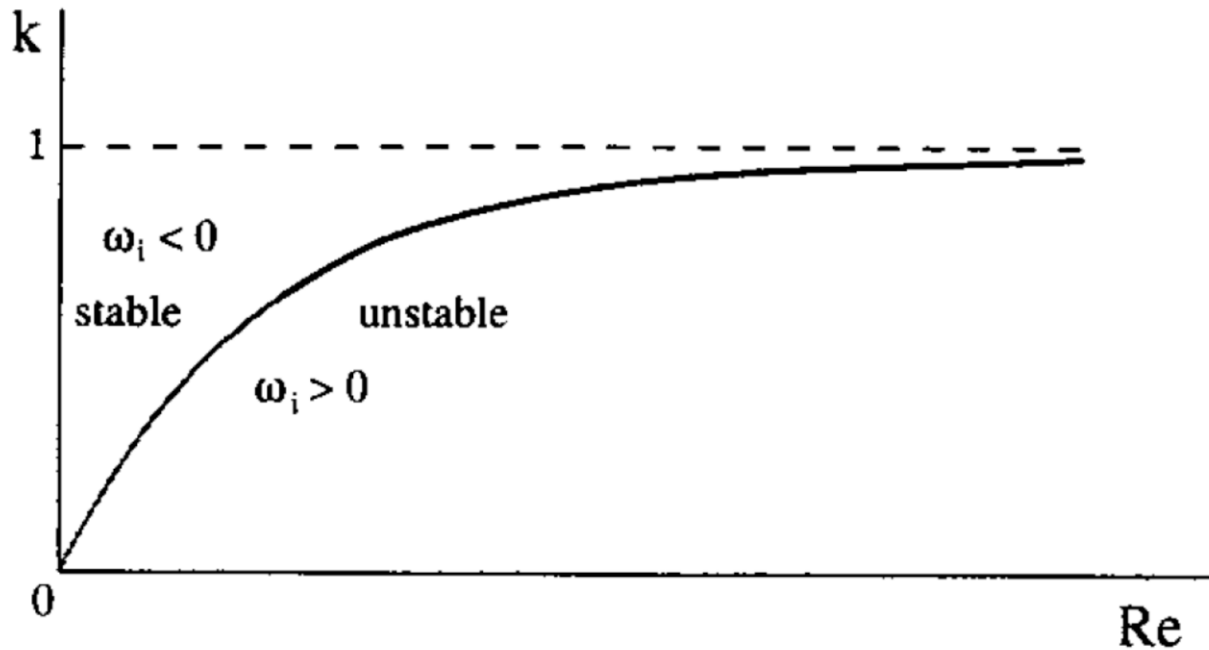
Viscosity has stabilizing influence on K-H instability



PARALLEL FLOW CONCEPTS

Viscous instabilities

Hyperbolic tangent mixing layer

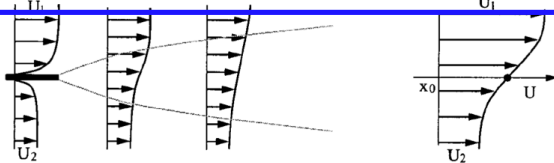


SPATIALLY DEVELOPING SHEAR FLOWS

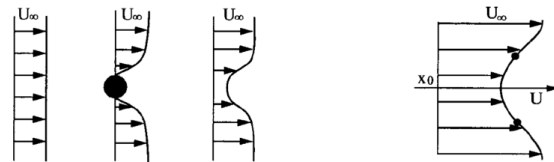
Flat plate boundary layer



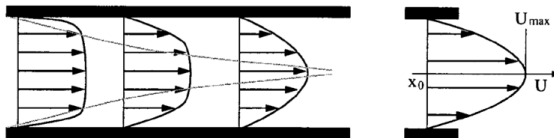
Mixing layer



Cylinder wake



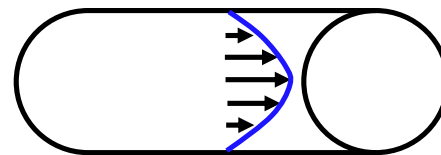
Plane channel flow



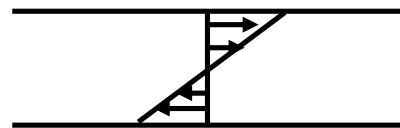
2D jet



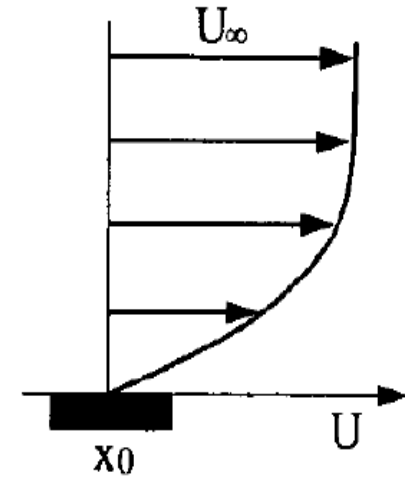
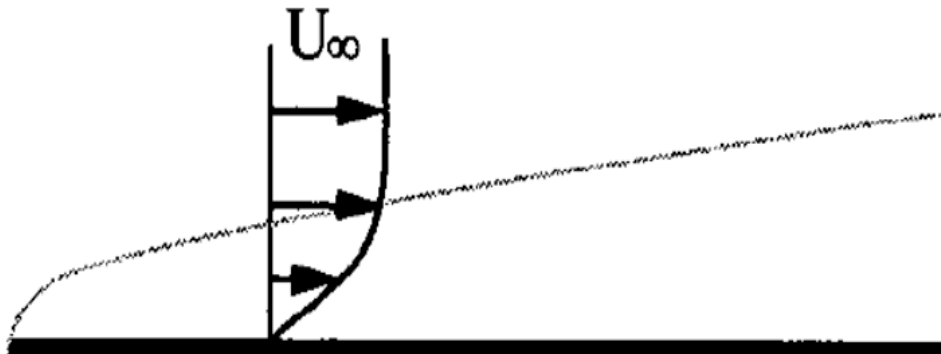
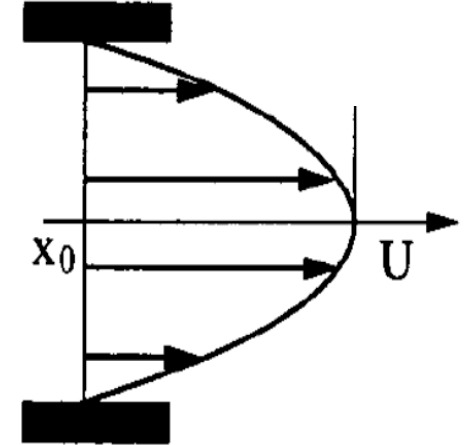
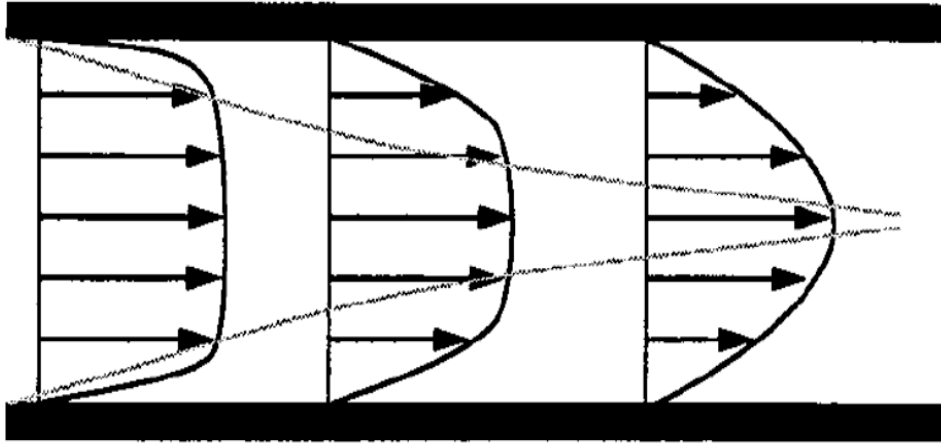
Hagen Poiseuille



Couette

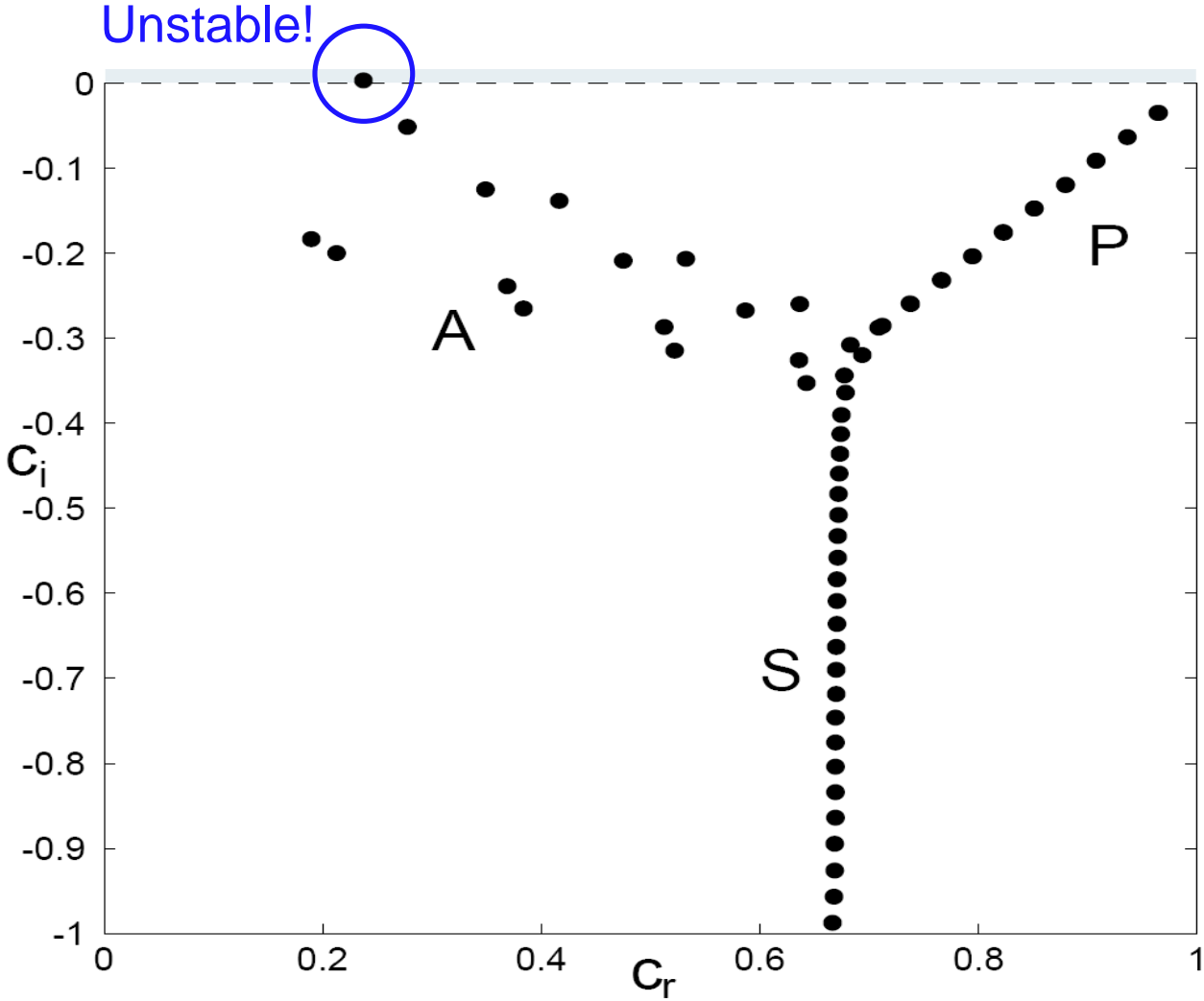


What about inviscidly stable flows (no inflexion point)?

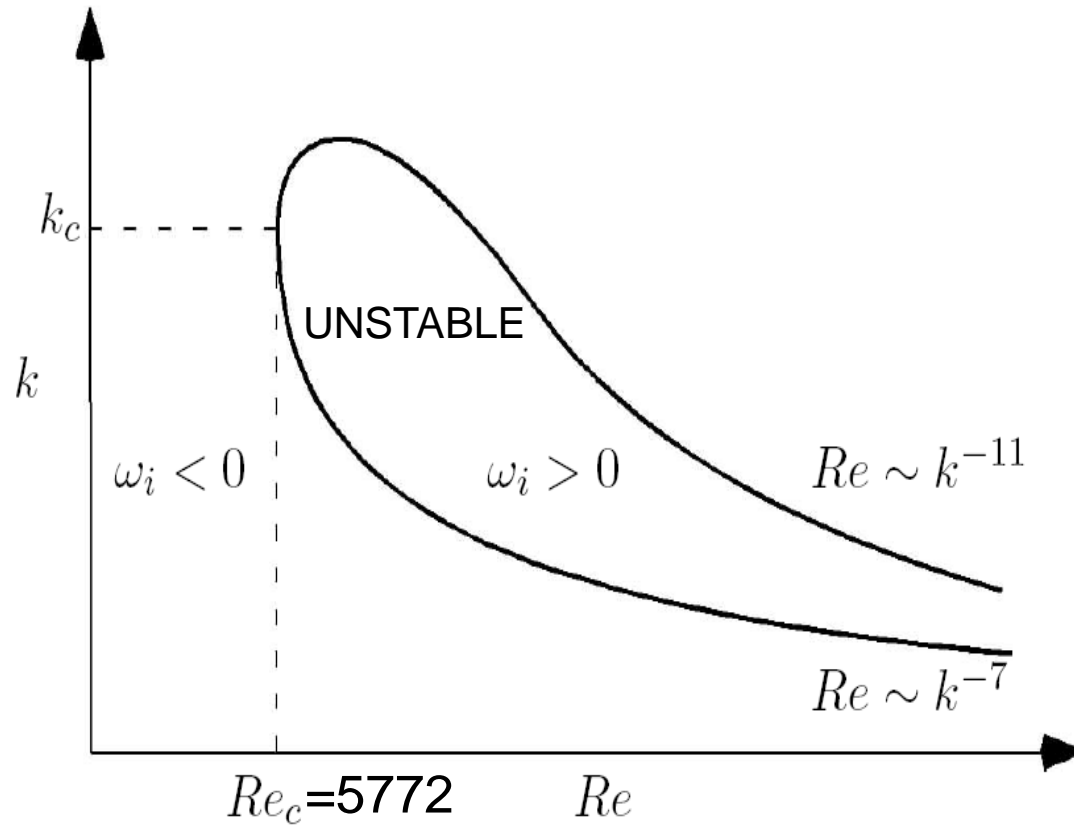


They can be unstable with finite viscosity

Plane poiseuille flow; $Re=10000$; $\alpha=1$, $\beta=0$

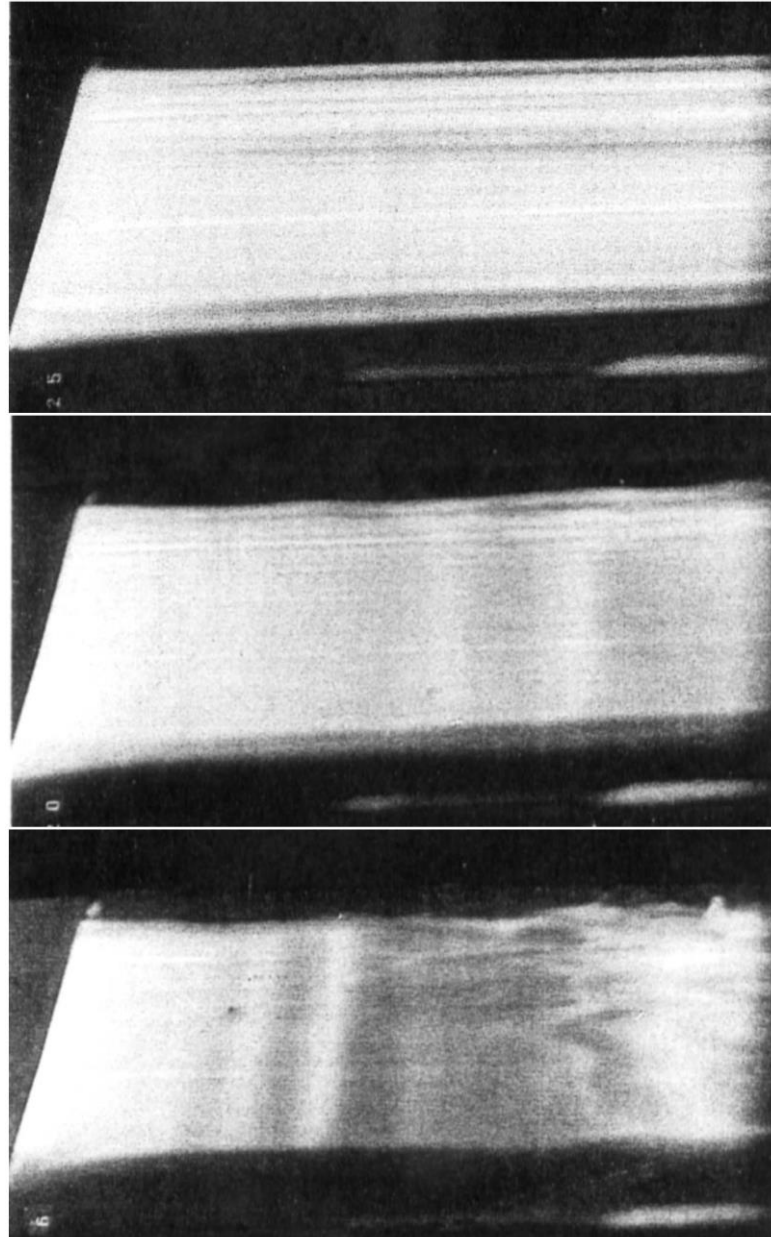


Neutral curve for plane poiseuille flow



– Allure de la courbe de stabilité marginale dans le plan $Re - k$ pour l'écoulement de Poiseuille plan.

Boundary layer at increasing Reynolds number



Boundary layers are destabilized by viscosity

Reynolds Orr equation

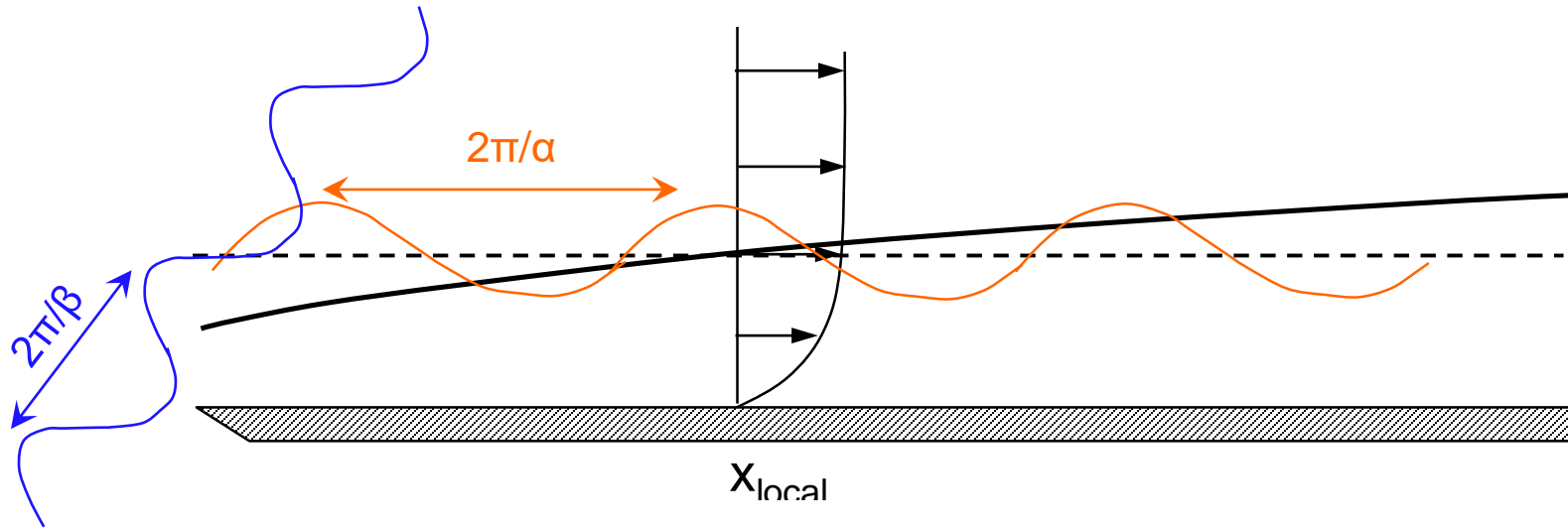
Perturbation kinetic energy: $e_c = \frac{1}{2}(u^2 + v^2 + w^2)$

$$\frac{d}{dt} \int_{y_1}^{y_2} \langle e_c \rangle dy = \int_{y_1}^{y_2} \partial_y \bar{U} \tau_{xy} dy - \frac{1}{Re} \int_{y_1}^{y_2} \langle \omega \cdot \omega \rangle dy$$

Production term

Dissipation term

Local parallel flow approximation



$$(\mathbf{u}, p) = (\mathbf{u}(y), p(y)) e^{\sigma t + i(\alpha x + \beta z)}$$

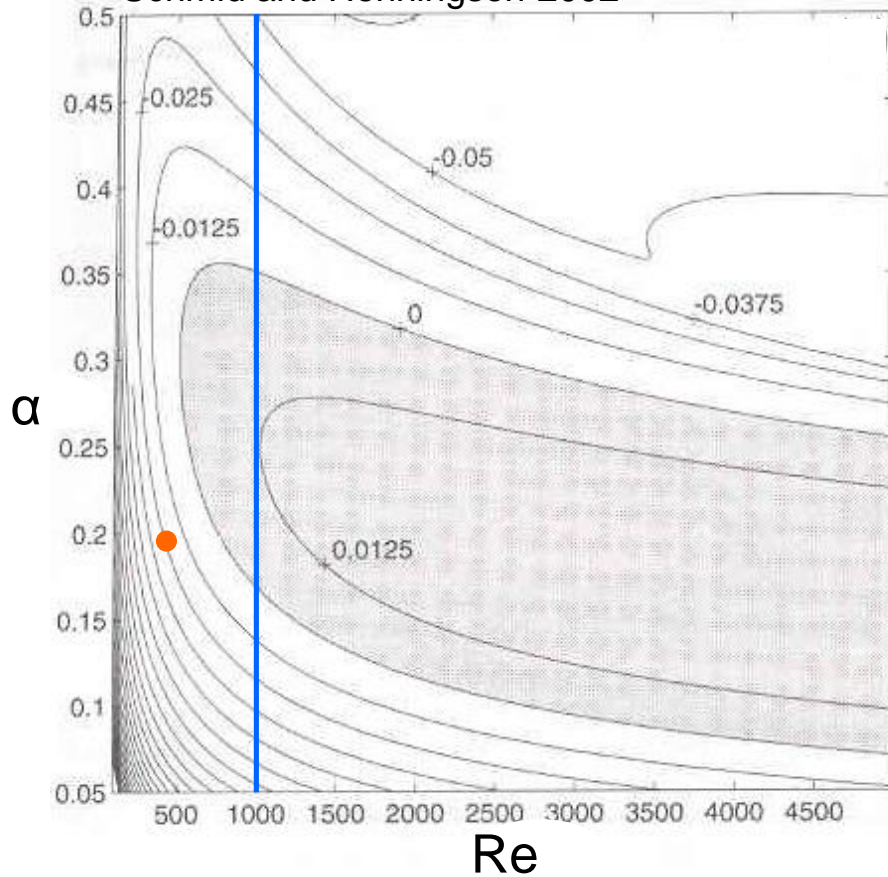
⇒ Orr-Sommerfeld-Squire equation

$$\frac{\partial \mathbf{u}}{\partial t} + \mathbf{U}(y) \nabla \mathbf{u} + \mathbf{u} \nabla \mathbf{U}(y) = -\nabla p + \frac{1}{Re} \nabla^2 \mathbf{u}$$

$$\nabla \cdot \mathbf{u} = 0$$

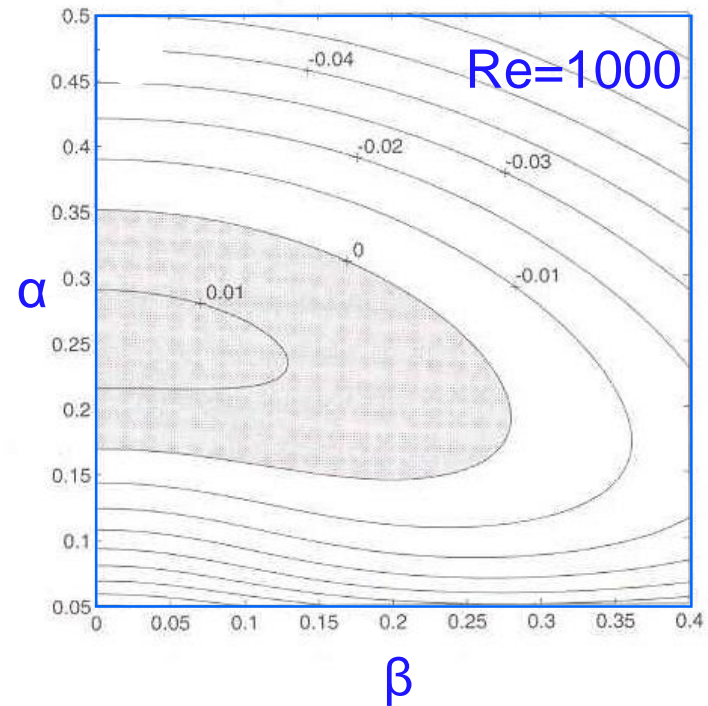
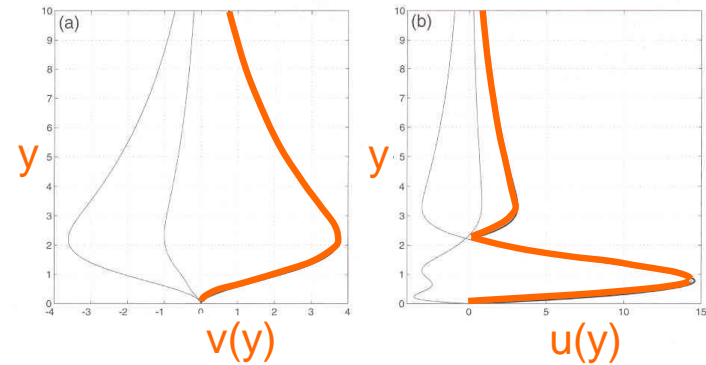
Tollmien Schlichting waves

Schmid and Henningson 2002



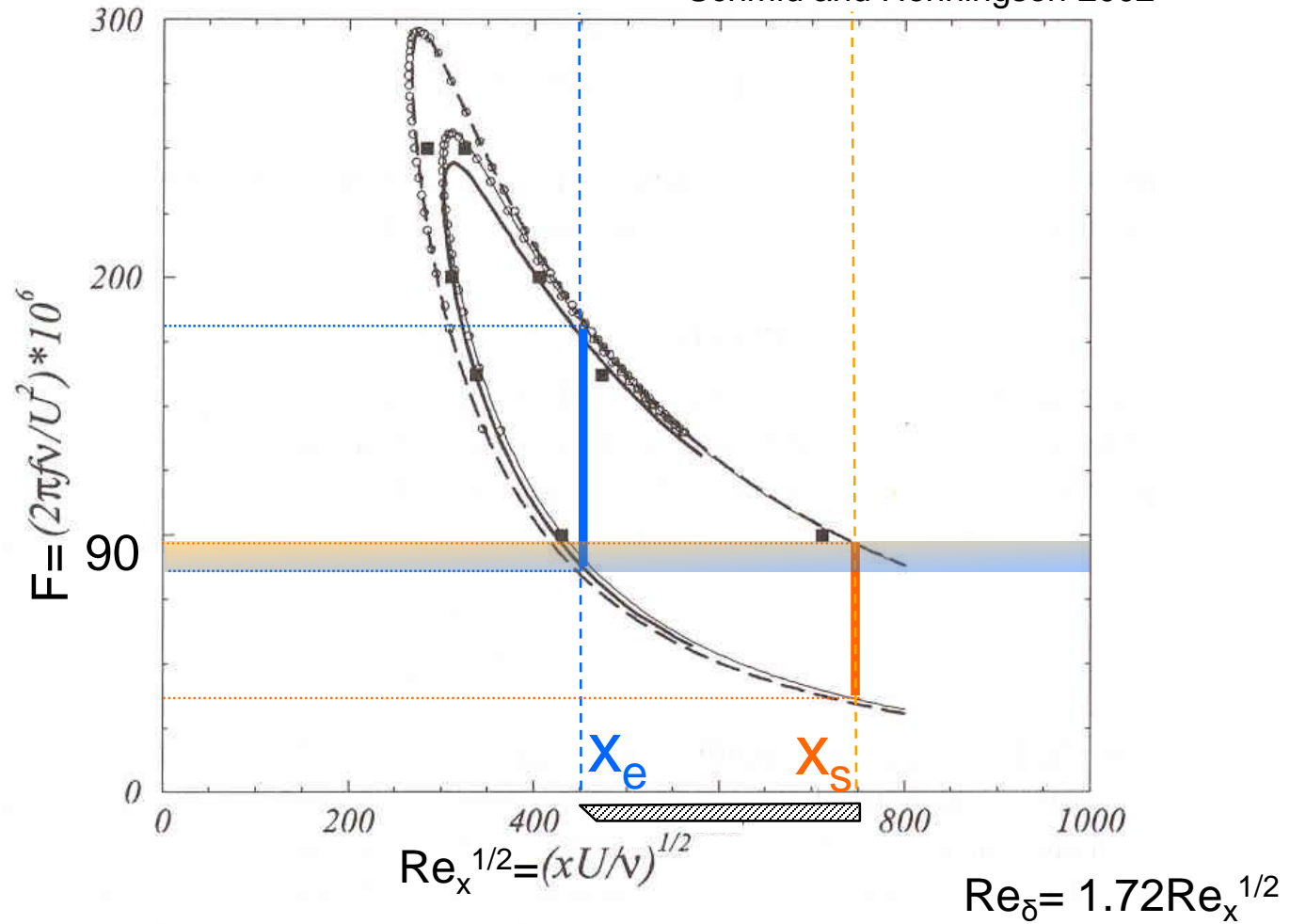
α : axial wavenumber

β : transverse wavenumber

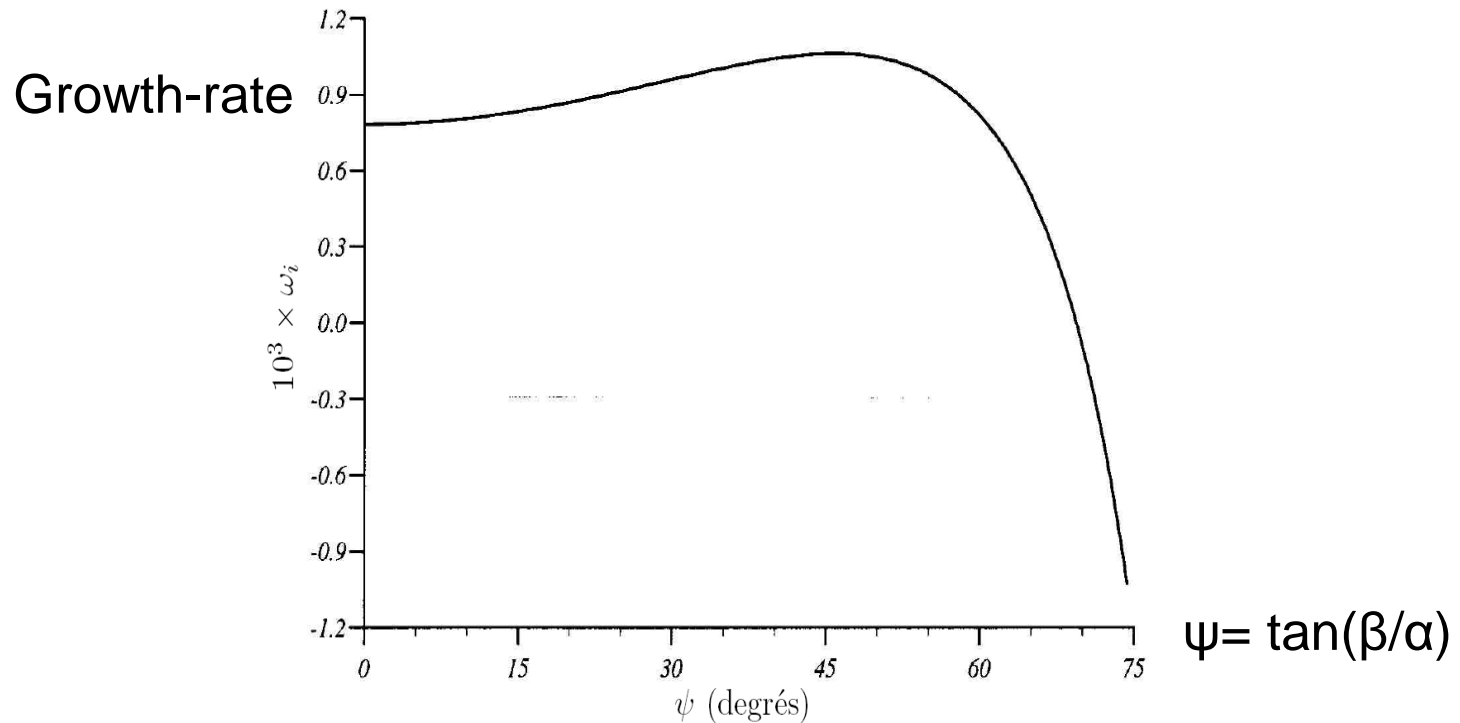


Neutral curve

Schmid and Henningson 2002



Boundary layer at $Re_\delta = 1500$



*Taux de croissance temporel (s^{-1}) de l'instabilité d'une couche limite, en fonction de l'angle ψ de la perturbation avec la direction de l'écoulement de base.
 $R_{\delta 1} = 1500$, $\omega\nu/U_\infty^2 = 0,3 \times 10^{-4}$ (calcul G. Casalis, ONERA).*

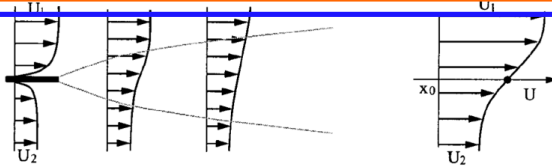
The most unstable perturbation is oblique!

SPATIALLY DEVELOPING SHEAR FLOWS

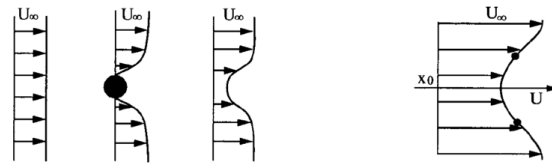
Flat plate boundary layer



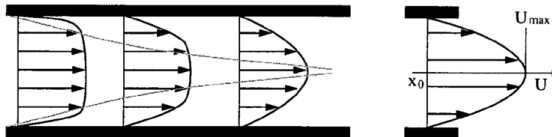
Mixing layer



Cylinder wake



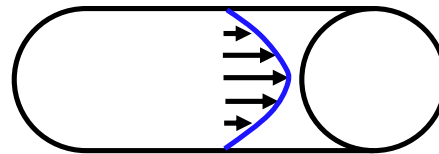
Plane channel flow



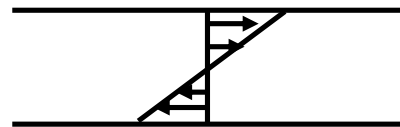
2D jet



Hagen Poiseuille

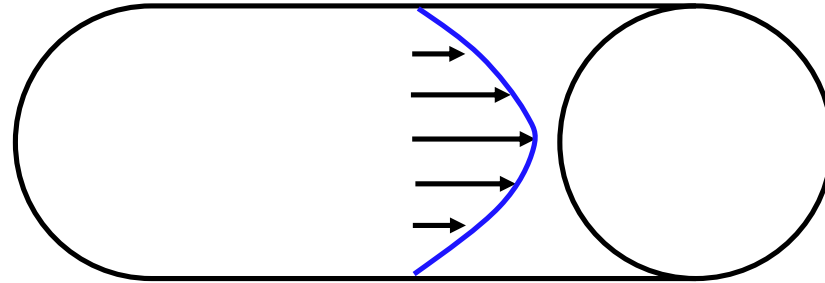


Couette

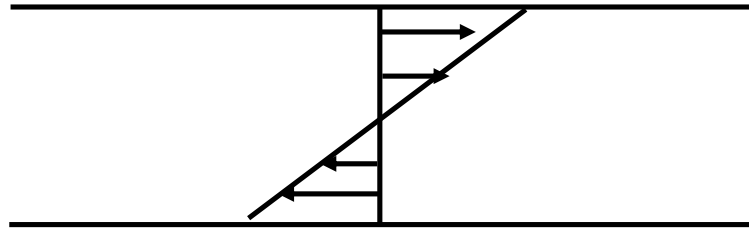


What about inviscidly stable flows (no inflexion point)?

Hagen Poiseuille



Couette



Flow type	Re_{exp}	Re_{lin}
Pipe flow	≈ 2000	∞
Plane Poiseuille flow	≈ 1000	5772
Plane Couette flow	≈ 360	∞

They can also remain stable with finite viscosity

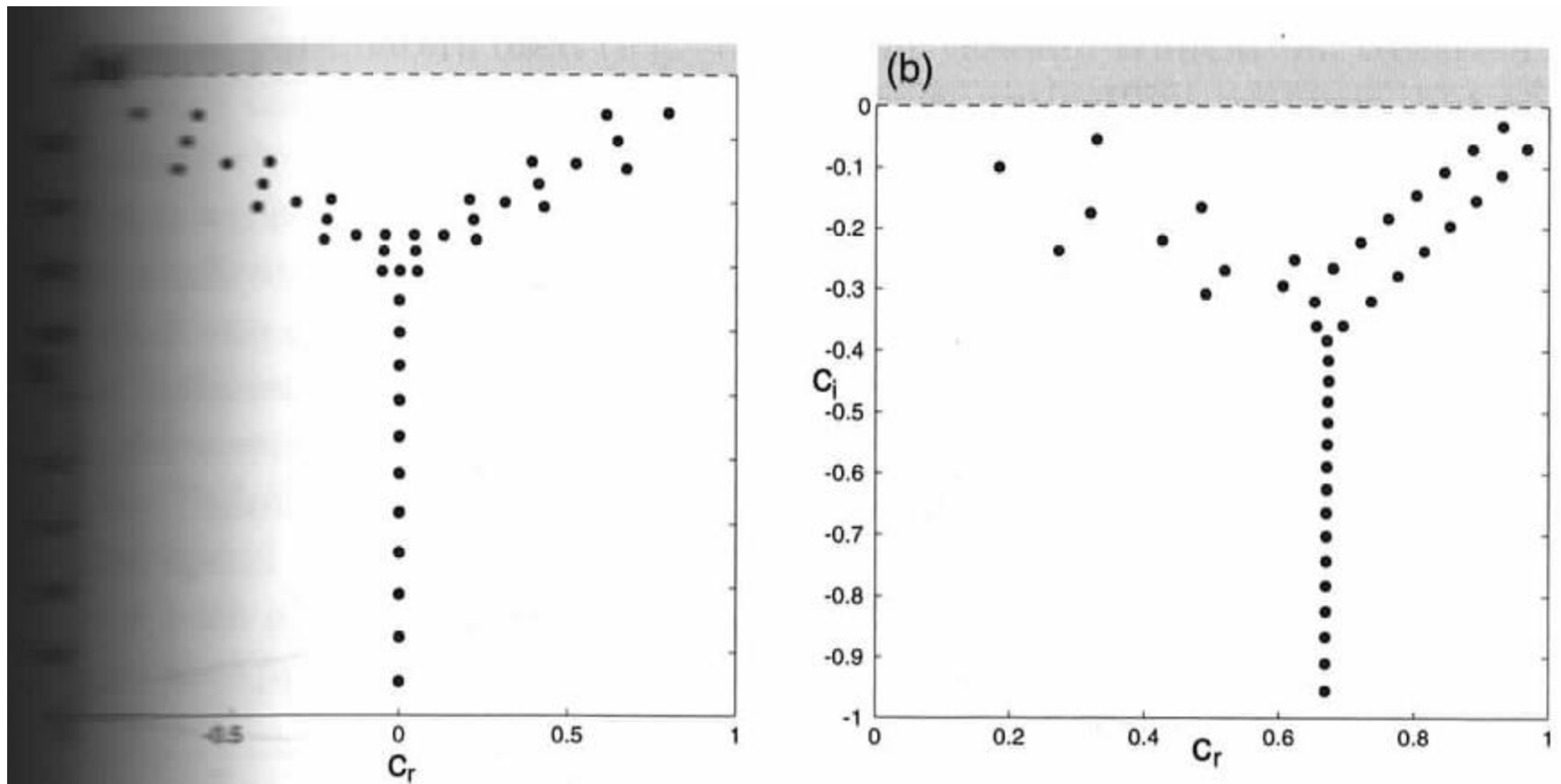


FIGURE 3.3. Spectrum of plane Couette and pipe flow. (a) Plane Couette flow for $\alpha = 1, \beta = 1, \text{Re} = 1000$; (b) Pipe flow for $\alpha = 1, n = 1, \text{Re} = 5000$.

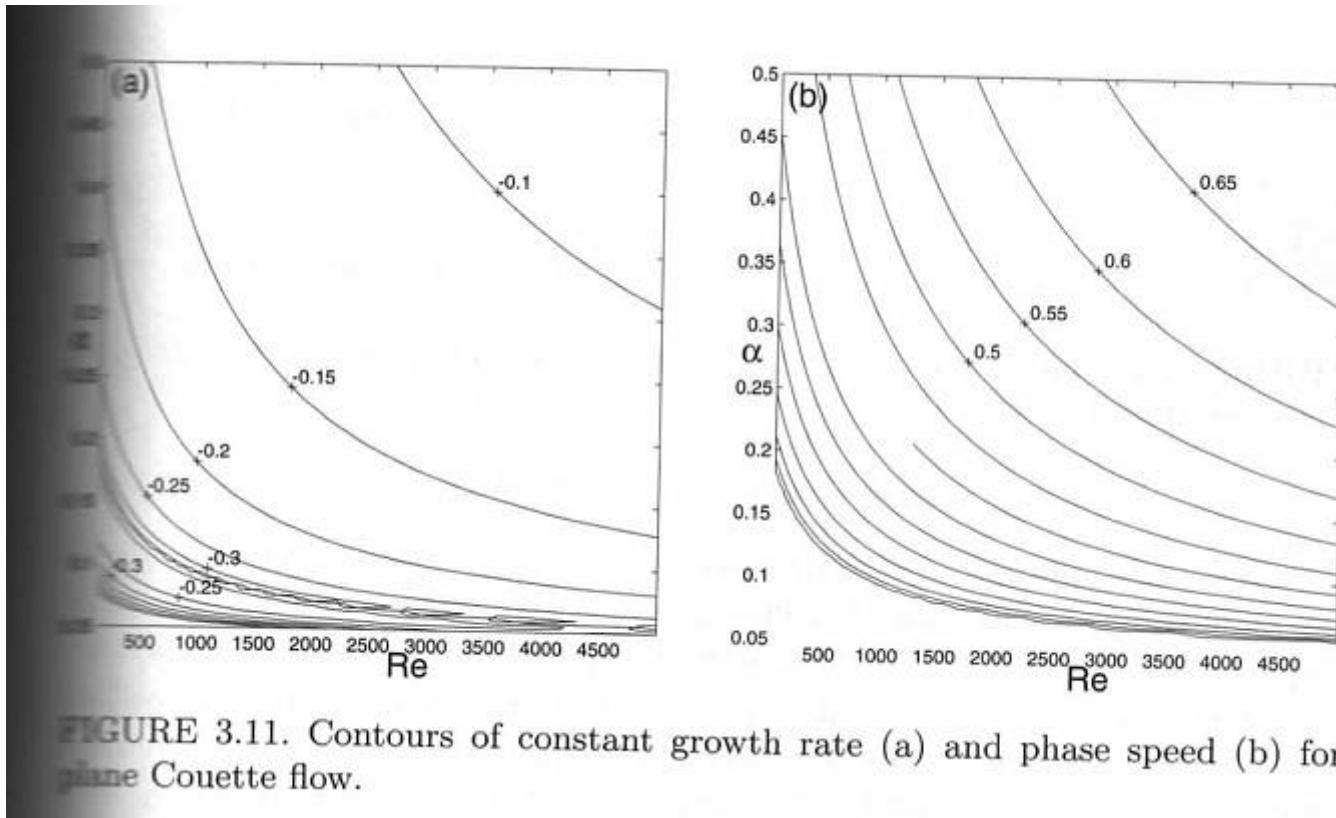


FIGURE 3.11. Contours of constant growth rate (a) and phase speed (b) for plane Couette flow.

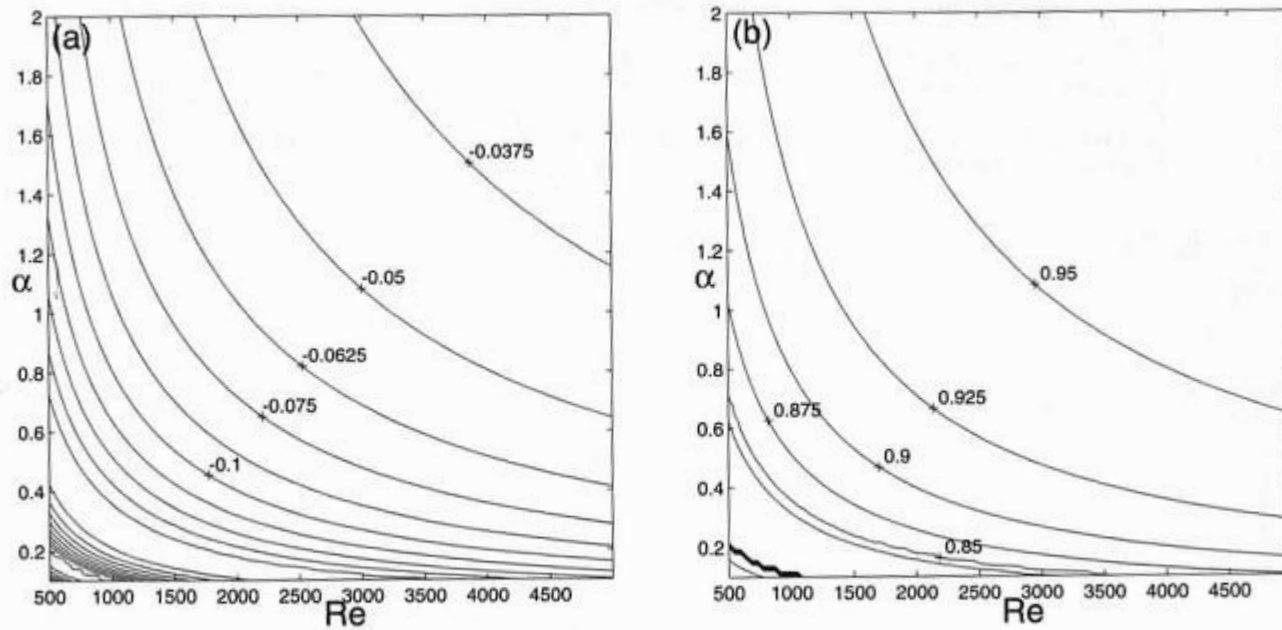
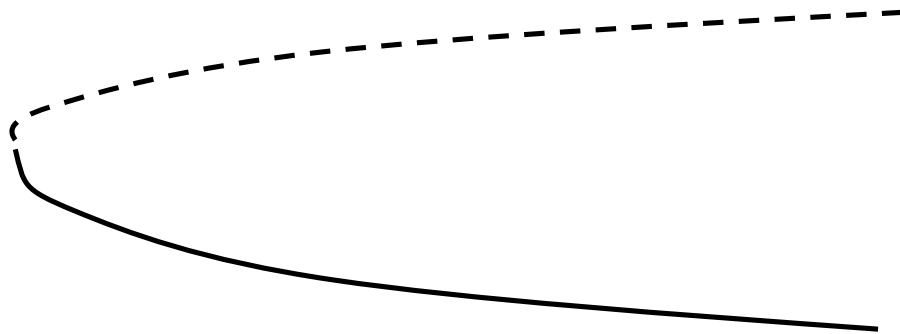
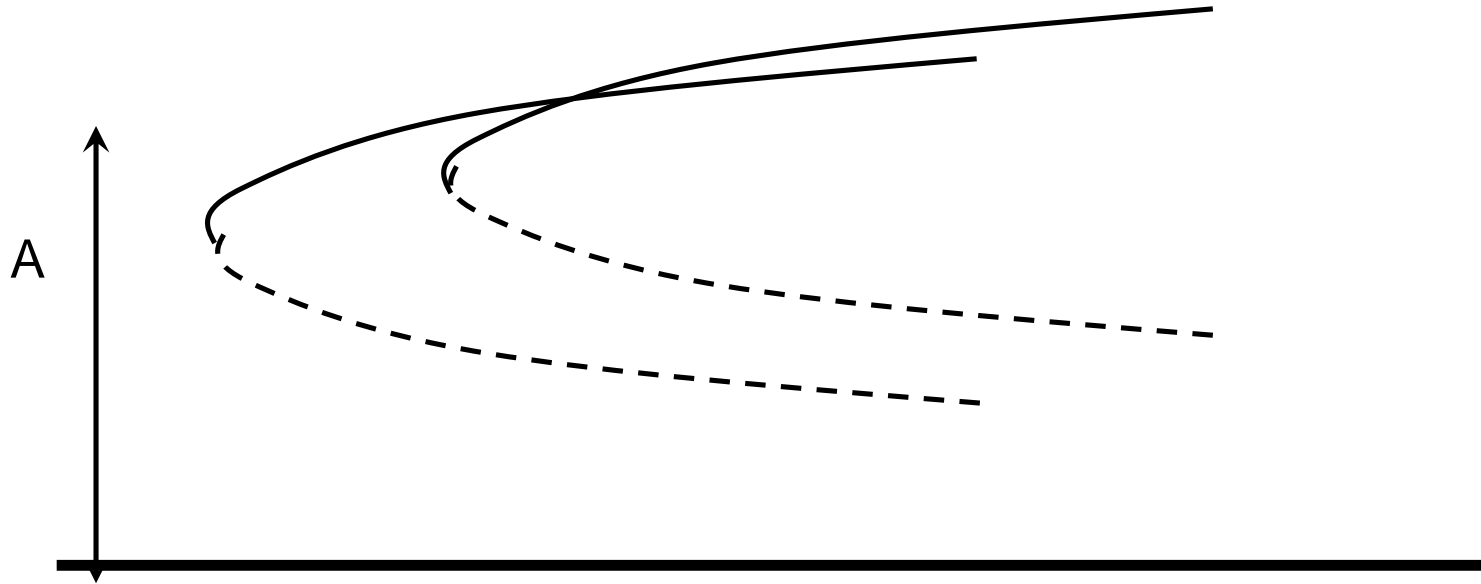


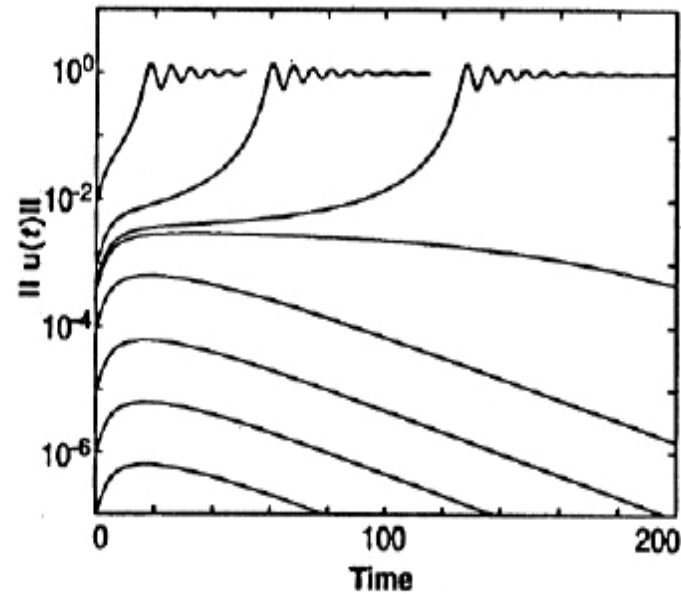
FIGURE 3.12. Contours of constant growth rate (a) and phase speed (b) for pipe Poiseuille flow.

What about nonlinearities?



Edge states

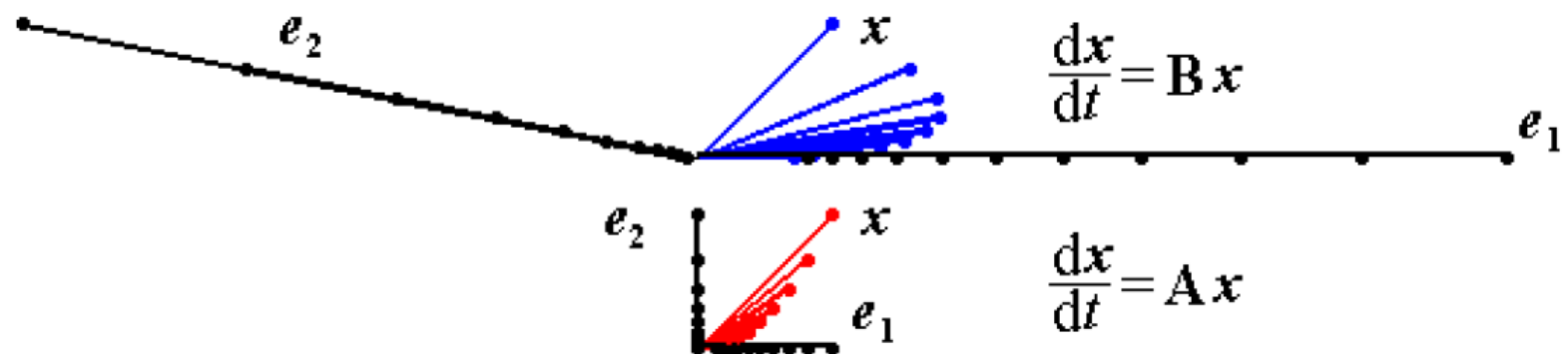
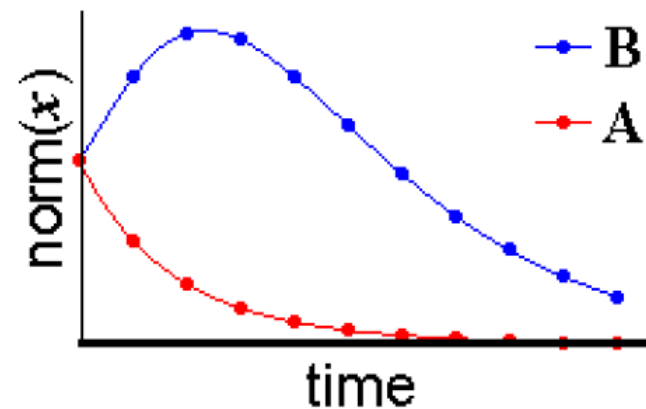
Transient growth and by pass transition



Conditional stability – subcritical bifurcation
Trefethen 1993

$$B = \begin{bmatrix} -1 & 5 \\ 0 & -2 \end{bmatrix}$$

$$A = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix}$$



Definition of optimal gain of a linear system

Linear system $\frac{dq}{dt} = \mathbf{L}q$

Initial condition $q(t = 0) = q_0$

Optimal gain $G(t) = \max_{q_0} \frac{\|q\|}{\|q_0\|} ?$

norm



Definition of optimal gain of a linear system

$$\frac{dq}{dt} = \mathbf{L}q$$

$$q(t = 0) = q_0$$

Matrix exponential

$$q(t) = \exp(\mathbf{L}t)q_0$$

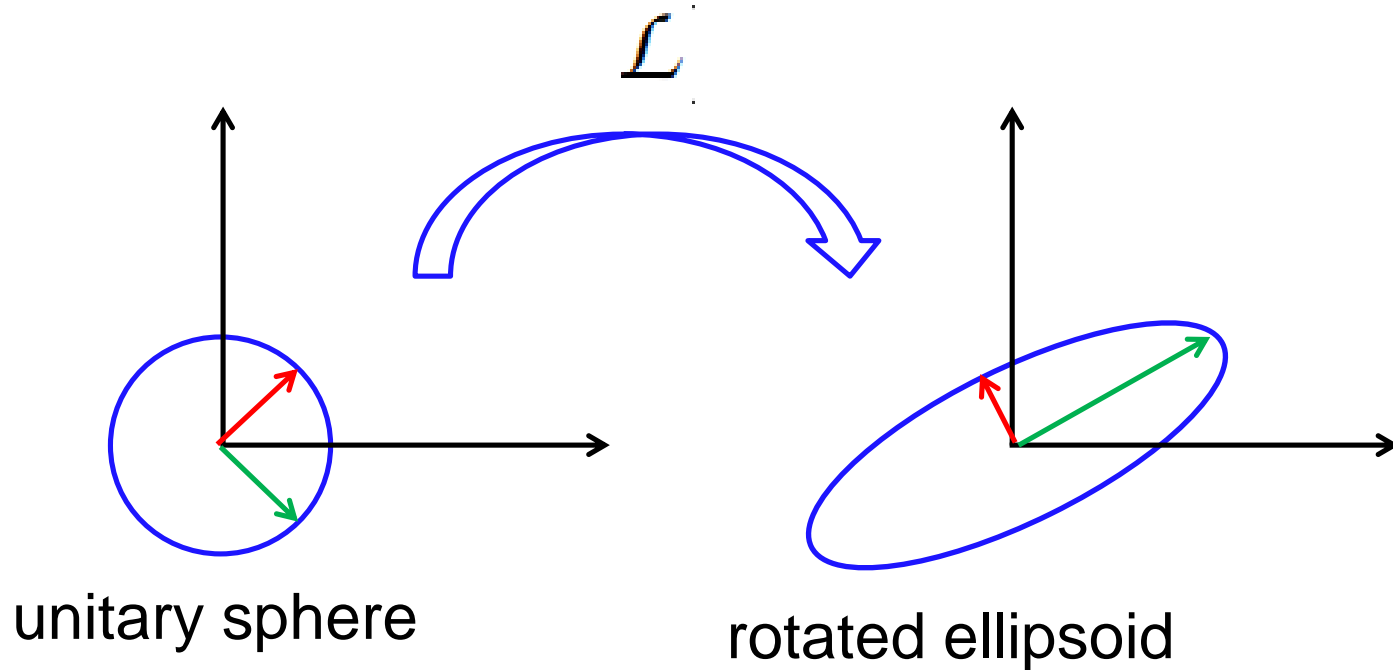
Definition of optimal gain of a linear system

Optimal gain

$$G(t) = \max_{q_0} \frac{\|q\|}{\|q_0\|}$$
$$= \max_{q_0} \frac{\|\exp(t\mathcal{L})q_0\|}{\|q_0\|}$$
$$= \|\exp(t\mathcal{L})\|$$

How to compute a matrix 2-norm?

Optimal gain $G(t) = \|\exp(t\mathcal{L})\|$



Optimal gain is associated to a norm

Kinetic energy written in v, η form

$i\alpha u = \mathcal{D}v - i\beta w$ and $\eta = i\beta u - i\alpha w$

$$E(t) = \frac{1}{2k^2} \int_{\Omega} [|\mathcal{D}v|^2 + k^2|v|^2 + |\eta|^2] d\Omega$$

Optimal gain is associated to a norm

Kinetic energy written in v, η form

$i\alpha u = \mathcal{D}v - i\beta w$ and $\eta = i\beta u - i\alpha w$

$$\begin{aligned} E(t) &= \frac{1}{2k^2} \int_{\Omega} [|\mathcal{D}v|^2 + k^2|v|^2 + |\eta|^2] d\Omega \\ &= \|q\|^2 = \frac{1}{2k^2} \int_{\Omega} \begin{pmatrix} v \\ \eta \end{pmatrix}^H \begin{pmatrix} -\mathcal{D}^2 + k^2 & 0 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} v \\ \eta \end{pmatrix} d\Omega \\ &= \frac{1}{2k^2} \int_{\Omega} q^H M q d\Omega \end{aligned}$$

energy matrix

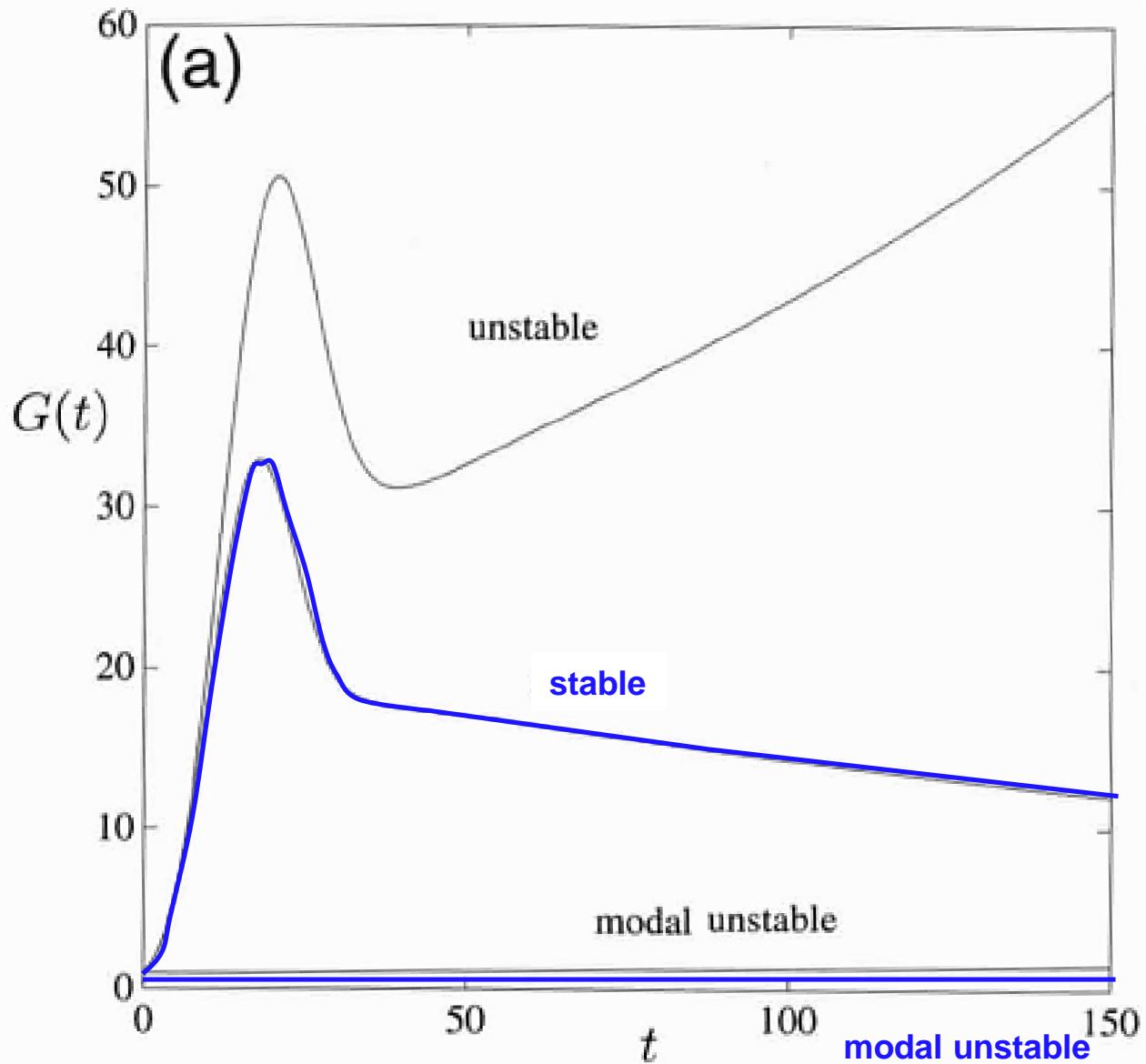
Definition of optimal gain of a linear system

Cholevski dec. $M = F^H F$

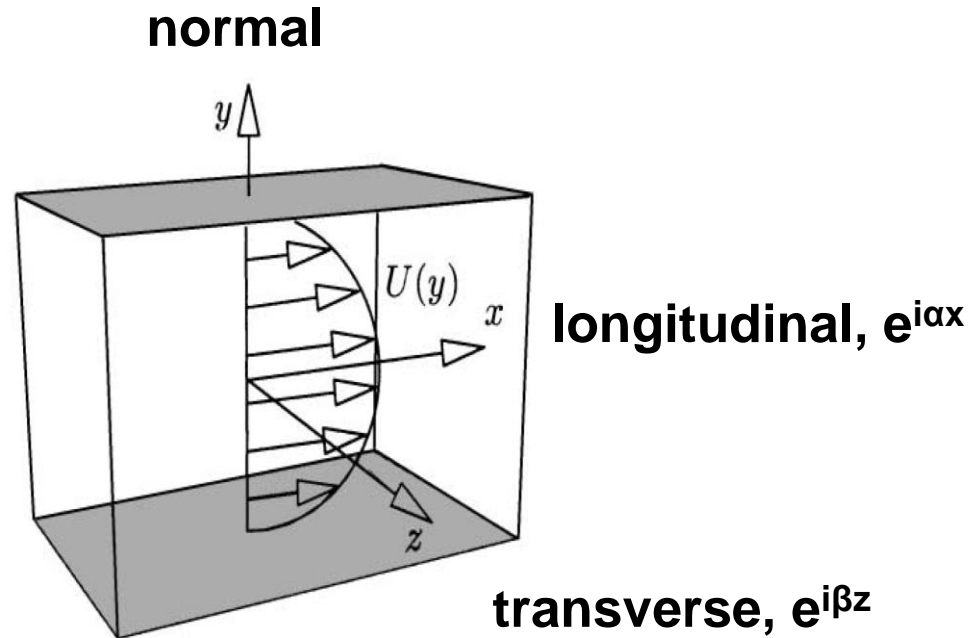
$$\|q\|^2 = \frac{1}{2k^2} \int_{\Omega} q^H F^H F q d\Omega = \frac{1}{2k^2} \int_{\Omega} (Fq)^H Fq d\Omega$$

Optimal gain

$$\begin{aligned} G(t) &= \max_{q_0} \frac{\|q\|_E}{\|q_0\|_E} = \max_{q_0} \frac{\|Fq\|_2}{\|Fq_0\|_2} = \max_{q_0} \frac{\|F \exp(tL)q_0\|_2}{\|Fq_0\|_2} \\ &= \max_{q_0} \frac{\|F \exp(tL)F^{-1} \underbrace{Fq_0}_{=q'_0}\|_2}{\underbrace{\|Fq_0\|_2}_{=q'_0}} = \|F \exp(tL)F^{-1}\|_2 \end{aligned}$$

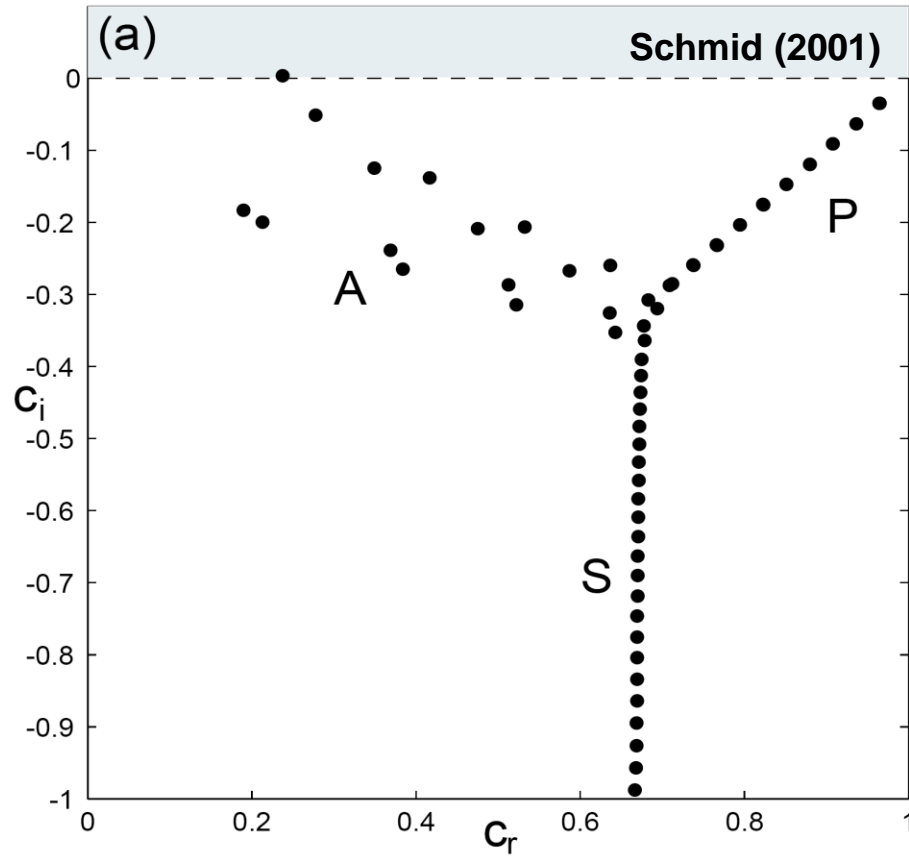


Plane Poiseuille flow



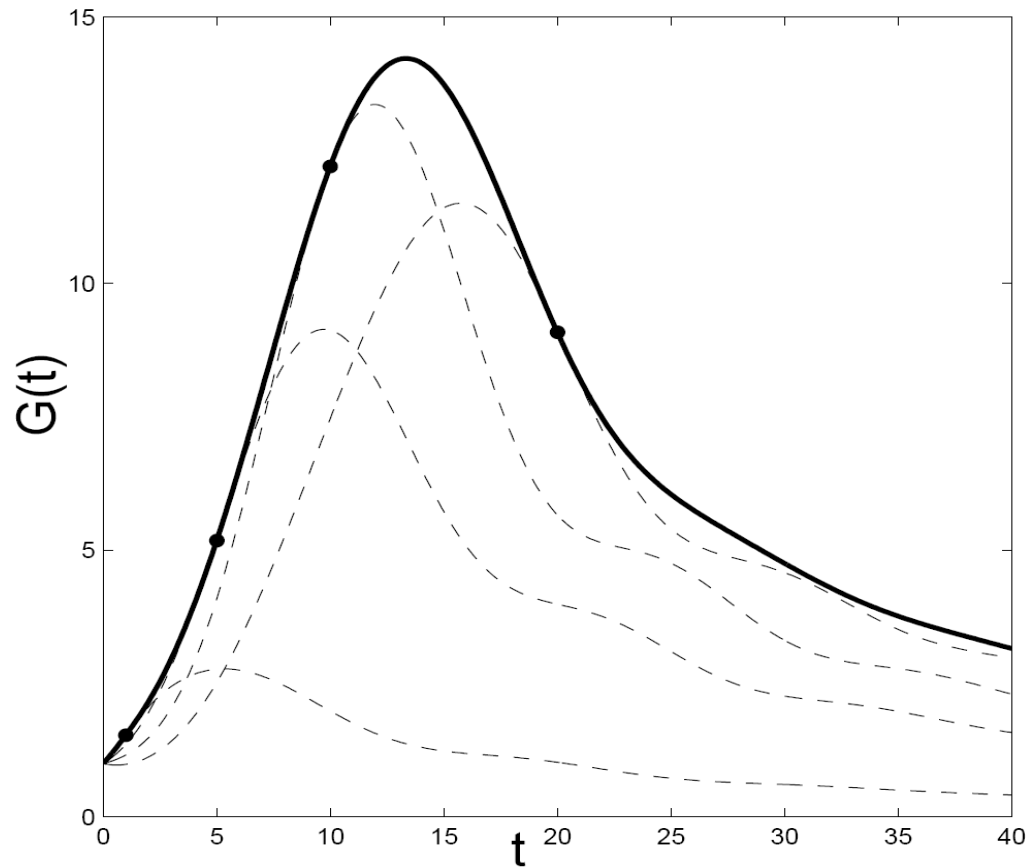
Linearly stable until $Re=5772$, but the transition is observed experimentally close to $Re=1000-2000$!

Plane Poiseuille flow - stability



Spectrum for plane Poiseuille flow for $\alpha = 1, \beta = 0, Re = 10000$.

Orr mechanism (2D)

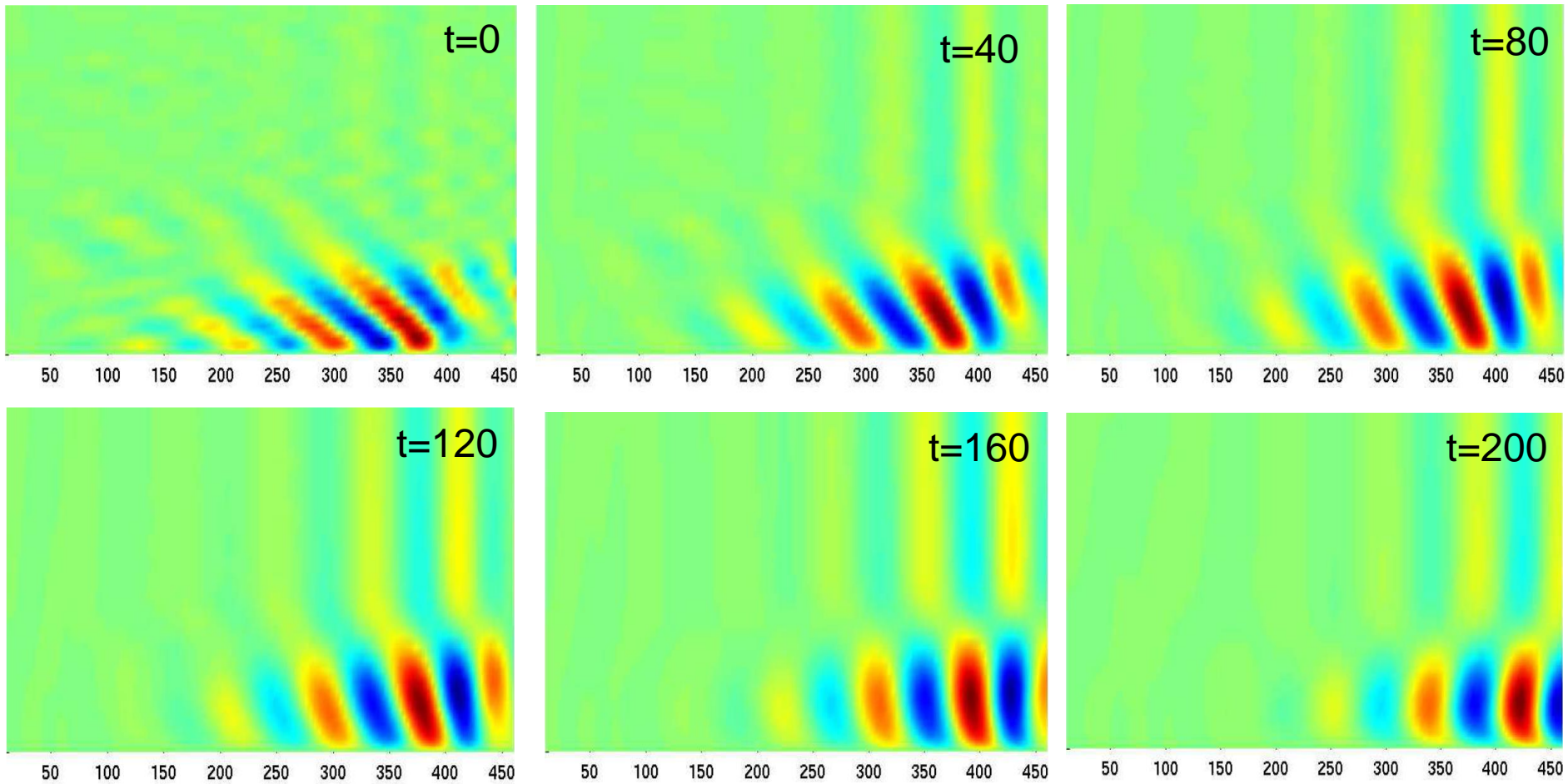


Amplification $G(t)$ for Poiseuille flow with $Re = 1000, \alpha = 1$ (solid line)

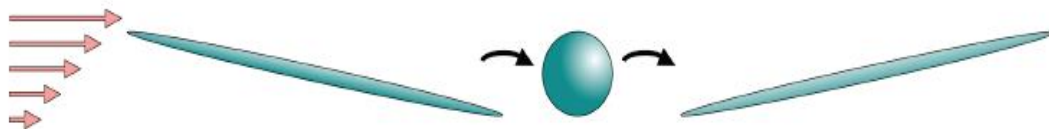
« **By-pass transition** »

Trefethen et al (1993), Buttlar & Farrell (1993), Schmid & Henningson (2001)

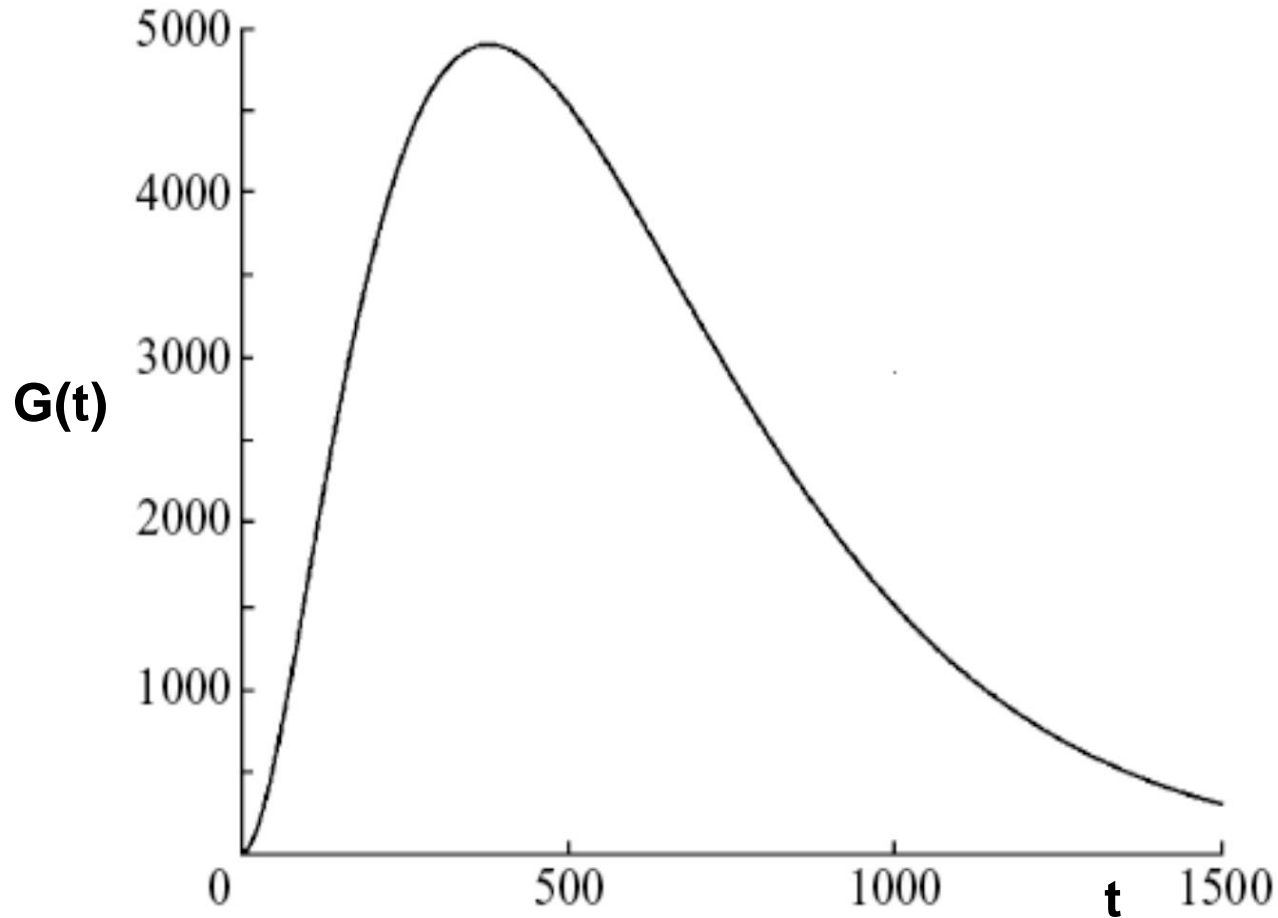
Optimal perturbation (here in boundary layer)



Orr mechanism



Plane Poiseuille flow Lift-up mechanism (3D)

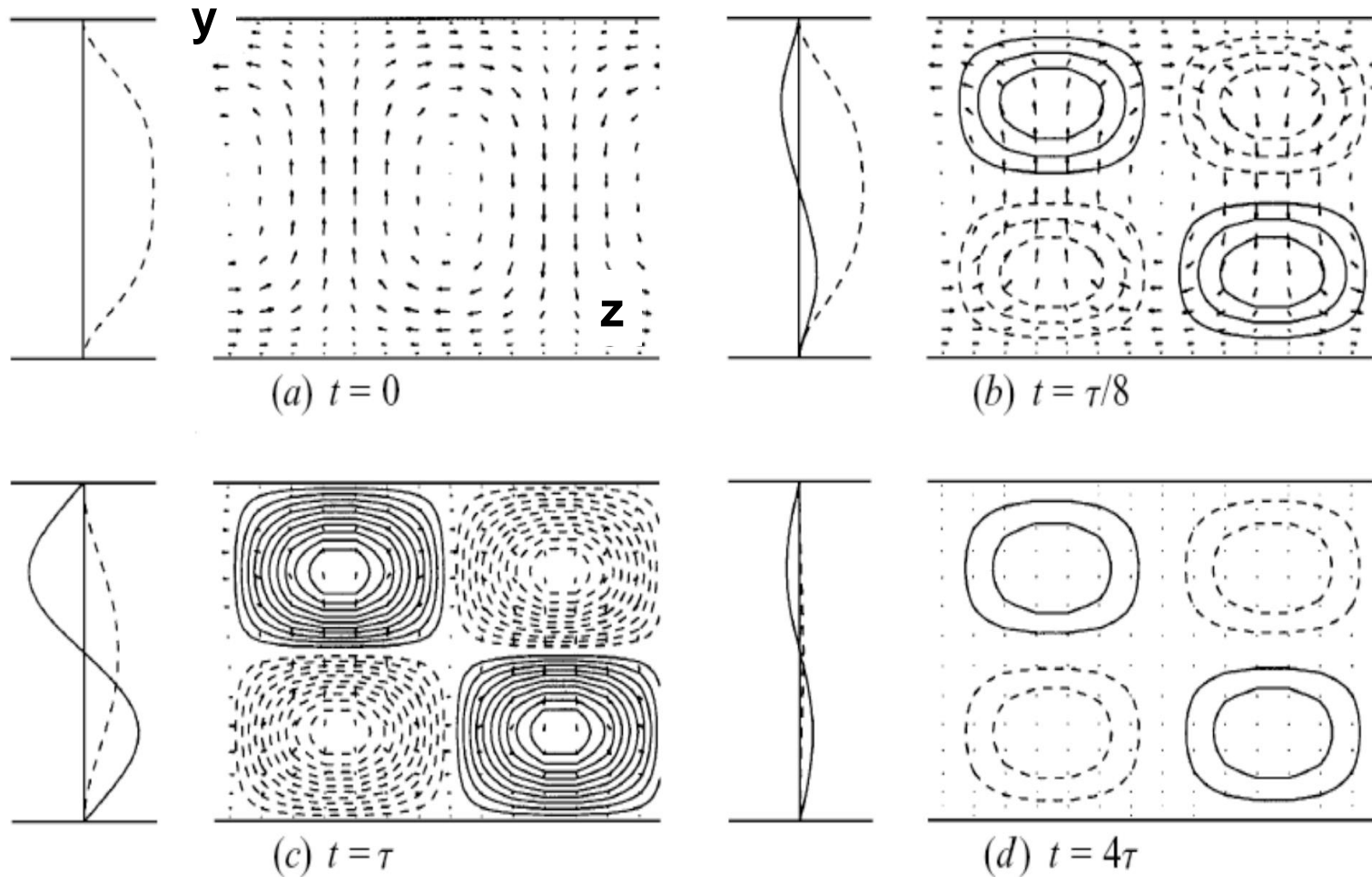


$Re=5000, \alpha=0, \beta=1$

« **By-pass transition** »

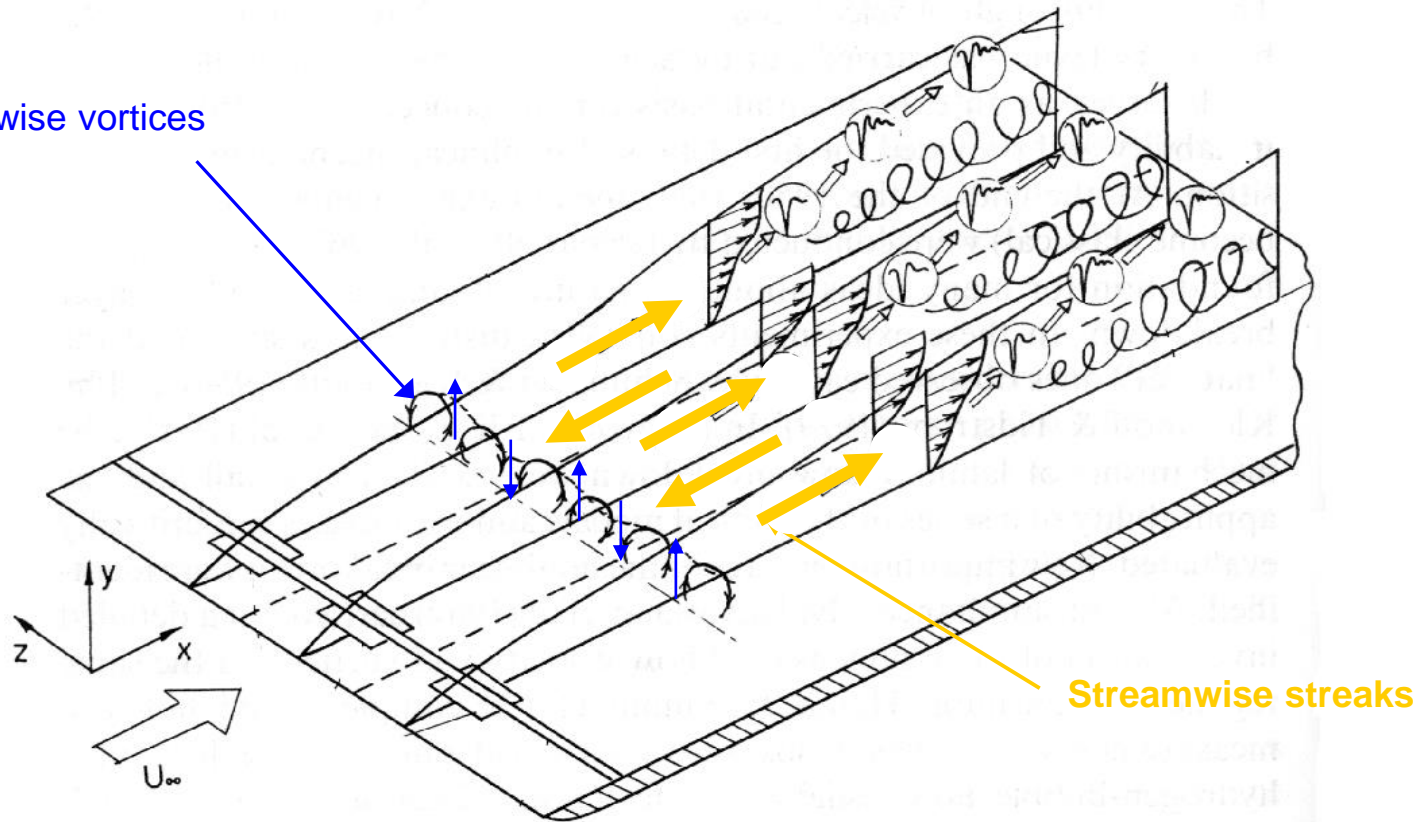
Lift-up mechanisms

Optimal transformation of vortices into streaks



Lift-up mechanism

Streamwise vortices

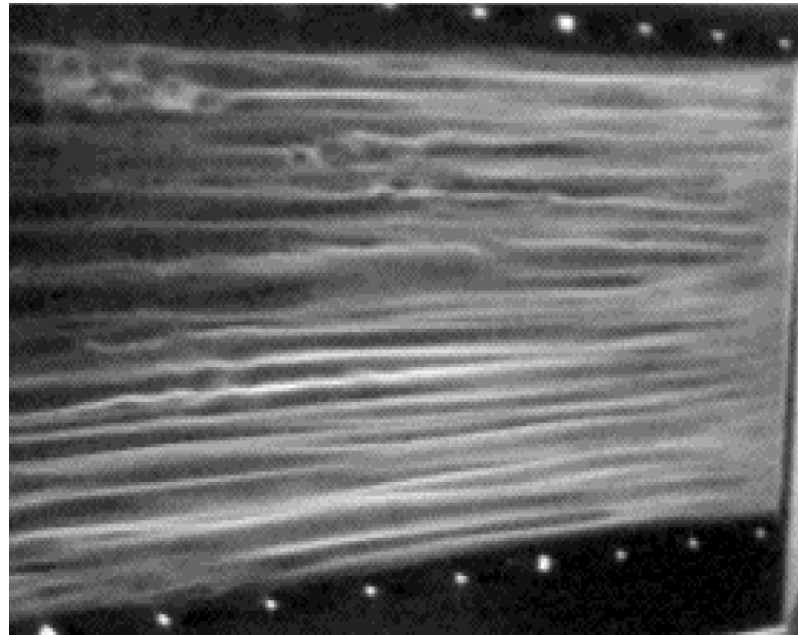


Streamwise streaks

Schmid & Henningson.(2001)

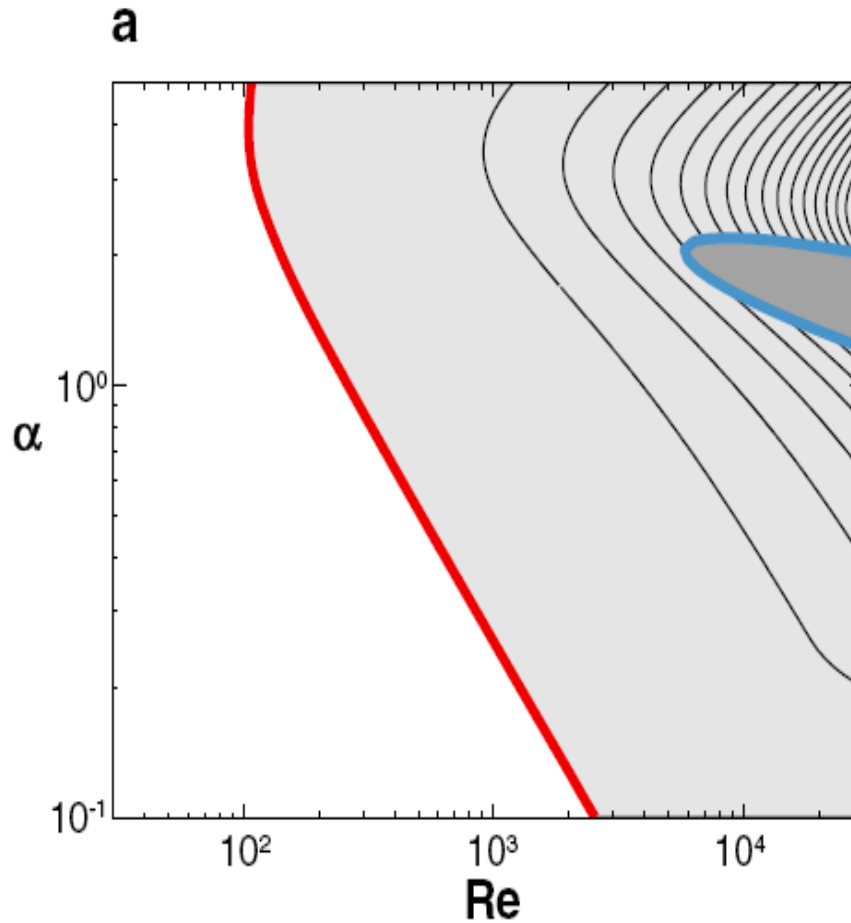
Lift-up mechanism

Optimal transformation of vortices into streaks



Alfredson & Matsubara (1996), streaky structures in the boundary layer

Isolines of maximum transient amplification $\beta=0$



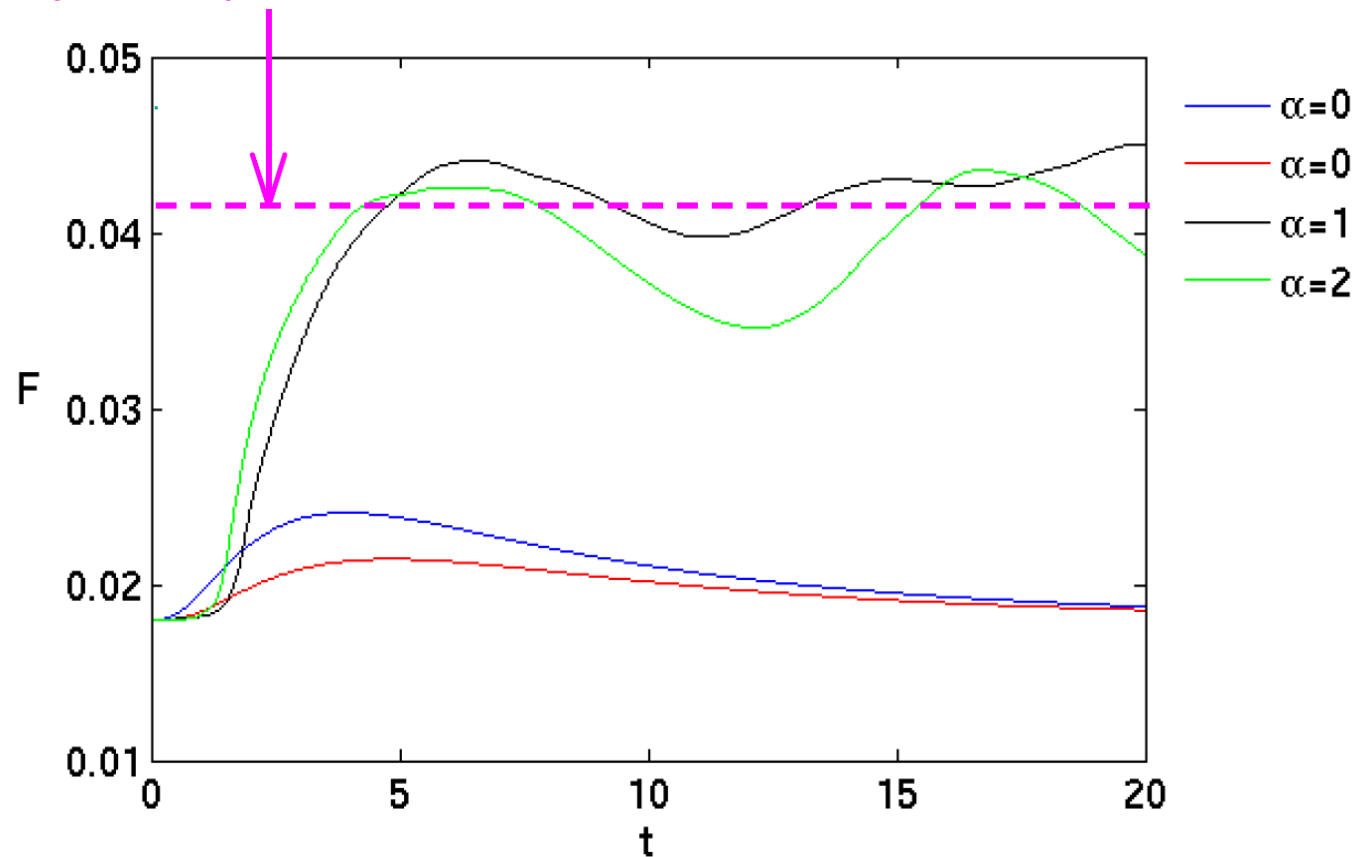
« **By-pass transition** »

	$G_{\max} (10^{-3})$	t_{\max}	α	β
Plane Poiseuille	0.20 Re^2	0.076 Re	0	2.04
Couette	1.18 Re^2	0.117 Re	$35/\text{Re}$	1.6
Pipe	0.07 Re^2	0.048 Re	0	1
Boundary layer	1.50 Re^2	0.778 Re	0	0.65

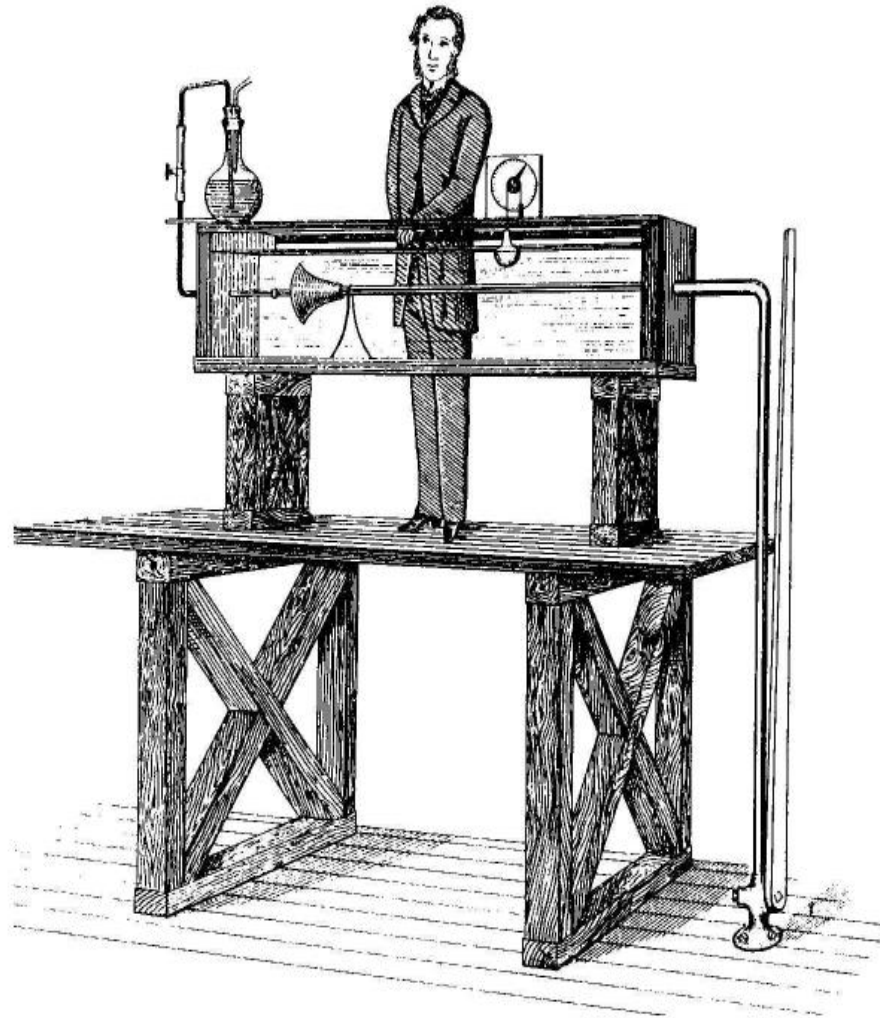
Lift up mechanism in a square duct in the stable regime

Bye-pass transition to turbulence

fully developed turbulence

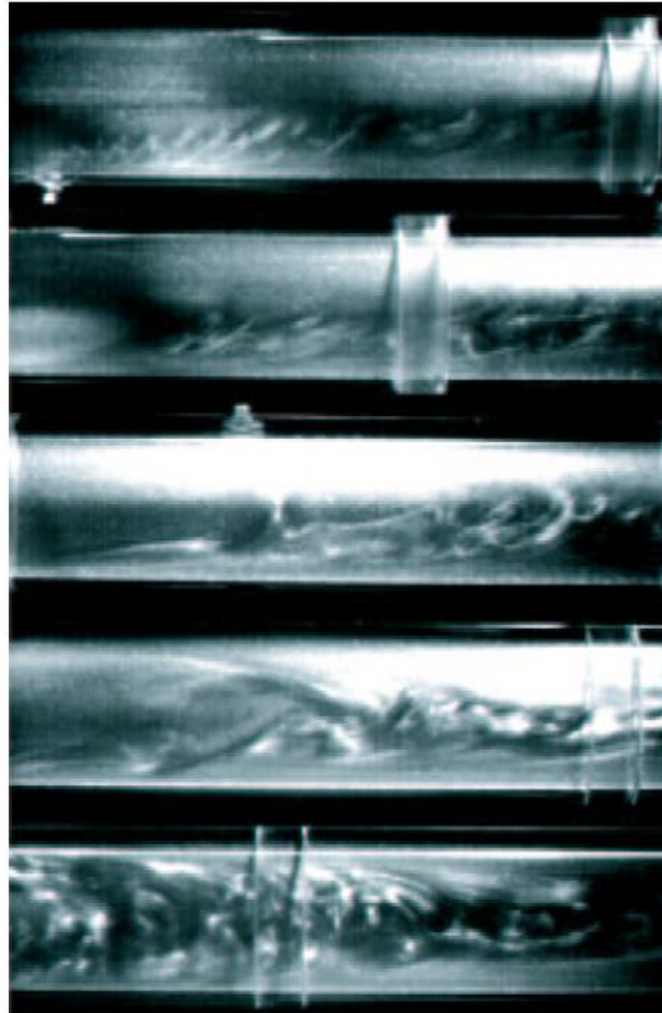


Bottaro et al. (2008)



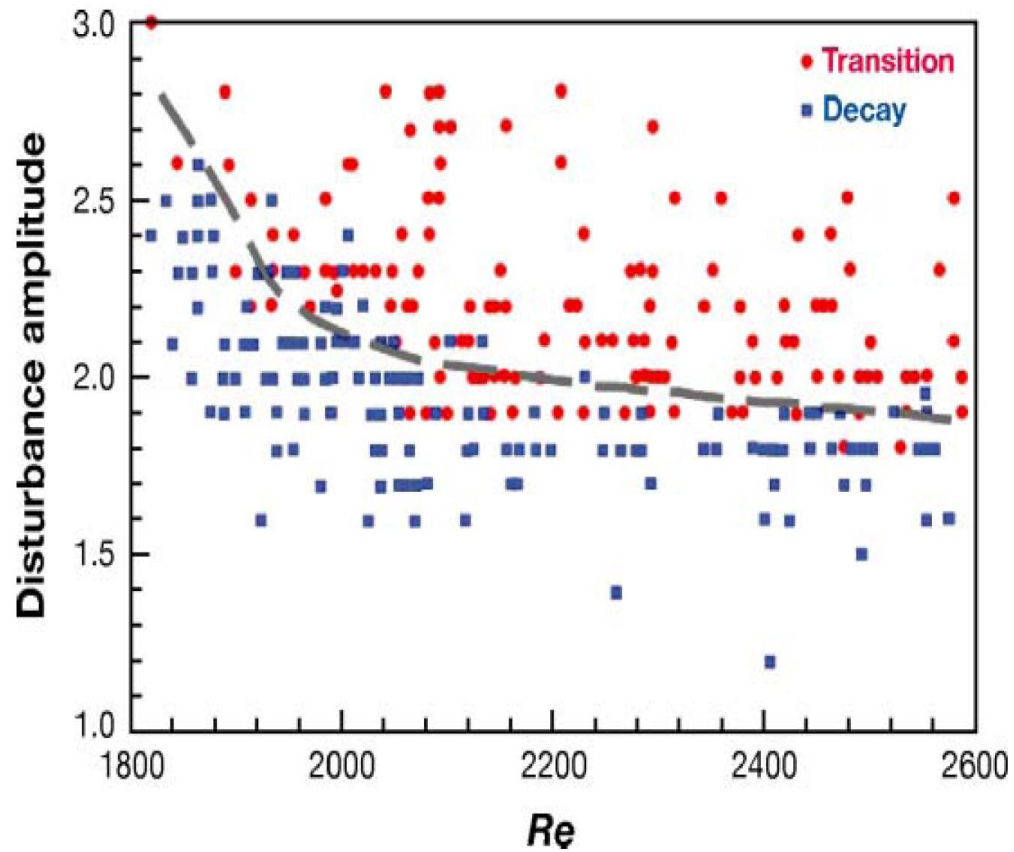
5.1 – Osborne Reynolds en 1883 derrière son expérience à Manchester.

Transition in Cylindrical Pipe Poiseuille flow



Mullin (2008)

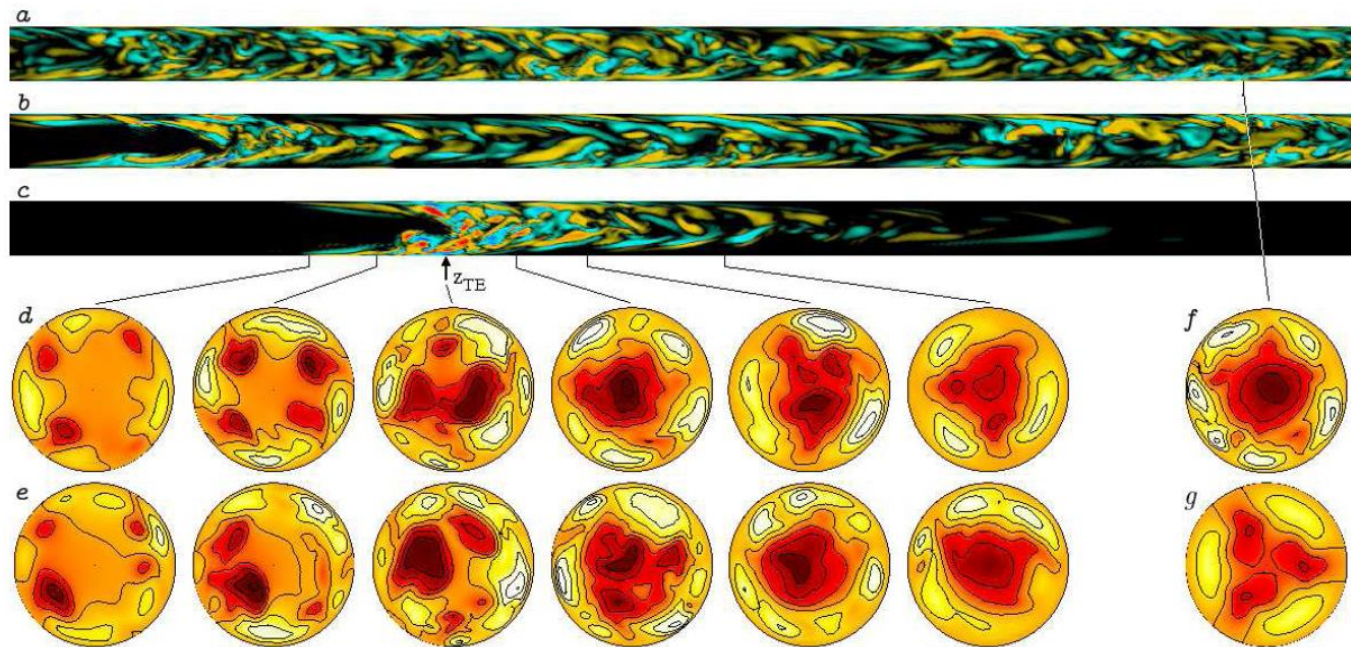
Transition in Cylindrical Pipe Poiseuille flow



Mullin (2008)

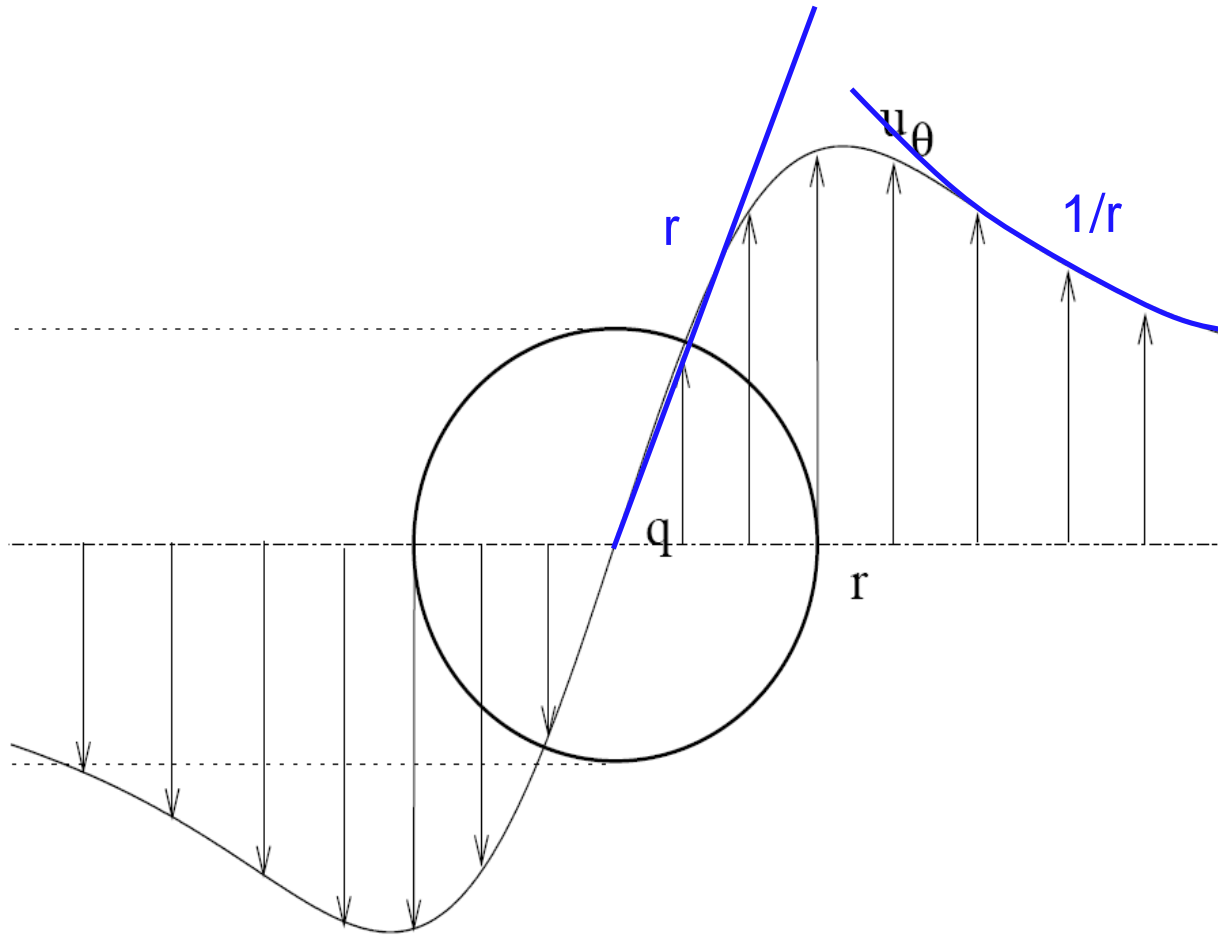
Transition in Cylindrical Pipe Poiseuille flow

Numerical study



Kerswell (2008)

Tourbillon de Lamb-Oseen



Stable lineairement!

TOWARDS AN ELLIPTICAL STATE

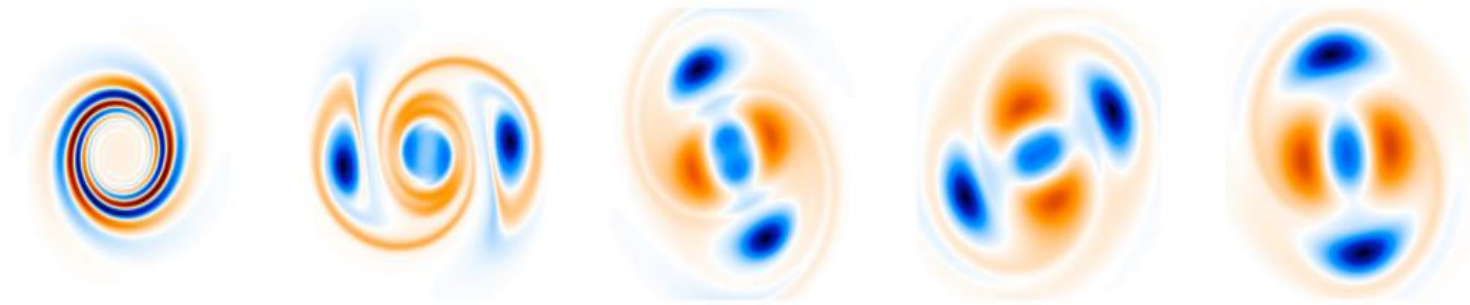
Nonlinear evolution of the optimal perturbation with initial amplitude below a given threshold...



$Re = 1000$

TOWARDS AN ELLIPTICAL STATE

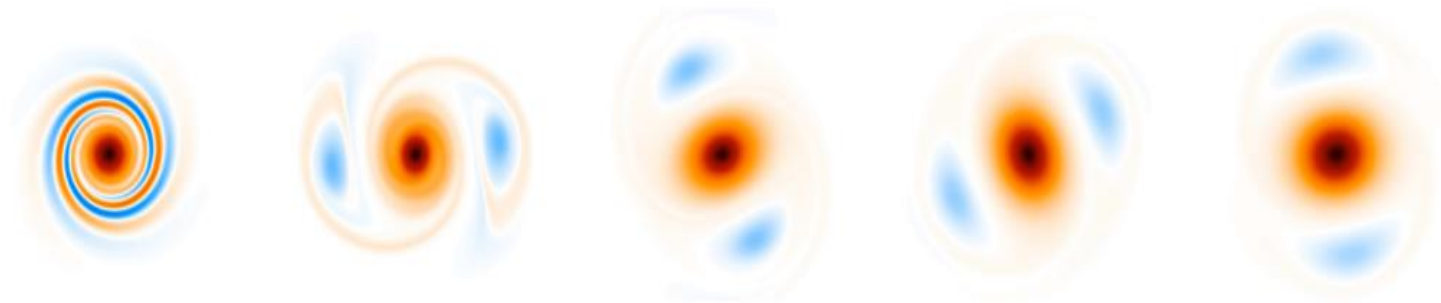
... and now *ABOVE* the threshold



$Re = 1000$

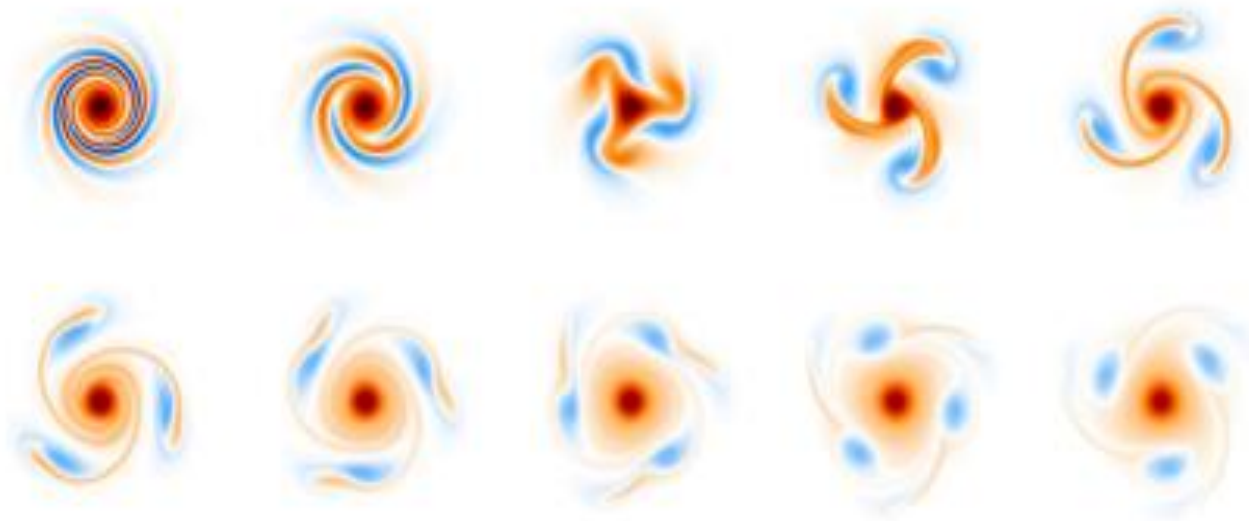
TOWARDS AN ELLIPTICAL STATE

Reconstructed flow

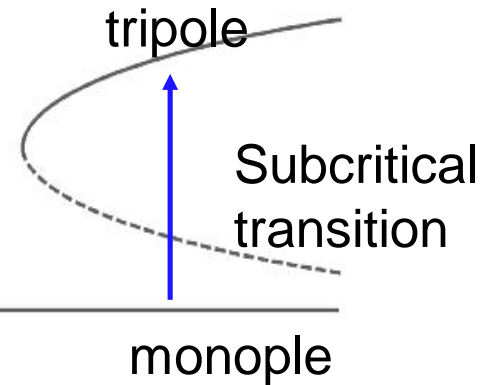


$Re = 1000$

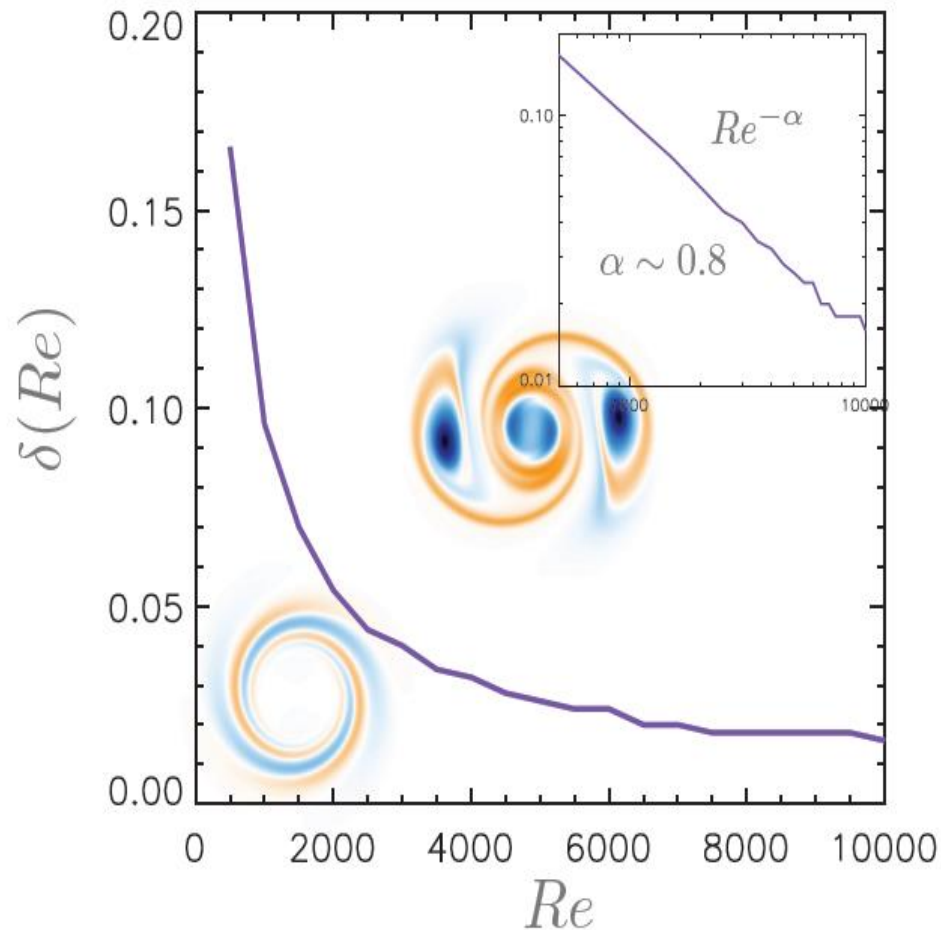
Tripolar vortices?



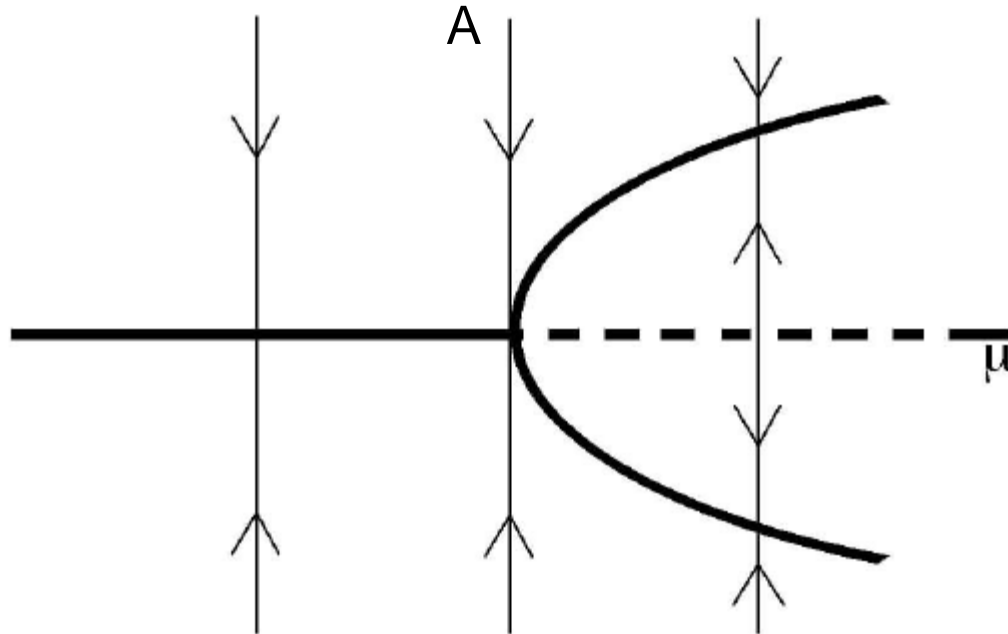
BASIN OF ATTRACTION'S SHRINKAGE



Lamb-Oseen vortex'
bifurcation diagram

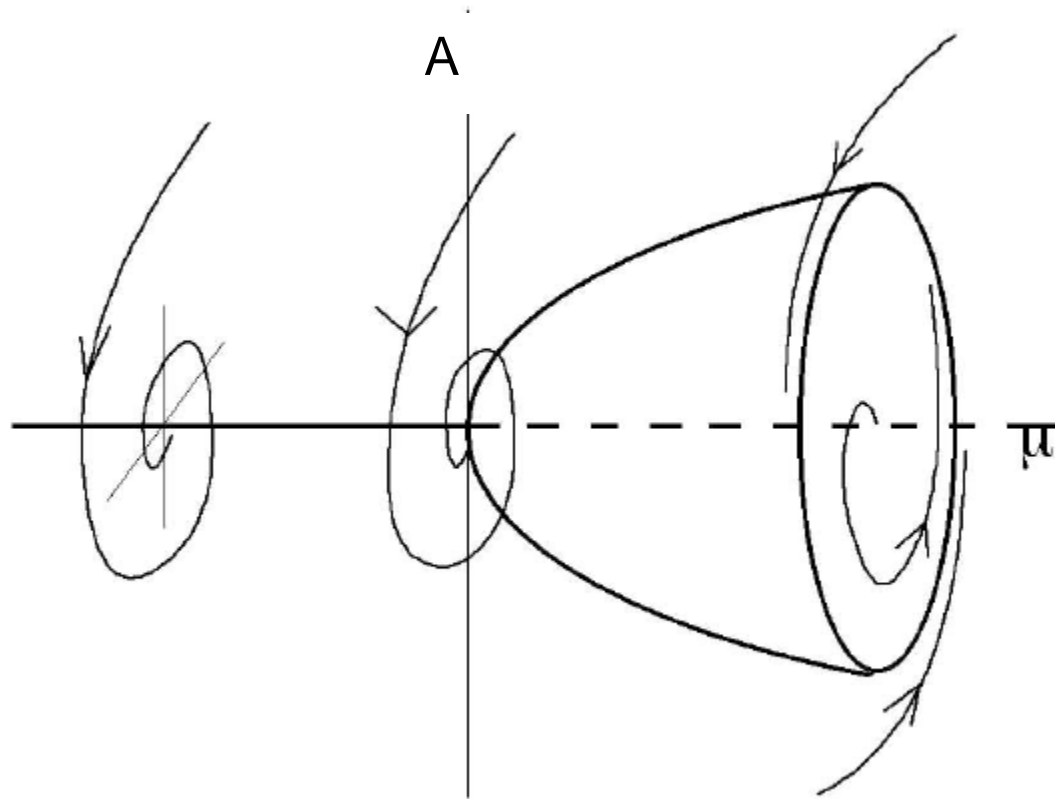


What about nonlinearities?



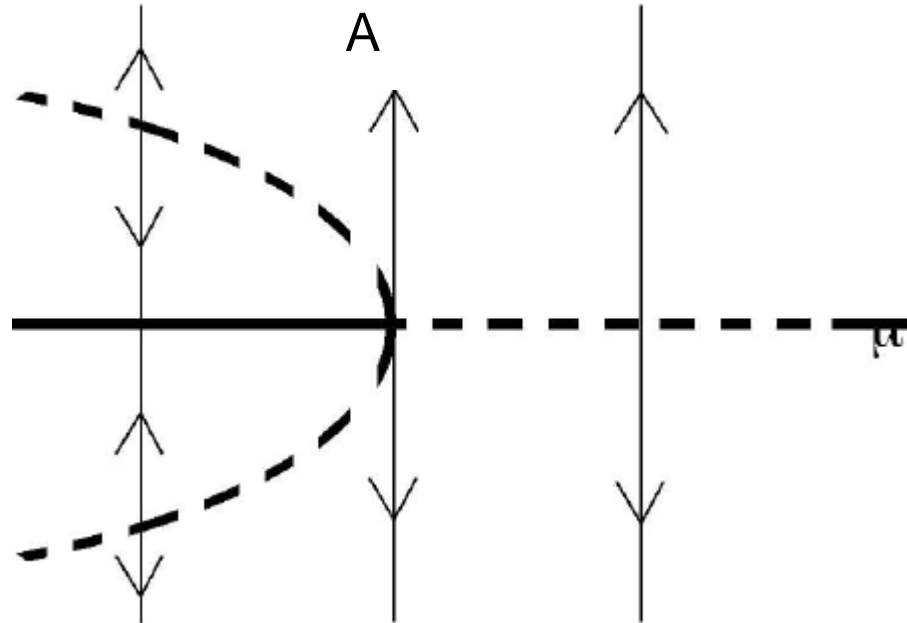
Supercritical fork bifurcation

What about nonlinearities?



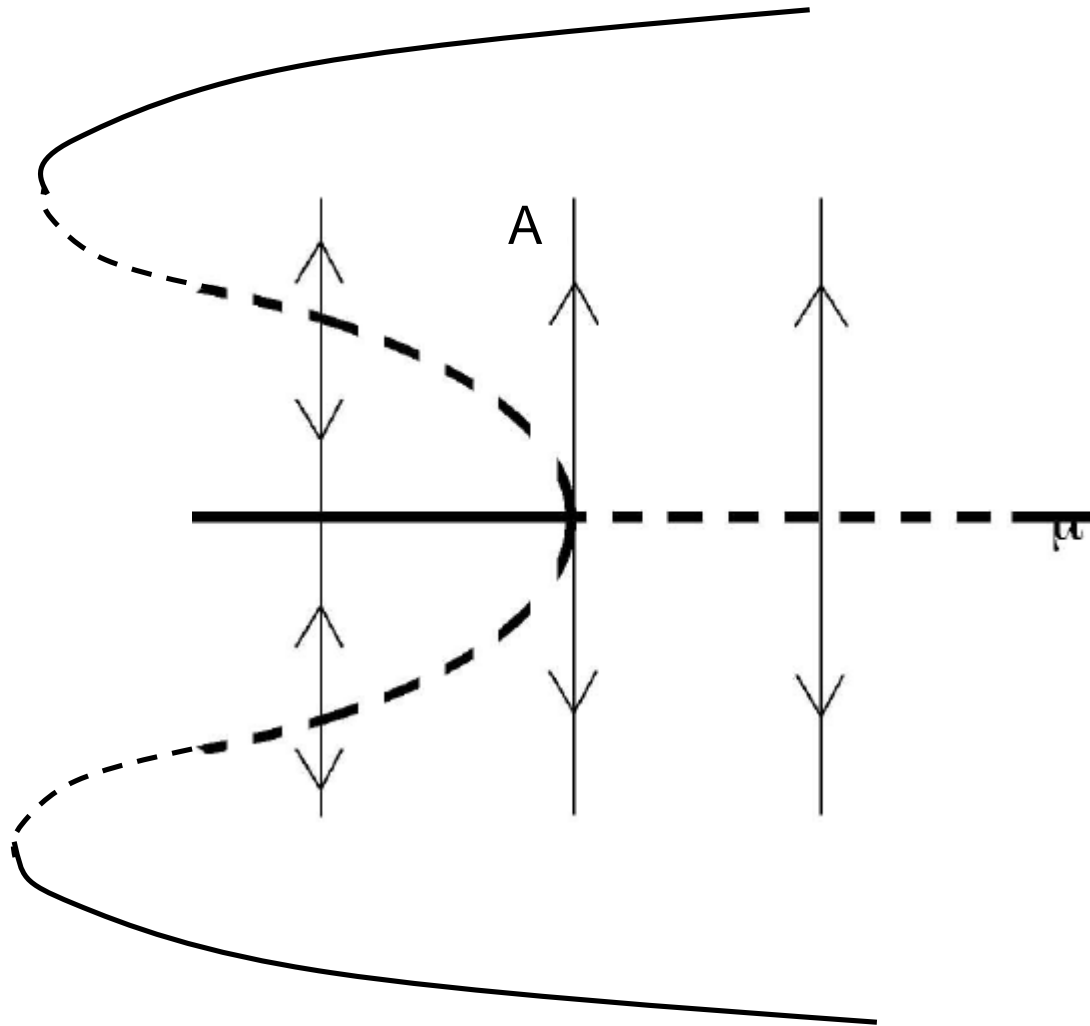
Hopf bifurcation

What about nonlinearities?



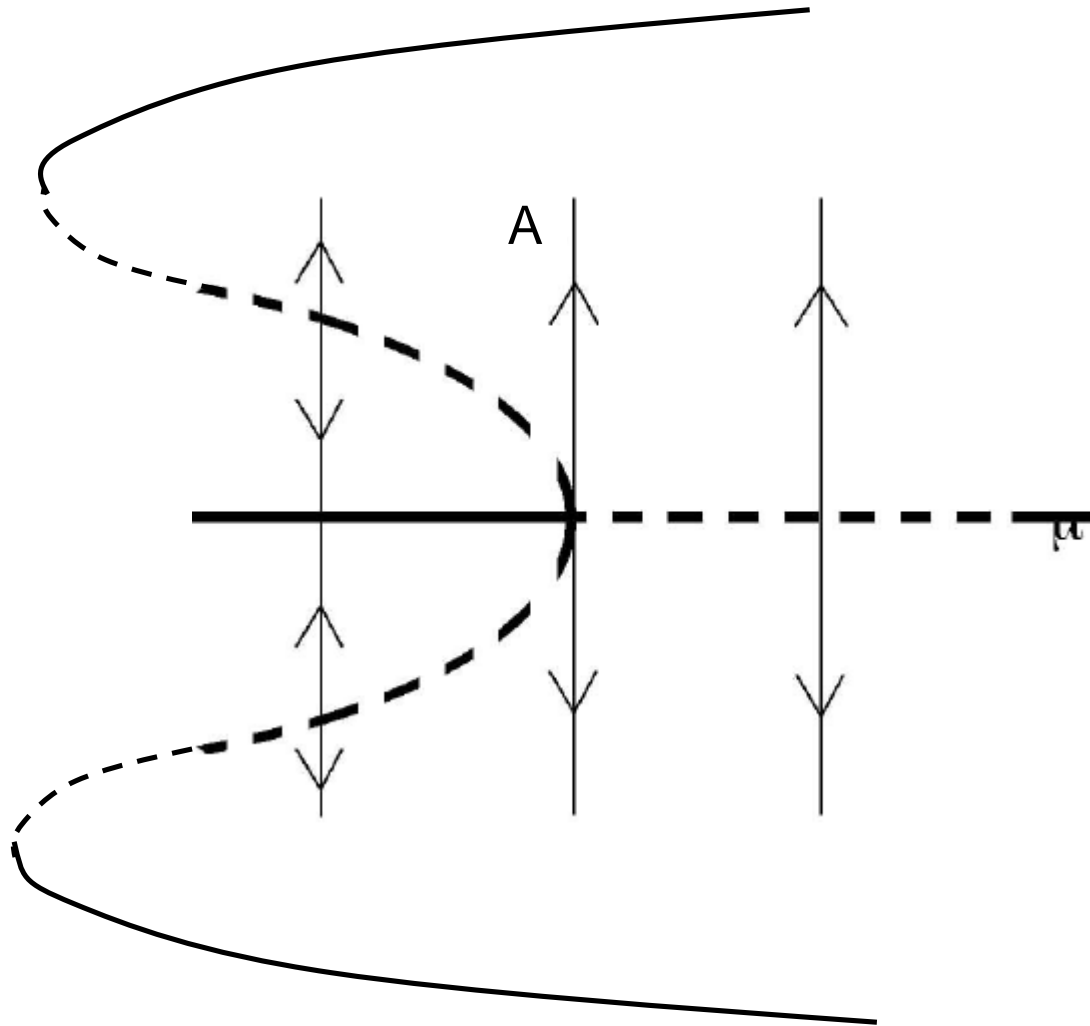
Subcritical fork bifurcation

What about nonlinearities?



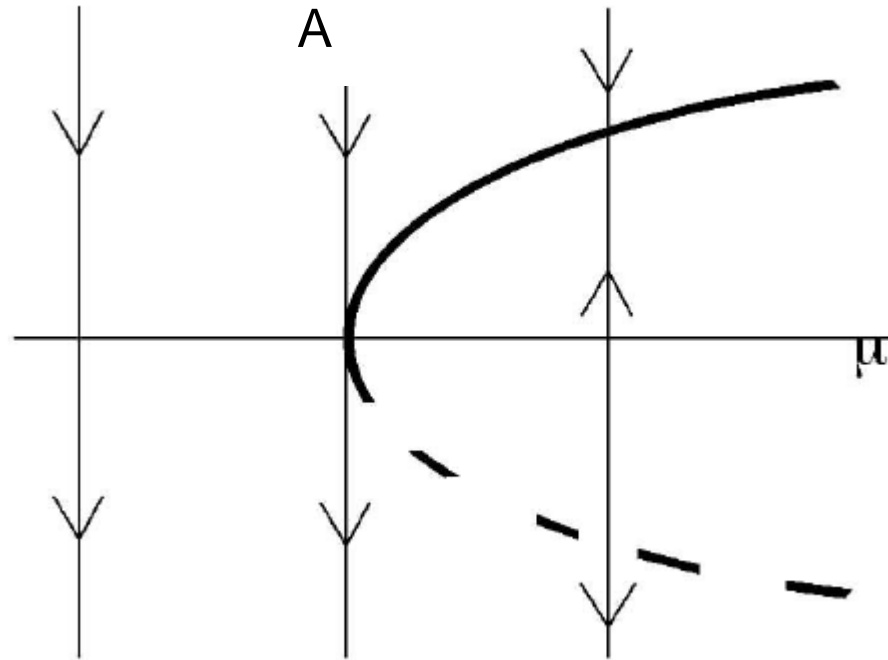
Subcritical bifurcation

What about nonlinearities?



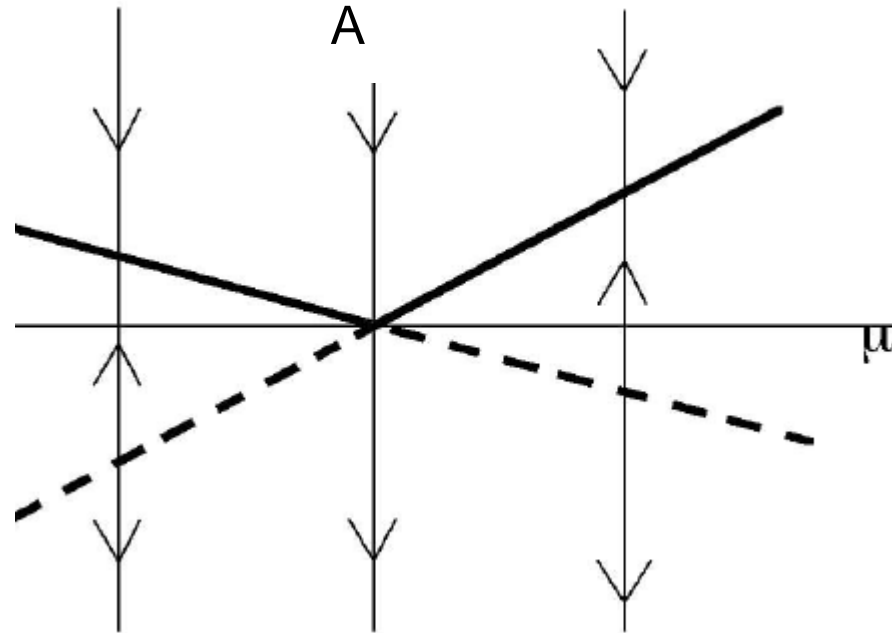
Hysteresis cycle!

What about nonlinearities?



Saddle Node bifurcation

What about nonlinearities?



Transcritical bifurcation