

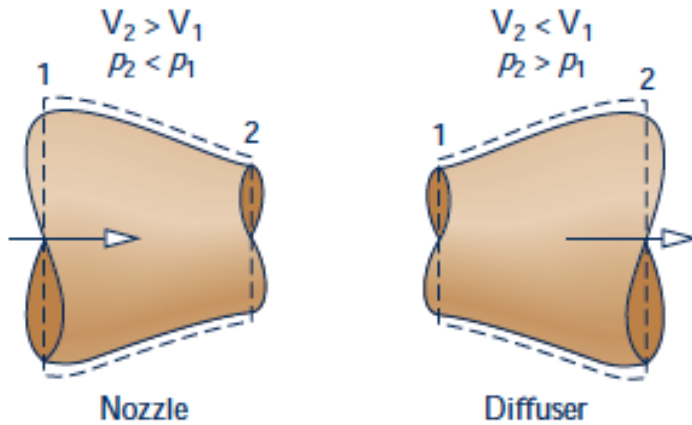
The background image is a composite of two scenes. On the left, a traditional wooden windmill stands on a grassy bank next to a body of water, with high-voltage power lines stretching into the distance under a blue sky with soft clouds. On the right, a large industrial power plant is visible, featuring a prominent cooling tower and various structures, set against a sky with a reddish-orange hue, suggesting a sunset or sunrise. A semi-transparent red rectangular box is overlaid on the right side of the image, containing the course title in white text.

ME-251: Thermodynamics and energetics I Open Systems III

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Energy Transport Advances
Laboratory
EPFL Mechanical Engineering

2025 Fall Semester

Photo Credit: Trougnouf



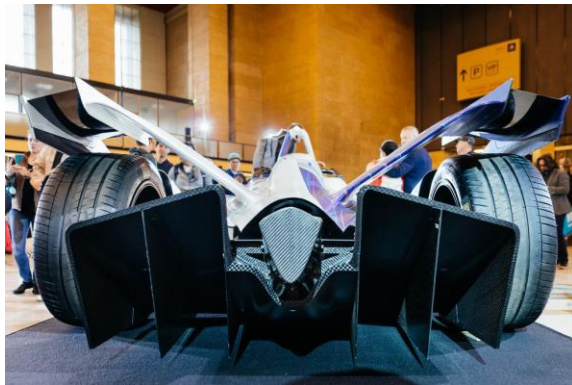
Steady state, one inlet and one exit

$$\dot{m}_i = \dot{m}_e = \dot{m}$$

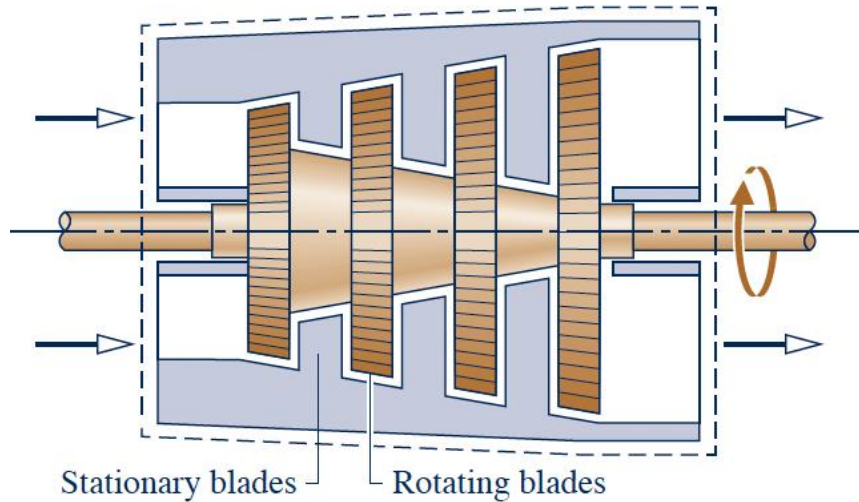
Neglecting changes in PE and heat transfer (assumption)

$$h_1 - h_2 + \frac{\vec{V}_1^2 - \vec{V}_2^2}{2} = 0$$

No work other than flow work, $\dot{W}_{cv} = 0$



Steady-state steam/gas turbine



Neglecting changes in KE and PE (assumption)

$$\dot{Q}_{cv} - \dot{W}_{cv} + \dot{m}(h_1 - h_2) = 0$$

Further neglecting heat transfer (assumption)

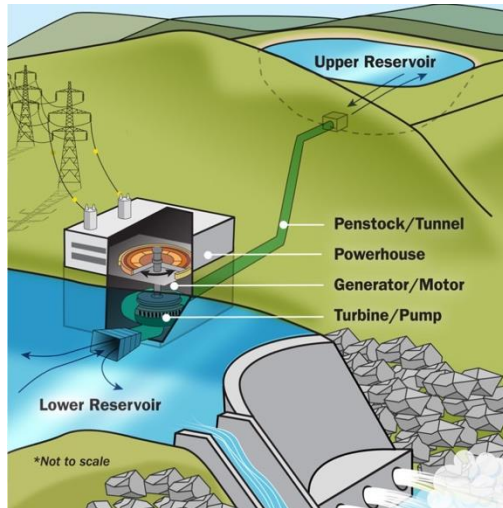
$$\dot{W}_{cv} = \dot{m}(h_1 - h_2)$$

$$\dot{W}_{cv} > 0 \text{ for turbines}$$

One inlet and one exit

$$\dot{m}_i = \dot{m}_e = \dot{m}$$

Pump and compressor



Steady state, one inlet one exit $\dot{m}_i = \dot{m}_e = \dot{m}$

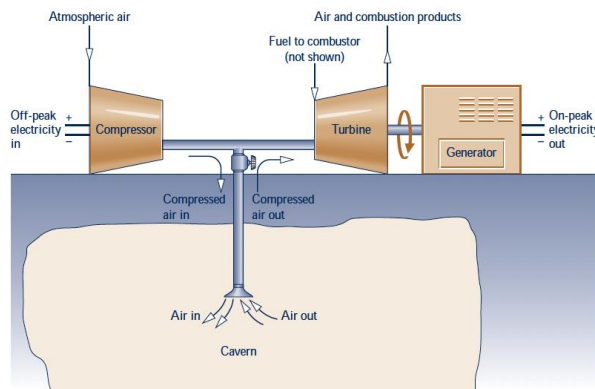
Ignoring KE change and heat transfer (assumption)

$$-\dot{W}_{cv} + \dot{m}(h_1 - h_2 + g(z_1 - z_2)) = 0$$

For compressors (gas), often further neglecting PE change (assumption)

$$\dot{W}_{cv} = \dot{m}(h_1 - h_2)$$

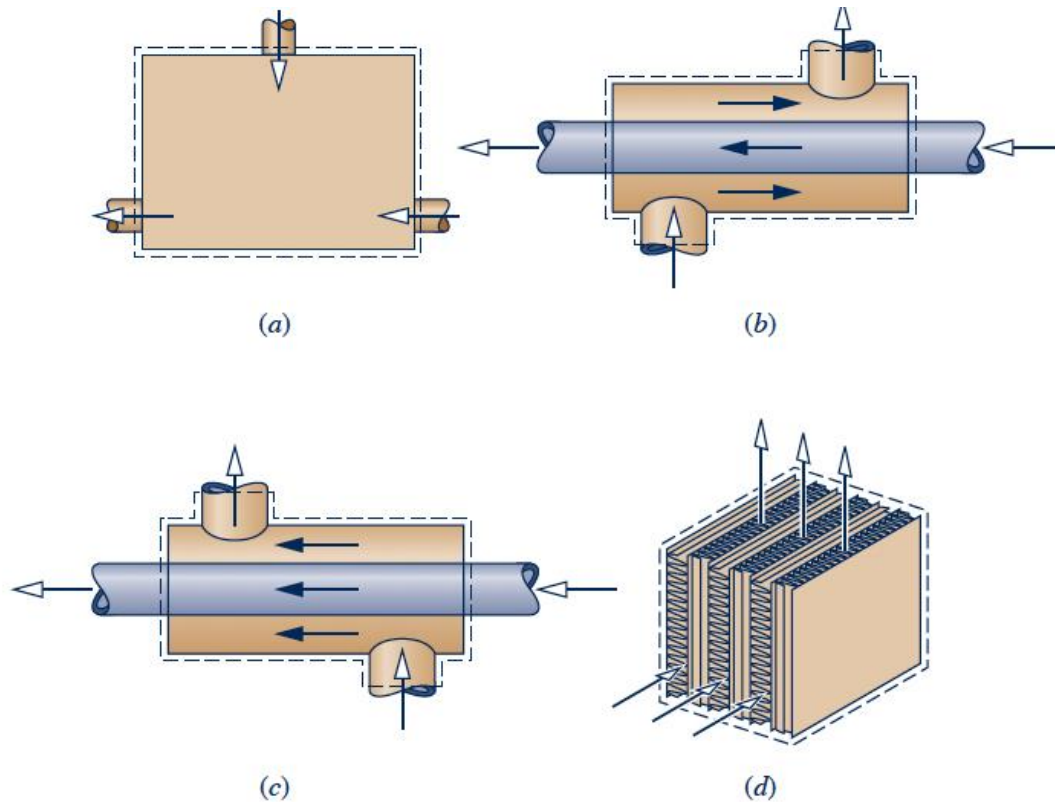
$\dot{W}_{cv} < 0$ for compressors and pumps





- Apply 1st law to heat exchangers and throttling valves
- Quick review of what we have learned so far
- Motivating the 2nd law of thermodynamics

Reading: 4.9-4.11, 5.1



- (a) Direct contact heat exchanger (mixing chamber)
- (b) Tube-within-a-tube counterflow heat exchanger
- (c) Tube-within-a-tube parallel flow heat exchanger
- (d) Cross-flow heat exchanger

Multi-inlets, multi-exits
$$\sum_i \dot{m}_i = \sum_o \dot{m}_o$$

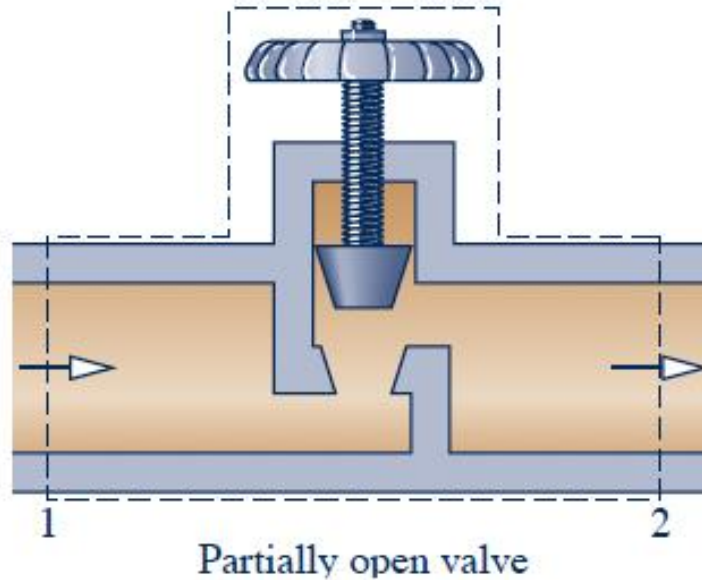
$$0 = \dot{Q}_{cv} - \dot{W}_{cv} + \sum_i \dot{m}_i \left(h_i + \frac{V_i^2}{2} + gz_i \right) - \sum_e \dot{m}_e \left(h_e + \frac{V_e^2}{2} + gz_e \right)$$

Flow work only $\dot{W}_{cv} = 0$ Neglecting KE and PE changes (assumption)

$$0 = \dot{Q}_{cv} + \sum_i \dot{m}_i h_i - \sum_e \dot{m}_e h_e$$

Further neglecting heat transfer with surroundings (assumption)

$$\sum_i \dot{m}_i h_i = \sum_e \dot{m}_e h_e$$



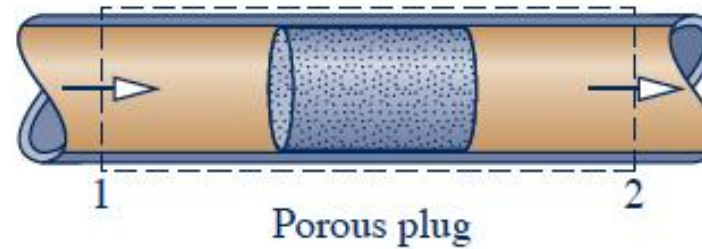
One inlet and one exit

$$\dot{m}_i = \dot{m}_e = \dot{m}$$

Neglecting heat transfer and PE change (assumption)

$$h_1 - h_2 + \frac{\vec{V}_1^2 - \vec{V}_2^2}{2} = 0$$

Adding a partially opened valve or a porous plug to reduce pressure

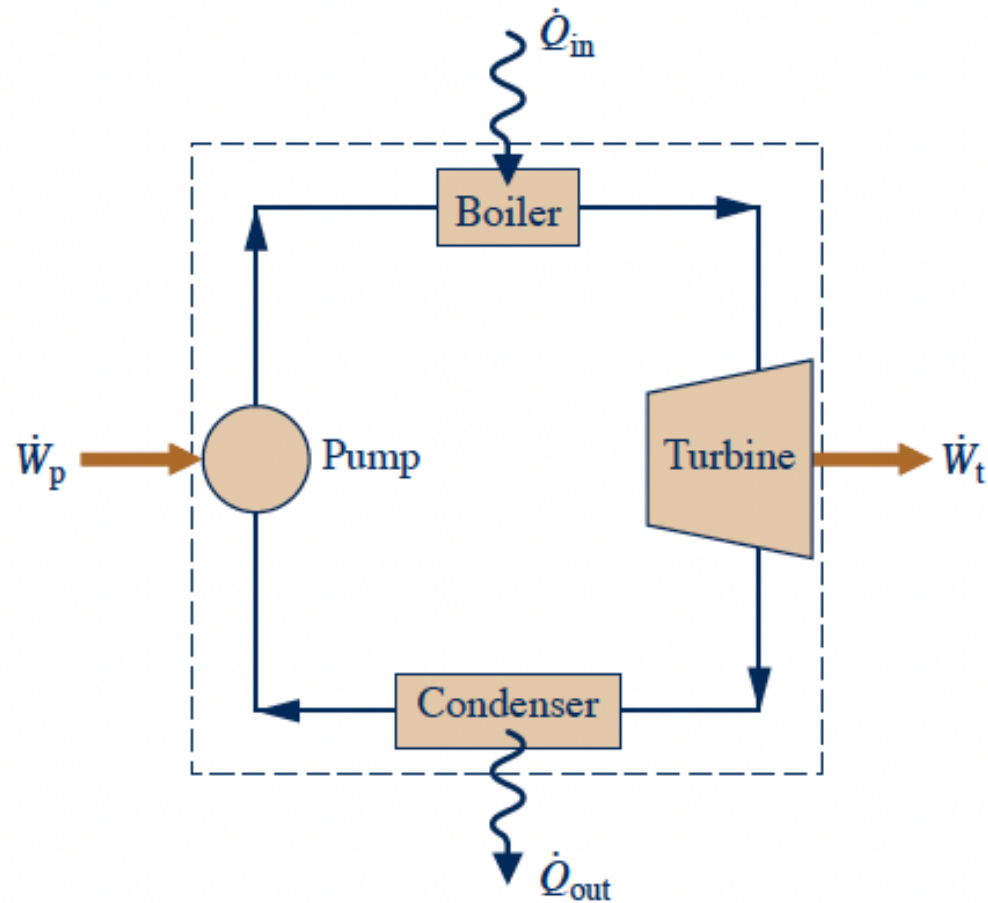


Flow work only $\dot{W}_{cv} = 0$

$$\dot{Q}_{cv} - \dot{W}_{cv} + \dot{m} \left(h_1 - h_2 + \frac{\vec{V}_1^2 - \vec{V}_2^2}{2} + g(z_1 - z_2) \right) = 0$$

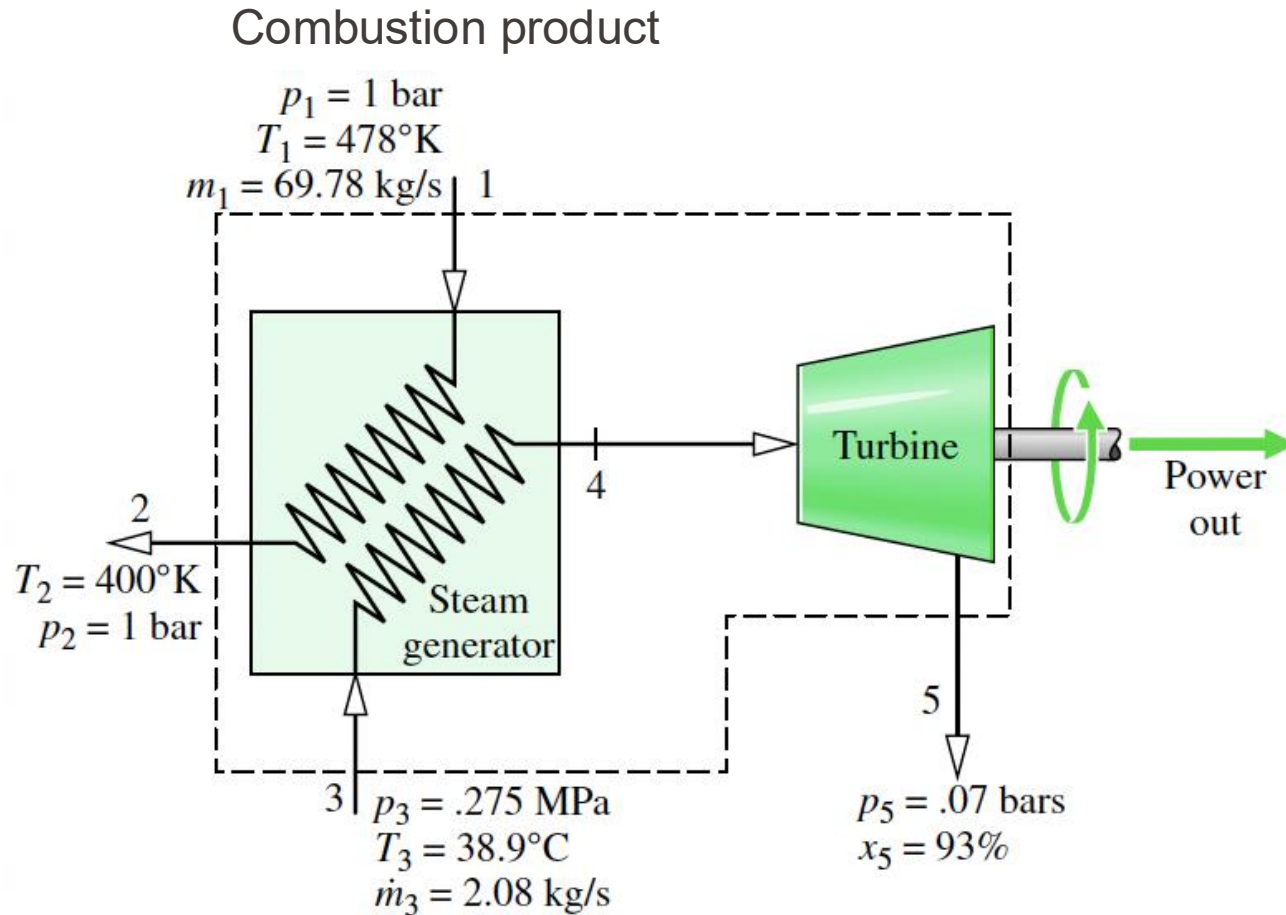
Further neglecting KE difference between downstream and upstream (assumption)

$$h_1 = h_2$$



Applying 1st law to a simple vapor power cycle at steady state

$$0 = (\dot{Q}_{in} - \dot{Q}_{out}) - (\dot{W}_t - \dot{W}_p)$$



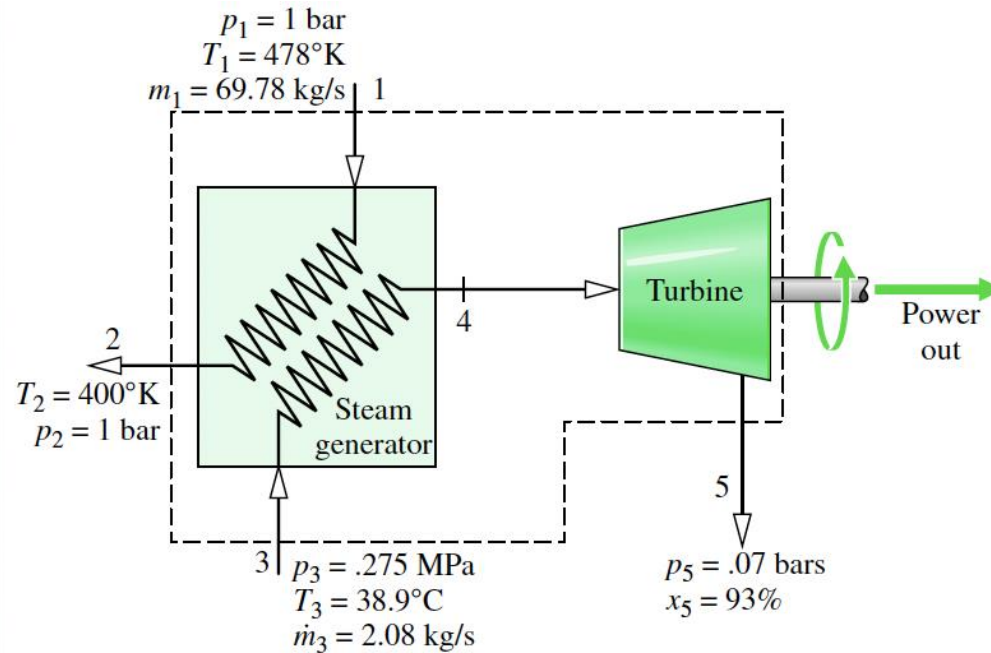
Steady-state waste heat recovery system

Heat exchange between the CV and the surrounding negligible

Neglect pressure drop for water flowing through the steam generator

Combustion product modeled as air with perfect gas behavior $c_p = 1005 \text{ J/kg/K}$

Determine the power output of the turbine and the turbine inlet temperature



Mass conservation

$$\dot{m}_1 = \dot{m}_2 \quad \dot{m}_3 = \dot{m}_5$$

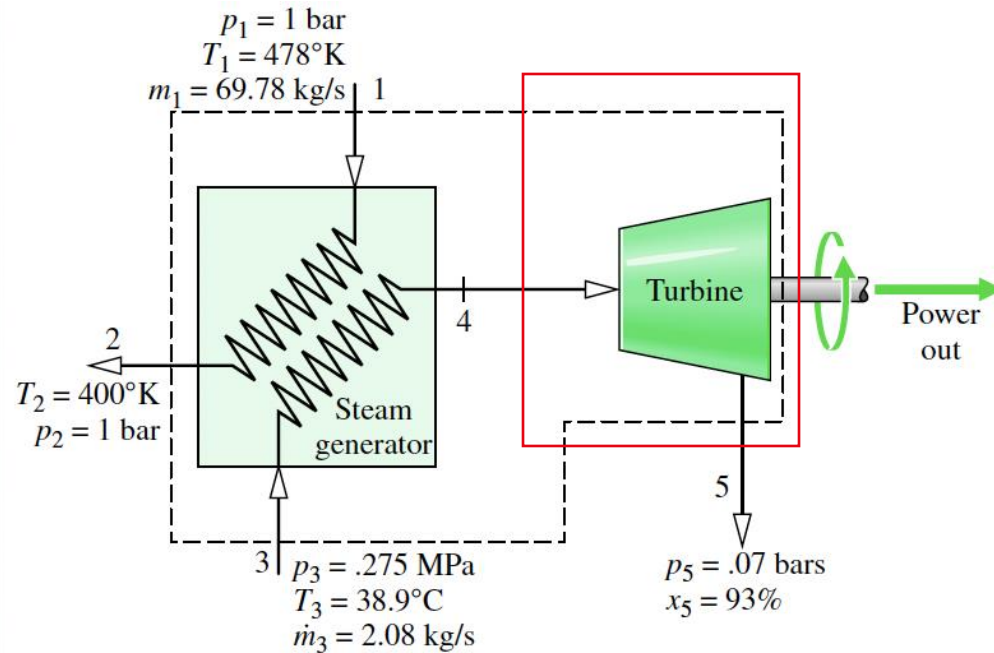
Steady-state energy balance

$$0 - \dot{W}_{cv} + \dot{m}_1 h_1 + \dot{m}_3 h_3 - \dot{m}_2 h_2 - \dot{m}_5 h_5 = 0$$

$$\begin{aligned} \dot{W}_{cv} &= \dot{m}_1 (h_1 - h_2) + \dot{m}_3 (h_3 - h_5) \\ &= \dot{m}_1 c_p (T_1 - T_2) + \dot{m}_3 (h_3 - h_5) \end{aligned}$$

With a property database, one can get $h_3(p_3, T_3)$ and

$$h_5 = h_f(p_5) + 0.93(h_g(p_5) - h_f(p_5))$$



No pressure drop along steam generator

$$p_4 = p_3$$

Mass conservation $\dot{m}_4 = \dot{m}_5 = \dot{m}_3$

Steady-state energy balance

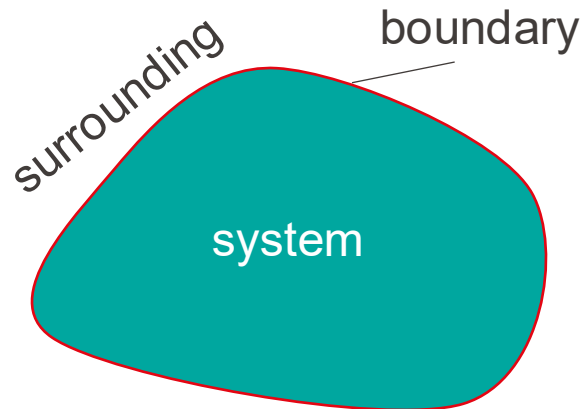
$$0 - \dot{W}_{cv} + \dot{m}_4 h_4 - \dot{m}_5 h_5 = 0$$

$$h_4 = h_5 + \dot{W}_{cv} / \dot{m}_3$$



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The Free Encyclopedia

Thermodynamics is a branch of physics that deals with heat, work, and temperature, and their relation to energy, entropy, and the physical properties of matter and radiation.



To perform thermodynamics analysis, we need to define the **system**, the **surrounding** and the **boundary** that separate the two

We consider **work transfer**, **mass transfer**, **heat transfer** across the boundary

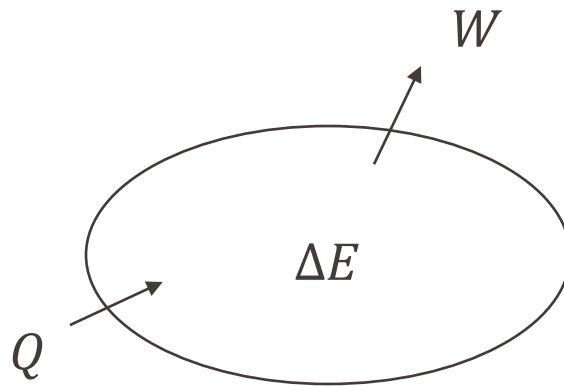
Change in the amount of energy contained within a system during some time interval

=

Net amount of energy transferred into the system by heat transfer during the time interval

−

Net amount of energy transferred out of the system by work during the time interval



$$\Delta E = E_2 - E_1 = Q - W \quad \text{in [J]}$$

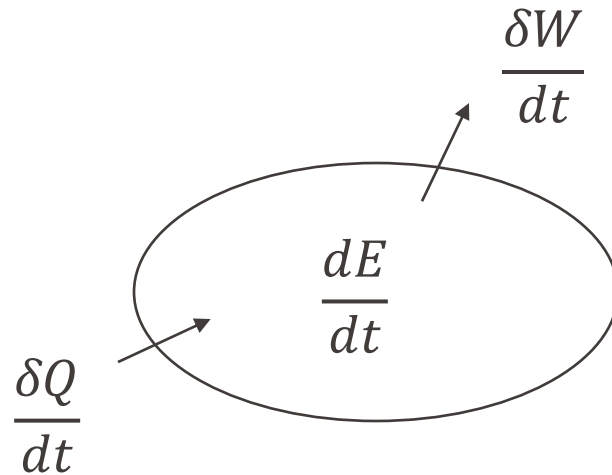
Time rate of change in the amount of energy contained within a system at time t

=

Net rate at which energy is transferred **into** the system by heat transfer at time t

-

Net rate at which energy is transferred **out of** the system by work at time t

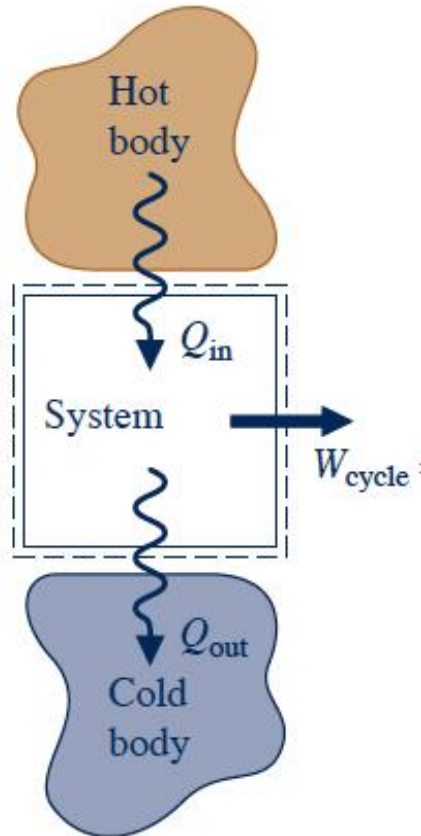


$$\frac{dE}{dt} = \dot{Q} - \dot{W} \quad \text{Heat flow rate - Power}$$

Everything is in [W]

Energy change in kinetic energy, potential energy, and internal energy

Energy transfer: **work** (expansion/compression, shaft, electric,...)
heat (conduction, convection, radiation)

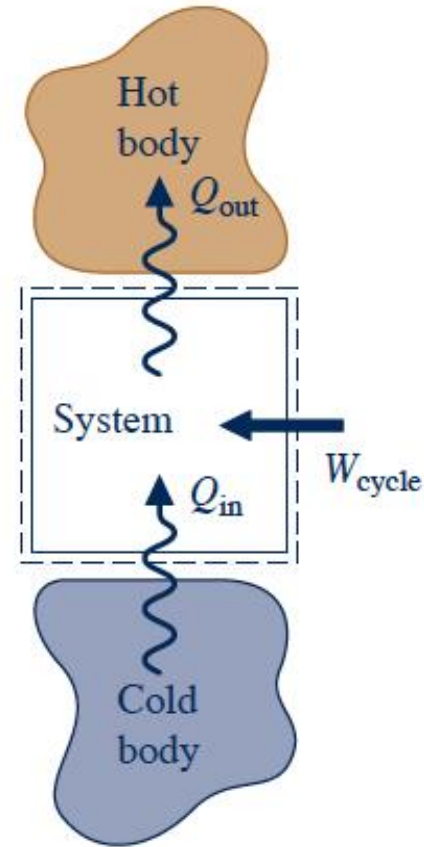


Power cycle

$$W_{cycle} = Q_{in} - Q_{out}$$

Output

$$\eta = \frac{W_{cycle}}{Q_{in}}$$



**Refrigeration and
heat pump cycle**

$$W_{cycle} = Q_{out} - Q_{in}$$

Input

$$\beta_{ACR} = \frac{Q_{in}}{W_{cycle}}$$

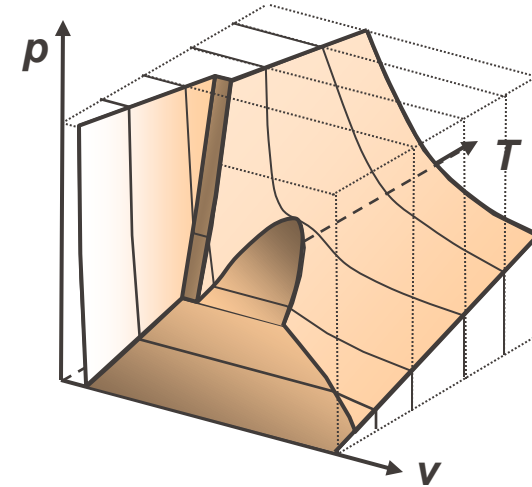
$$\gamma_{HP} = \frac{Q_{out}}{W_{cycle}}$$

- **State principle:** for closed systems

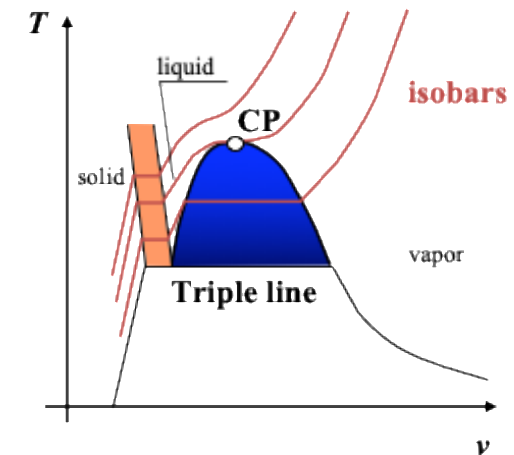
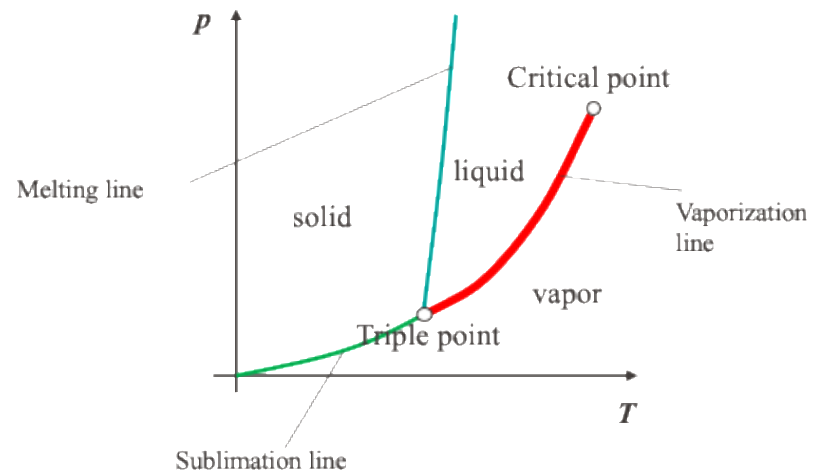
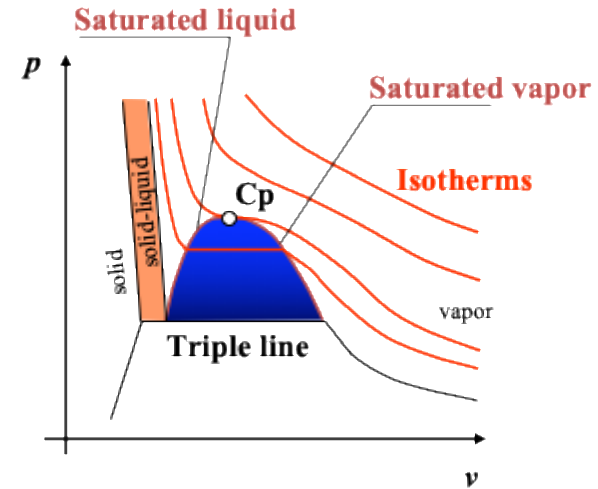
$$\# \text{ of independent properties} = \# \text{ of relevant work exchange modes} + 1 \text{ (associated with heat)}$$

- E.g., for gas in a piston-cylinder assembly, number of independent properties 2 (**temperature** associated with heat transfer and pressure associated with **compression/expansion work**)
- **Simple system:** only one work exchange mode as the system undergoes quasiequilibrium processes (**two independent properties**).

- Single phase region
- Two phase region
- Saturation states
- Critical point
- Triple line



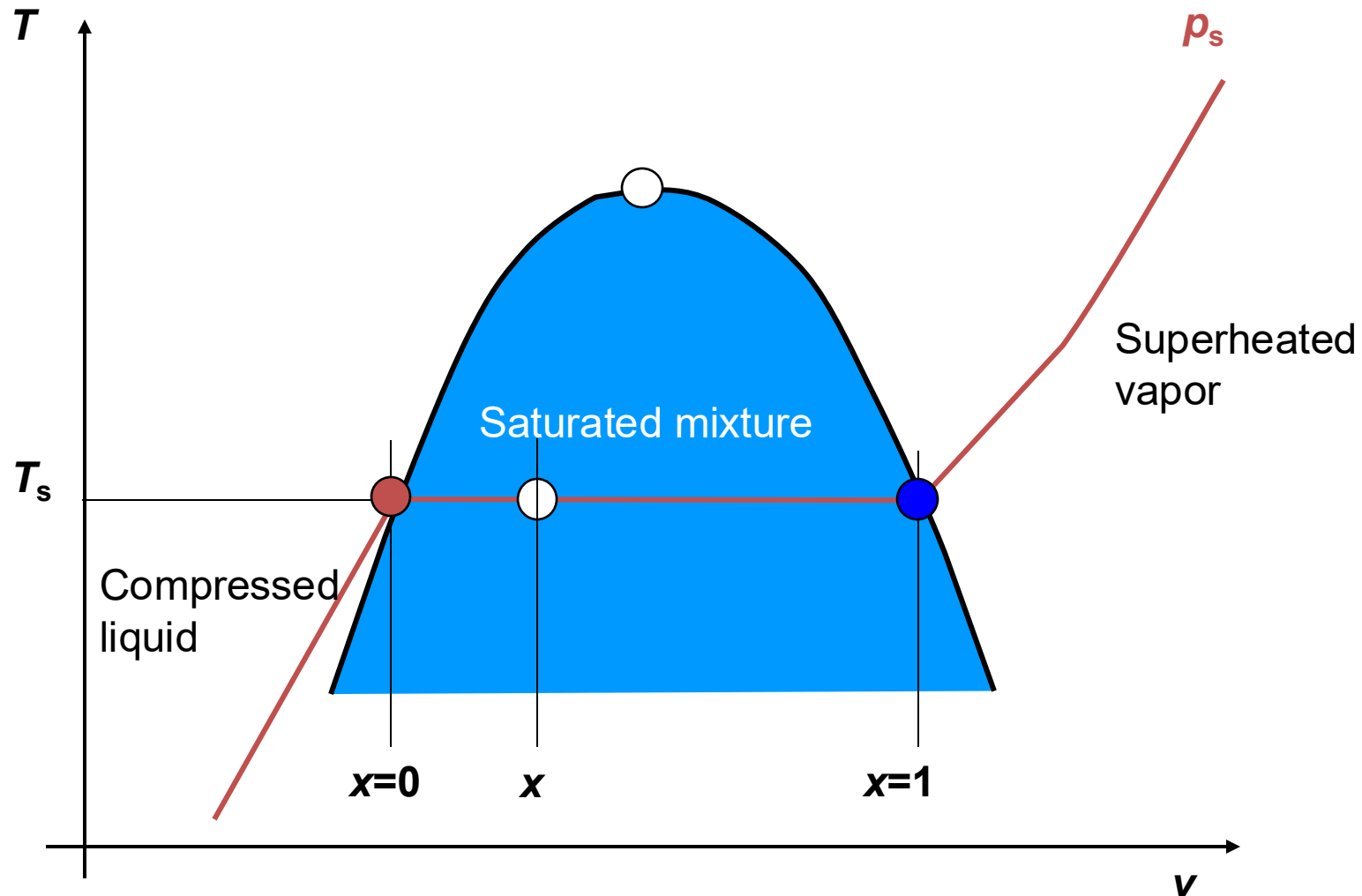
- p-v diagram
- T-v diagram
- p-T phase diagram
- Steam quality



Compressed Liquid and Superheated Vapor

For per mass properties y (e.g., v , h , u)

$$y(x) = xy_g + (1 - x)y_f$$



- Specific enthalpy $h = u + pv$ [J/kg]
- Specific heat at a constant volume $c_v = \left(\frac{\partial u}{\partial T}\right) \Big|_v$
- Specific heat at a constant pressure $c_p = \left(\frac{\partial h}{\partial T}\right) \Big|_p$

- Liquids and solids are often modeled as incompressible $v = \text{const}$

$$u = u(T) \quad c_v = \frac{du}{dT} = c(T) = c_p \quad \text{At constant } T, dh = vdp$$

- $\frac{pv}{RT} = \frac{p\tilde{v}}{\tilde{R}T} = Z \equiv 1$, the dilute limit of real gases

T : temperature [K]

\tilde{R} : universal gas constant [J/K/mol]

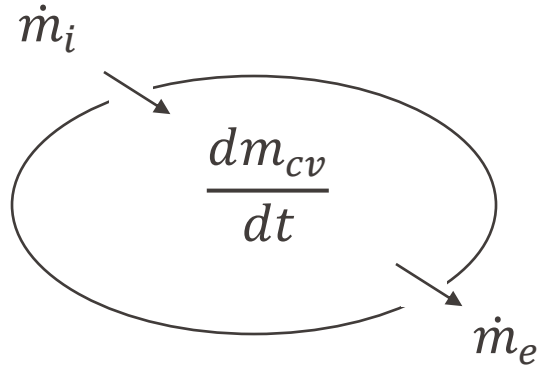
R : specific gas constant [J/K/kg]

\tilde{v} : molar volume [m³/mol]

$$u = u(T) \quad h = u + pv = u(T) + RT \quad c_v = \frac{du}{dT} = c(T) \quad c_p = c_v(T) + R$$

$$\text{Specific heat ratio } k = \frac{c_p}{c_v} = 1 + \frac{R}{c_v}$$

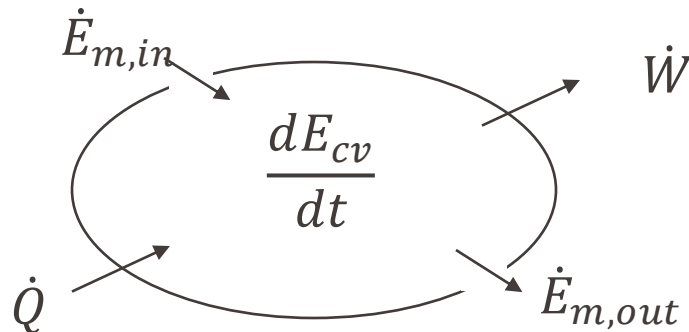
Perfect gas c_v is constant, or equivalently c_p is constant or k is constant



Mass balance

$$\frac{dm_{cv}}{dt} = \sum_i \dot{m}_i - \sum_e \dot{m}_e$$

Energy balance



$$\begin{aligned} \frac{dE_{cv}}{dt} = & \dot{Q}_{cv} - \dot{W}_{cv} \\ & + \sum_i \dot{m}_i \left(h_i + \frac{\vec{V}_i^2}{2} + gz_i \right) - \sum_e \dot{m}_e \left(h_e + \frac{\vec{V}_e^2}{2} + gz_e \right) \end{aligned}$$

