

Irrigation and Drainage Engineering

(Soil Water Regime Management)

(ENV-549)

4ETCS, Master option

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Platform of Hydraulic Constructions



Project: flooding in
Nouakchott (Mauritania) –
Groundwater modelling and
numerical solutions for steady
state

Water budget

- Input:
 - Precipitation
 - Groundwater recharge = definition
 - Injection
- Output:
 - Evapotranspiration
 - Pumping
 - Groundwater flow

Groundwater flow

- Groundwater = continuous variable (a value at a time depends on the value at the previous time)
- Determination of groundwater flow by measuring groundwater depth in observation wells (single point measurement)
- From groundwater depth measurements → piezometric map
- Groundwater flow from the highest hydraulic heads to the lowest → diffusivity equation

Diffusion equation

- Continuity equation

- 2D situation $\rightarrow w = 0$
- Steady state $\rightarrow \frac{\partial}{\partial t} = 0$

$$\frac{\partial \rho}{\partial t} + \rho \nabla \cdot \vec{U} = 0$$

$$\vec{U} = (u, v, w)$$

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0$$

- Darcy equation

$$\vec{U}_i = -K_i \frac{dh}{di}$$

$$\frac{\partial}{\partial x} \left(-K_x \frac{\partial h}{\partial x} \right) + \frac{\partial}{\partial y} \left(-K_y \frac{\partial h}{\partial y} \right) = 0$$

Directionally homogeneous and isotropic

$$K_x \frac{\partial^2 h}{\partial x^2} + K_y \frac{\partial^2 h}{\partial y^2} = 0$$

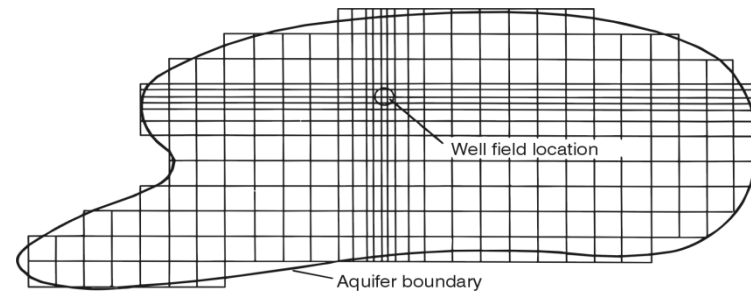
Fully homogeneous and isotropic ($K_x = K_y$)

$$\frac{\partial^2 h}{\partial x^2} + \frac{\partial^2 h}{\partial y^2} = \nabla^2 h = 0$$

Laplace equation

Numerical modelling

- Simplifying assumptions for the diffusion equation
 - Spatial discretization (cells of a grid) and temporal discretization (time steps)
- Finite difference to estimate the partial derivative in each cell (one equation per cell)



Fetter, 1994

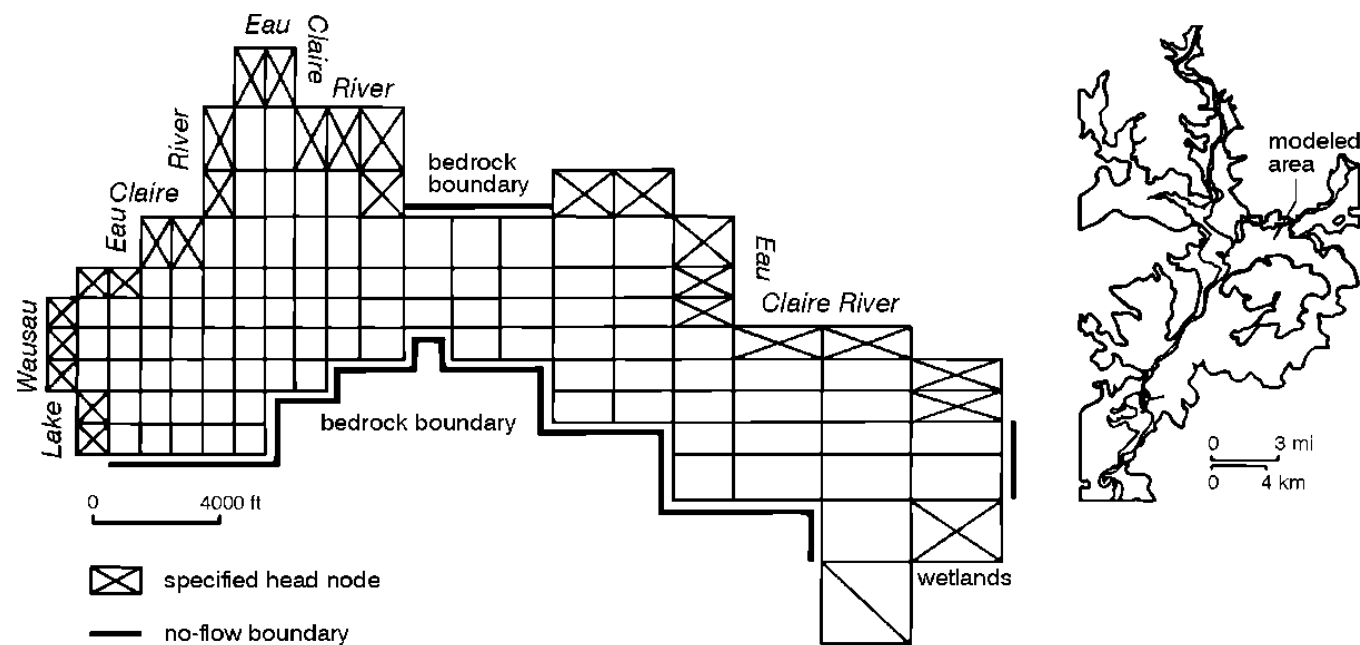
More on numerical solutions vs analytical solutions?

→ Bear, J., & Cheng, A. H.-D. (2010). Modeling Groundwater Flow and Contaminant Transport. Springer Netherlands.

<https://doi.org/10.1007/978-1-4020-6682-5>

Needed information for simulation

- Hydraulic conductivity (or transmissivity) in each cell
- Pumping and groundwater recharge in each cell
- Aquifer geometry and spatial discretization
- Boundary conditions (constant head; specified flow, including no flow)



Anderson et Woessner, 1991

Numerical solution

- Finite difference solution $U_{ci} = -K_{ci} \frac{\Delta h_{ci}}{L} = K_{ci} \frac{\Delta h_{ic}}{L}$

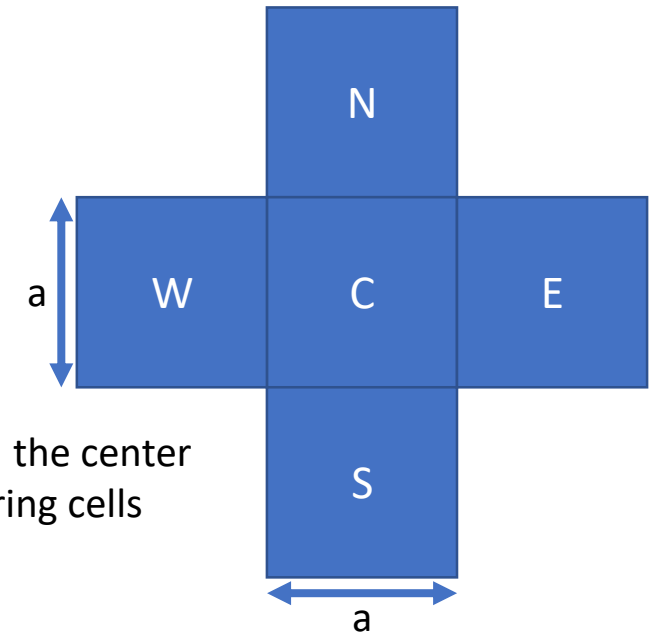
Hp: unconfined water table, 2D horizontal flow, homogeneous and isotropic soil

- Darcy law on a square-shaped grid $U_{ci} = -K_{ci} \frac{\Delta h_{ci}}{L} = K_{ci} \frac{\Delta h_{ic}}{L}$

- Flow rate $Q_{ci} = U_{ci} a b = K_{ci} \frac{\Delta h_{ic}}{L} a b = T_{ci} \frac{\Delta h_{ic}}{L} a$

$$T_{ci} = K_{ci} b \quad \text{Transmissivity}$$

L is the distance between the center of two neighbouring cells
 b is the aquifer thickness



- Continuity equation (steady state) $\sum_i Q_{ci} = 0$

$$\sum_i Q_{ci} = 0 \quad \rightarrow \quad \sum_i T_{ci} \frac{\Delta h_{ic}}{L} a = 0 \quad \xrightarrow{L=a} \quad \sum_i T_{ci} \Delta h_{ic} = 0$$

for square cells

Steady state

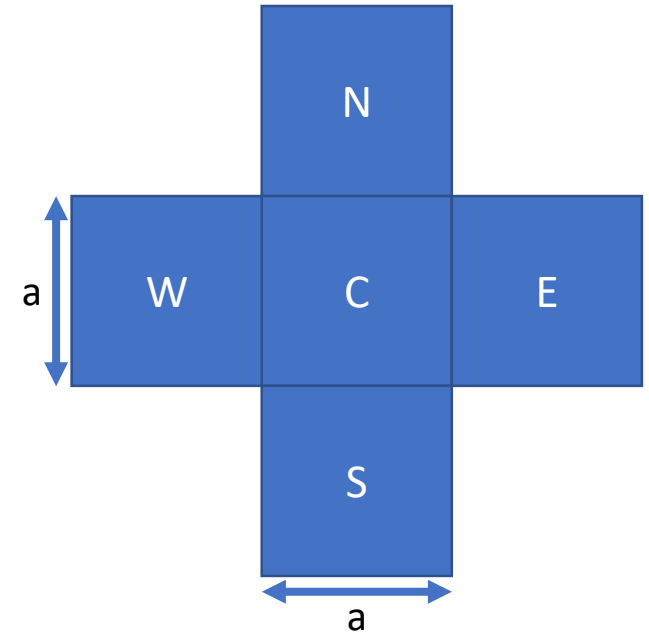
$$\sum_i T_{Ci} \Delta h_{iC} = 0$$

$$T_{CN}(h_C - h_N) + T_{CS}(h_C - h_S) + T_{CE}(h_C - h_E) + T_{CW}(h_C - h_W) = 0$$

$$h_C = \frac{T_{CN}h_N + T_{CS}h_S + T_{CE}h_E + T_{CW}h_W}{T_{CN} + T_{CS} + T_{CE} + T_{CW}}$$

$$h_C = \frac{\sum T_{Ci} h_i}{\sum T_{Ci}}$$

For $T = \text{constant} \rightarrow$
$$h_C = \frac{T \sum h_i}{4T} = \frac{\sum h_i}{4}$$



Steady state

External flow in cell C (recharge/injection $\rightarrow Q_w > 0$, pumping $\rightarrow Q_w < 0$)

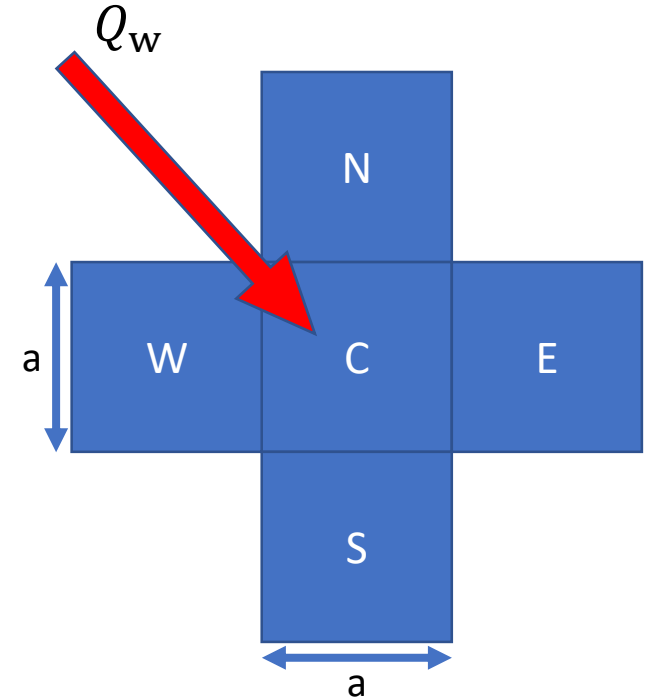
$$\sum_j Q_j = 0 \rightarrow \sum_{i=N,S,W,E} Q_{ic} + Q_w = 0$$

$$Q_{ic} = T_{ic} \Delta h_{ic}$$

$$\sum_{i=N,S,W,E} T_{ic} \Delta h_{ic} + Q_w = 0$$

$$h_c = \frac{\sum T_{ic} h_i + Q_w}{\sum T_{ic}}$$

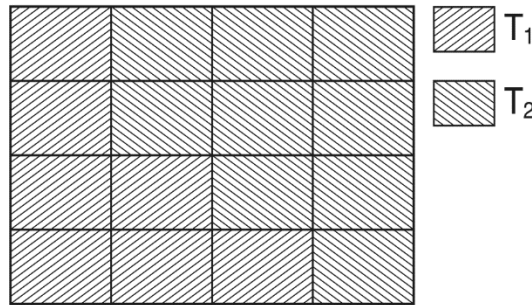
- Recharge / injection $\rightarrow Q_w > 0$
- Pumping / extraction $\rightarrow Q_w < 0$



Steady state

- In Excel??
- ➔ One equation for each cell
- ➔ System with N equations
- ➔ Iterative computing

Transmissivity



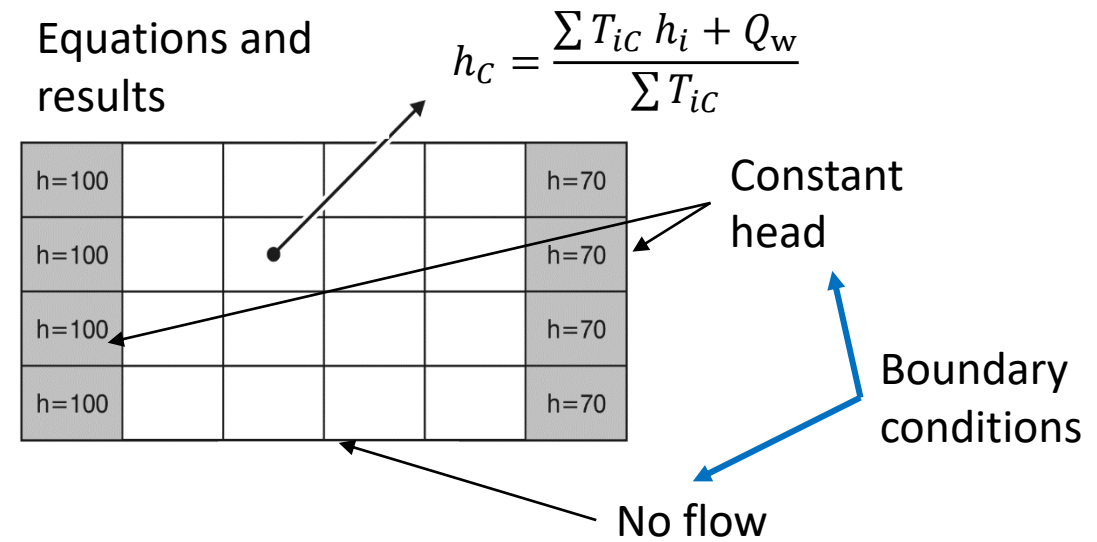
Groundwater recharge

W ₂	W ₂	W ₂	W ₂
W ₁	W ₂	W ₂	W ₂
W ₁	W ₁	W ₁	W ₂
W ₁	W ₁	W ₁	W ₁

Pumping

	Q ₁	Q ₂	
		Q ₃	

Equations and results



More on groundwater modelling?

➔ Anderson, M. P., Woessner, W. W., & Hunt, R. J. (2015). Applied Groundwater Modeling: Simulation of Flow and Advective Transport (Second Edition). Academic Press, Elsevier Inc.

Model precision

What do we use to compute the precision of a simulation?

→ The comparison of the simulated and observed variable(s) of interest

Which data for the Nouakchott project?

→ Simulated hydraulic head (groundwater level) and measured hydraulic heads

→ Simulated hydraulic head = 1 value for each cell of the simulated area (hydraulic head constant within each cell)

→ Measured hydraulic head = 3 observation wells + 1



Objective functions

Objective functions → indication on the performance of the model

« how well did the model perform? »

→ Comparison between simulated and observed variables

$$ME = \frac{1}{n} \sum_{t=1}^n (\text{sim}_t - \text{obs}_t)$$

With
 n the number of measurements
 Sim the simulated value
 Obs the observed value

$$AME = \frac{1}{n} \sum_{t=1}^n |\text{sim}_t - \text{obs}_t|$$

An objective function is optimized ⇔ maximization or minimization depending on the formula

Name	Description	Formula*
DRMS	Daily Root Mean Squared Error	$\sqrt{\frac{1}{n} \sum_{t=1}^n (d_t - o_t(\theta))^2}$
TMVOL	Total Mean Monthly Volume Squared Error	$\sum_{i=1}^{n_{\text{month}}} \left(\frac{1}{n_{\text{day}(i)}} \sum_{t=1}^{n_{\text{day}(i)}} (d_t - o_t(\theta)) \right)^2$
ABSERR	Mean Absolute Error	$\frac{1}{n} \sum_{t=1}^n d_t - o_t(\theta) $
ABSMAX	Maximum Absolute Error	$\max_{1 \leq t \leq n} d_t - o_t(\theta) $
NS	Nash-Sutcliffe Measure	$1 - \frac{\frac{1}{n} \sum_{t=1}^n [d_t - o_t(\theta)]^2}{\frac{1}{n} \sum_{t=1}^n (d_t - \bar{d})^2}$
BIAS	Bias (mean daily error)	$\frac{1}{n} \sum_{t=1}^n (d_t - o_t(\theta))$
PDIF	Peak Difference	$\max_{1 \leq i \leq n} \{d_i\} - \max_{1 \leq i \leq n} \{o_i(\theta)\}$
RCOEF	First Lag Autocorrelation	$\frac{\frac{1}{n} \sum_{t=1}^n (d_t - o_t(\theta))(d_{t+1} - o_{t+1}(\theta))}{\sigma_d \sigma_{o(\theta)}}$
NSC	Number of Sign Changes	(Count the number of times the sequence of residuals changes sign)

*Minimize with respect to θ .