

Thermochemical conversion of biomass

Electricity production from syngas

François Maréchal

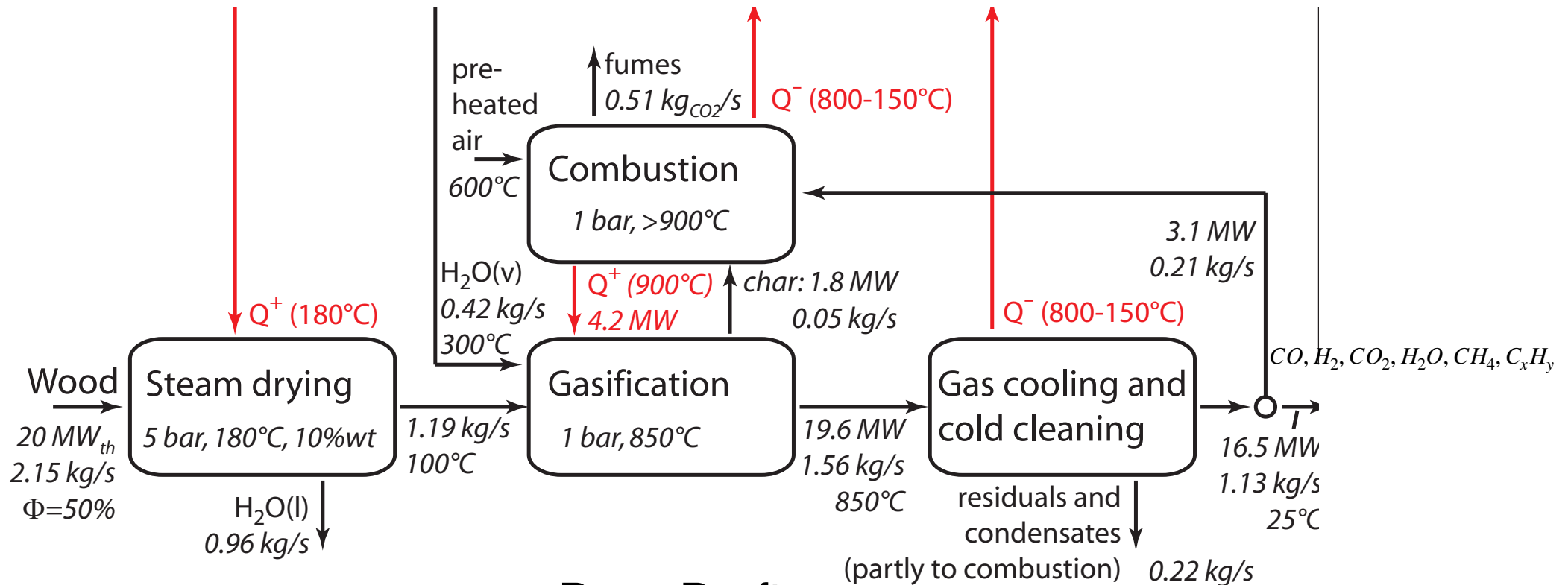
IPESE

Industrial Process and Energy Systems Engineering

EPFL Valais-Wallis

CH - 1950 Sion

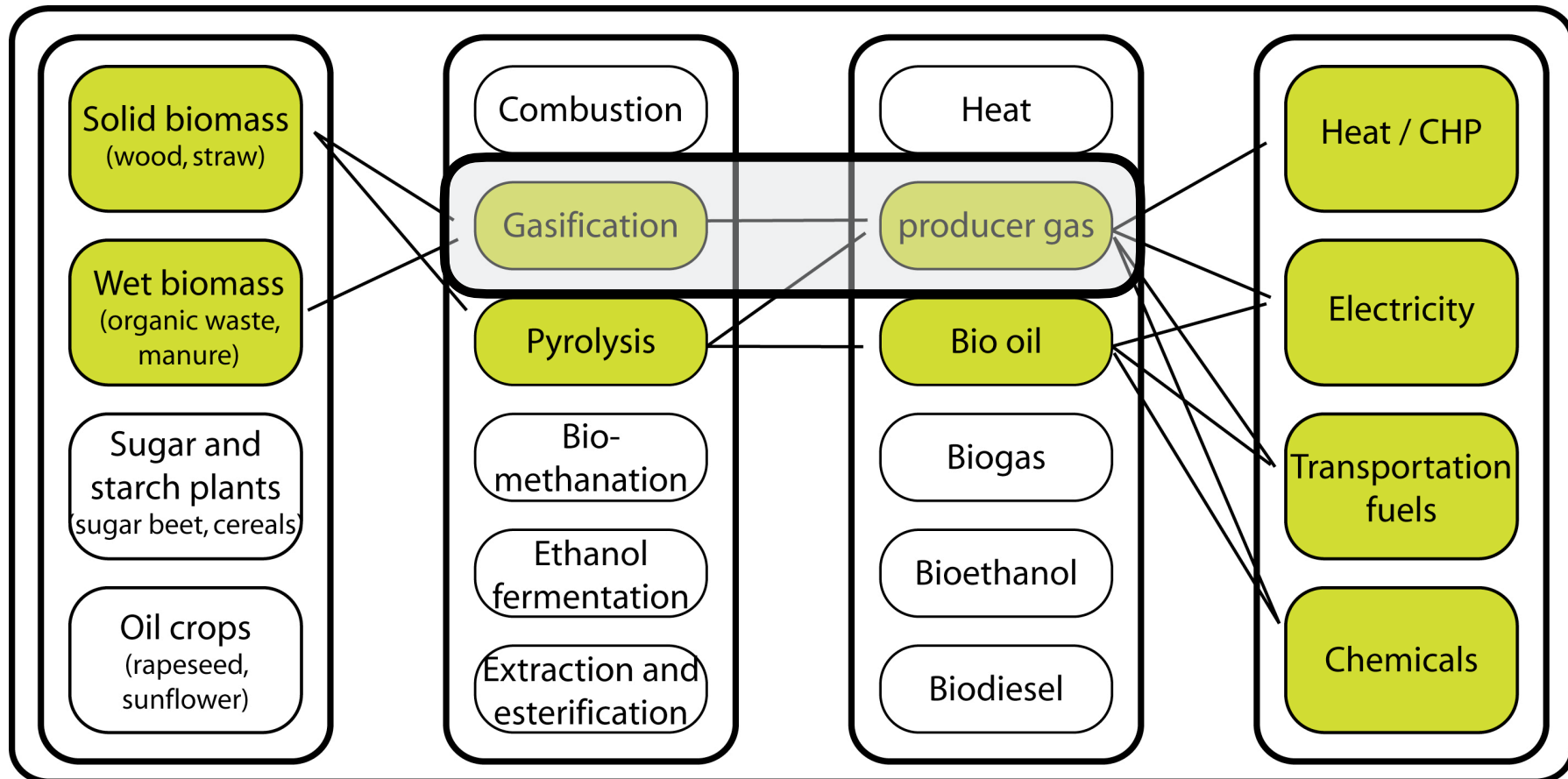
SOLID -> SYNGAS



DownDraft
 Entrained flow
 Indirectly heated
 Multi-stage

Biomass conversion

Thermochemical routes



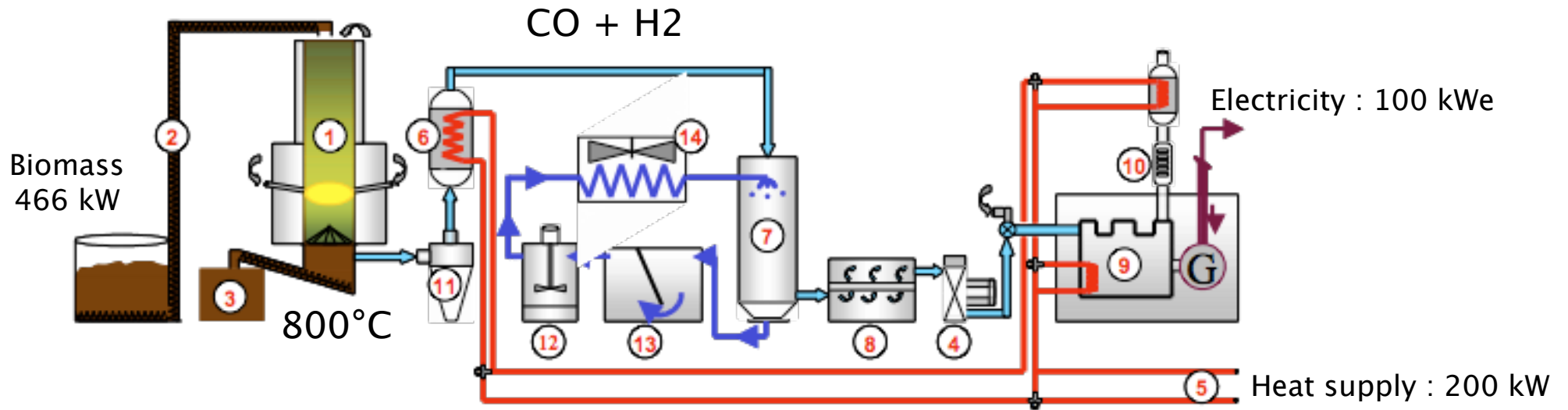
adapted from Chemical Engineering 10 (2006)

Gasification

Gas cleaning

Internal combustion engine

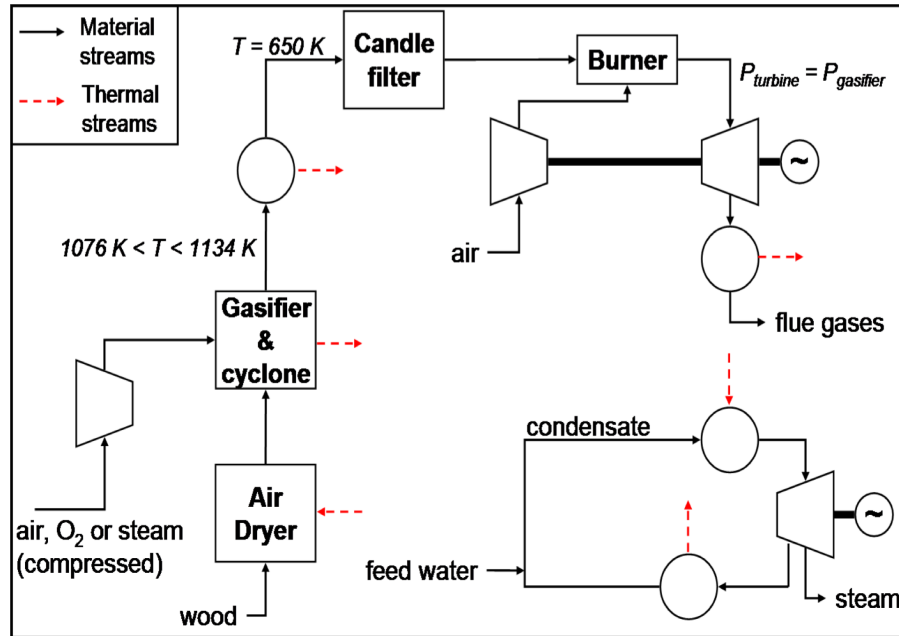
COMPOSANTS



Légende :

- | | | |
|---------------------------|--------------------------------|-------------------------|
| 1. Réacteur | 6. Echangeur de chaleur | 11. Cyclone |
| 2. Chargement du bois | 7. Colonnes de lavages | 12. Cuve de floculation |
| 3. Evacuation des cendres | 8. Filtrations | 13. Décanteur |
| 4. Ventilateur | 9. Moteur à gaz et génératrice | 14. Aéro-refroidisseur |
| 5. Circuit de chauffage | 10. Catalyseur | |

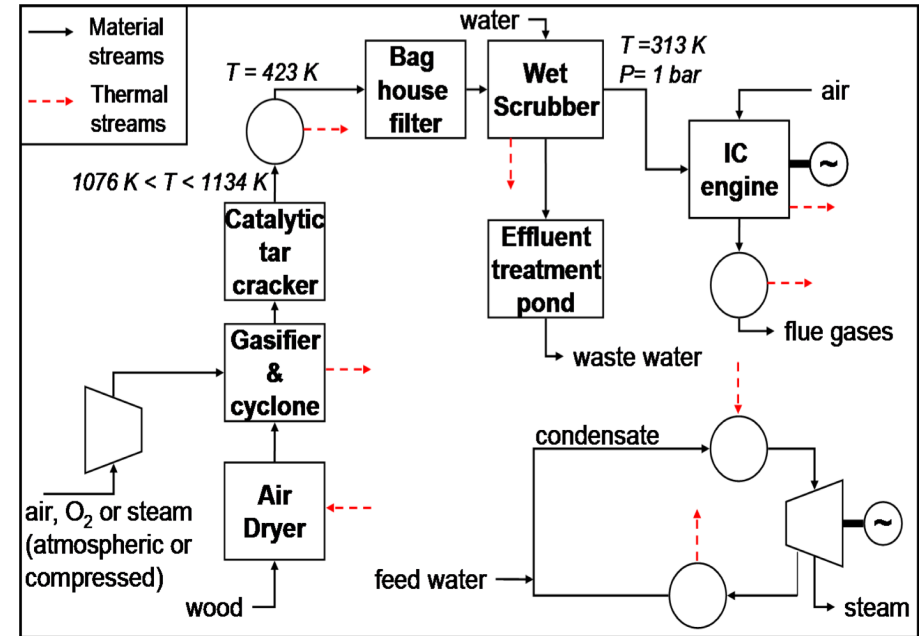
Hot gas cleaning and gas turbine



Hot Gas Cleaning (pros and cons)

- + no tar condensation (→ only particulates)
- Limited application
 - only gas turbine closed-coupled to gasifier
 - not feasible with IC engine
 - not possible to export syngas from site
- Cleaning technology not as established as CGC

Cold gas cleaning and IC engine

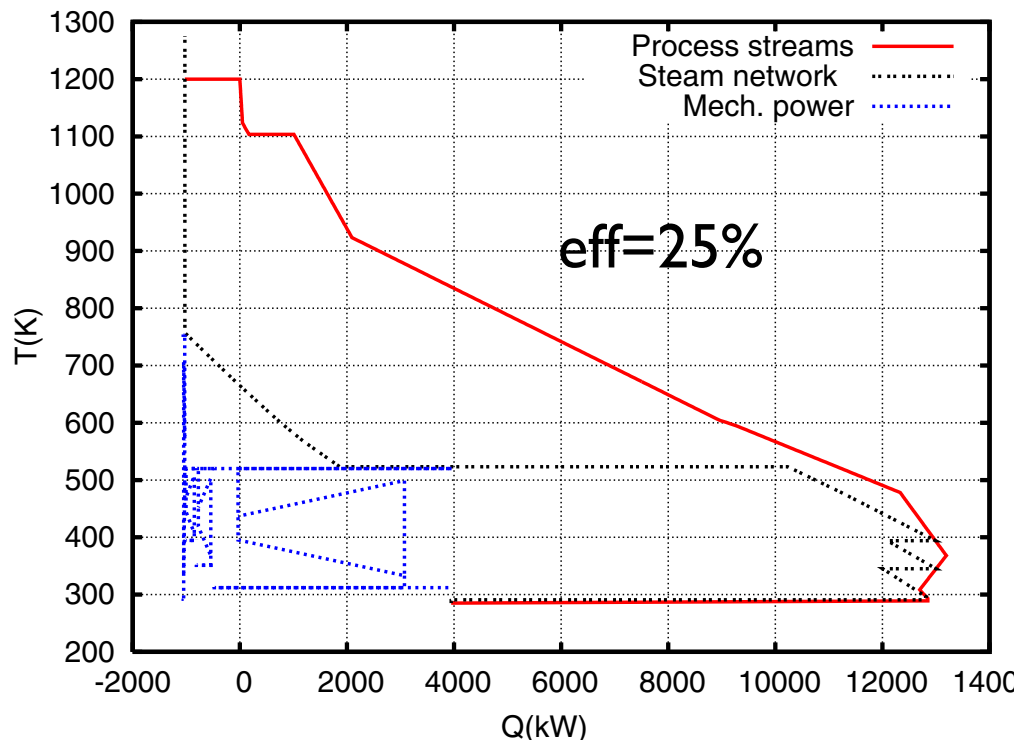


Cold Gas Cleaning (pros and cons)

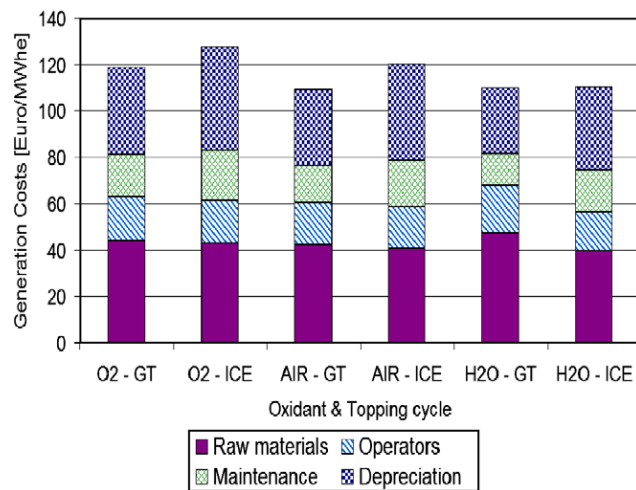
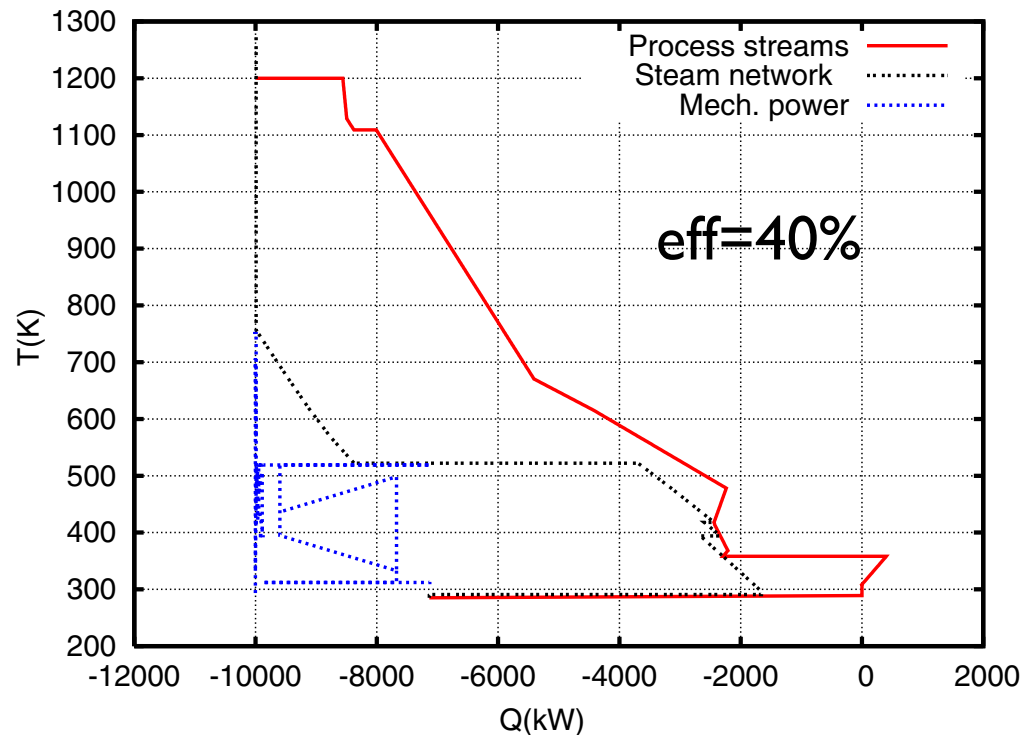
- tar condensation (→ tar disposal & equipment fouling concerns)
- + Flexibility
 - + possible to export, or to further process syngas –e.g. SNG)
 - + also feasible with gas turbine
- + Relatively mature cleaning technologies

Reactor (n. iterations)		O ₂ gasification (15000)		Air gasification (15000)		H ₂ O gasification (15000)	
	Units	Max eff.	Min cost	Max eff.	Min cost	Max eff.	Min cost
Invest. Costs	k€	29717	19129	32939	17122	26335	14339
Exergy eff.	-	0.32	0.13	0.33	0.10	0.34	0.19
Electric eff.	-	0.41	0.17	0.43	0.13	0.43	0.24
Cold gas eff.	-	0.63	0.28	0.65	0.27	0.78	0.81
Power	kWe	8269	3303	8534	2690	8685	4786
Specific cost	k€/kWe	3.59	5.79	3.86	6.37	3.03	3.00
Comp. curve	-	Not shown	Not shown	Fig. 5 left	Fig. 6 right	Not shown	Not shown
m.c wood	-	0.25	0.06	0.23	0.06	0.03	0.03
ER / SBR	-	0.25	0.25	0.25	0.25	0.34	0.33
P gasifier	bar	6.40	16.50	2.5	8.65	3.7	11.85
T gasifier	K	1123.5	1077.5	1134	1076	1119	1114
T inlet	K	753	737	611	591.5	753	749.5
Top. Cycle	-	ICE	GT	ICE	GT	ICE	GT

Gas turbine integration

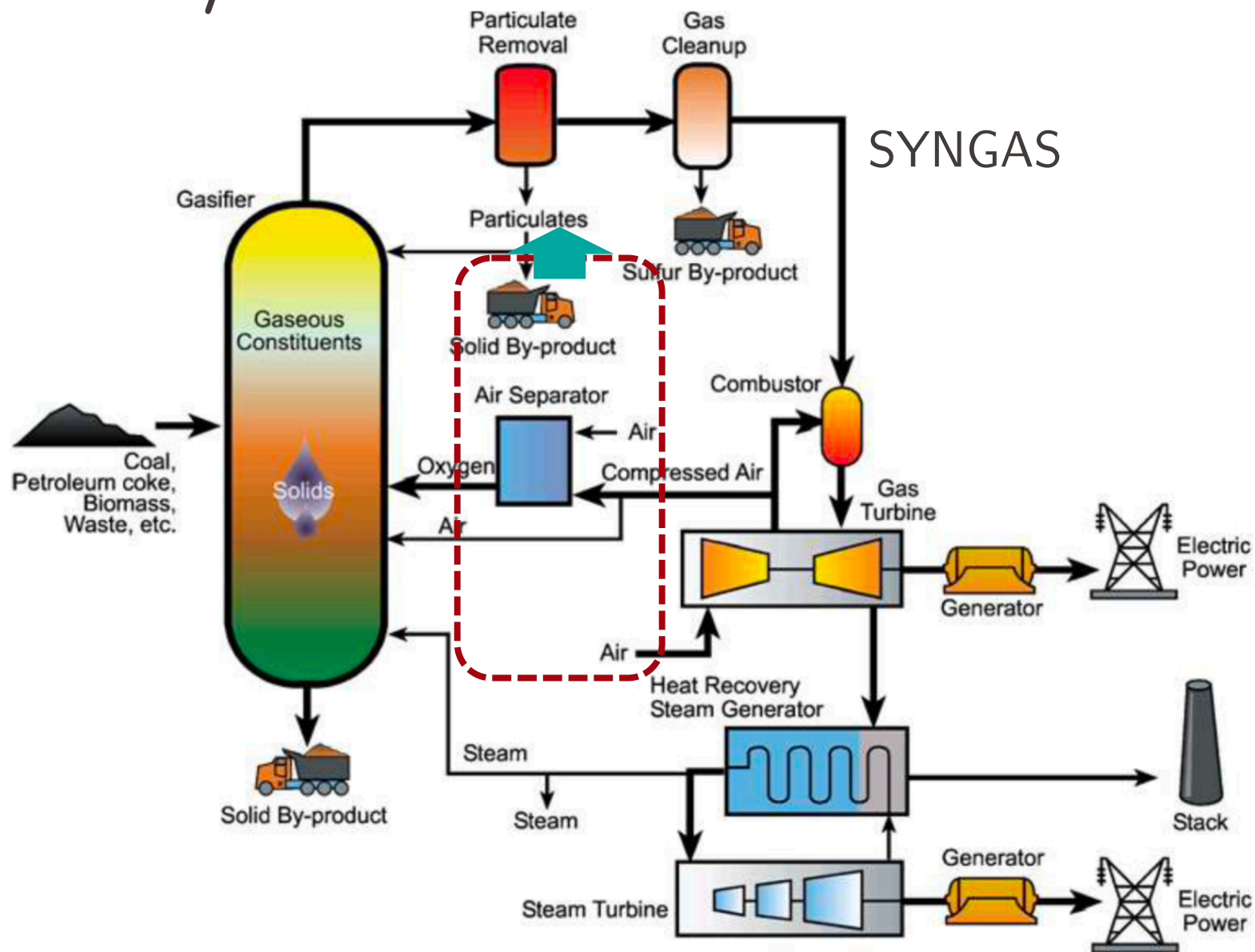


Gas engine integration



Biomass/Coal

ME-409 ENERGY CONVERSION AND RENEWABLE ENERGY



Integrating a fuel cell

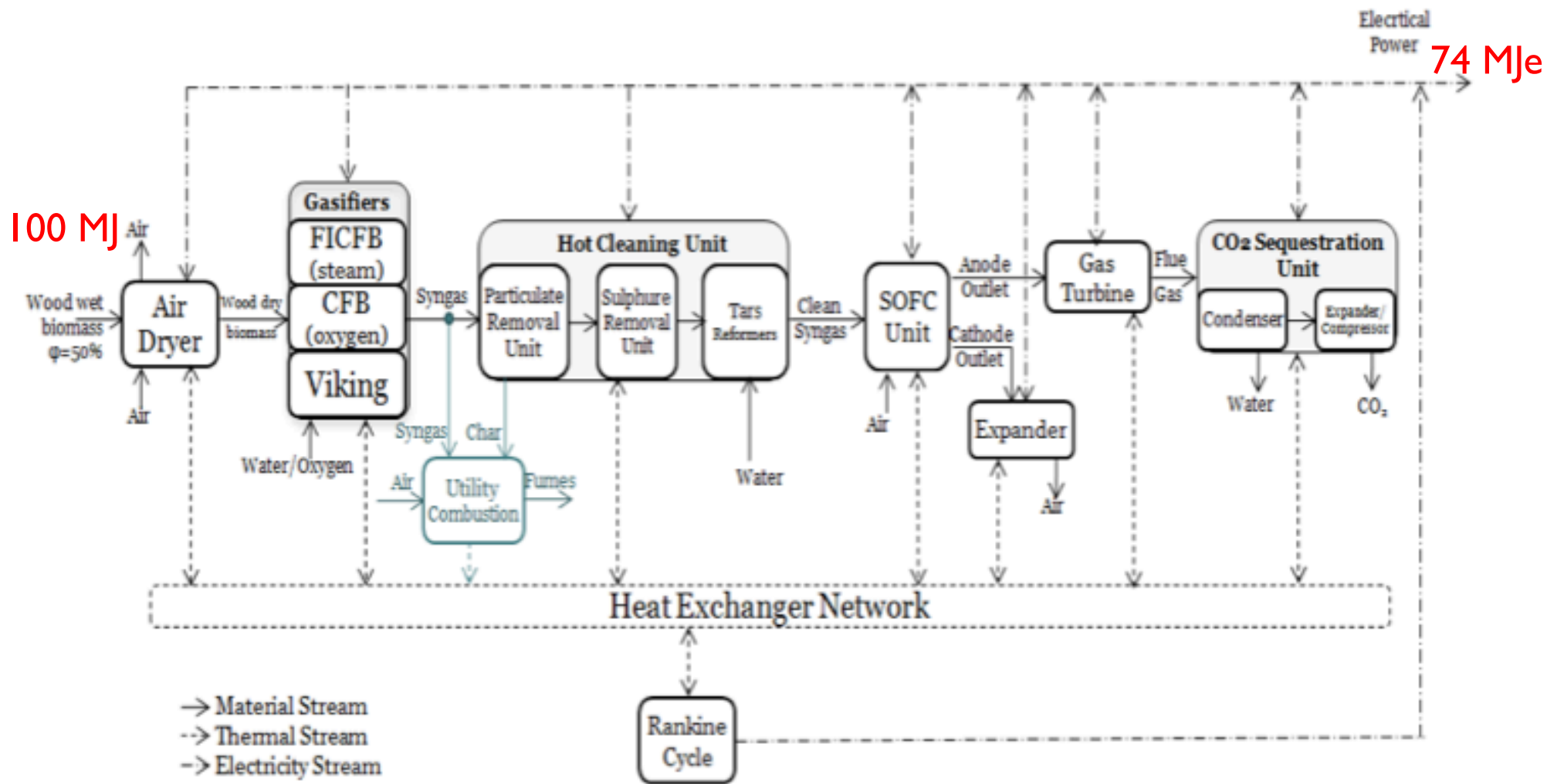
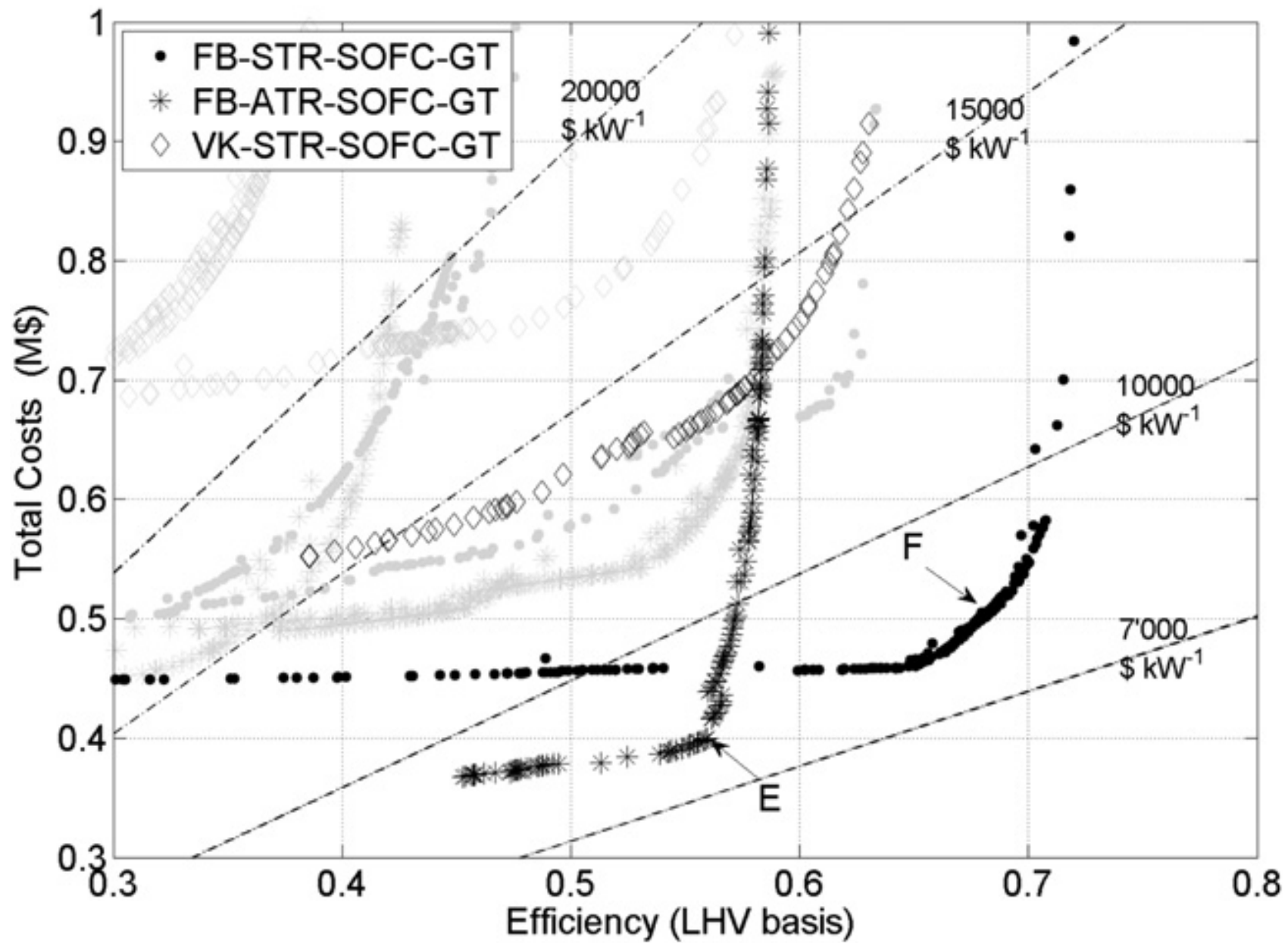


Table 1 – Summary of recent literature on biomass integrated gasification SOFC systems. Fixed: fixed bed gasifier; FB: Fluidized bed; GT: gas turbine (hybrid); ST: steam cycle (combined).

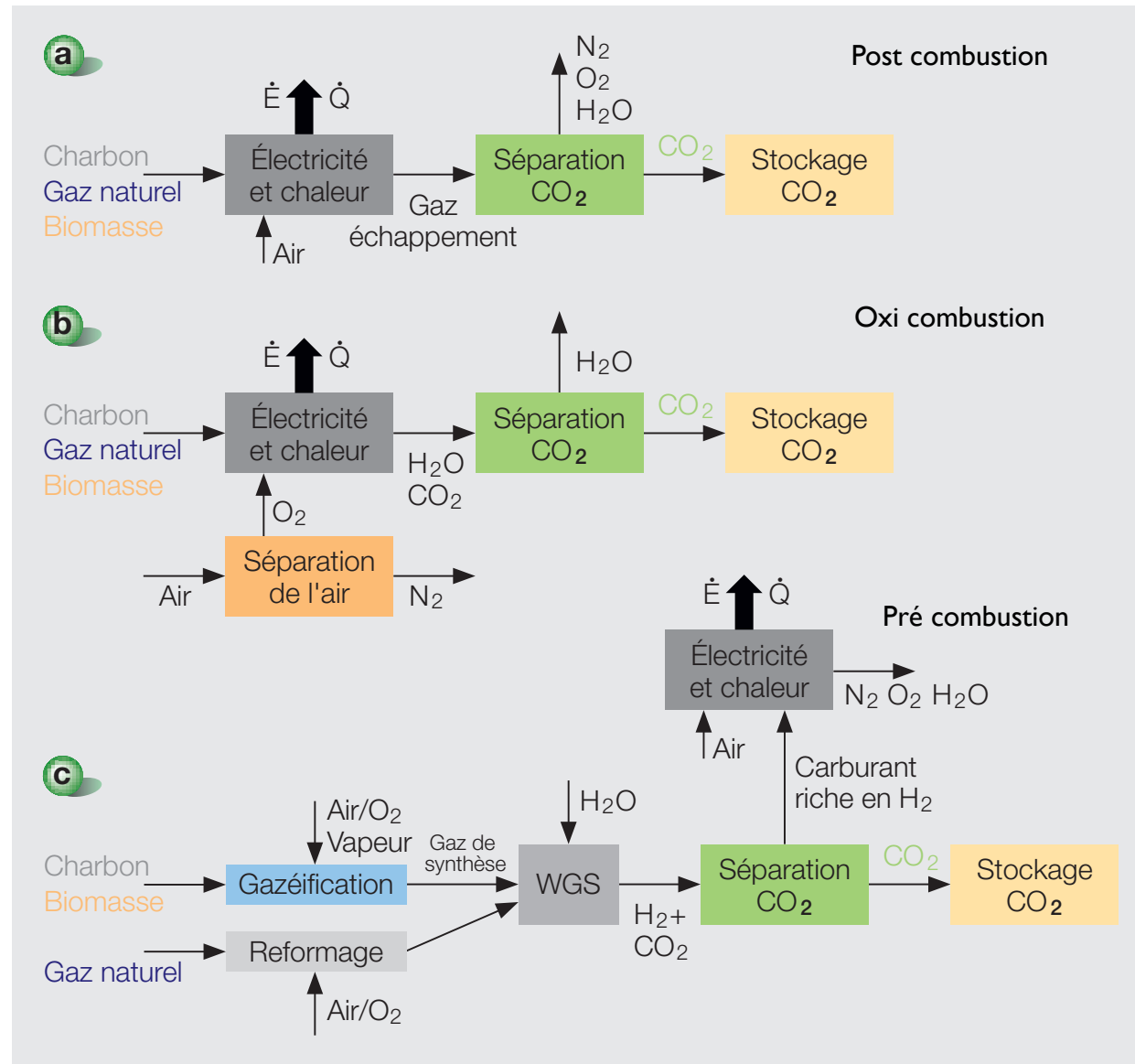
Reference	[9]	[10]	[11]	[12]	[13]	[14]	[15]	[16]
Scale	100 kW	10.1 MW	250 kW	170 kW	200 kW	140 kW	1 MW	30 MW
<i>Fuel composition mass fraction dry basis</i>								
C (%)	49.3	55.5	[17]	51.2	n.a.	51.2	40	50
H (%)	5.9	5.55		6.1	n.a.	6.1	5.35	6.12
N (%)	0.6	–		0.76	n.a.	0.76	0.62	0.55
O (%)	44	38.9		39.3	n.a.	39.3	44.5	42.5
S (%)	0.02	–		0.09	n.a.	0.09	0.15	0.06
Cl (%)	0.162	–		–	n.a.	–	–	–
Ash (%)	–	–		2.6	n.a.	2.6	9.41	0.8
Moisture (%ar)	12	10		10	n.a.	10	10	25.2
<i>Equip. specs</i>								
Type gasifier	Fixed	n.a.	Viking	FB	FB	FB	FB	Circ. FB [18]
Oxidizing agent	Air	Cathode air	Air	Steam	Air	Steam	Steam	Air
Gasifier temp (K)	1073	1573	–	1073	1173	1073	1223	1223
Min. gas cleaning temp. (K)	873	817	573	723	573	343	973	n.a.
TAR reformer	Yes	Yes	No	Yes	No	Yes	No	Yes
Type SOFC	Ni/GDC	n.a.	Risø [19]	n.a.	Planar	Ni/YSZ	n.a.	n.a.
	LSM				int. ref.	LSM/YSZ		
SOFC outlet temp. (K)	1273	1268	1073	1173	1223	1173	1073	1223
Current density ($A\ cm^{-2}$)	0.25	n.a.	0.3	0.3	n.a.	0.25	0.37	0.25
Fuel utilization (%)	85	80	85	85	n.a.	70	85	80
SOFC recirculation	Anode, cathode	n.a.	Anode, cathode	–	–	–	–	Anode, cathode
Auxiliary	Micro-GT	GT	GT (η 75%)	–	–	–	ST (η 75%)	GT (η 91%)
Turbine inlet temp. (K)	1273	1473	1173	–	–	–	–	1393
Maximum pressure (MPa)	0.7	n.a.	0.25	0.1013	0.1013	0.3	0.5	0.8
Heat exchangers	7	2	6	3	2	3	6	5
Max. eff. LHV (%)	54	42	50	34	23	36	64.4	50

Morandin, Matteo, François Maréchal, and Stefano Giacomini. “Synthesis and Thermo-economic Design Optimization of wood-gasifier-SOFC Systems for Small Scale Applications.” *Biomass and Bioenergy* 49 (2013): 299–314.



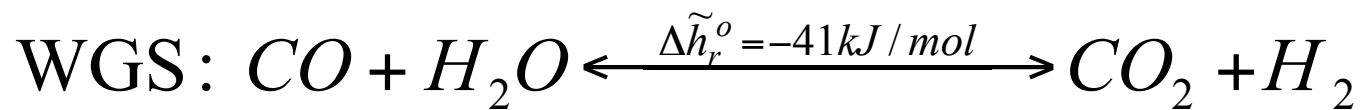
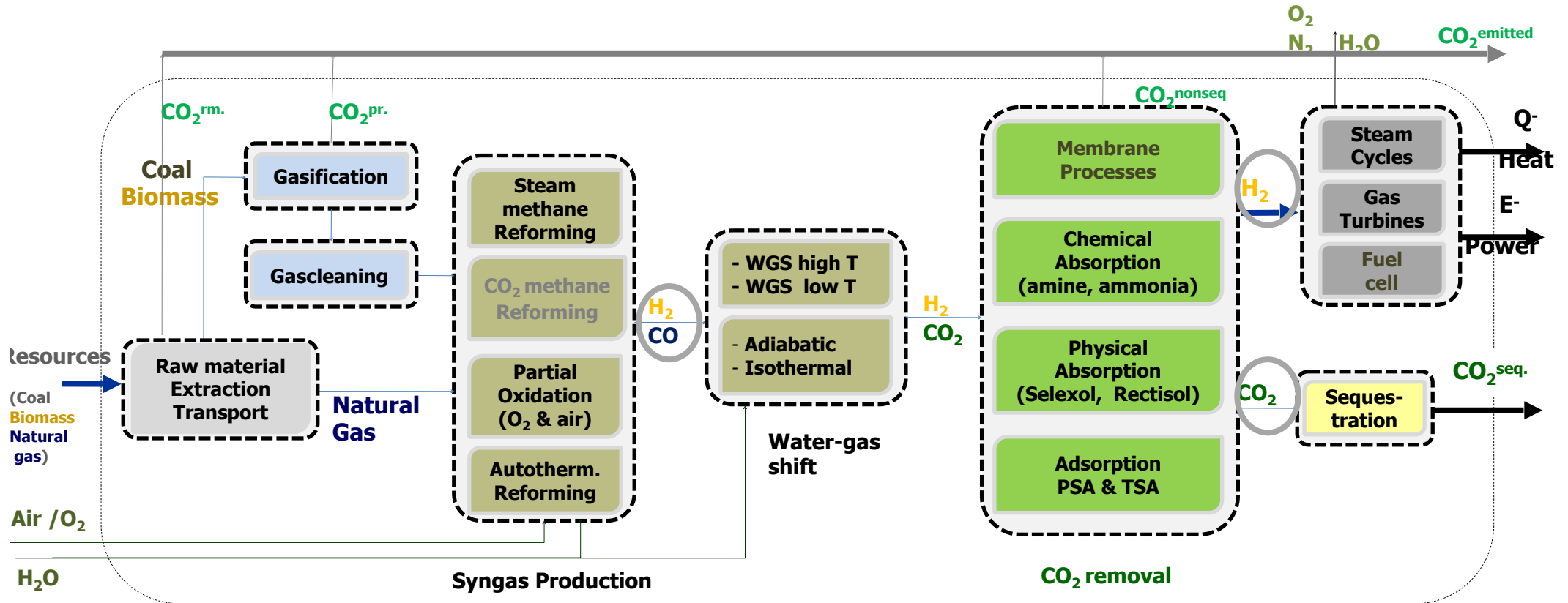
		Small size		Medium size		
Parameters	Unit	FICFB_NP_S	VKG_S	FICFB_NP_M	FICFB_P_M	CFB_M
Humidity wood dryer outlet	%	0.16	0.21	0.11	0.11	0.11
Steam/biomass ratio	-	0.76	-	0.85	0.9	0.56
Steam to carbon ratio in the reformers	-	1	1.08	1.12	1.86	1
Fuel cell Inlet temperature	K	1026	1023	101	1011	1022
Steam excess ratio in the post combustor	-	0.30	0.26	0.27	0.23	0.32
Energy efficiency	[%]	64.5	68.7	65.6	67	71%
Specific investment cost	[\$/kW]	22048	27196	11113	10280	9305
Specific Cost (electricity output)	[\$/kWh el]	1.03	1.10	0.35	0.33	0.30
Specific Cost (biomass input)	[\$/kWh th,BM]	0.63	0.71	0.21	0.20	0.19

- NG Penalty
 - Compression
 - 2% (LHV)
 - Capture :
 - 4-7% (LHV)
 - Total
 - 6 à 9% (LHV)
- Investissement
 - + 30%

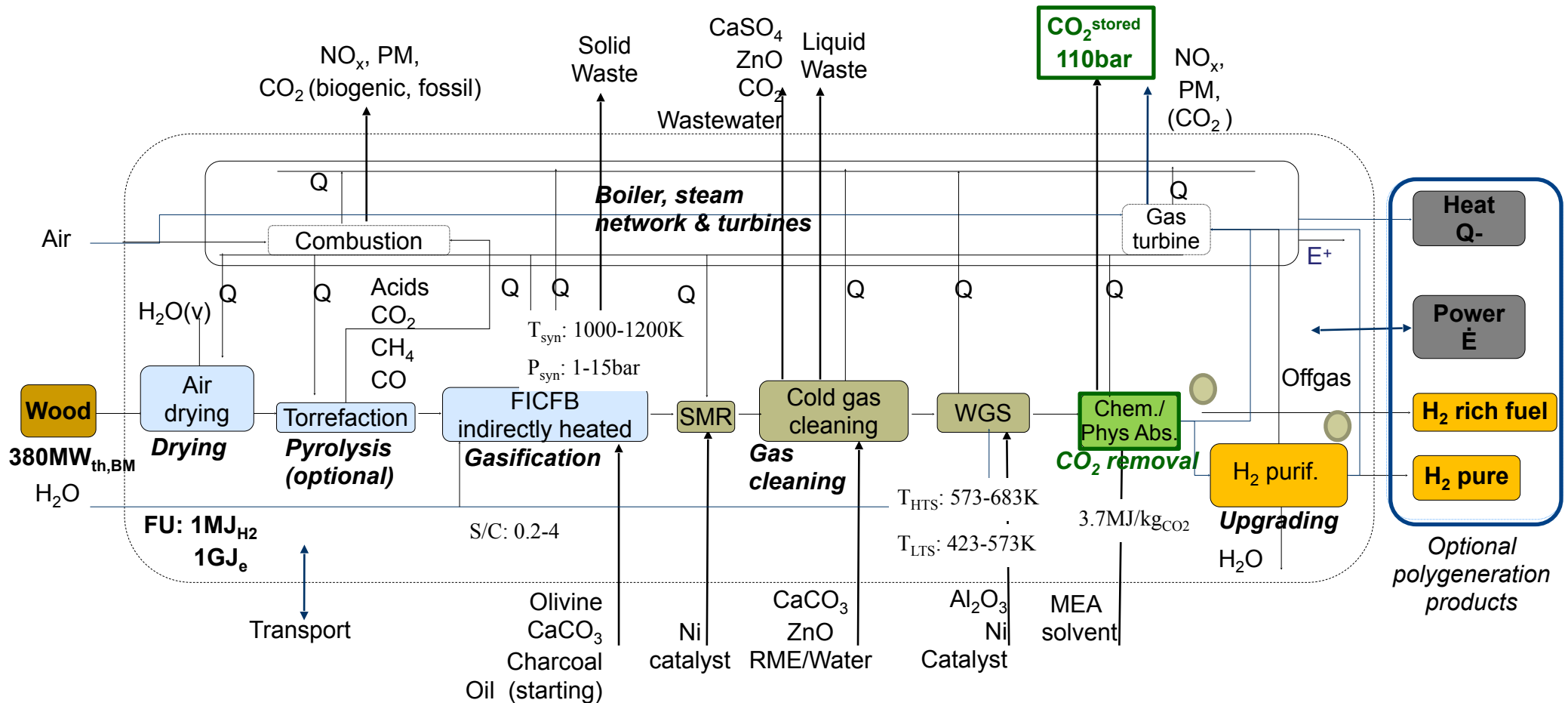


Physical model

- ◆ Superstructure of pre-combustion processes⁶
 - Conceptual process design of fuel decarbonisation



Electricity production with CO₂ capture



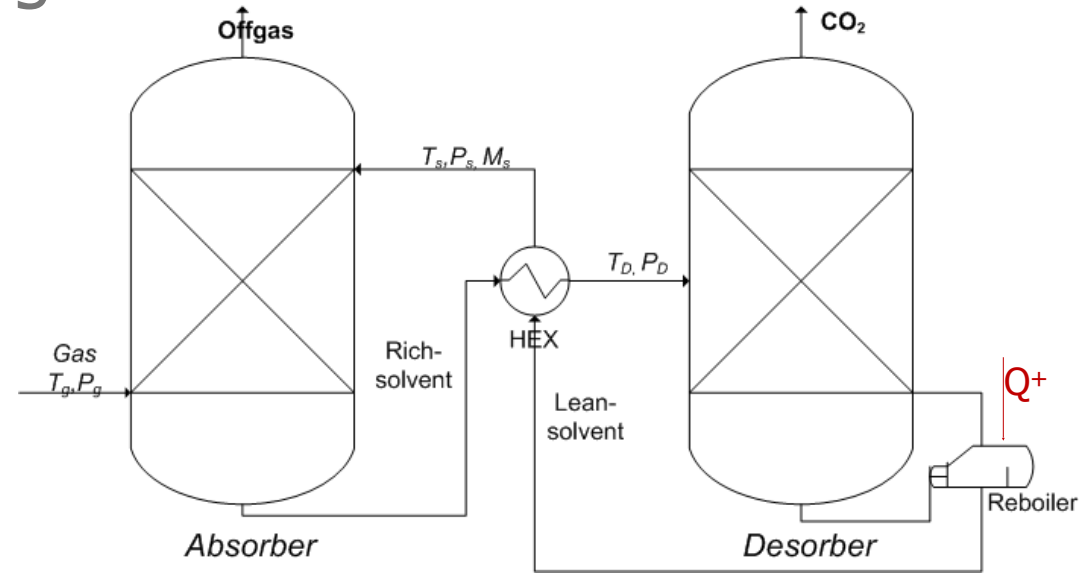
➤ Configurations (380MW_{th, BM})

- Without/with CO₂ capture (compression to 110bar)
- H₂ process with E-dot import or self-sufficient or E-dot generation

Context

◆ CO₂ separation technologies

- Chemical absorption
- Physical absorption
- Physical adsorption
- Membrane processes



Process ²	Operating conditions ?	Separation/purification capacity ?	Energy requirement ?	Costs ?	
	Conditions	Gas removed	Thermal energy [kWh/kgCO ₂]	Mechanical work [kWh/kgCO ₂]	CO ₂ purity [%mol]
Rectisol	$T_{abs} \approx -10 / -70^{\circ}C$ $p_{CO_2} > 10$ bar	CO ₂ , NH ₃ H ₂ S, COS, HCN	0.025	0.038	<90%
Selexol	$p_{CO_2} \approx 7-30$ bar	CO ₂ , NH ₃ H ₂ S, COS, HCN	0.016-0.024	0.03-0.06	
MEA	$T_{abs} \approx 40^{\circ}C$, 1-5 bar $T_{desorb} = 95 - 120^{\circ}C$	CO ₂ , CS ₂ H ₂ S, SO ₂ , COS	2.3 ($\approx 0.48 kWh_e / kg_{CO_2}$)	0.05-0.3	< 99%
PSA-Flue gas 28-34% CO ₂	$P_{ads} = 1$ bar $P_{desorb} = 0.05-0.9$ bar	CO ₂	0.16-0.18		
PSA - syngas	$P_{ads} = 13-21$ bar $P_{desorb} < 1$ bar	CO ₂			>90%

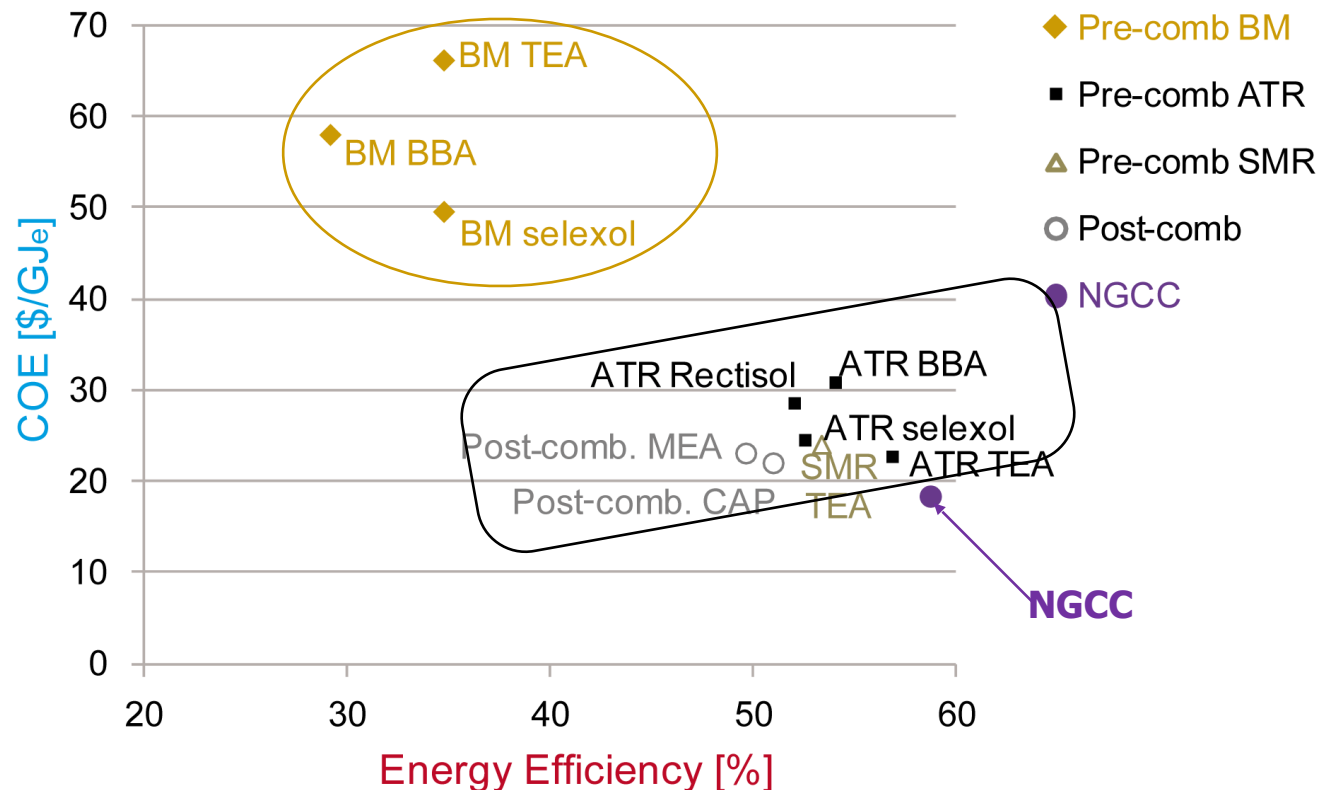
²Göttlicher 1999

CO₂ capture options comparison

◆ CO₂ capture energy and cost penalty

➤ Different process configurations

- Natural gas fed processes 90% CO₂ capture, biomass 60%



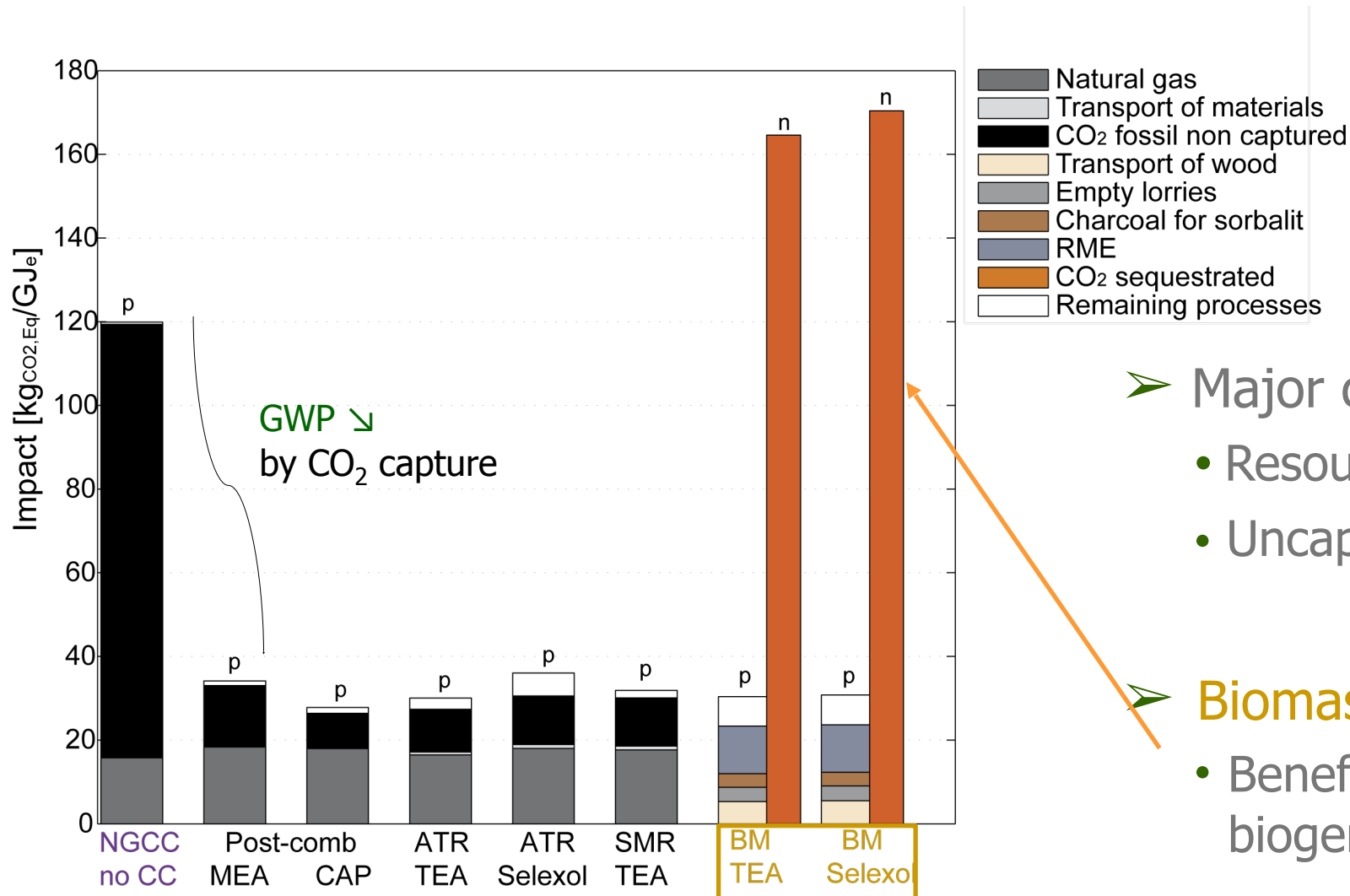
➤ Competition between post- and pre-combustion

Economic scenario base: 9.7\$/GJ_{res}, 7500h/y, 25y, 6%_{irr}

CO₂ capture options comparison

◆ CO₂ capture environmental performance

- IPCC 07: Global warming potential (FU=1GJe)



- Major contributions
 - Resource extraction
 - Uncaptured CO₂
- Biomass fed process
 - Benefit of capturing biogenic CO₂ !

Decision-making

◆ Most economically competitive process configurations

System	NGCC	Post-comb	ATR	BM
Performance	no CC	MEA	Selexol	Selexol
Feed [MW_{th}]	559	582	725	380
CO ₂ capture [%]	0	82.9	78.6	69.9
ϵ_{tot} [%]	58.75	50.6	53.5	35.4
Net electricity [MW_e]	328	295	383	135
[$kg_{CO_2, local}/GJ_e$]	105	13.9	22.2	-198.1
COE incl. tax [$\$/GJ_e$]	18.2-28.8	9-40	12.8-42	15-69
Avoid. Costs incl. tax [$\$/t_{CO_2, avoided}$]	-	-63-121	-49-127	0-253

➤ CO₂ capture penalty

- **Efficiency** ↓: 6-10%-pts (CO₂ compression ~2%-pts)
- **COE** ↑: 20-25%

➤ Best performing process

- **Efficiency**: Nat gas. pre-comb.
- **Economic**: Nat gas. post-comb.
- **Environmental**: Biomass pre-comb.

➤ Competition between processes and objectives!

Producing electricity from biomass

- ◆ efficiency <40% : Combustion + Rankine cycle
=> cogeneration
- ◆ efficiency up to 70% : Gasification +
 - ◆ Gas turbines
 - ◆ Engines
 - ◆ Fuel cells + Rankine cycle
- ◆ efficiency 40% : Gasification + Reforming
 - ◆ H₂ production
 - ◆ CO₂ separation for sequestration