

# **Fundamentals of Analog VLSI Design**

## **Exercise 2 - Problem**

**Differential pair - Inverter - Velocity saturation**

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# 1 Problem 1: The differential pair

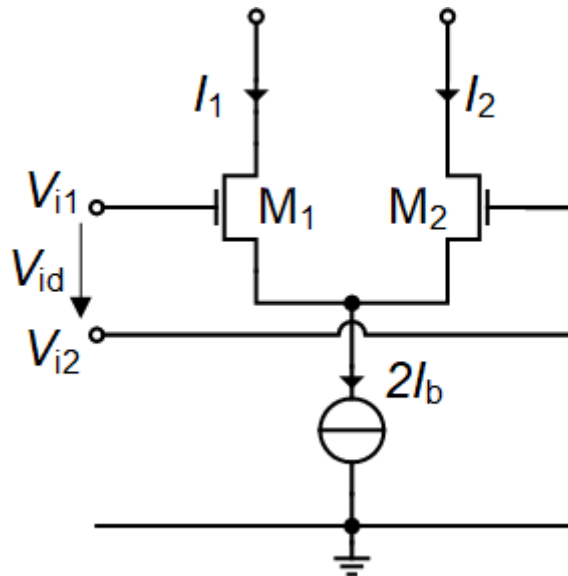


Figure 1.1: Differential pair schematic.

Figure 1.1 shows the schematic of the basic differential pair. The differential input voltage is defined as  $V_{id} \triangleq V_{i1} - V_{i2}$ , whereas the differential output current is defined as  $I_{od} \triangleq I_1 - I_2$ .

## **i** Note

We assume that  $M_1$  and  $M_2$  are perfectly matched. also assume that  $M_1$  and  $M_2$  are long-channel transistors so we can ignore short-channel effects such as velocity saturation.

## 1.1 Both transistors in weak inversion

### 1.1.1 Large-signal characteristic

Derive the large-signal expression of the differential output current  $I_{od}$  as a function of the differential input voltage  $V_{id}$  assuming that both transistors are biased in weak inversion and saturation.

### 1.1.2 Small-signal characteristic

Derive the small-signal transconductance from the large-signal transfer function obtained above and its particular value  $G_{m0}$  at  $V_{id} = 0$ . What is the approximate linear range if the differential pair is modeled by a piece-wise linear characteristic having a slope  $G_{m0}$  equal to that of the differential pair at  $V_{id} = 0$ ?

## 1.2 Both transistors in strong inversion

### 1.2.1 Large-signal characteristic

Derive the large-signal expression of the differential output current  $I_{od}$  as a function of the differential input voltage  $V_{id}$  assuming that both transistors are biased in strong inversion and saturation.

### 1.2.2 Small-signal transconductance

Derive the small-signal transconductance from the large-signal transfer function obtained above and its particular value  $G_{m0}$  at  $V_{id} = 0$ . What is the approximate linear range if the differential pair is modeled by a piece-wise linear characteristic having a slope  $G_{m0}$  equal to that of the differential pair at  $V_{id} = 0$ ?

## 1.3 Optional: Both transistors in any modes of operation (saturation)

We can use the EKV charge-based model to derive an expression of the differential input voltage as a function of the differential output current valid in any modes of operation (in saturation). In order to do this, first express the input voltages  $V_{i1}$  and  $V_{i2}$  normalized to  $2nU_T$  as a function of the normalized source charges  $q_{s1}$  and  $q_{s2}$ . Then find an expression of  $i_1$  and  $i_2$  defined as

$$i_1 \triangleq \frac{I_1}{2I_b} = \frac{i_{d1}}{2IC_q}, \quad (1.1)$$

$$i_2 \triangleq \frac{I_2}{2I_b} = \frac{i_{d2}}{2IC_q}, \quad (1.2)$$

with  $i_{d1} \triangleq I_1/I_{spec}$ ,  $i_{d2} \triangleq I_2/I_{spec}$  and  $IC_q \triangleq I_b/I_{spec}$  and where  $I_{spec}$  is the specific current of  $M_1$  and  $M_2$  and  $IC_q$  is the inversion coefficient of  $M_1$  and  $M_2$  at the quiescent point, i.e. for  $V_{id} = 0$ . You can then invert  $i_1$  and  $i_2$  to obtain expressions of  $q_{s1}$  and  $q_{s2}$  in terms of  $i_{od} \triangleq i_1 - i_2$  and parameter  $IC_q$ . Sweeping the normalized output current  $i_{od}$  for a given  $IC_q$ , you get the corresponding differential input voltage  $v_{id}$ .

## 2 Problem 2: The inverter as a transconductance amplifier

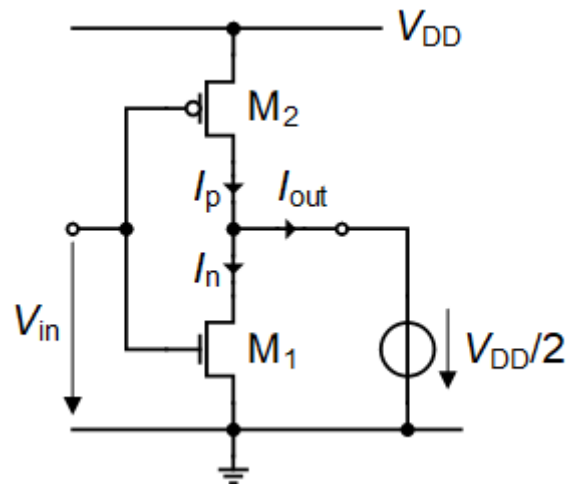


Figure 2.1: The CMOS inverter.

As shown in Figure 2.1, the inverter can be used as a class AB transconductance amplifier. Derive the large-signal output current  $I_{out} = I_p - I_n$  versus the input voltage  $V_{in}$  assuming that both transistors are biased in weak inversion and saturation and have the same slope factor  $n_n = n_p = n$ . Note that the output voltage is maintained constant at  $V_{DD}/2$  to calculate the output current  $I_{out}$ . What is limiting the output current?

## 3 Problem 3: Effect of velocity saturation on the gate transconductance

In this problem we want to investigate the effect of velocity saturation on the gate transconductance of an nMOS transistor. We will compare the long-channel case to the short-channel first in strong inversion and then in weak inversion.

### 3.1 Strong inversion

For strong inversion we assume a bias current  $I_b = 20 \mu A$  and an inversion coefficient  $IC = 30$  to drive a large load capacitance  $C_L = 5 pF$ . Calculate its gate transconductance  $G_m$  and bandwidth assuming its slope factor is  $n = 1.3$  and  $U_T = 26 mV$  in the following cases.

#### 3.1.1 Long-channel case

Assume the channel is long enough to ignore the effect of velocity saturation.

#### 3.1.2 Short-channel case

Assume the transistor length is short resulting in a velocity saturation parameter  $\lambda_c = 1/3$ . How much smaller is the gate transconductance and bandwidth with velocity saturation compared to the long-channel case?

### 3.2 Weak inversion

In the case of weak inversion we assume an inversion coefficient  $IC = 0.1$ , a bias current  $I_b = 100 nA$  and a load capacitance  $C_L = 0.1 pF$ .

#### 3.2.1 Long-channel case

Assume again that the channel is long enough to ignore the effect of velocity saturation.

#### 3.2.2 Short-channel case

Assume the transistor length is short resulting in a velocity saturation parameter  $\lambda_c = 1/3$ . How much smaller is the gate transconductance and bandwidth with velocity saturation compared to the long-channel case?

What can we conclude from this simple example?