

Course 06/2

Nosé-Hoover thermostats.

- Real variables vs virtual variables (scaling of time)
- Equations of Nosé-Hoover thermostat
- Setting of inertia parameter Q

Real variables vs virtual variables (scaling of time)

Real variables

$$r' = r$$

$$p' = p/s$$

$$dt' = dt/s$$

Virtual Nosé variables

$$r$$

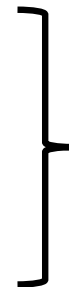
$$p$$

$$dt$$

This implies that the scaling of momenta occurs through the scaling of time!

$$p' = m \frac{dr'}{dt'} = m \frac{dr}{dt'}$$

$$p' = p/s = ms \frac{dr}{dt}$$



$$dt' = dt/s$$

In the Nosé simulation, the integration is done at integer multiples of the virtual time step Δt . Given the relation $\Delta t' = \Delta t/s$, the real time step $\Delta t'$ fluctuates with s .

Time averages

So far

$$\bar{A} = \lim_{\tau \rightarrow \infty} \frac{1}{\tau} \int_0^{\tau} dt \, A(p^N(t)/s(t), r^N(t))$$

virtual time virtual time

Suppose that we want to sample at integer multiples of a real time step

$$\lim_{\tau' \rightarrow \infty} \frac{1}{\tau'} \int_0^{\tau'} dt' \, A(p^N(t')/s(t'), r^N(t')) = ?$$

real time real time

Time averages in real time

Since $dt' = dt/s$, the following relation holds:

$$\int_0^{\tau'} dt' = \int_0^{\tau} dt \frac{1}{s(t)} \quad \Rightarrow \quad \tau' = \int_0^{\tau} dt \frac{1}{s(t)}$$

Let us now transform the time average calculated over the real time steps:

$$\begin{aligned} & \lim_{\tau' \rightarrow \infty} \frac{1}{\tau'} \int_0^{\tau'} dt' A(p^N(t')/s(t'), r^N(t')) \\ &= \lim_{\tau' \rightarrow \infty} \frac{\tau}{\tau'} \frac{1}{\tau} \int_0^{\tau} dt A(p^N(t)/s(t), r^N(t))/s(t) \quad \begin{array}{l} \text{change of variable} \\ t' \rightarrow t \end{array} \\ &= \frac{\lim_{\tau \rightarrow \infty} \frac{1}{\tau} \int_0^{\tau} dt A(p^N(t)/s(t), r^N(t))/s(t)}{\lim_{\tau \rightarrow \infty} \frac{1}{\tau} \int_0^{\tau} dt 1/s(t)} = \frac{\langle A(p^N/s, r^N)/s \rangle_{\text{Nosé}}}{\langle 1/s \rangle_{\text{Nosé}}} \end{aligned}$$

Time averages in real time

But what is

$$\lim_{\tau' \rightarrow \infty} \frac{1}{\tau'} \int_0^{\tau'} dt' A(p^N(t')/s(t'), r^N(t')) = \frac{\langle A(p^N/s, r^N)/s \rangle_{\text{Nosé}}}{\langle 1/s \rangle_{\text{Nosé}}} \quad ?$$

For this, we use the partition function of the Nosé system:

$$\frac{\langle A(p^N/s, r^N)/s \rangle_{\text{Nosé}}}{\langle 1/s \rangle_{\text{Nosé}}} = \frac{\int dp_i^N dr_i^N A(p'^N, r^N) \exp \left[-\frac{3N}{g} \beta \mathcal{H}^{\text{PHYS}}(p'^N, r^N) \right]}{\int dp_i^N dr_i^N \exp \left[-\frac{3N+1}{g} \beta \mathcal{H}^{\text{PHYS}}(p'^N, r^N) \right]} = \frac{\int dp_i^N dr_i^N \exp \left[-\frac{3N}{g} \beta \mathcal{H}^{\text{PHYS}}(p'^N, r^N) \right]}{\int dp_i^N dr_i^N \exp \left[-\frac{3N+1}{g} \beta \mathcal{H}^{\text{PHYS}}(p'^N, r^N) \right]}$$

Time averages in real time: result

$$\frac{\langle A(p^N/s, r^N)/s(t) \rangle_{\text{Nosé}}}{\langle 1/s \rangle_{\text{Nosé}}} = \frac{\int dp_i'^N dr_i'^N A(p'^N, r^N) \exp \left[-\frac{3N}{g} \beta \mathcal{H}^{\text{PHYS}}(p'^N, r^N) \right]}{\int dp_i'^N dr_i'^N \exp \left[-\frac{3N}{g} \beta \mathcal{H}^{\text{PHYS}}(p'^N, r^N) \right]}$$

$$= \langle A(p'^N, r^N) \rangle_{\text{NVT}}$$

$$g = 3N$$

The sampling at integer multiples of real time gives the correct canonical sampling provided one sets $g = 3N$!

Equations of motion

Nosé Hamiltonian

$$\mathcal{H}_{\text{Nosé}} = \sum_{i=1}^N \frac{p_i^2}{2m_i s^2} + U(r^N) + \frac{p_s^2}{2Q} + \frac{g}{\beta} \ln s$$

Hamilton equations in virtual Nosé variables

$$(1.) \quad \frac{d\vec{r}_i}{dt} = \frac{\partial \mathcal{H}_{\text{Nosé}}}{\partial \vec{p}_i} = \frac{\vec{p}_i}{m_i s^2}$$

$$(2.) \quad \frac{d\vec{p}_i}{dt} = - \frac{\partial \mathcal{H}_{\text{Nosé}}}{\partial \vec{r}_i} = - \frac{dU(r^N)}{d\vec{r}_i}$$

$$(3.) \quad \frac{ds}{dt} = \frac{\partial \mathcal{H}_{\text{Nosé}}}{\partial p_s} = \frac{p_s}{Q}$$

$$(4.) \quad \frac{dp_s}{dt} = - \frac{\partial \mathcal{H}_{\text{Nosé}}}{\partial p_s} = \left(\sum_{i=1}^N \frac{p_i^2}{m_i s^2} - \frac{g}{\beta} \right) \frac{1}{s}$$

Change of variables

$$\begin{array}{cccc}
 dt \rightarrow dt' = dt/s & r \rightarrow r' = r & p \rightarrow p' = p/s & p_s \rightarrow p'_s = p_s/s \\
 \text{virtual} \quad \text{real} & \text{virtual} \quad \text{real} & \text{virtual} \quad \text{real} & \text{virtual} \quad \text{real}
 \end{array}$$

Transformation of the equations of motions

$$(1'.) \quad \frac{d\vec{r}_i'}{dt'} = s \frac{d\vec{r}_i}{dt} \stackrel{(1.)}{=} \frac{\vec{p}_i}{m_i s} = \frac{\vec{p}_i'}{m_i}$$

$$(2'.) \quad \frac{d\vec{p}_i'}{dt'} = s \frac{d\vec{p}_i/s}{dt} = \frac{d\vec{p}_i}{dt} - \frac{1}{s} \vec{p}_i \frac{ds}{dt}$$

$\downarrow \quad (2.)$

$\downarrow \quad (3.)$

$$= - \frac{dU(r^N)}{d\vec{r}_i} - \vec{p}_i' \frac{p_s}{Q} = - \frac{dU(r^N)}{d\vec{r}_i} - \vec{p}_i' \frac{s p_s'}{Q}$$

(3'.) ... and so on

(4'.)

Equations of motion in real variables

$$\left[\begin{array}{l} \frac{d\vec{r}_i'}{dt'} = \frac{\vec{p}_i'}{m_i} \\ \frac{d\vec{p}_i'}{dt'} = - \frac{dU(r'^N)}{d\vec{r}_i'} - \vec{p}_i' \frac{s p_s'}{Q} \\ \frac{1}{s} \frac{ds}{dt'} = \frac{s p_s'}{Q} \\ \frac{d}{dt'} \left(\frac{s p_s'}{Q} \right) = \frac{1}{Q} \left(\sum_{i=1}^N \frac{p_i'^2}{m_i} - \frac{g}{\beta} \right) \end{array} \right.$$

Constant of motion

$$E_{\text{NH}}^{\text{const}} = \sum_{i=1}^N \frac{p_i'^2}{2m_i} + U(r_i'^N) + \frac{s^2 p_s'^2}{2Q} + \frac{g}{\beta} \ln s$$

More convenient set of variables

We define $\dot{x}_{\text{NH}} = \frac{s p_s'}{Q}$

Equations of motion

$$\left. \begin{aligned} \dot{\vec{r}}_i &= \frac{\vec{p}_i}{m_i} \\ \dot{\vec{p}}_i &= - \frac{dU(r'^N)}{d\vec{r}_i} - \dot{x}_{\text{NH}} \vec{p}_i \\ \ddot{x}_{\text{NH}} &= \frac{1}{Q} \left(\sum_{i=1}^N \frac{p_i^2}{m_i} - \frac{g}{\beta} \right) \\ \frac{\dot{s}}{s} &= \frac{d \ln s}{dt} = \dot{x}_{\text{NH}} \end{aligned} \right\} \text{closed system}$$

Constant of motion

$$E_{\text{NH}}^{\text{const}} = \sum_{i=1}^N \frac{p_i^2}{2m_i} + U(r'^N) + \frac{Q \dot{x}_{\text{NH}}^2}{2} + \frac{g}{\beta} x_{\text{NH}}$$

Setting of inertia parameter Q

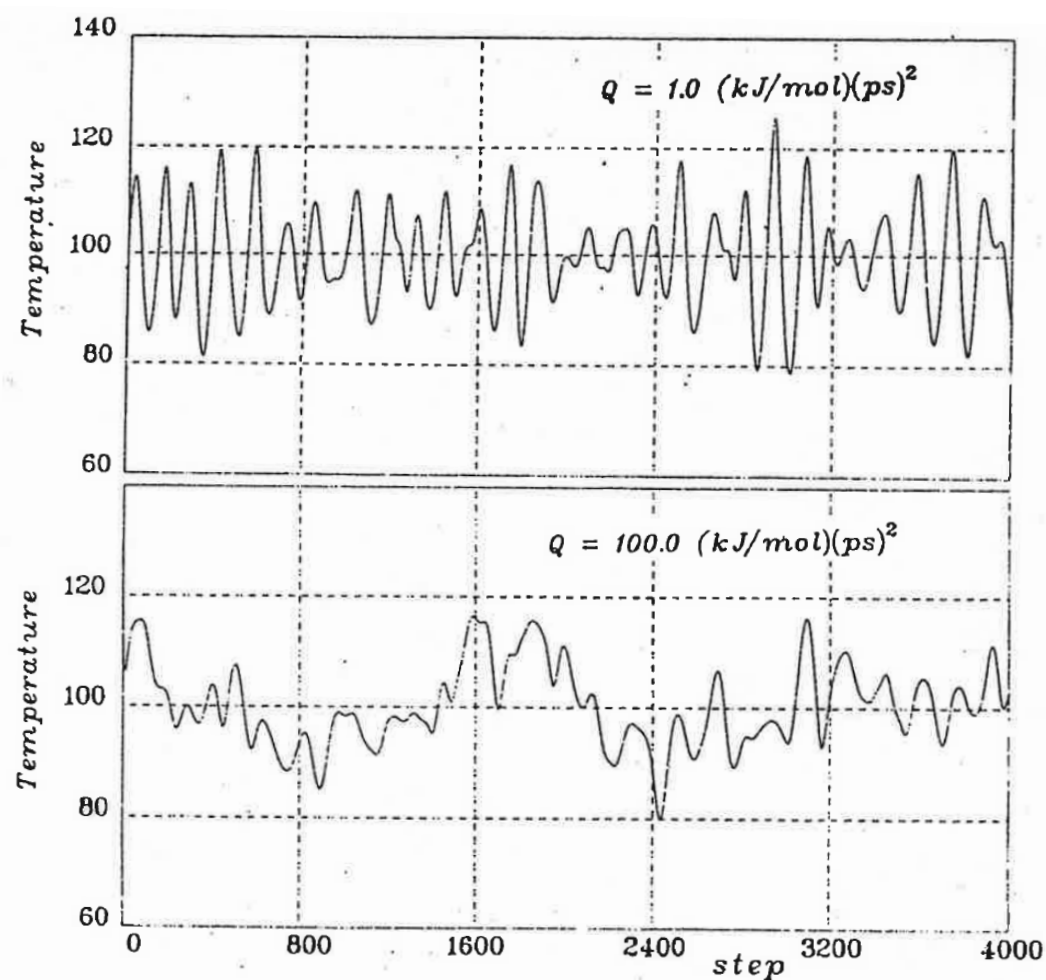
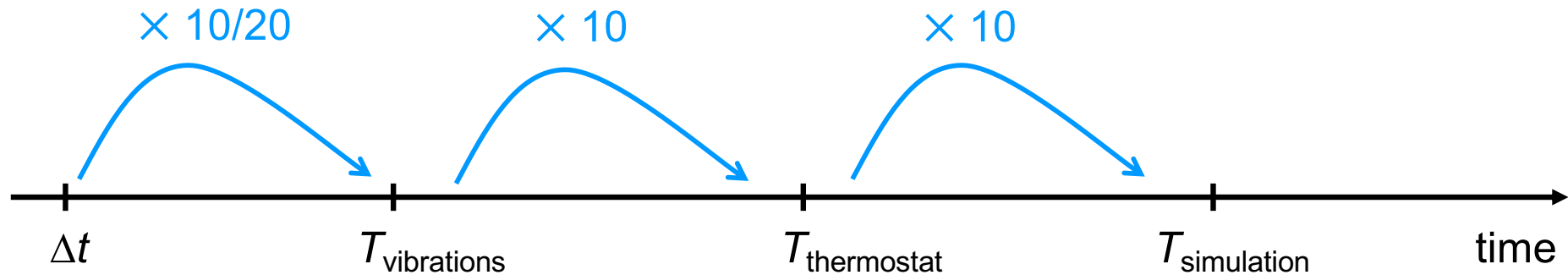


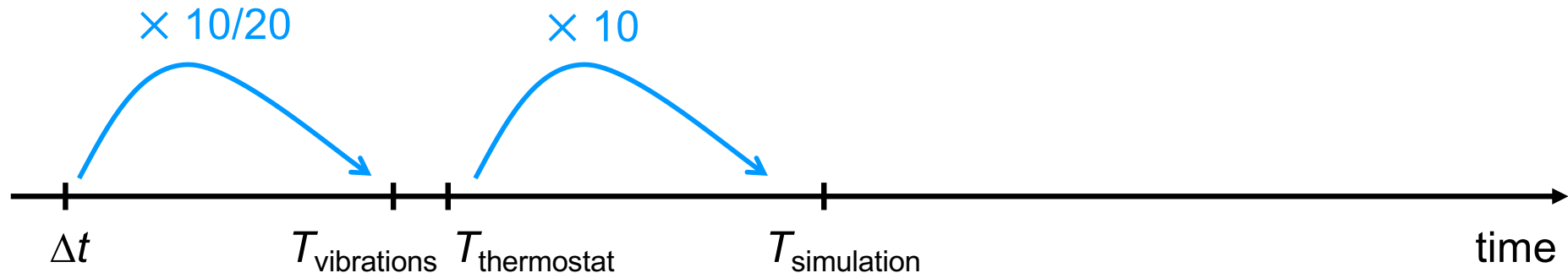
Figure 2. Comparison of the temperature fluctuations in runs with different Q values at 100 K. Above: $Q = 1 \text{ (kJ mol}^{-1}\text{)(ps)}^2$, Below: $Q = 100 \text{ (kJ mol}^{-1}\text{)(ps)}^2$. The total real time is about 7 ps.

Setting of inertia parameter Q : choice of time-scales

Ideally

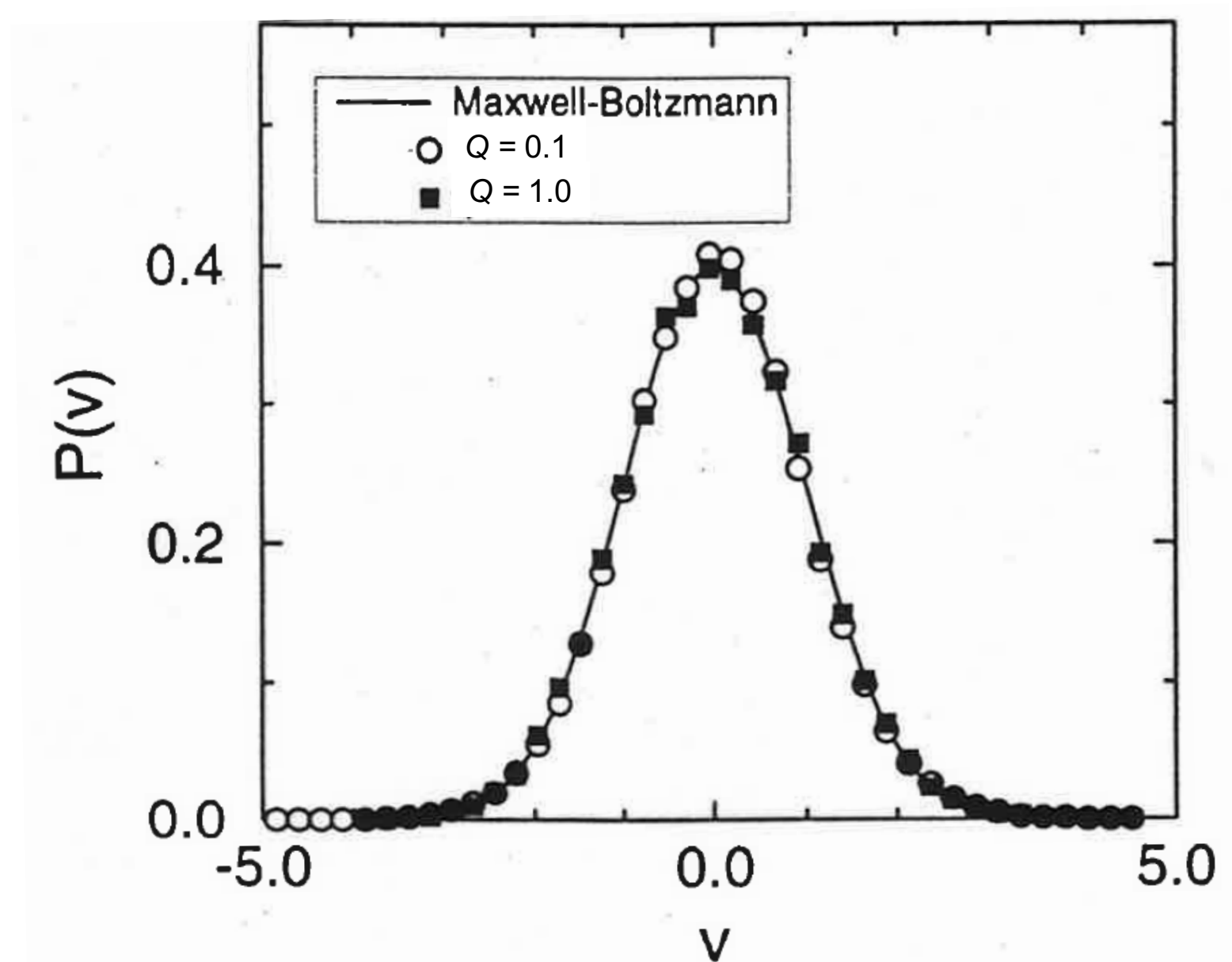


In practice



The trajectories are poorly affected because there is only one auxiliary variable s for $3N$ particles: $3N \gg 1$.

Distribution of velocities for various Q



Mean square displacement for various Q

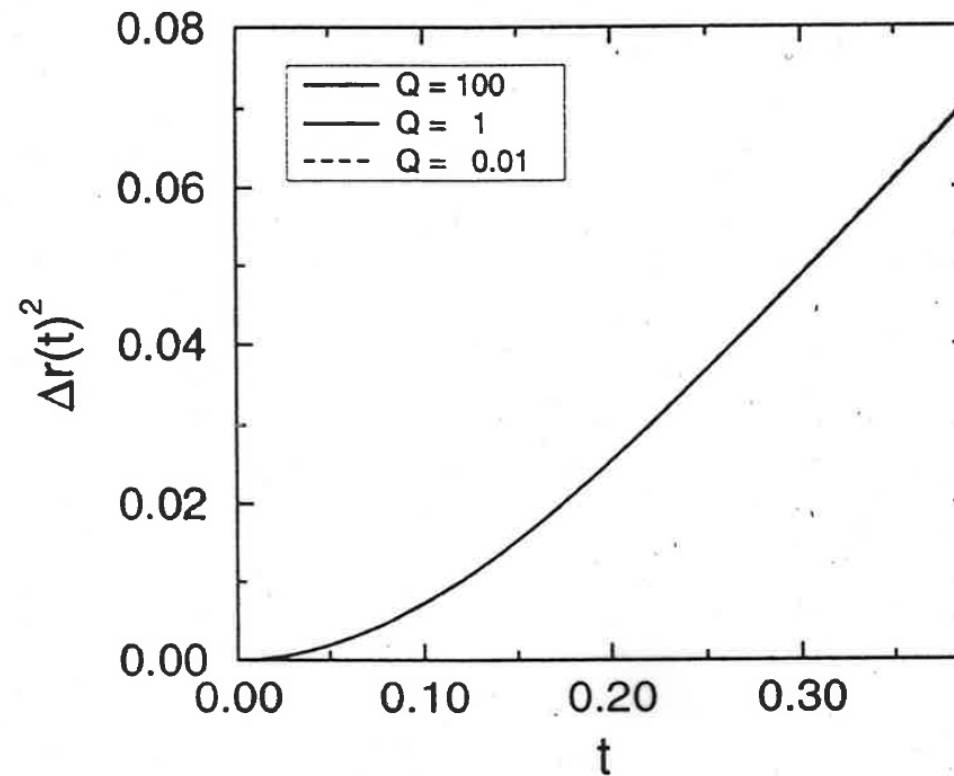


Figure 6.6: Effect of the coupling constant Q on the mean square displacement for a Lennard-Jones fluid ($T = 1.0$, $\rho = 0.75$, and $N = 256$).

Conclusive remarks

- Uniform sampling in real time: $g = 3N$.
- Only static properties like $A(\{p\}, \{r\})$ are correctly sampled.
This method does not allow one to obtain time-correlations.
- However, when the inertial mass Q is chosen suitably (time-scales),
the trajectories are poorly affected because there is only one auxiliary variable
 s for $3N$ particles: $3N \gg 1$.
- Caveat: do not use this method to thermalize starting from a fully
relaxed structure.

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