

# Adhesive wear

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TA: Son Pham-Ba

# Outline

[https://c4science.ch/source/Tribology\\_Course\\_nb/](https://c4science.ch/source/Tribology_Course_nb/)

- Lecture 1
  - Introduction of lecturer and laboratory LSMS (lsms.epfl.ch)
  - Introduction to tribology (my vision)
  - From da Vinci to rate and state friction laws
- Exercise 1 (optional HW): Some fundamental solutions in mechanics of solids
- Lecture 2
  - Surface roughness, self-affine roughness
  - Single asperity contact: Hertz contact theory
  - Multiple asperities contact, rough contact mechanics
- Exercise 2 (optional HW)
  - Generation with open-source software Tamaas of rough surfaces
  - Resolution of Hertz contact with Tamaas
- Lecture 3: From friction to wear
- Exercise 3 (optional HW): Resolution of rough contact mechanics with Tamaas

# Wear of materials

Friction is complicated. Wear is even more complicated and messier...

Ernest Rabinowicz:

“Although wear is an important topic,  
it has never received the attention it deserves”

Perceived as a “dirty” topic

1) Complex physics and chemistry

2) Many forms of wear

Adhesive (#1)

Abrasive (#2)

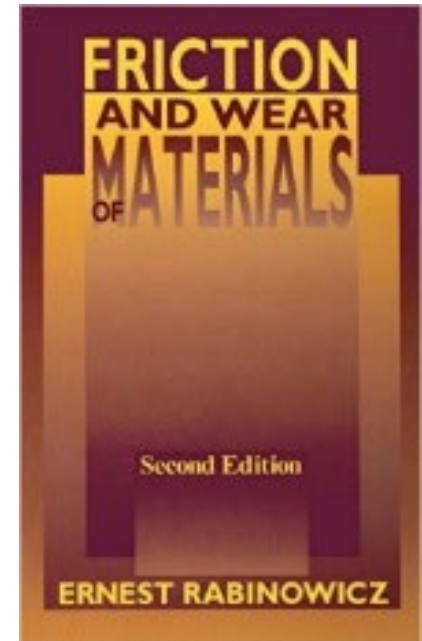
Surface fatigue, Fretting,

Erosive, Corrosion and oxidation...

3) Different stages (history), evolution of roughness, debris (or third bodies)

4) Different regimes (mild wear versus severe wear)

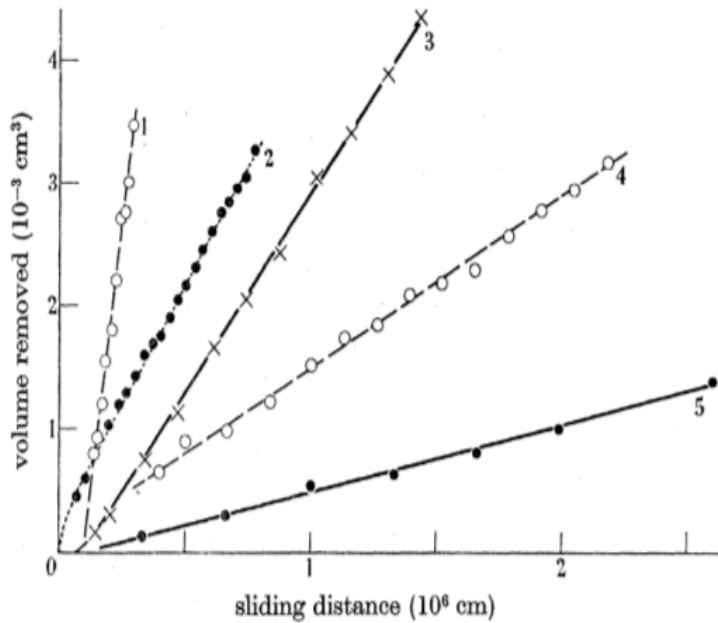
etc...



***Meng and Ludema, 1995: 300 equations on friction and wear (1957-1992)***

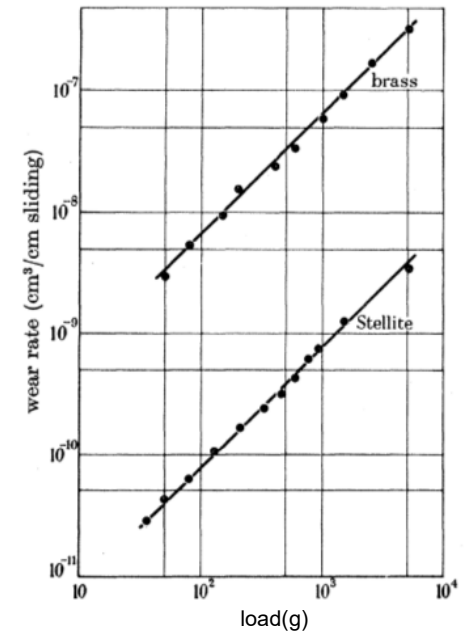
# Archard's concept of wear

Very popular engineering model for adhesive wear



*Archard, and Hirst,  
Proceedings of the Royal  
Society of London A, 1956*

*Burwell and Strang,  
Proceedings of the Royal  
Society of London A, 1952*

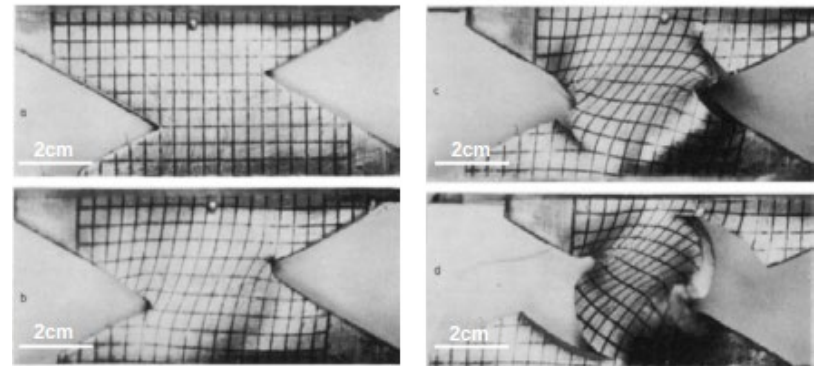


$$V = \frac{N S}{H_v}$$

$K=10^{-8}$  to  $10^{-4}$

independent of  $N$  (in mild wear regime)

What is  $K$ ?



*Brockley and Fleming, Wear, 1965*



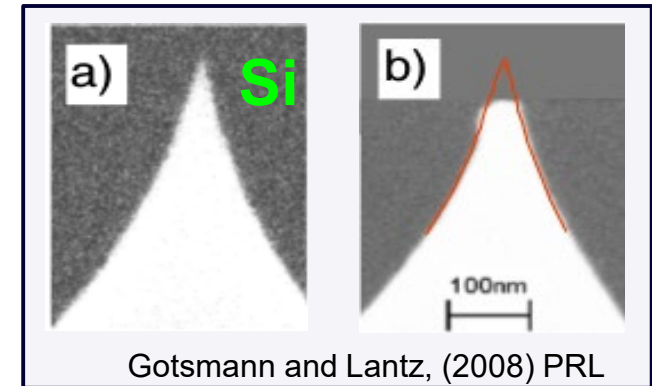
# Adhesive wear mechanisms

## Two macroscopic interpretations: Holm versus Archard

Small load limit: atom by atom attrition; breakdown of Archard (Jacobs & Carpick, Nat. Nanotech, 2013, ... )

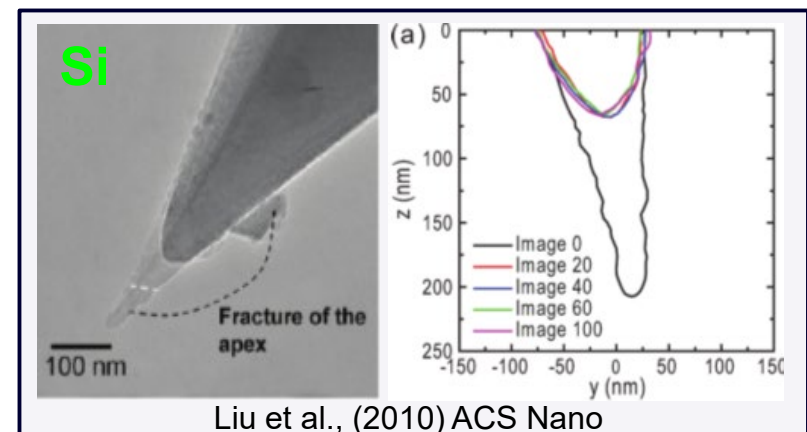
Higher loads:

1) Holm (1946): surface asperities worn away by *plasticity* induced *atoms removal*



**Plastic flow or brittle fracture?  
Holm versus Archard?**

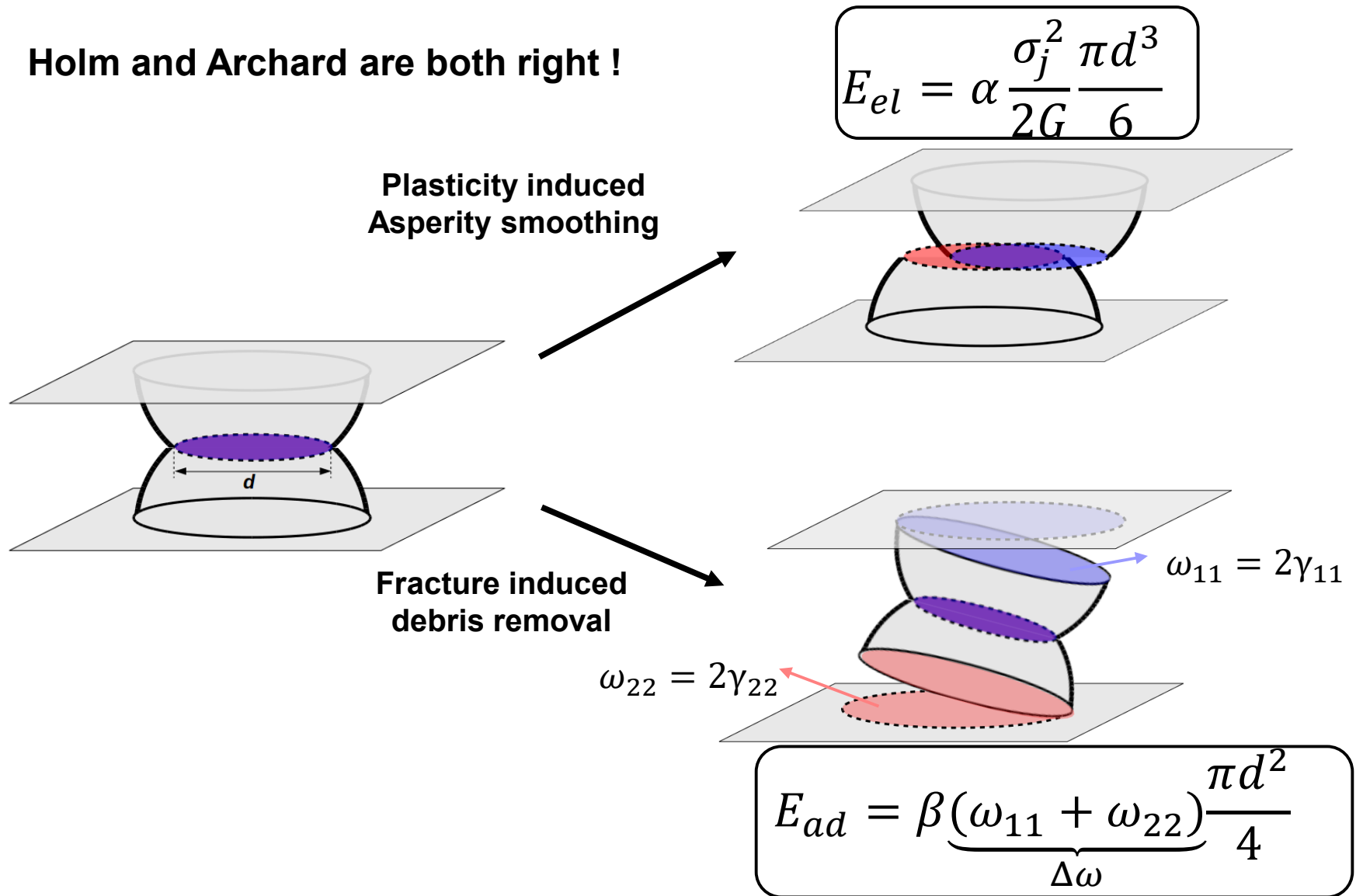
2) Burwell and Strang (1953), Archard (1953): surface asperities are worn away by *fracture* induced *debris removal*



# Brittle to ductile transition

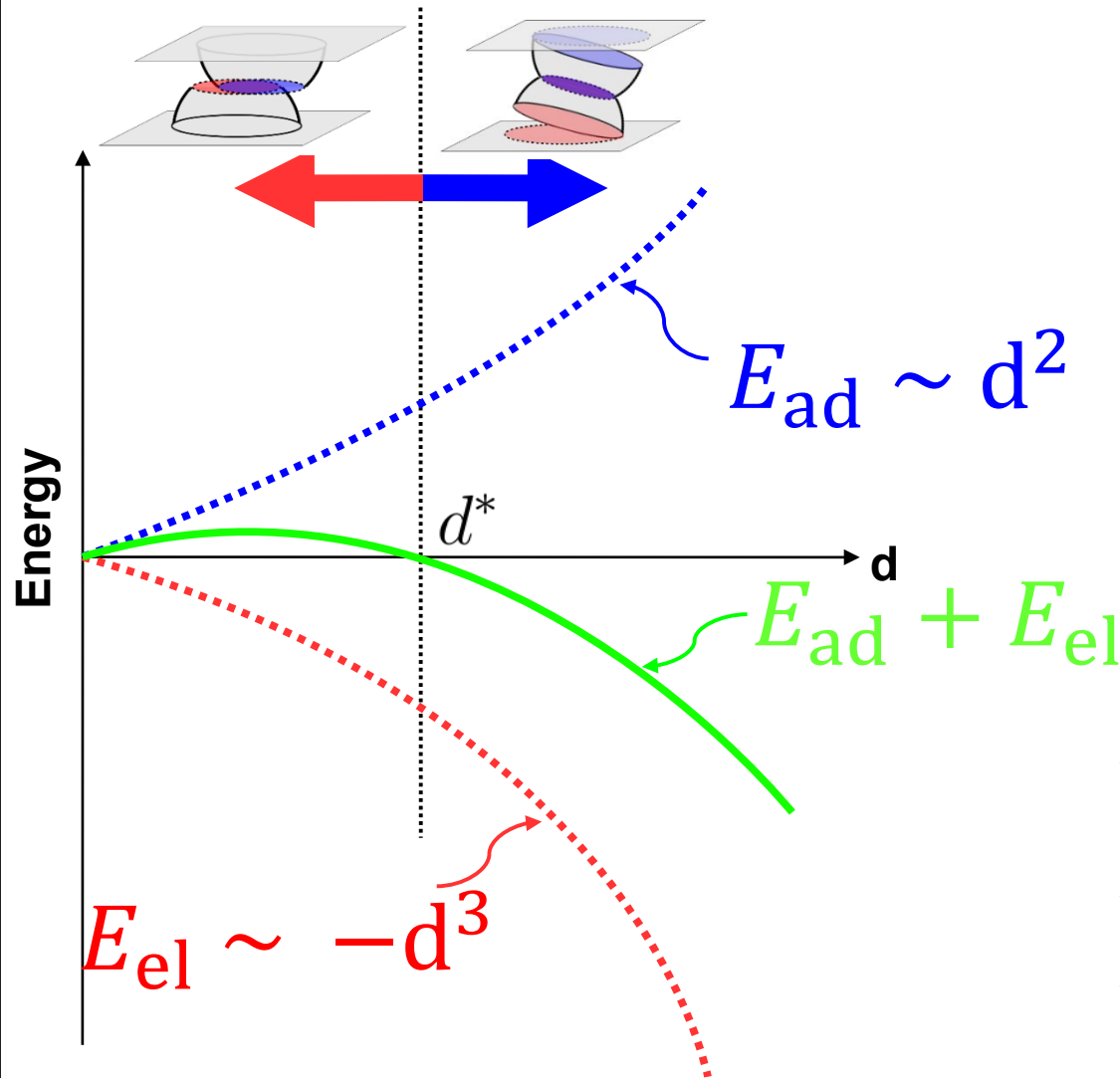
Simply Griffith; Aghababai Warner Molinari, Nat. Comm. 2016

Holm and Archard are both right !



# Energy balance

Ductile to Brittle transition explained by Griffith



Wear Transition occurs when:

$$E_{ad} + E_{el} \leq 0$$

Critical Junction size

$$d^* = \lambda \frac{\Delta\omega}{\sigma_j^2 / G}$$

Explains discrepant AFM data:

Aghababaei, Warner, Molinari, *Nat. Comm.*, 2016

Brink Molinari, *Phys. Rev. Mat*, 2019

Aghababaei, Warner, Molinari, *PNAS*, 2017

Frérot, Aghababaei, Molinari, *JMPS*, 2018

Aghababaei, Brink, Molinari, *PRL*, 2018

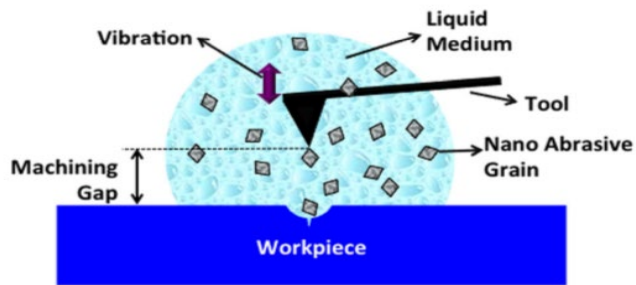
Molinari et al., *Friction*, 2018

Milanese et al., *Nat. Comm*, 2019 ...

# AFM data

Transition to debris formation for increasing AFM tip size

Vibration assisted nano  
impact-machining by  
loose abrasives



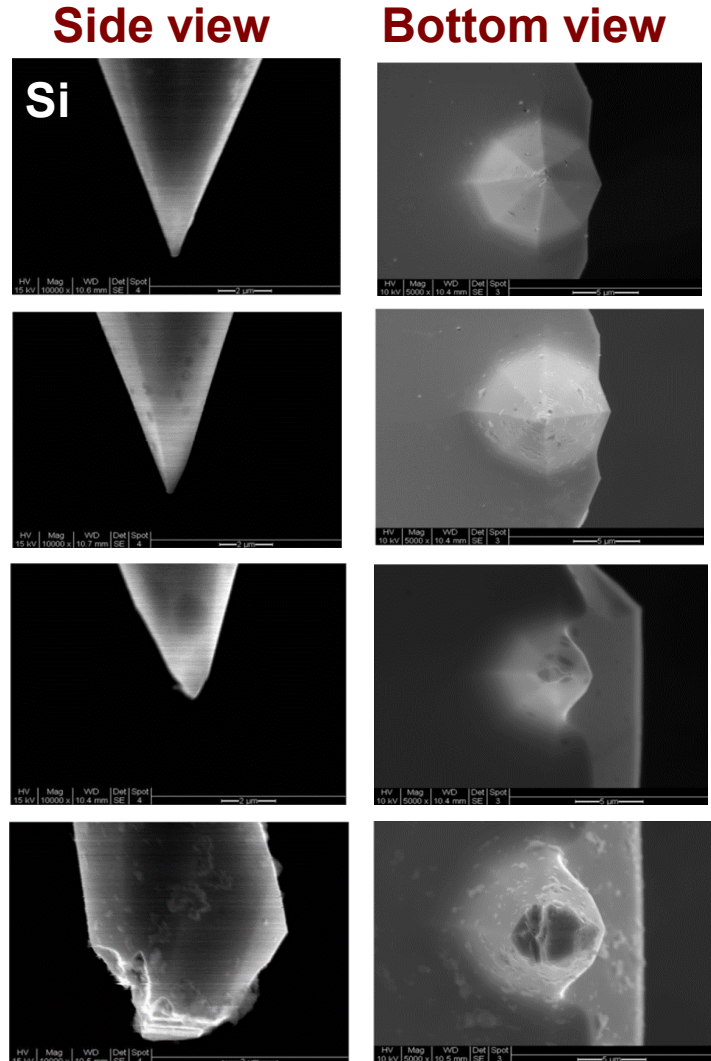
James and Sundaram (2015)  
*J. of Micro-Nano Manuf.*

Before  
machining

Atom-by-  
atom wear

Plastically  
dominated wear

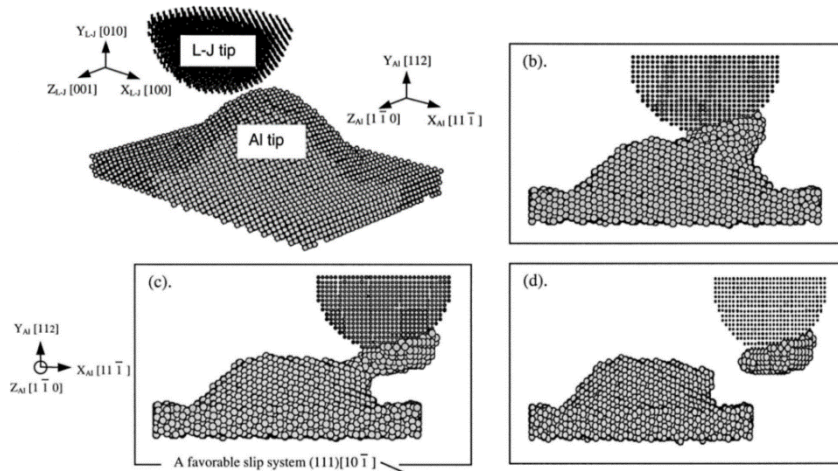
Brittle fracture  
dominated wear



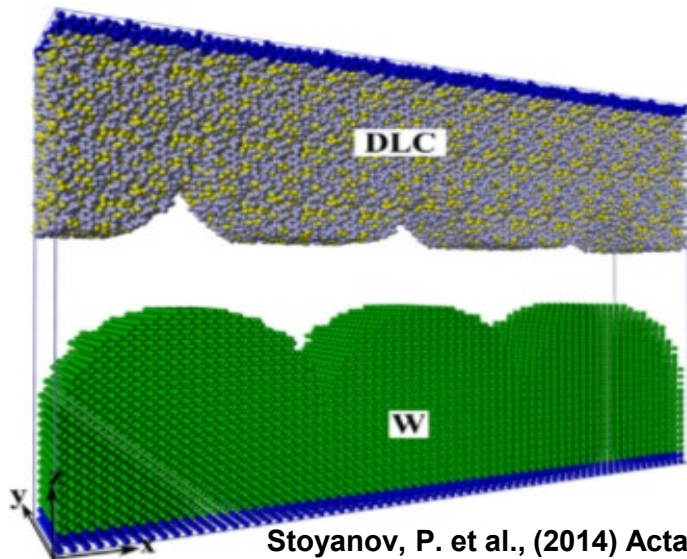
Increasing tip size

# MD simulations

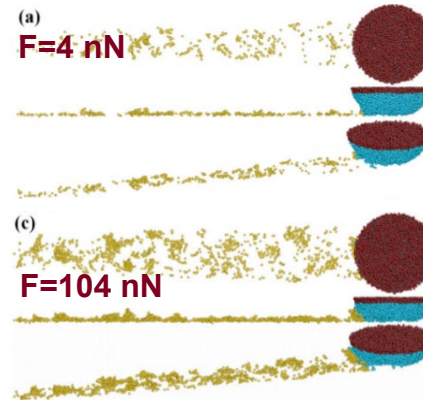
Show asperity smoothing (before 2016)



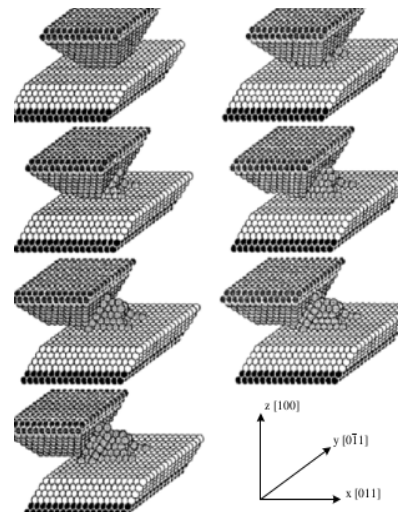
Zhang, J. et al., (2013) J. App. Phys.



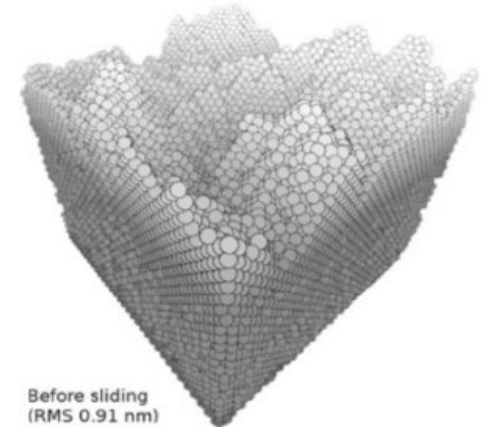
Stoyanov, P. et al., (2014) Acta Mat.



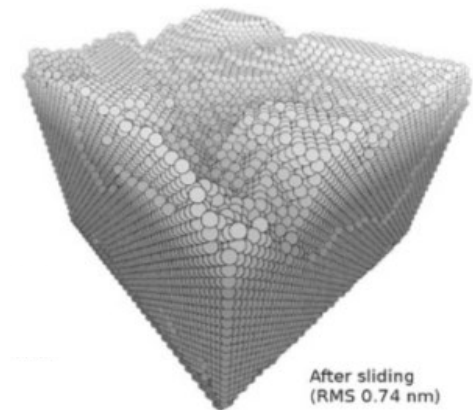
Sha, J. et al., (2013) APL



Sorensen et al., (1996) PRB



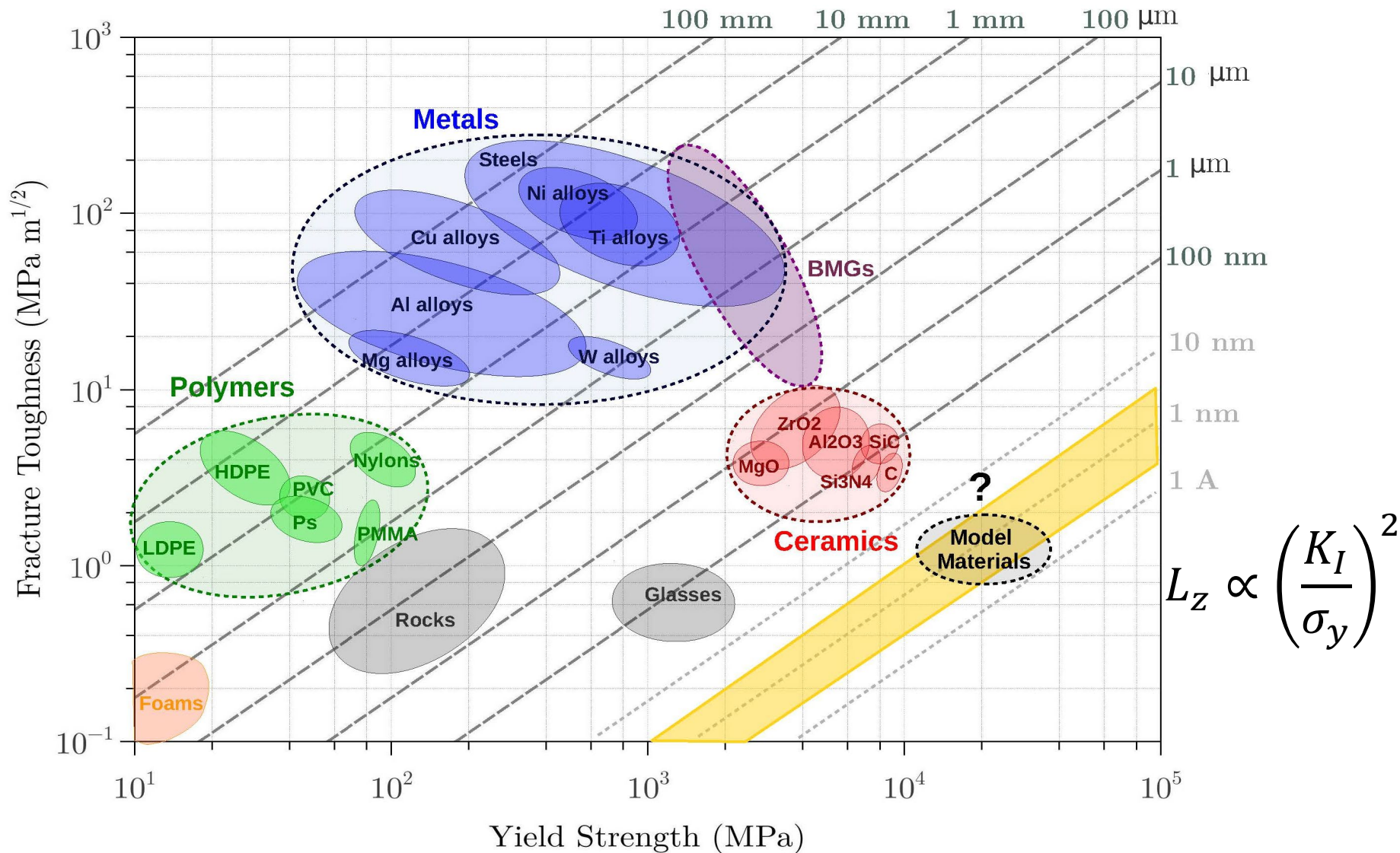
Spijker et al., (2011) Tribology Let.





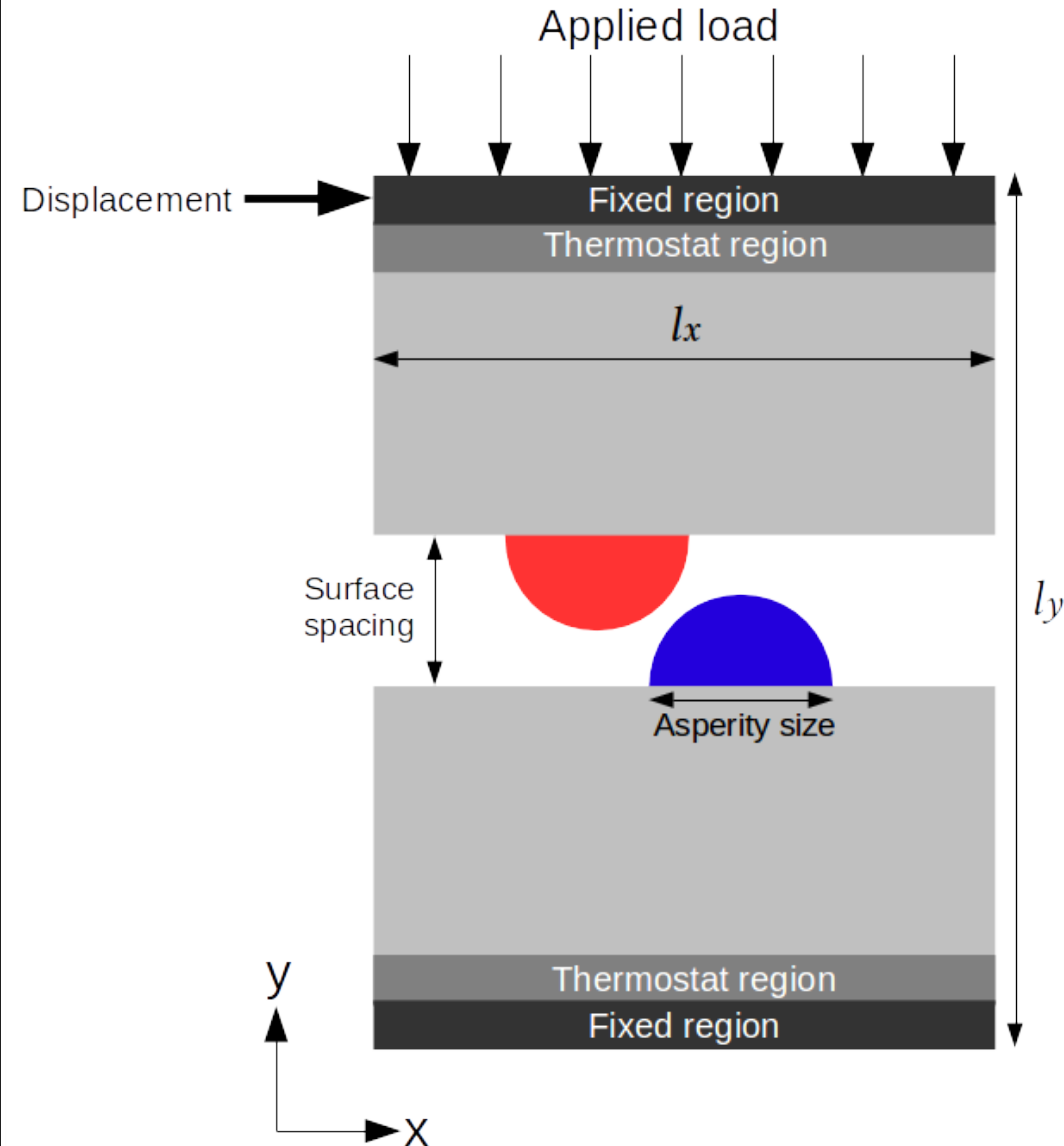
# Ashby map of process zone size

Challenge of scales of MD simulations



# MD toy model

Aghababaei Warner Molinari, Nat. Comm., 2016



## Parameters:

Bulk and interface properties  
(simple pair potential)

Pressure

Velocity

Temperature

Geometry

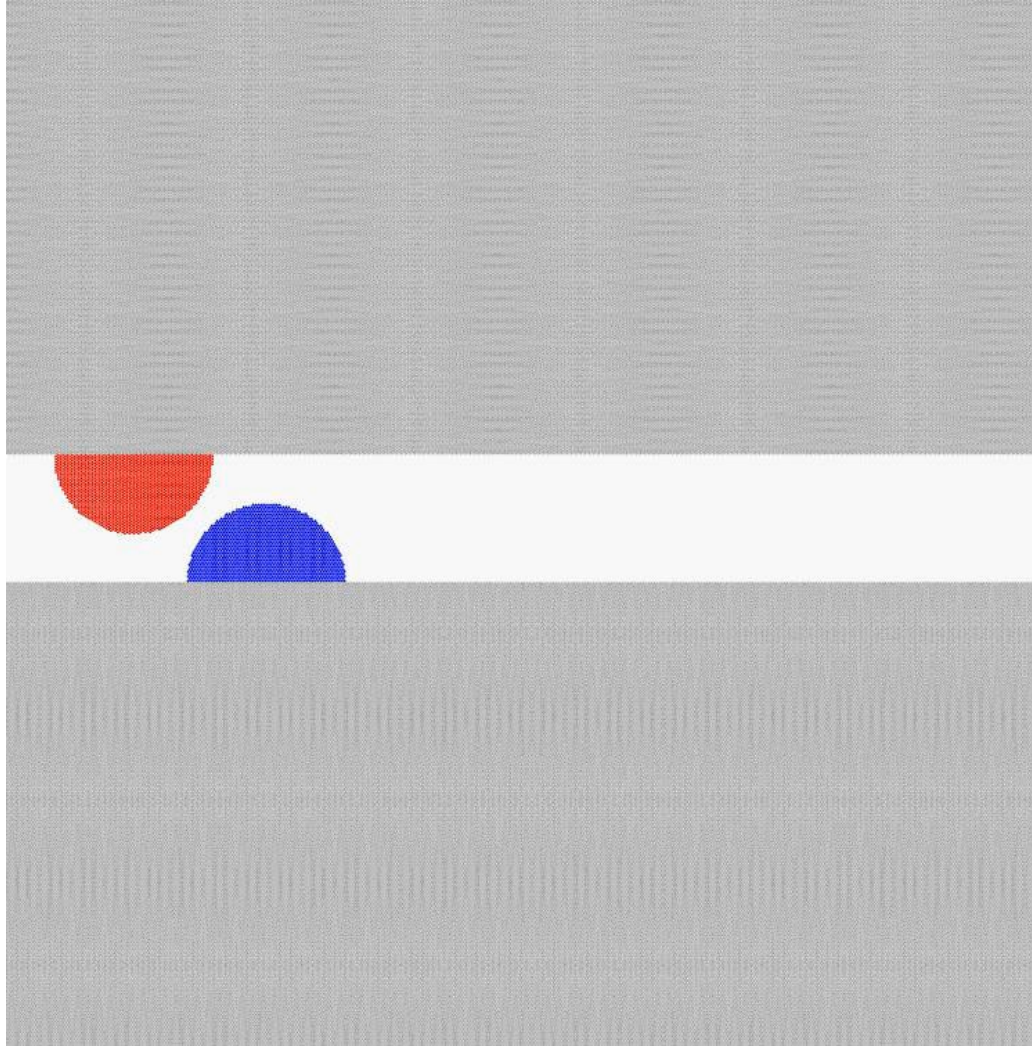
Single, multiple asperities

Asperity size and shape

Interlocking

# Ductile potential with $d < d^*$

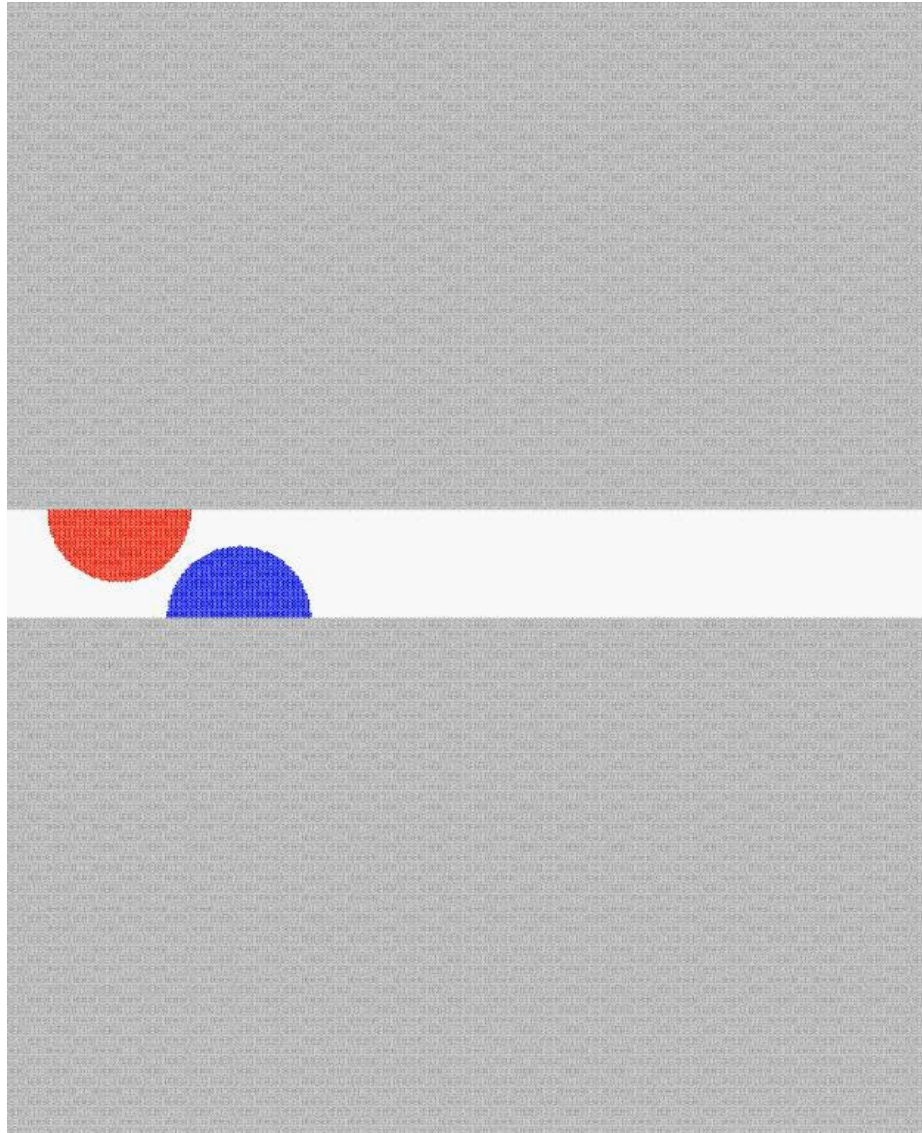
Reveals Holm's mechanism (plastic smoothing)





# Brittle potential with $d > d^*$

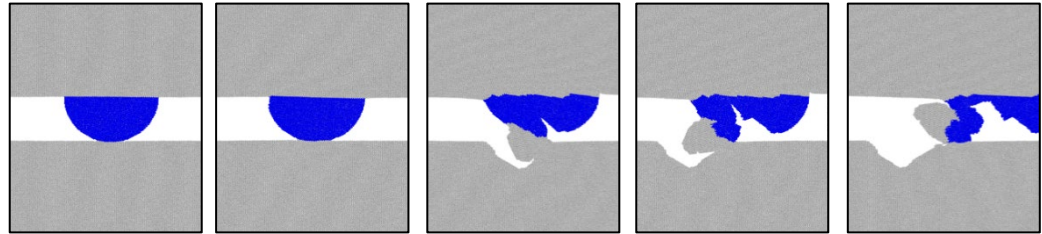
Reveals Archard's mechanism (debris formation)



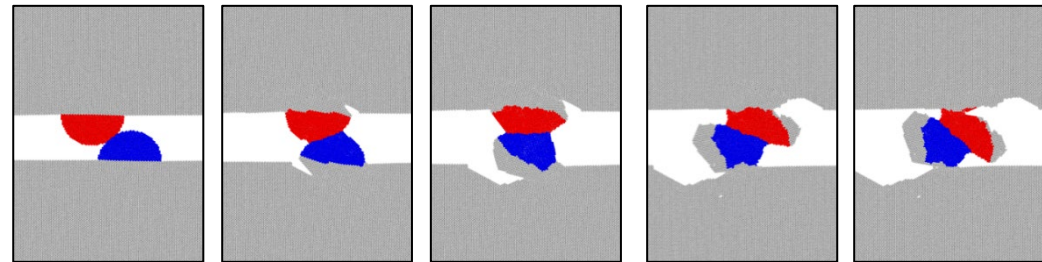
# Debris formation

For  $d > d^*$  for different configurations;

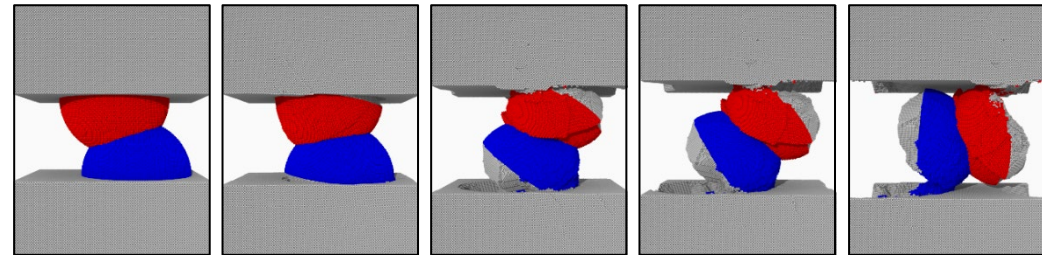
2D single asperity  
Model potential



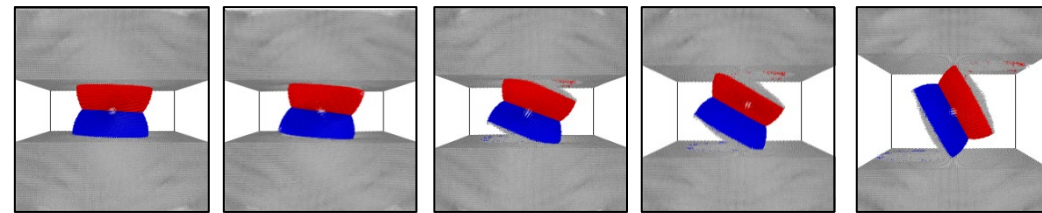
2D asperity/asperity  
Model potential



3D asperity/asperity  
Model potential



3D asperity/asperity  
With diamond potential  
(of Pastewka et al., 2013)



# Back to Archard's wear law

## What is K? At the asperity level

1) At the macroscopic/engineering scale, Archard's model is essentially probabilistic

K interpreted as probability of asperity/asperity encounter yielding a debris

2) But at the scale of an asperity/asperity junction, our model is fully deterministic

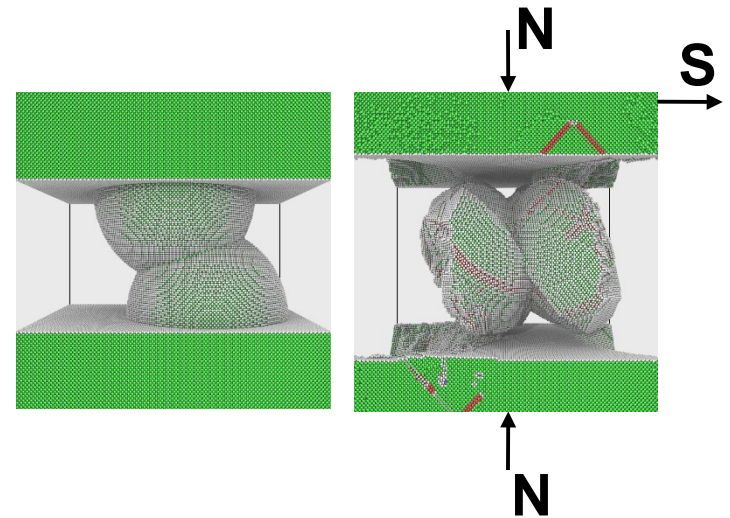
If  $d > d^*$ , a debris is formed,  $K=1$   
Otherwise  $K=0$

How big is this debris?

**Question: do we recover Archard's law at the asperity level?**

$$V = K \frac{N S}{H_v}$$

$K=10^{-8}$  to  $10^{-4}$



$$V \stackrel{?}{=} 1 \frac{N S}{H_v}$$

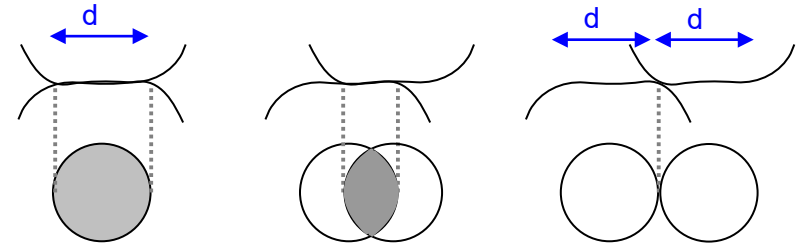
# Rationale for Archard's model

## At the asperity level

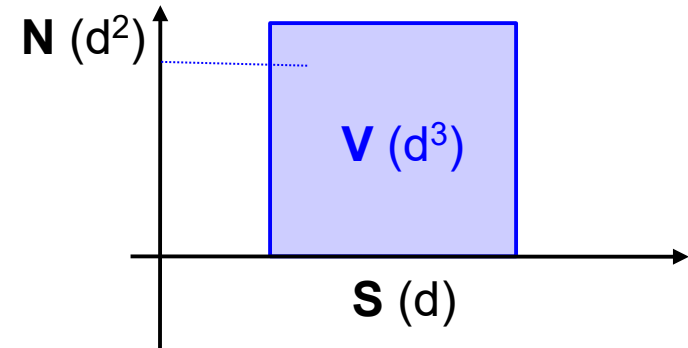
Archard (1953) J. App. Phys.

### I. Plastic deformation of asperities

$$(N \sim d^2)$$



### II. Contact duration



### III. Shape/Volume of wear debris

$$(V \sim d^3)$$

The depth, to which the material is worn, is proportional to the junction size.

$$W \sim \frac{V(d^3)}{S(d)} \sim A(d^2) \sim \frac{N}{H}$$

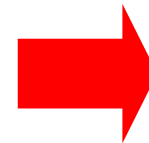


$$V \sim \frac{N \times S}{H}$$

# Recovering Archard ?

Aghababaei Warner Molinari, PNAS, 2017

—|1



$$V = \frac{N S}{H_v}$$

Debris volume,  $V$  ( $r_0^3$ )



# But should it be a surprise?

Adhesion:  $A$  is not proportional to  $N$

—|1

Adhesion?

Plastic shearing?

Asperities collision?

Junction area,  $A$

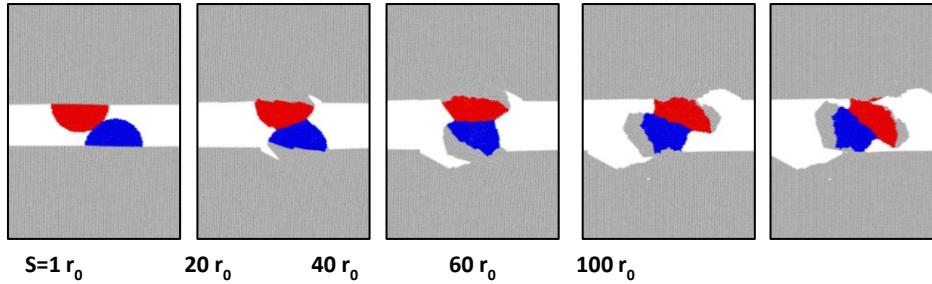
$(N \sim A)$  is influenced by the roughness parameters and adhesion!

Mo and Szlufarska, (2010) *PRB*, Enachescu, et al., (1998) *PRL*.

Gao, et al., (2004). *J. Phys. Chem. B*, Pastewka, and Robbins, (2014) *PNAS*.

# Accumulated frictional work

Predicts debris size



$$\frac{\int F ds}{\sigma_j}$$

1

$$\longrightarrow V = \frac{\int F ds}{\sigma_j}$$

Rediscovering T. Reye:  
(1860) *Zur theorie der zapfenreibung*.  
*J. Der Civilingenieur* 4:235–255

Debris volume,  $V$

# Minimum particle size?

Set by critical length scale  $d^*$

Growing societal concern with regard to air pollution due to ultra fine particles

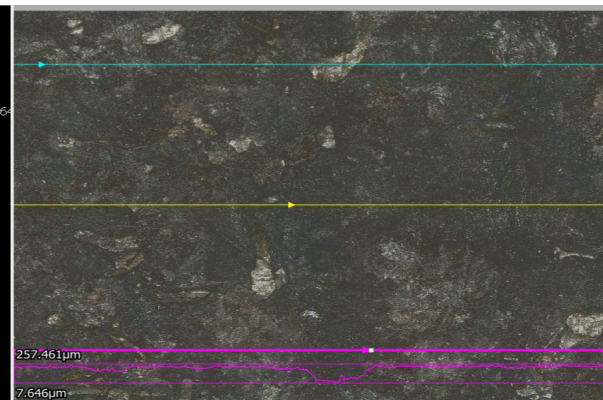
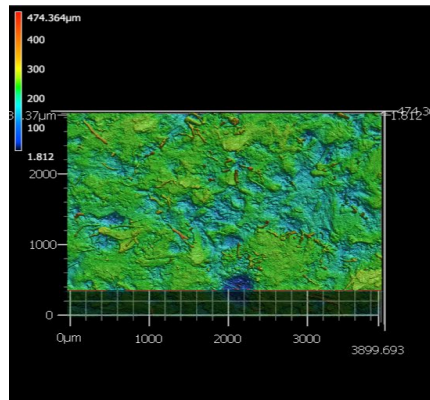
BBC news, July 2019: «Pollution warning over car tyre and brake dust»

In a world of electric cars, these will dominate air pollution, and there are concerns that they present more health hazards and exhaust particles pollution.

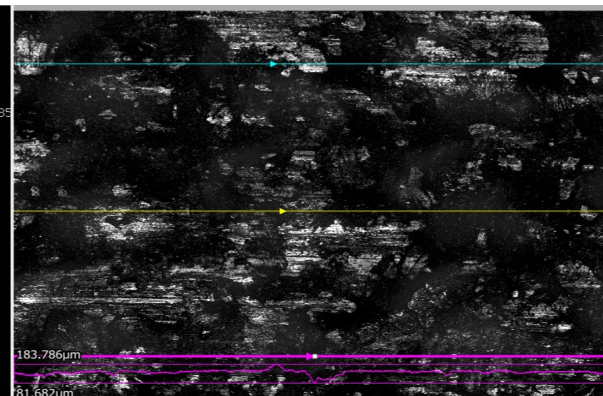
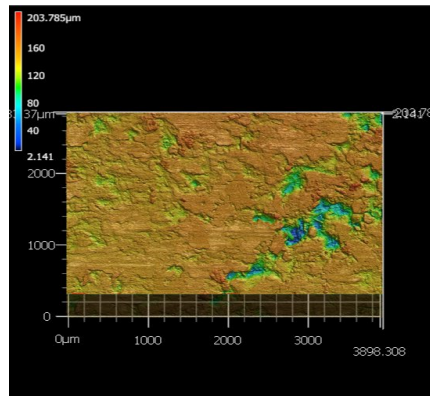
Junction size,  $d$ , sets  
debris size (if  $d > d^*$ )

$$d^* = \lambda \frac{2Gw}{\tau_j^2}$$

Junction strength  
(decreases with  
reduced adhesion)



**New brake pad**



**Worn brake pad**

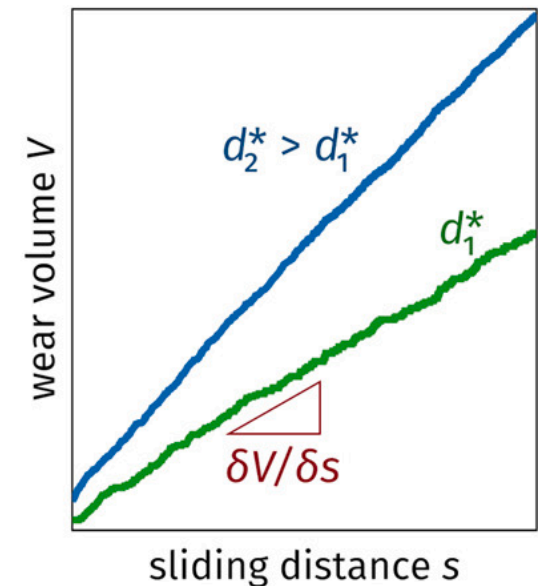
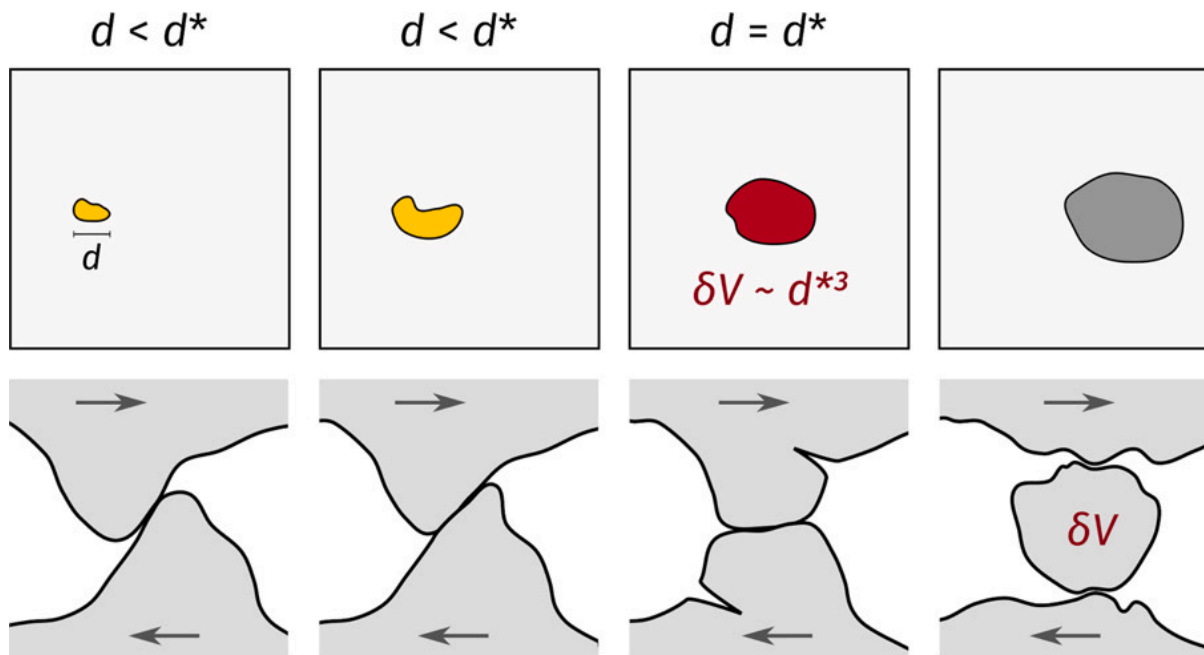
# Mesoscale model

Brink Frérot Molinari, JMPS 2021, A parameter-free mechanistic model

Brittle materials (high hardness) wear less, Archard:  $V = K \frac{N S}{H_v}$

But  $d^*$  is smaller when hardness increases:  $d^* = \lambda \frac{\Delta\omega}{\sigma_j^2/G}$

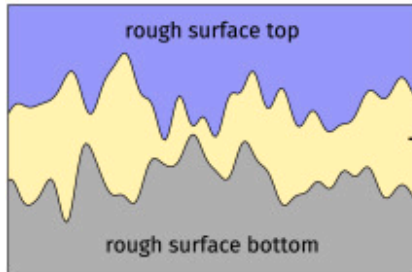
Which results in more debris production. **Contradiction...** solved by sliding history



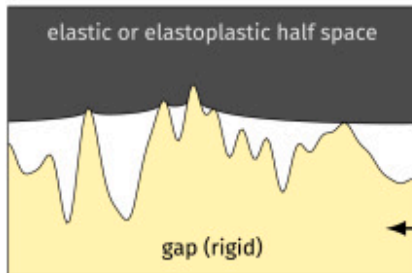
# Rough on rough sliding

Solved with BEM, at each sliding step, TAMAAS software (BEM, FFT), JOSS 2020

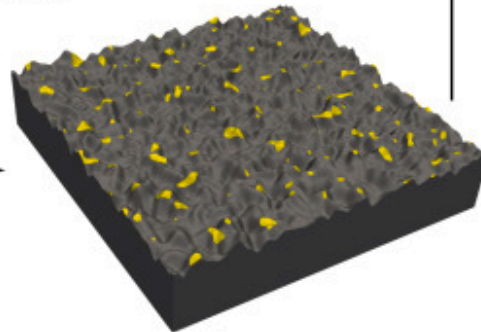
(a) Contact solution



convert to rough-on-flat geometry using Johnson's assumption

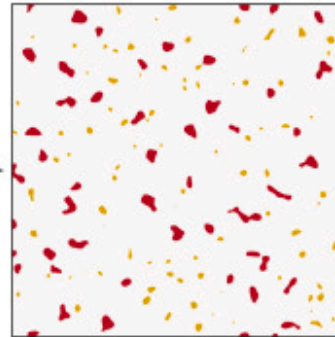


solve contact



bottom surface, yellow areas: in contact

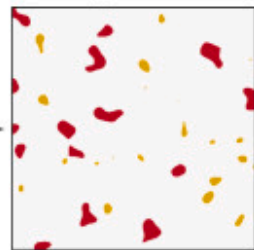
(b) Frérot et al. 2018



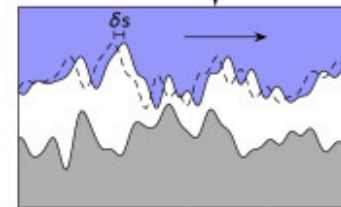
- no particle detachment at junction ( $A < A^*$ )
- junction emits a wear particle ( $A \geq A^*$ )

$$k = \frac{\sum_{i: A_i \geq A^*} A_i}{\sum_i A_i} = \frac{\text{red}}{\text{red} + \text{yellow}}$$

(c) Sliding wear model

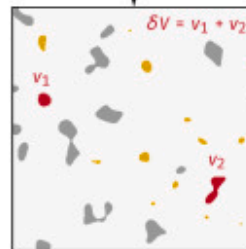


shift top surface by  $\delta s$

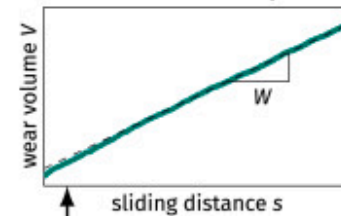


solve contact as in (a)

repeat



- junction has already produced a particle: not counted

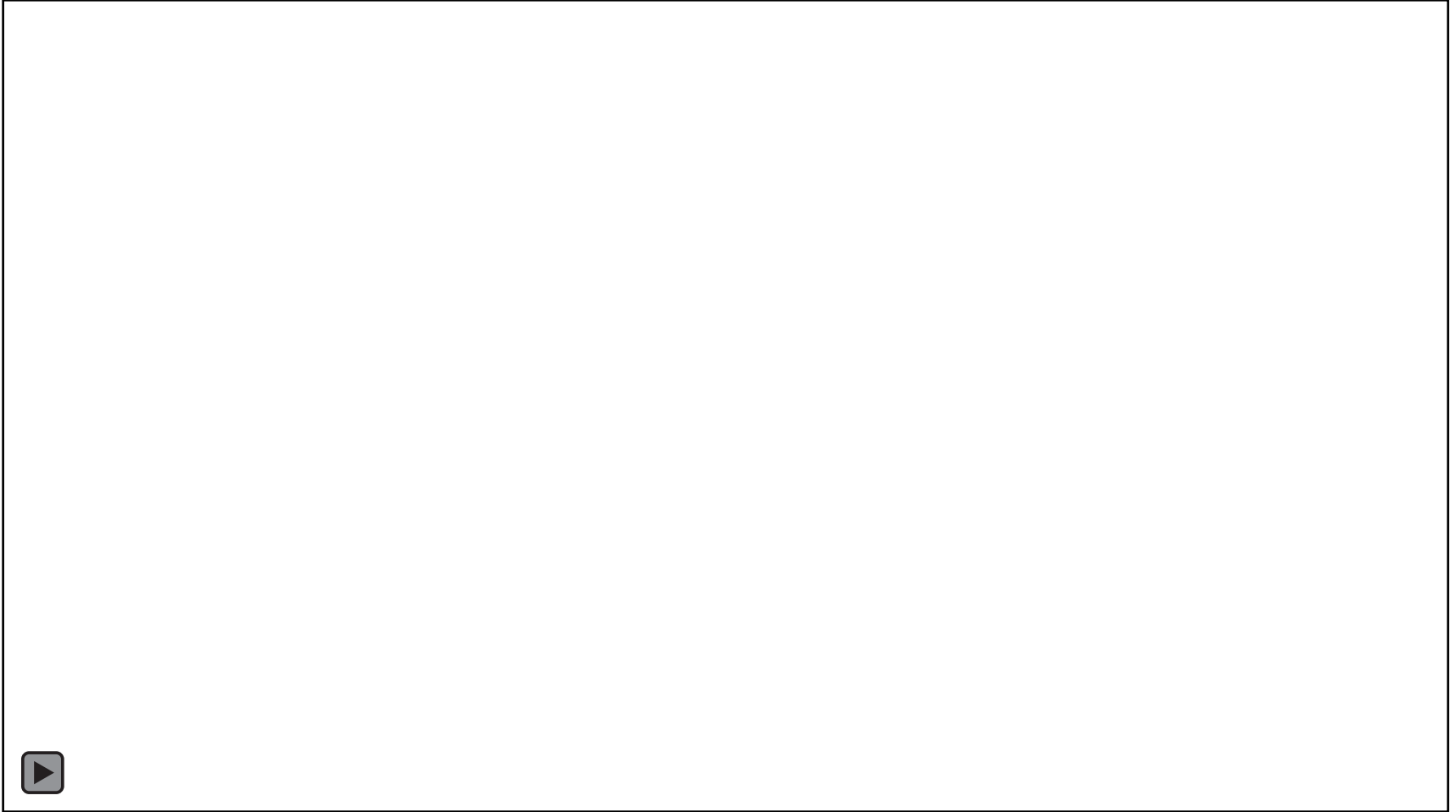


add wear volume  $\delta V$  each step



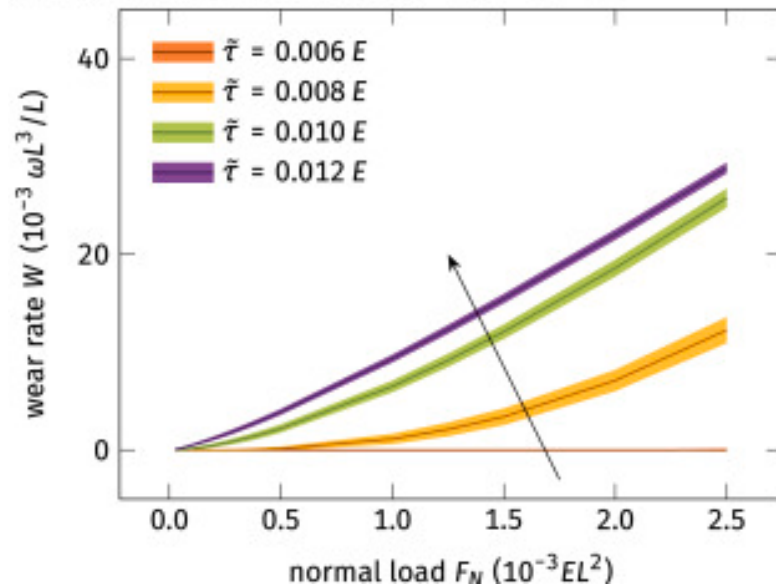
# Rough on rough sliding

Solved with BEM, at each sliding step

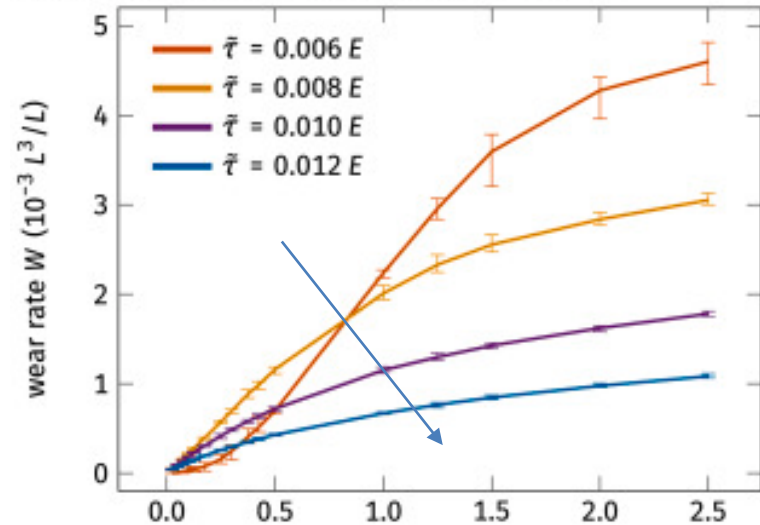


# Importance of sliding history

## And disabling debris formation



No silding history; wrong qualitative trend  
Frérot, Aghababaei, Molinari, JMPS, 2018

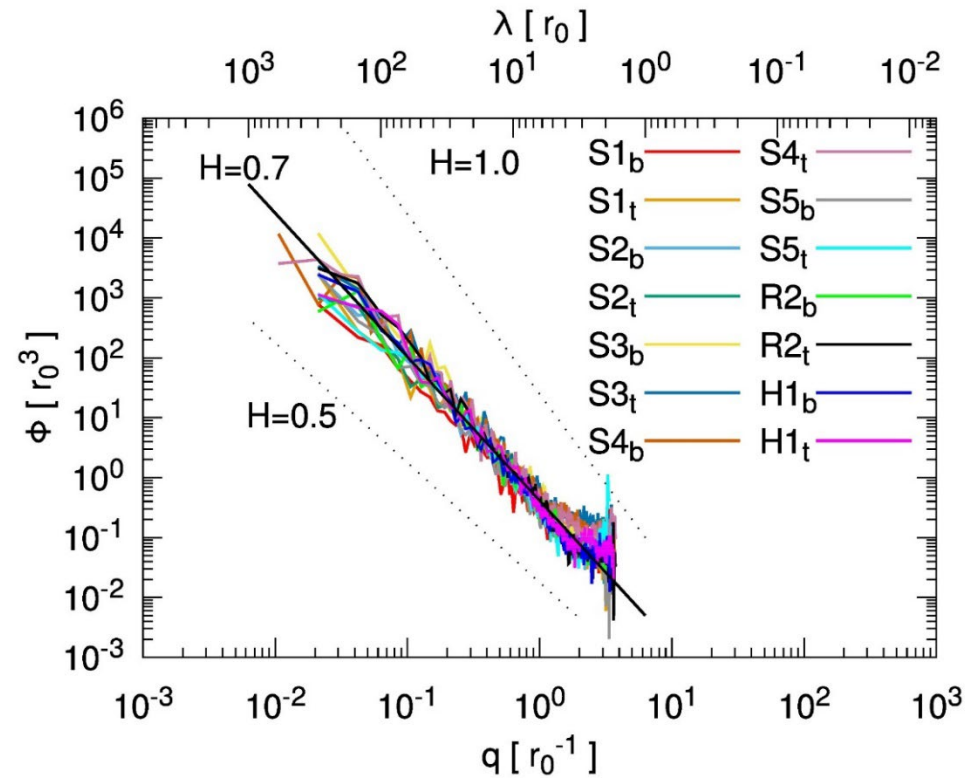
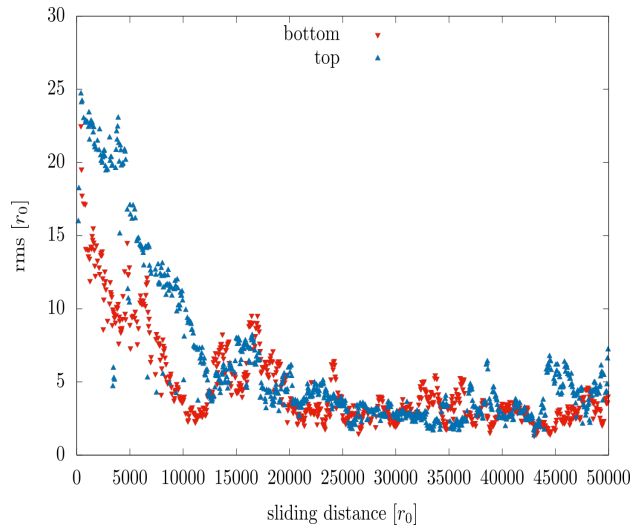
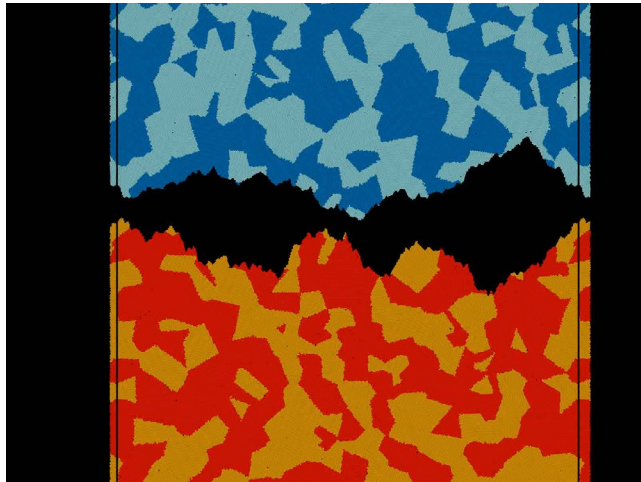


With silding history; correct qualitative trend  
Brink, Frérot, Molinari, JMPS, 2021

- + Mechanistic model that reproduces qualitative trends
- Quantitatively not predictive (need controlled experiments)
- Missing: roughness evolution, tracking of debris, accumulation of third body

# Roughness evolution (2D)

Evolves to a steady state; Enrico Milanese et al., Nat. Comm, 2019



Evolves to Self-affine fractal surface  $H \in [0.64, 0.81]$

Requires third bodies (here debris particles)

Two competing mechanisms:

- 1) Ductile deformation (smoothing, diffusion)
- 2) Brittle fracture: cracks, roughening

# Roughness evolution (3D)

Brink et al., in progress



[Piz Daint - Cray XC50, Xeon E5-2690v3 12C 2.6GHz, Aries interconnect, NVIDIA Tesla P100](#), Cray Inc., [Swiss National Supercomputing Centre \(CSCS\)](#), Switzerland (Ticino)

Rmax, 21,230 Tflop/s, 387,872 cores, #6 world, #1 Europe (in 2019, not anymore)

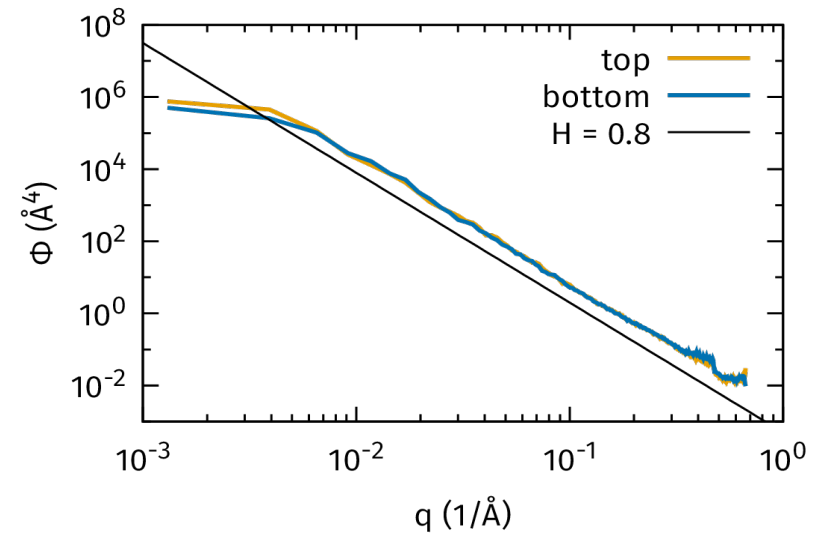


# Roughness evolution (3D)

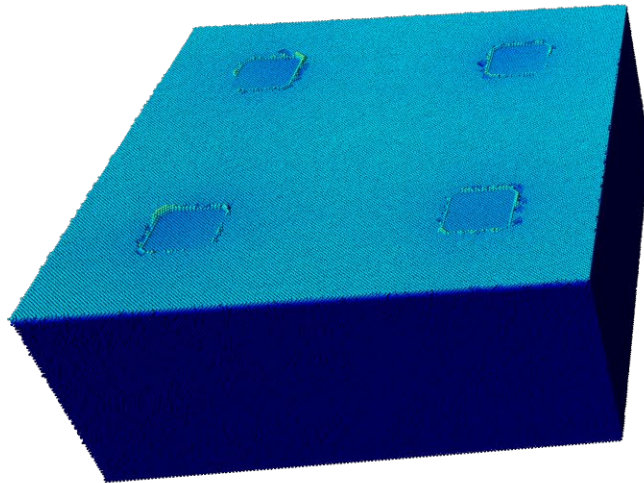
Brink et al., in progress

Abrasive particles on copper

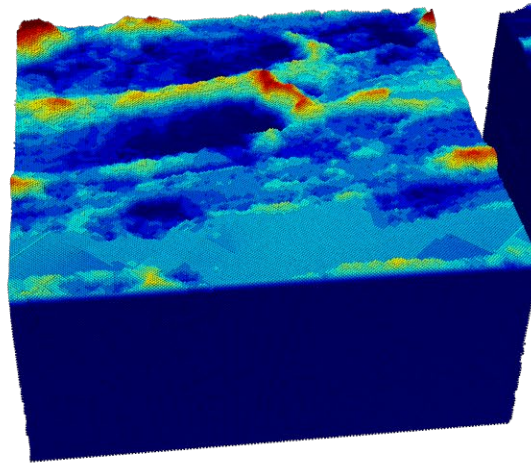
Initially flat surface evolves to around  $H = 0.7$



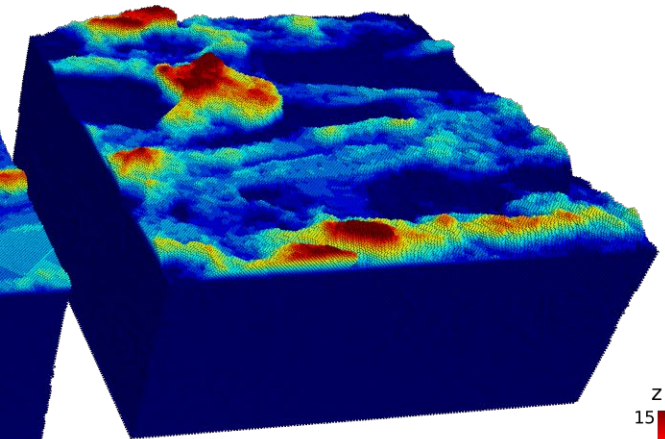
Initially flat



$s = 0 \text{ nm}$



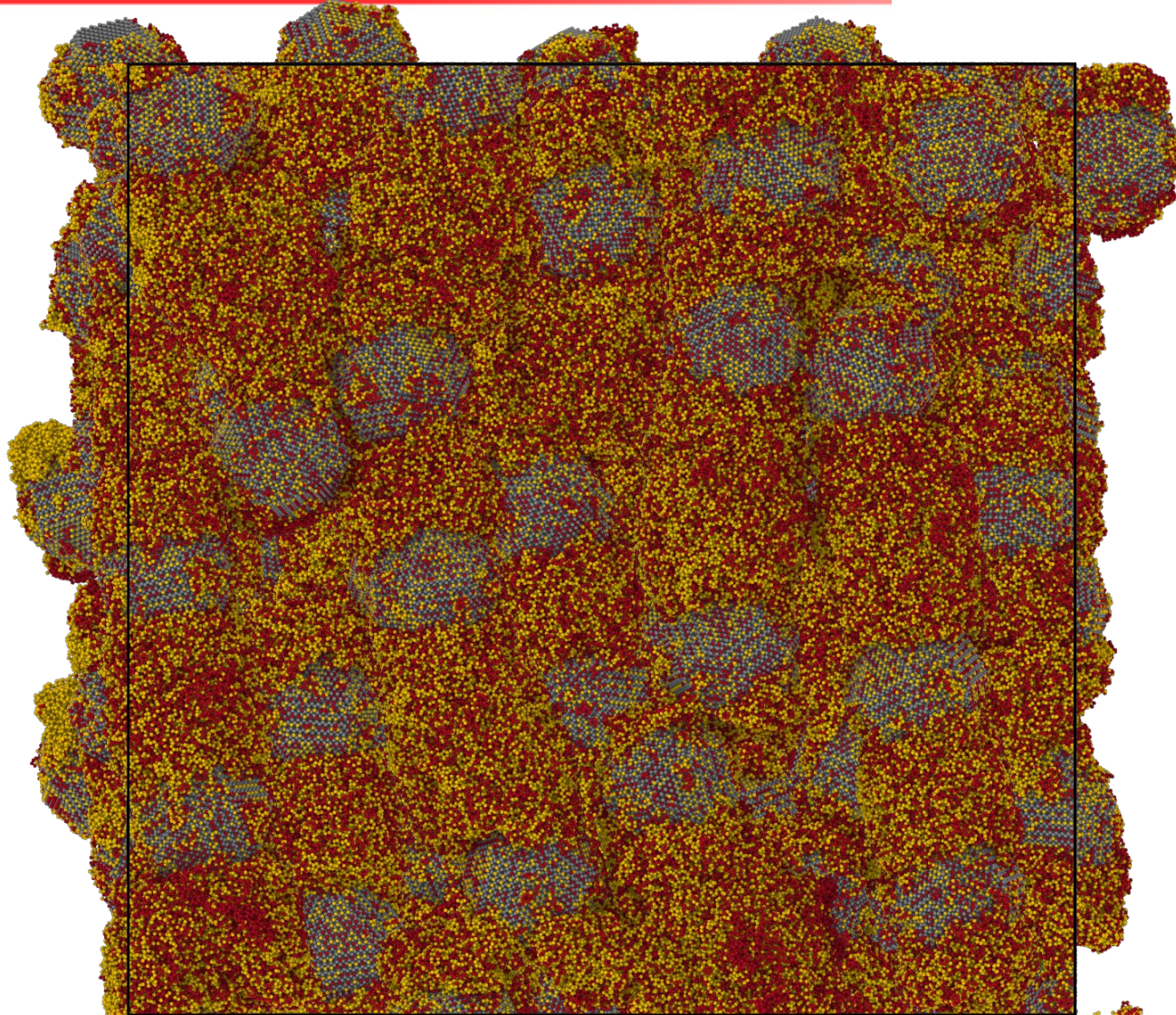
$s = 400 \text{ nm}$



$s = 700 \text{ nm}$





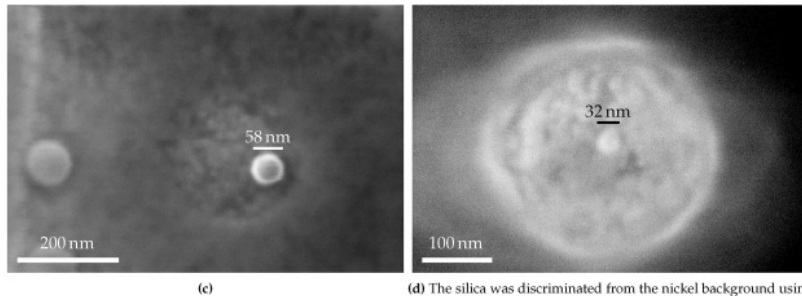
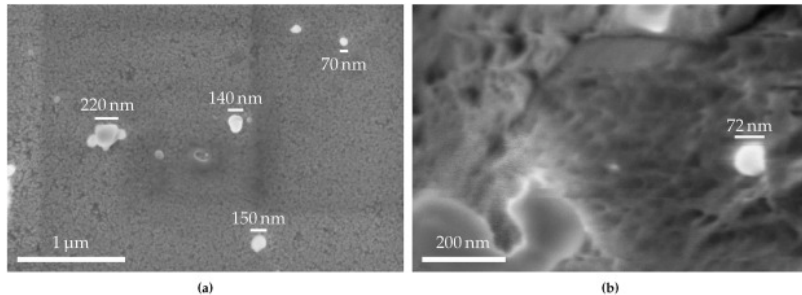
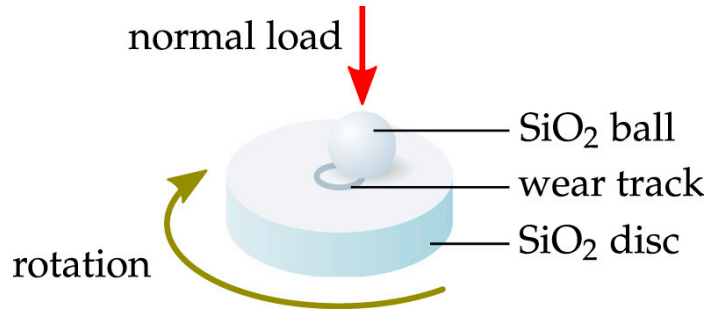


Emergence of wear cylinders in model brittle material, Brink et al., in progress



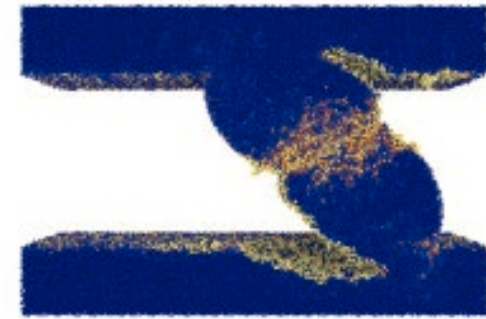
# Pin on disc experiments, silica

Pham-Ba Molinari, Wear, 2021; Emergence of cylindrical rollers

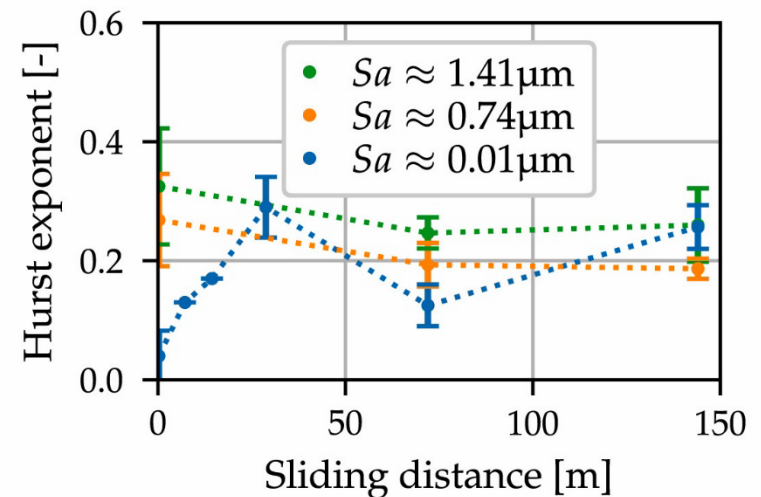


(d) The silica was discriminated from the nickel background using energy-dispersive X-ray (EDX) spectroscopy

Early stages; few wear particles on track, no sign of particles smaller than  $d^*$

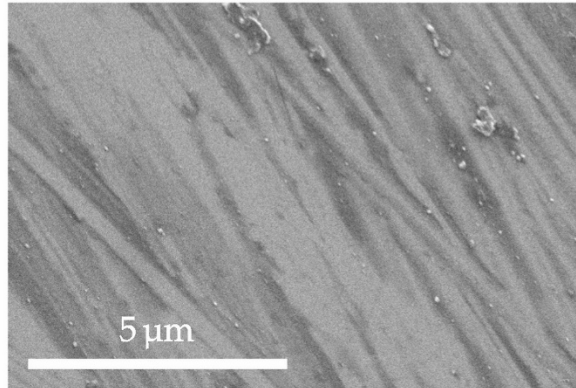


MD simulations with Vashishta potential,  $d^*$  around 15 nm

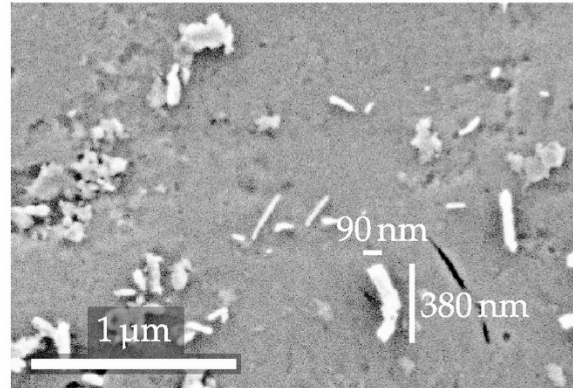


# Different stages of 3rd body formation

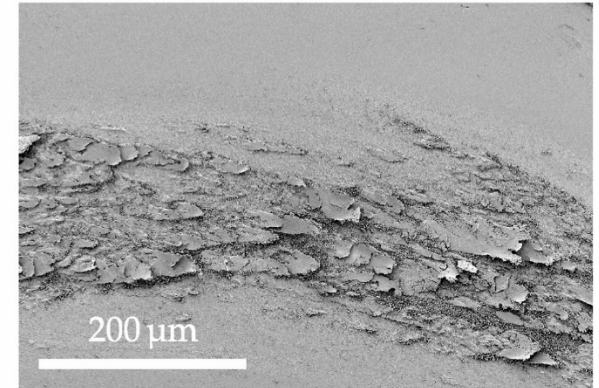
Emergence of cylindindrical rollers, and then assembly in complex structures



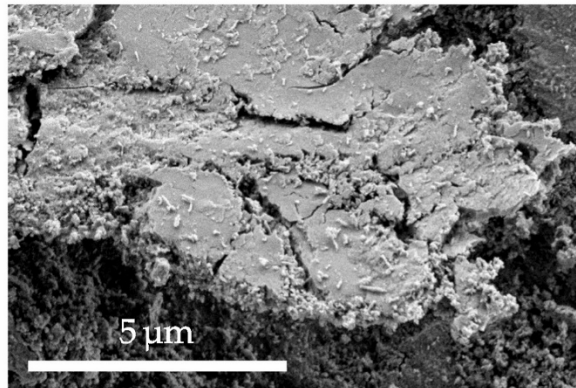
(a) 1 s: formation of first wear particles



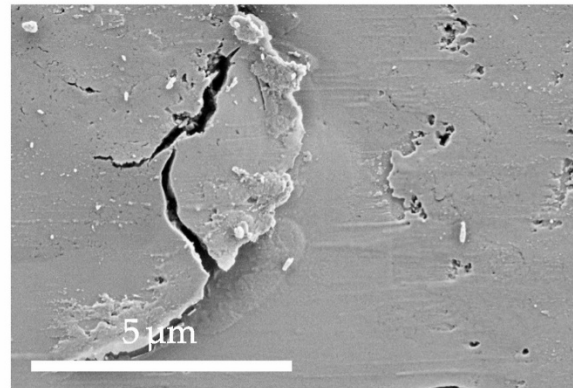
(b) 30 s: cylinders and aggregates



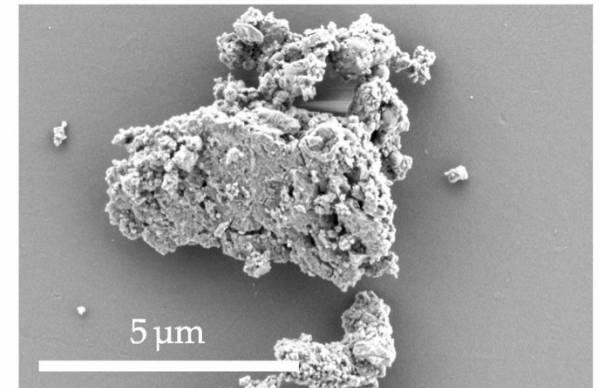
(c) 1 h: large flakes on the disc forming the wear track



(d) 1 h: detail: aggregates forming a large flake



(e) 1 h: detail: cylinders and aggregates on top of a flake



(f) 1 h: detail: aggregated wear particle fallen outside the wear track

# Conclusions

1) Critical junction size explains transition in adhesive wear mechanisms (above small load limit):

$$d^* = \lambda \frac{\Delta\omega}{\sigma_j^2 / G}$$

2) Tangential (frictional) work predicts initial debris size at the asperity level

3) Opens a path to deterministic wear coefficient K

4) Third bodies and competition between ductile/brittle mechanisms yield self-affine surface roughness

5) Ongoing: experiments on roughness evolution, friction and wear for various materials

6) Interactions between asperities can lead to innovative designs (not discussed today)