Polymer nanocomposites – Christopher Plummer (LMOM), December 2024

Introduction

- Clay-based polymer nanocomposites (in situ, melt-compounded)
- Some Basic Properties (stiffness, HDT, ultimate properties, fire resistance)
- Applications
- Examples of nanocomposite research at IMX

Perspectives



Why nanomaterials?

"There's plenty of room at the bottom!" Some examples ...

- Better insulation (nanofoams, aerogels)
- Display technology (cheap "nanophosphors", better electrochromic displays)
- Tougher, harder, smaller cutting tools (nanocrystalline carbides)
- High energy density batteries (aerogels, nanocrystalline nickel, metal hydrides)
- *High-power magnets* (nanocrystalline yttrium-samarium-cobalt)
- High-sensitivity sensors, filters (nanocrystalline zirconia)
- Automobile fuel efficiency (light-weight structures, engine liners, spark plugs)
- Aerospace components (temperature, fatigue resistant materials, weight saving)
- Satellites (nanocrsytalline tungsten-titanium diboride-copper ignitors)
- Medical implants (wear resistant nanocrystalline carbides, zirconia)
- *Ductile, machinable ceramics* (nanocrystalline carbides, nitrides)



Why polymer nanocomposites?

Increased strength and stiffness: while maintaining the high elongation of the matrix.

Permeation Resistance: (plate-like fillers e.g. exfoliated clays) interest in nanocomposites barriers from packaging companies.

Transparency: low loadings and filler dispersion maintain inherent polymer transparency in thin sections (again interest for packaging)

Recyclability: nanofillers are not affected or degraded during processing → physical properties not seriously affected by recycling

Flame resistance: rapid char layer formation, excellent flame resistance

Transport properties: percolation at very low loadings in high aspect ratio systems,

important for thermal, electrical conductivity (e.g. carbon nanotubes)

Functionality: bioactivity, hydrophilicity, magnetic and electrical properties etc. etc.

And all at loadings of a few wt% weight saving!!

Are nanofillers worth it? Examples (2019)

- Natural clays (mined, refined, and treated)—\$3–\$15/lb.
- Synthetic clays—\$10-\$20/lb.
- Nanostructured silicas—\$5–\$200/lb.
- Nanoceramics—\$100-\$280/lb.
- Nanotubes (carbon based, MWNT)—\$100-\$200/lb.

Applications now include packaging, automotive, and wire and cable industries, and huge increase in demand for these fillers is projected

> Lower prices in the future





Some important dates in the history of polymer nanocomposites

US 2,531,396 *1950 National Lead* Onium ion treated clay to reinforce elastomers
US 3,084,117 *1963 Union Oil Company* Organoclay-polyolefin composition masterbatch, melt blend, solvent,

protonated amine

JP 10,998 **1976 Unitika** <u>In situ process</u> for layered silicate

clay polyamide

US 4,739,007 1988 Toyota Layered silicate clay polyamide composition

US 5,747,560 1998 Allied Signal Melt compounding for nanocomposites;

clay treated with protonated primary

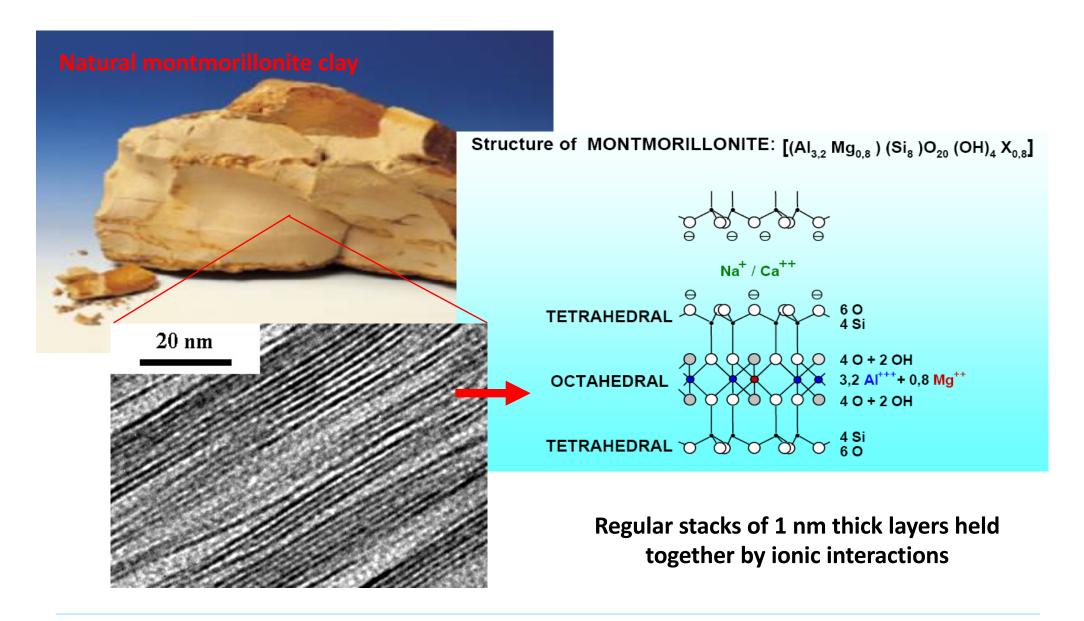
and secondary amines

Toyota, GM/Montel, GE, Dow/Magna, etc. currently active in nanocomposites

- Currently preferred nanoclay is **montmorillonite (MMT)**, whose **individual platelets are 1 nm thick** and of the order of one micron in diameter, giving them an aspect ratio of about 1000:1.
- Main (US) suppliers of MMT and modified MMT: Nanocore Inc. and Southern Clay Products.



Montmorillonite clay: the most important current nanofiller

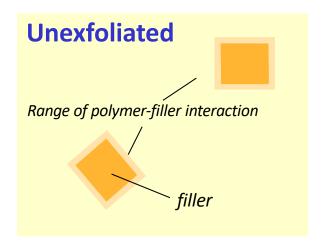


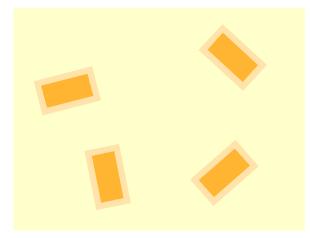


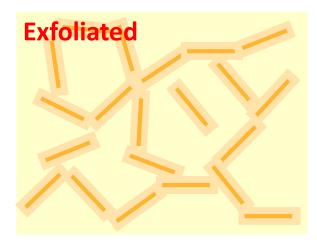
Clay-based thermoplastic nanocomposites

Exfoliation of layered silicates in a polymer matrix . . .

. . . high surface to volume ratios, large aspect ratios, percolation at low loadings





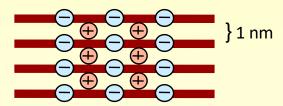


Goal: significantly modified physical properties

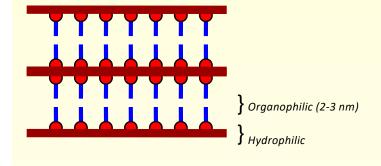


Manufacturing clay-based nanocomposites

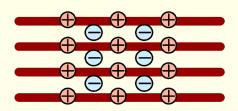
Natural clays (e.g. montmorillonite)



Ion exchange with organic modifiers



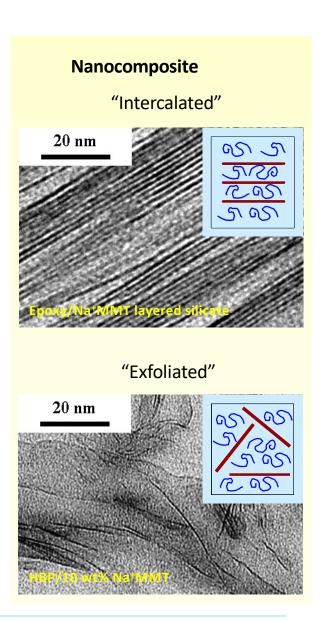
Synthetic silicates (e.g. hydrotalcite)



Clay/organo-clay + Polymer

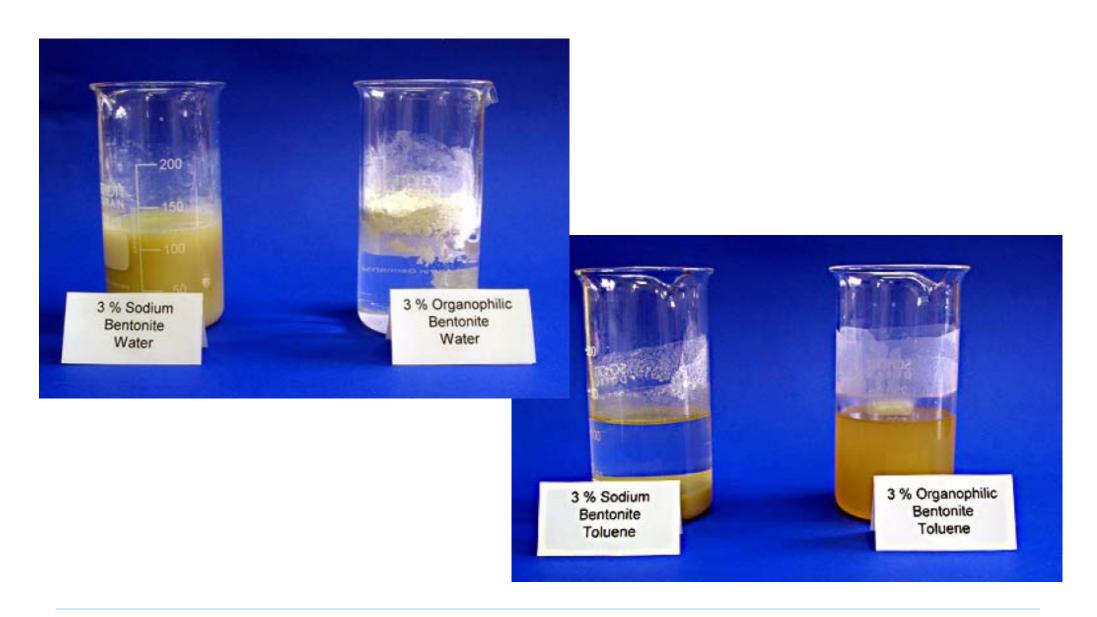
- Solution processing*
- Melt mixing
- *In situ* polymerisation

*Not used commercially for thermoplastics



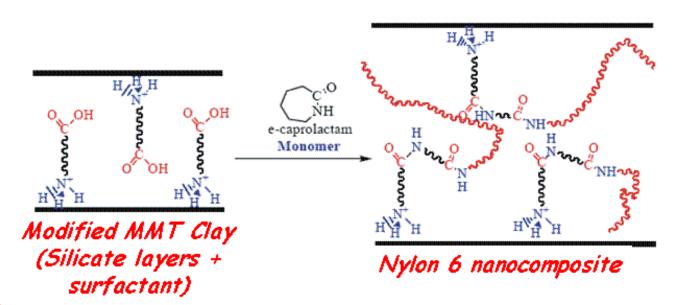


Practical demonstration of effect of organic modifiers





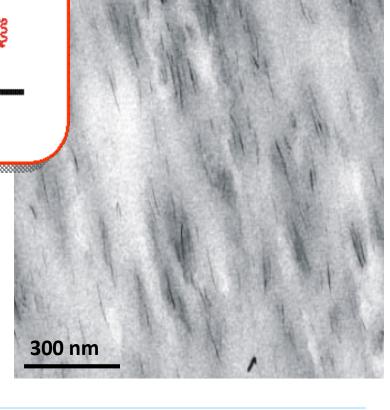
In situ Nanocomposites – Synthesis from monomer + clay



Toyota technology licensed to Nanocor, Ube, sublicensed to other producers:

Ube ("NCH"), Unitika (Nylon M2350), Bayer (Durethan), Mitsubishi, Allied Signal etc.

Barrier films (packaging), structural mouldings (e.g. car parts, knife handles, light covers),

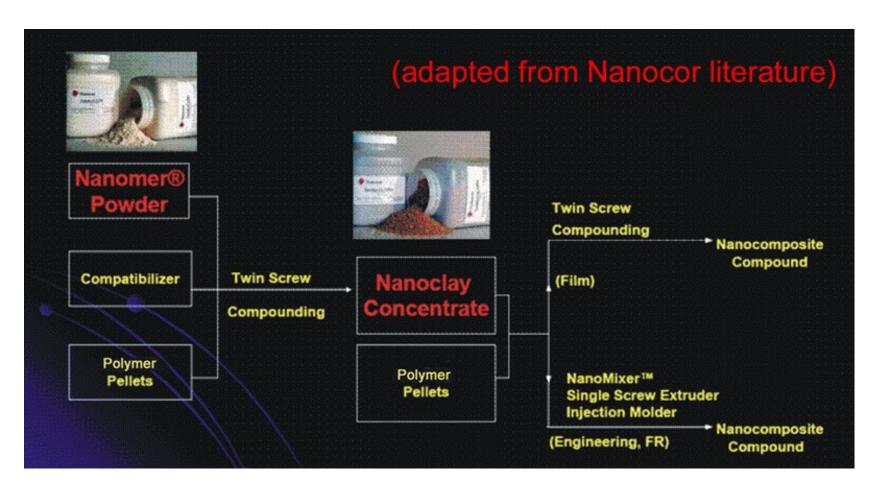


Mitsubishi/Nanocor Imperm®

MXD6



Melt compounding – mixing preformed polymer with clay



- Melt compounded PA6 nanocomposites now available as injection, film grades (RTP Co)
- "NPC" concentrate (Nanocor) allows compounders to produce a nylon 6 compound with about 90% of property levels achieved by the in-situ route

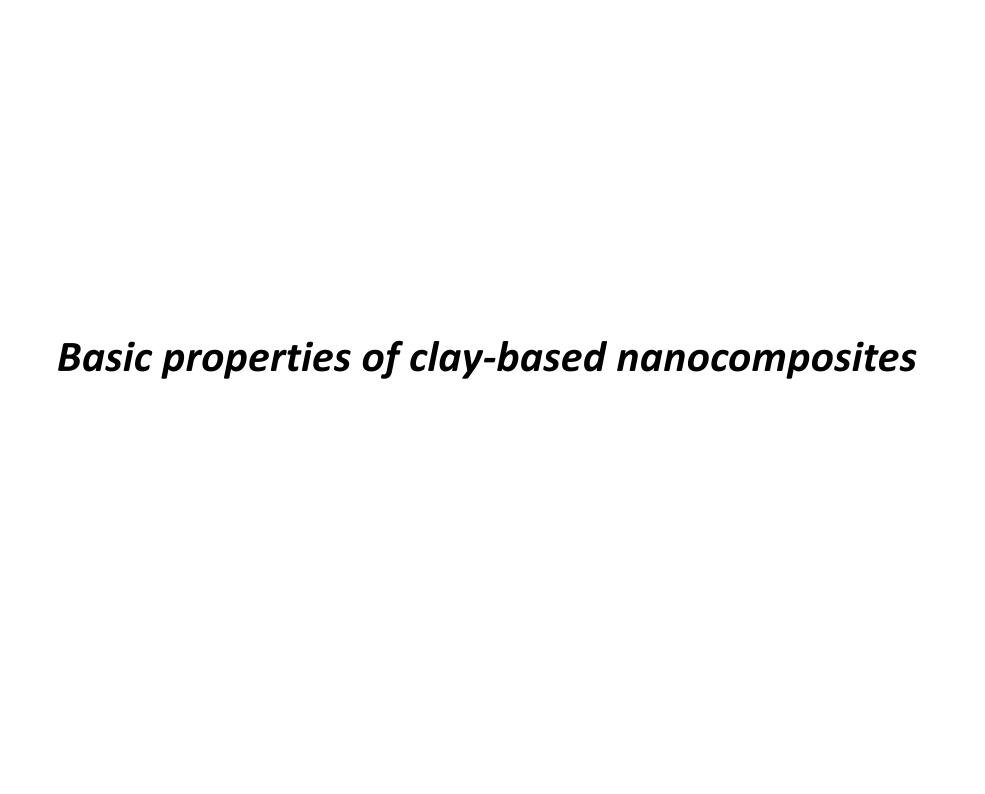


Polyolefin Nanocomposites (PP, TPO's, TPE's)

- Unlike nylon 6 nanocomposites, <u>commercial polyolefin nanocomposites are not available through resin producers</u>. Rather they are <u>offered by independent compounders</u> or produced at customer locations, using masterbatches supplied by masterbatch producers. <u>Masterbatches available from Clariant Corporation and RTP Co., among others.</u>
- Masterbatches contain 40-50 wt% organically modified clay
- Nanocomposites contain up to 6 wt% clay
- Polyolefin-type materials have a wide range of hydrophobicity, so a specific grade of clay must be matched to a specific resin grade.

<u>Mechanical and barrier improvements</u> currently drive polyolefin nanocomposite use – but need for compatibiliser (usually MAH-grafted PP)





Thermomechanical properties: "in situ" polyamides

The <u>in situ</u> material first developed by **Toyota** was claimed to have the following property improvements (RT/ambient humidity, about 5 wt% clay):

- 40 % higher tensile strength
- 68 % higher tensile modulus
- 60 % higher flexural strength
- 126 % higher flexural modulus
- Heat distortion temperature (HDT) increased from 65 °C (nylon-6) to 152 °C

Data given below are for a representative commercial system for diffferent clay contents (RT/ambient humidity, data from Nanocor):

Nanomer [wt %]	Flexural Modulus [MPa]	Tensile Modulus [MPa]	Heat distortion temperature [°C]
0	3404	3117	56
2	3474	4220	125
4	4578	4897	131
6	5388 (+90%)	5875	136



Thermomechanical properties: compounded polyamides

Supplier's data for a latest generation <u>melt compounded</u> PA6 nanocomposite from RTP Co., compared with conventional fillers:

	Nylon 6	Nylon 6 5% Organo-Clay	Nylon 6 30% Mineral	Nylon 6 30% Glass
Tensile Strength [MPa]	60	92	65	96
Flex. Modulus [MPa]	2900	4300	4800	4100
HDT (at 1820 kPa)	65 °C	102 °C	92 °C	190 °C
Specific Gravity	1.13	1.14	1.36	1.35

Representative values for different polyamides compounded with the Nanocor NPC concentrate:

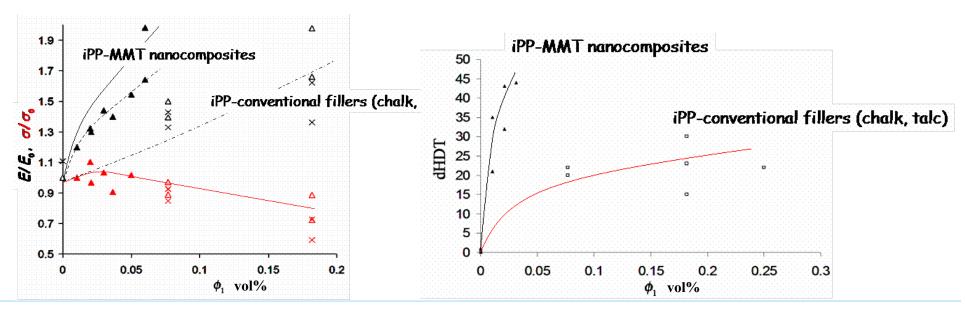
concentrate.	NPC Content	Flexural Modulus [MPa]	HDT [°C]
Zytel 101 (PA66)	0	3413	68
	20%	5062	93
PA6	0	2480	53
	20%	3545	107



Thermomechanical properties: polypropylene mouldings

PP grade	Clay content [wt%]	Tensile Modulus [MPa]	HDT [°C]
Homopolymer	0	1412	87
(low melt flow)	6	2804 (+98%)	116
Homopolymer	0	1327	86
(medium melt flow)	6	2180 (+64%)	109

(All melt compounded with NPC concentrate - source: Nanocor)





Why such improvements? Micromechanical models for MMT dispersions

Basic Halpin-Tsai predictions for aligned discs with aspect ratio α

$$E \approx E_0 \left(\frac{1 + \zeta \eta \phi_1}{1 - \eta \phi_1} \right) \qquad \eta = \frac{E_1 / E_0 - 1}{E_1 / E_0 + \zeta} \qquad \begin{array}{c} \zeta = 2\alpha \Longrightarrow longitudinal \ modulus \\ or \\ \zeta = 2 \Longrightarrow transverse \ modulus \end{array}$$

$$\eta = \frac{E_1 / E_0 - 1}{E_1 / E_0 + \zeta}$$

$$\zeta = 2\alpha$$
 longitudinal modulus or



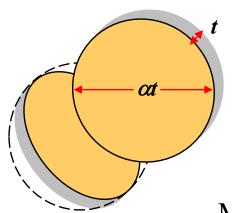
Modulus of an isotropic composite

$$E = 0.49E_l + 0.51E_t$$

For typical MMT particle aspect ratios, α , of up to 1'000, composite modulus, E, should increase as roughly $\alpha \phi_1$ ($E_1 \approx 120 \text{ GPa} >> E_o \approx 2$ GPa (most thermoplastics)) – huge improvement at large ϕ_1 !?



Is this possible in practice for isotropic mouldings?



Excluded volume =
$$\frac{\pi^2(\alpha t)^3}{8}$$



Maximum packing fraction
$$\phi_{\text{max}}^{\alpha} = \frac{1}{1.29 + 0.0598\alpha} \approx \frac{1.5}{\alpha}$$

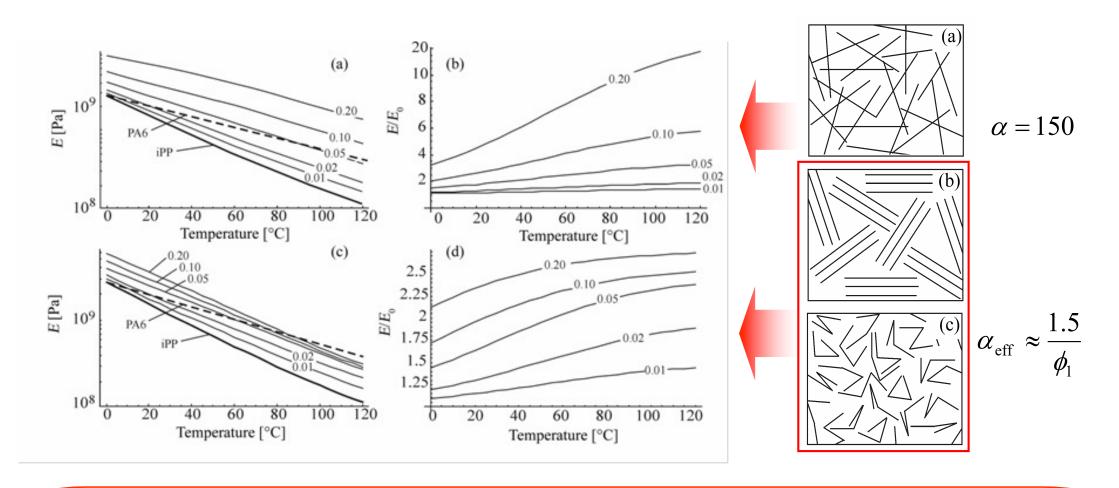


For concentrations greater than $\phi_{\rm max}$, the platelets must either agglomerate or fold, and the effective aspect ratio will be limited to

$$\alpha_{\rm eff} \approx \frac{1.5}{\phi_1}$$



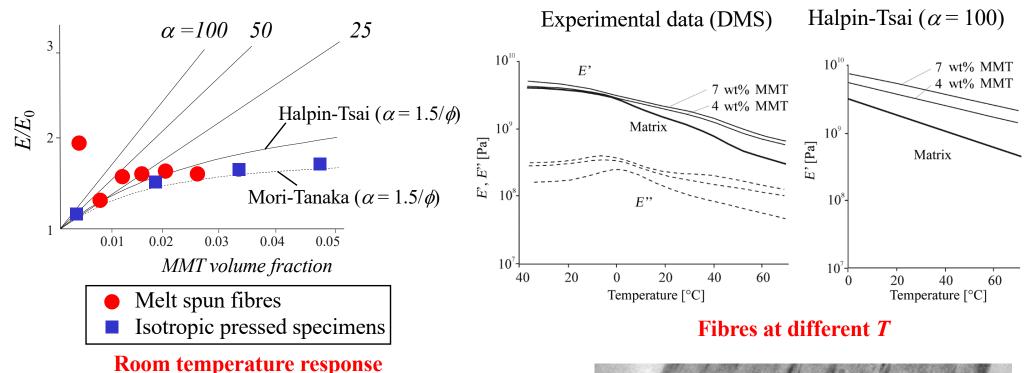
Predictions for iPP as a function of temperature



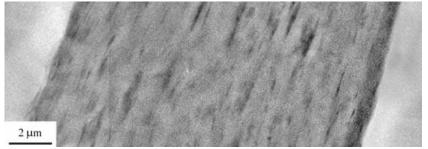
Estimates of (a) E and (b) E/E_0 in iPP as a function of T for different volume fractions of randomly oriented rigid exfoliated MMT platelets, taking $\alpha \approx 150$ and using experimental data for E_0 ; (c) and (d) show E and E/E_0 recalculated taking $\alpha = 1.5/\phi_1$. Data for dry polyamide 6 are also shown in (a) and (c) for comparison (dotted lines).



Comparison with data for iPP nanocomposites



- Reasonable agreement between Halpin-Tsai (with restrictions on α) & data for isotropic specimens
- Qualitative prediction of T dependence of fibre modulus; quantitative agreement poor incomplete exfoliation? Non-uniform fibre sections?



Microstructure of a spun fibre with 7 wt% MMT



Some intermediate conclusions

- Highly exfoliated MMT (high aspect ratio, high stiffness) should lead to outstanding stiffness reinforcement
- In practice, reinforcement in mouldings is limited owing to local alignment, agglomeration and/or bending of the nanoparticles above a certain critical concentration
- Not much benefit from concentrations above about 5 vol% (or about 10 wt%) if random orientation explains. the concentration range of commercial nanocomposites
- Could we align the nanoparticles? Possible, but difficult to achieve high degrees of alignment in mouldings



Other limitations: thermal stability during processing

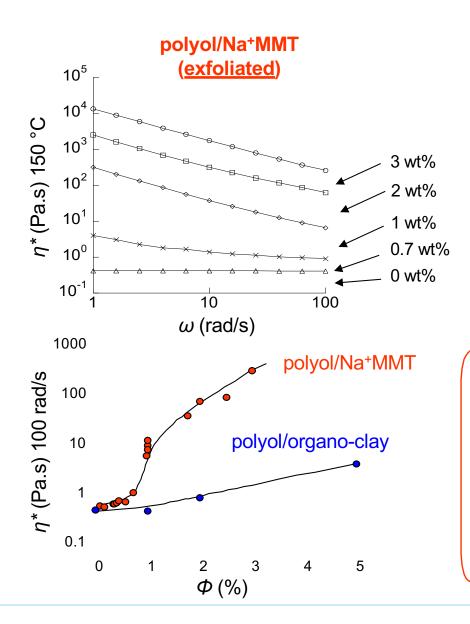
Limitations of current nanoclay formulations

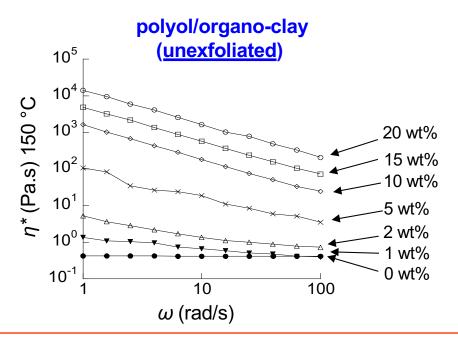
- Hoffman elimination
- Alkyl chain scission
- Processing temperatures < 250 °C

Formulations with new heat-resistant chemistries under development



Rheological behaviour: MMT/low viscosity resins





Data here for a polyurethane precursor and two types of clay: shear thinning behavior and strong increase in viscosity at very low exfoliated clay contents

<u>Potential processing problems for thermosets (we need low viscosity e.g. for mixing with hardener)</u>, less critical for thermoplastics (high initial viscosity)



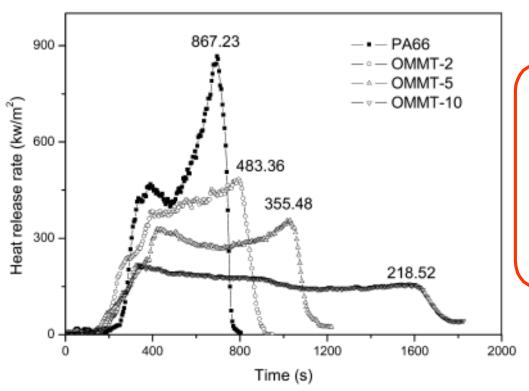
Flame retardant (FR) properties

Clay as a "Nano fire extinguisher" (data from NIST)

- Rate of heat release (RHR) in cone calorimetry tests for nylon 6 nanocomposites containing 5% clay is about 60% lower than for pure nylon 6.
- No increase in carbon monoxide or soot generated during combustion.
- Mechanism of improved nanocomposite FR is not fully understood, but a <u>durable carbon-silicate char</u> is observed to form very rapidly in the burn tests.
- Similar results for other polymers: RHR reduction of more than 75% with the PP-g-MA nanocomposite containing 4% silicate.
- Nano-clay in combination with reduced amounts of conventional FR fillers (e.g. MgOH) are likely to meet FR standards <u>cheaper, environmentally friendly solutions FR materials</u>



Typical Cone Calorimetry Results (PA66)



	PA66	2 wt% OMMT	5 wt% OMMT	10 wt% OMMT	5 wt% MMT
Peak HRR [kW/m²]	802.4	496.1	335.5	209.4	537.8
Total heat	249.2	245.0	247.5	247.8	235.3
Ignition time [s]	169	163	139	152	127

Heat release rates (HRR) for PA66 and different organically modified MMT (OMMT) contents (heat flux 35 kW/m²)

Thermal stability and flammability of polyamide 66/montmorillonite nanocomposites, Huaili Qina, Quansheng Sub, Shimin Zhanga, Bin Zhaoa, Mingshu Yanga, Polymer **44** (2003) 7533–7538



Comparison with PA6, PP nanocomposites

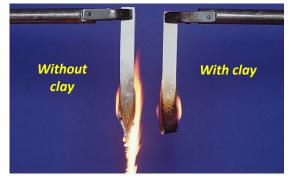
Material	Residue [%]	Peak HRR [kW/m²]
PA6	1	1010
PA6/2wt% OMMT	3	245
PA6/5wt% OMMT	6	378
PP	0	1525
PP/2 wt% OMMT	5	450
PP/5wt% OMMT	-	305

Peak heat release rates (HRR) for PP and PA6 and different organically modified MMT (OMMT) contents (heat flux 35 kW/m²)

In both cases, significant drop in HRR, but also decrease in ignition times on MMT addition

Also, antidrip effect, important for limiting spread of fires



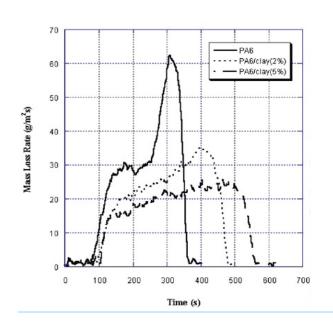


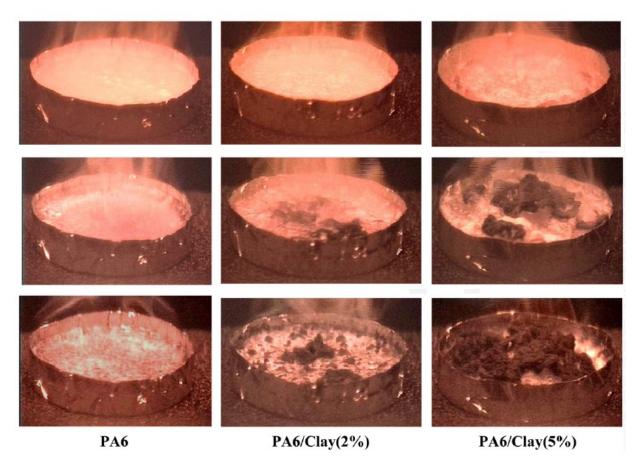


Possible Mechanisms?

Reduction in peak HRR is achieved by the *formation of. protective flocs* at the sample surface (80 % MMT)

Accumulation of MMT due to either degradation of resin or migration of MMT to the sample surface (convective flow)



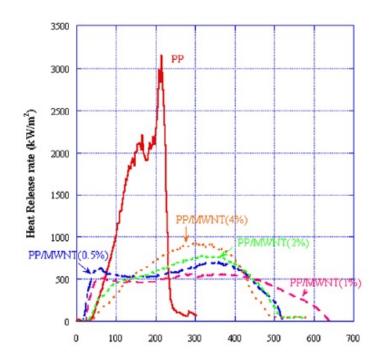


100, 200 and 400 s in nitrogen at 50 kW/m²

Flame retardant mechanism of polyamide 6–clay nanocomposites, Takashi Kashiwagia, Richard H. Harris Jra, Xin Zhangb, R.M. Briberb, Bani H. Ciprianoc, Srinivasa R. Raghavanc, Walid H. Awada, John R. Shields, Polymer 45 (2004), 881-891



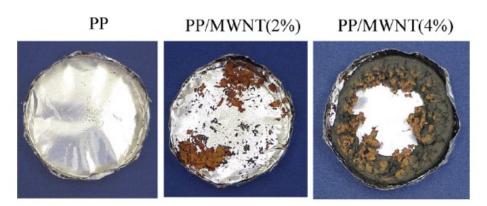
Similar effects with other (nano)fillers, e.g. Carbon nanotubes



Heat release rates (HRR) for PP with different CNT contents (heat flux 50 kW/m^2)

Reduction in peak HRR again by <u>formation of</u>
<u>protective flocs</u>; ignition times decrease with CNT content as previously

Thermal and flammability properties of polypropylene/carbon nanotube nanocomposites, Takashi Kashiwagia, Eric Grulke, Jenny Hilding, Kartrina Groth, Richard Harris, Kathryn Butler, John Shields, Semen Karchenko, Jack Douglas, Polymer 45 (2004) 4227-4239

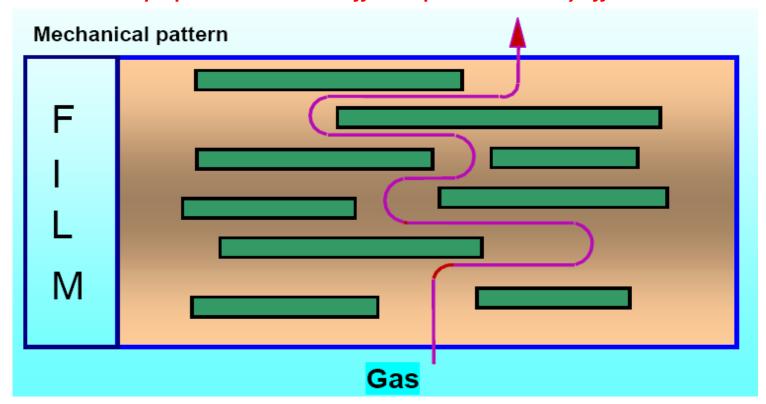


Residues after flame-out and further 2 minutes heating (heat flux 50 kW/m²)



Barrier property improvements: theory

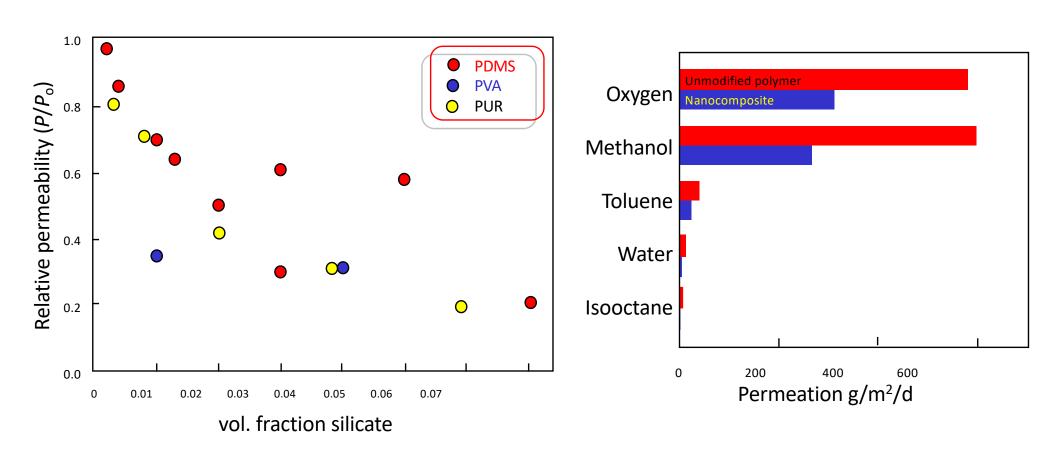
Improvement of barrier properties with montmorillonite layers oriented perpendicular to the diffusion path: "tortuosity effect"



$$D = \frac{D_0}{\tau}$$
 where $\tau = 1 + \frac{\text{filler aspect ratio}}{2} \times \text{filler volume fraction}$



Barrier property improvements: practice



Water vapour permeability through various polymer/MMT nanocomposites as a function of silicate volume fraction

Permeation of different gases in polyamide 12 and PA12/MMT nanocomposites (data from EMS-chemie)



Conclusions

A major advantage of thermoplastic nanocomposites is the <u>increase in heat deflection</u> <u>temperatures (HDT)</u> over the unfilled resin, comparable to that obtained with 20-30% load of a standard mineral-filled compound. Particularly for under-the-hood automotive applications, <u>engineers can maintain the HDT while reducing the weight of the component</u> (fuel and energy savings).

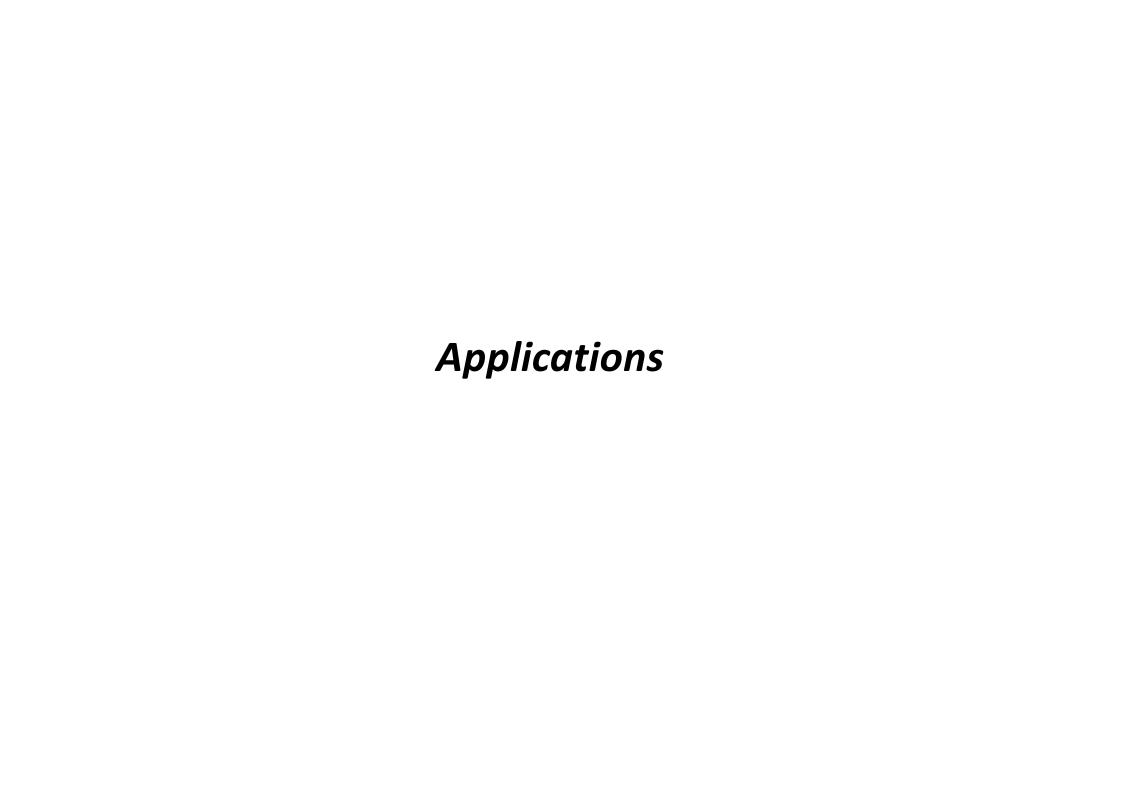
<u>Improved flame retardancy</u> of current interest e.g. for the aeronautics industry, possibility of reducing use of conventional toxic flame retardants

Improved barrier properties

Processing and recycling similar to virgin polymers, better transparency than conventional composites

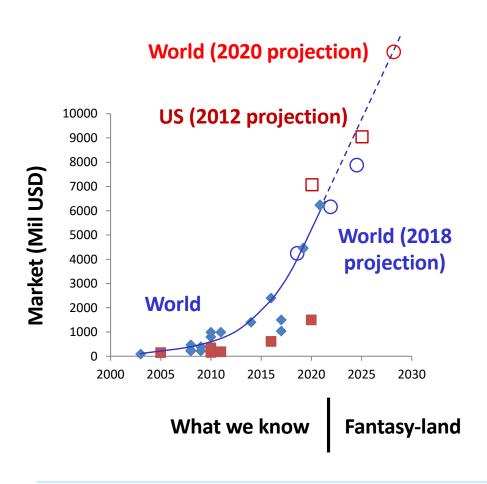
... plus many other benefits specific to particular applications (paintability, surface finish etc.)





The nanocomposites market: some quotations ...

The global nanocomposites market size was USD 4.32 Bn in 2019 and is projected to reach USD 14.34 Bn by 2027 (Fortune, 2020)



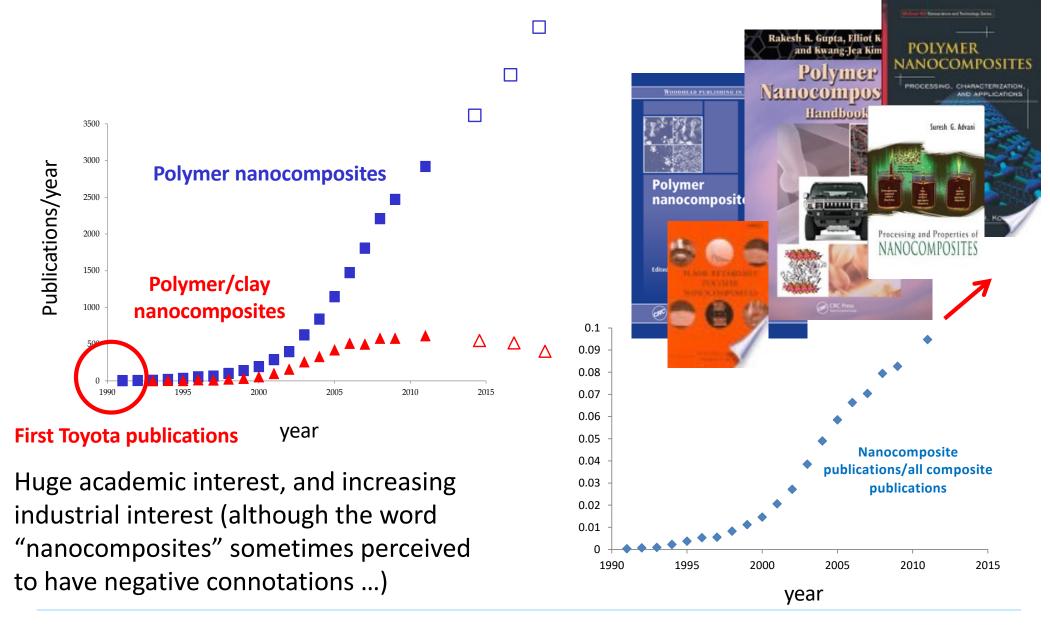
"It is estimated that widespread use of polymer nanocomposites could save over 1.5 billion liters of gasoline annually and reduce carbon dioxide emissions by nearly 10 billion pounds." (MRS Report, 2003)

US NANOCOMPOSITES DEMAND (million pounds)					
plastemart com	2005	2010	2020	% Annual Growth 2005-2020	
Nanocomposites Demand	154	344	7030	29	
Thermoplastic	152	329	5600	27	
Thermoset	2	15	1430	55	

(2009 projection)



Academic interest in polymer nanocomposites





Current applications: transportation (around 15 % of market)





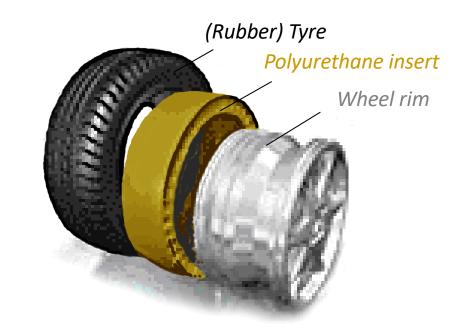
A long shot: polyurethane nanocomposites for tyres?

Fuel emissions: fuel efficiency may increase by more than 3%

Road noise: reduced volume of air, decreasing noise pollution

Weight: total weight of four tyres + insert. Less than five standard tyres (no spare needed)

(The first cars carried up to 6 spare tyres)!



Lightweight nanoreinforced polyurethanes will provide the next generation materials - towards an all PU tyre? (source Goodyear/Amerityre)

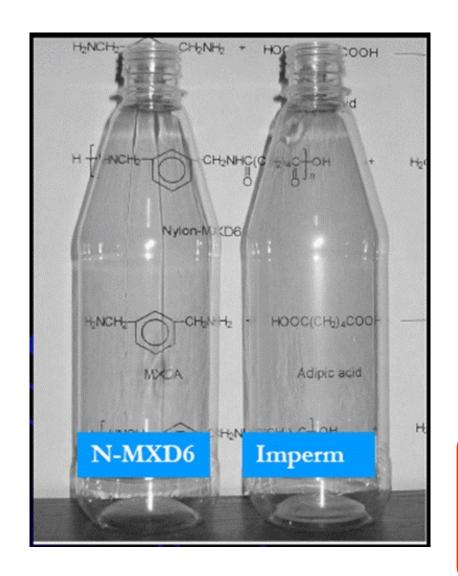
Replacement of conventional technology by structural reactive injection moulding with reinforced PU

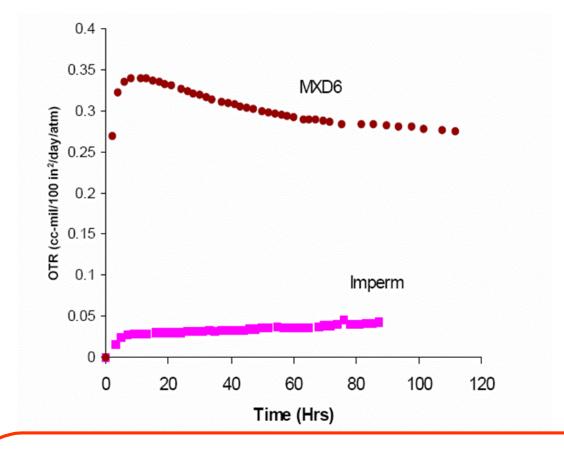


- 9' cycle time 1/3 labour and **1/10 energy**
- 50% increase in tyre life
- Decrease in rolling resistance **10% fuel efficiency**



Current applications: packaging (around 50 % of market!)



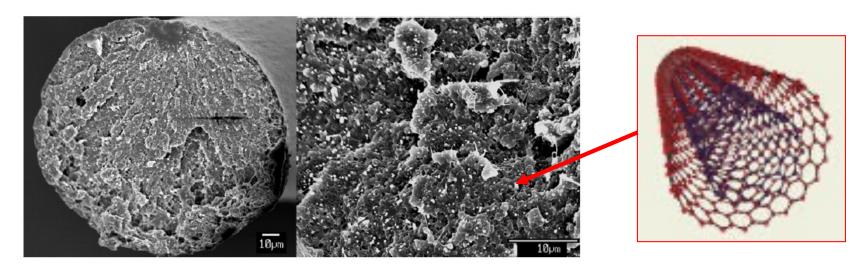


PA6 nanocomposite (Imperm®) compared with PA6 (MXD6) for blow moulded non-pasteurized beer bottle (tri-layer with PET)

Bottle haze 5% (OK for amber tinted bottles), Oxygen transmission > 100 times less than for monolayer PET, shelf-life about 30 weeks



Other polymer nanocomposites (i): PEEK/carbon nanotubes

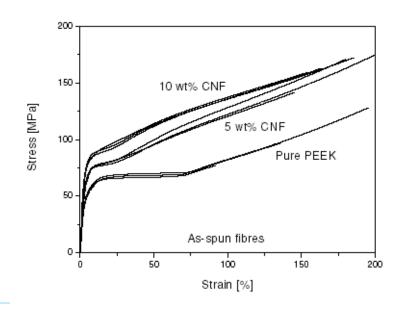


J. SANDLER, A. H. WINDLE JOURNAL OF MATERIALS & CIENCE 38 (2003) 2135-2141

An oriented carbon nanotube CNT has potentially a huge reinforcing effect as well as benefits for e.g. electrical properties (lower percolation threshold than standard carbon black?)

BUT ...

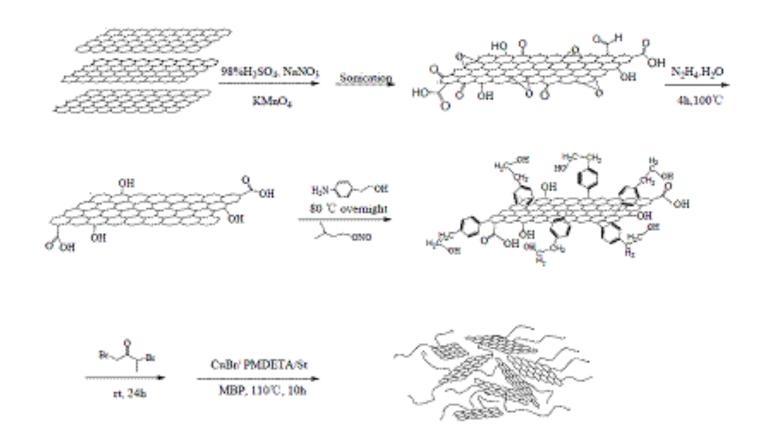
How do we control dispersion and orientation in a polymer matrix? Here is an attempt to do so using fiber spinning.





Other nanocomposites (ii): graphene nanocomposites

Example of a chemical route to incorporating exfoliated graphene sheets in a polymer matrix Lu H. et al., Journal of Materials Chemistry, 2009, 19, 7098–7105



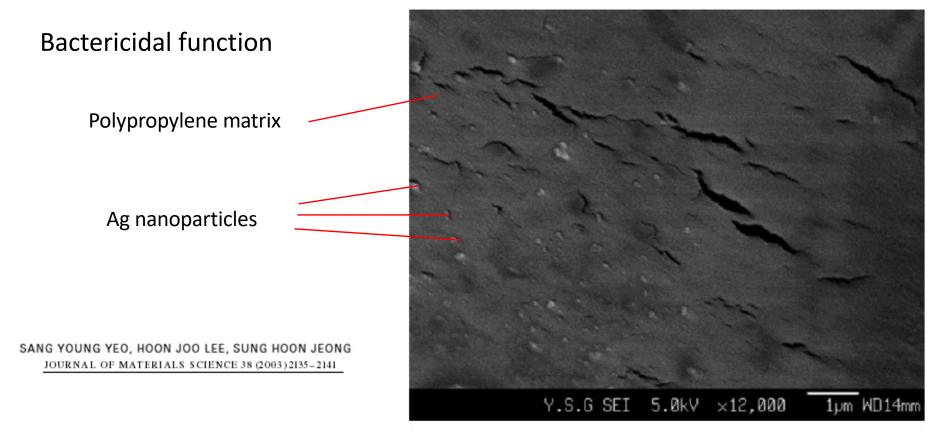
Flat version of CNT Similar goals and problems as for the dispersion of MMT clay and CNT in a polymer matrix

BUT ...

As with CNT, possibility of electrical conductivity for a percolating network



Other nanocomposites (iii): PP/Ag nanoparticles



Sample	Ag content		Antibacterial evaluation (%)		
	Weight (%)	Volume (%)	Staphylococcus aureus	Klebsiella pneumoniae	
PPC-0	0	0	26.3	10.8	
PPC-5	5.0	0.433	19.4	14.8	
PPS-0.3	0.3	0.026	99.9	99.9	
PPS-1.5	1.5	0.130	99.9	99.9	



Electrospun polymer nanofibres

Electrospinning is the process of using electrostatic forces to distort a pendant droplet of polymer solution into a fine filament to be deposited onto a substrate.

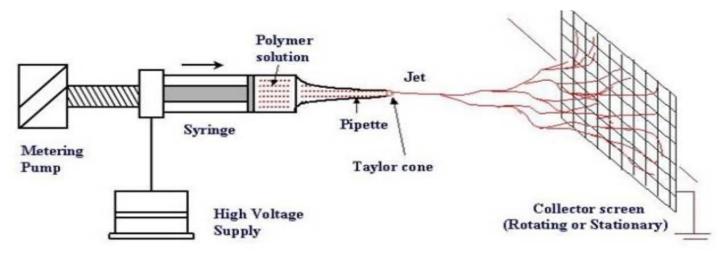
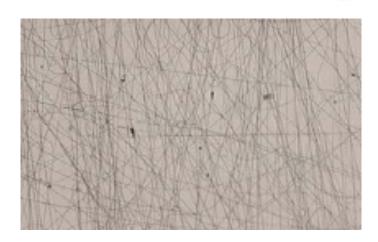


Figure 1. Schematic of the Electrospinning setup.



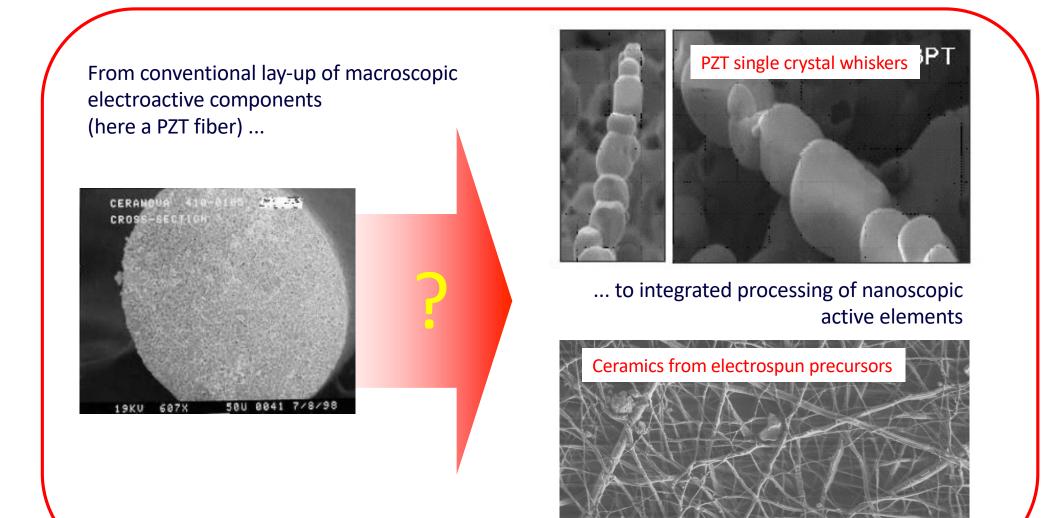
1-10 nm diameter continuous polymer fibres
(here PVDF electroactive fibers)
Can be used as precursors for ceramic e.g. carbon nanofibers



separation membranes, wound dressing materials, artificial organs, nanocomposites, and protective clothing.



Electroactive nanocomposites





Low shrinkage nanocomposite resins

Resins for dental repair, devices, nanostructures ...

We need – fast setting, resistant, low shrinkage, low viscosity resins that are biocompatible (non-toxic ...)

Highly mineral filled UV-curable resins

- UV cure can be very rapid, and the filler reduces macroscopic shrinkage
- Very small (nano)fillers allow precision moulding e.g. for devices (feature sizes of the order of a micron), limited UV light scattering/abosrption during cure
- Mineral fillers may also contribute to hardness, thermal stability

The challenges

- At high nanofiller contents a liquid resin may show a solid-like response at low flow rates
- Avoiding development of excessive internal stresses during cure



A multiple approach to meeting the challenge

Intrinsically low shrinkage resins

Hyperbranched acrylate polymers – low viscosity, high molar mass "pre-crosslinked" resins, delay stress build-up during cure

Nanofillers with controlled surface properties

Tailoring particle-particle interactions in order to optimize dispersion and viscous response

Sol-gel approach

Inorganic particles precipitate during cure, high effective particle contents without the viscosity problem, but longer reaction times?



UV-curable acrylated hyperbranched polymers

Compact, nanometric spheres with high surface functionality

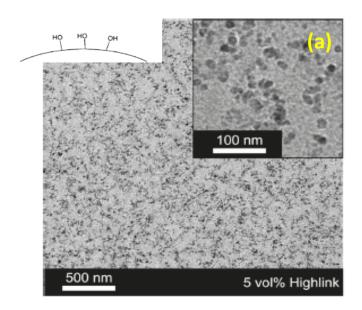
2nd & 3rd generation hyperbranched polyesters & polyethers (HBP)

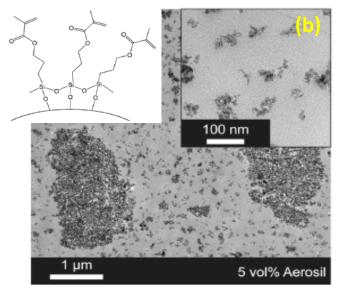
10 to 30 acrylate groups/molecule M_w of 1'800 to 8'000 g/mol

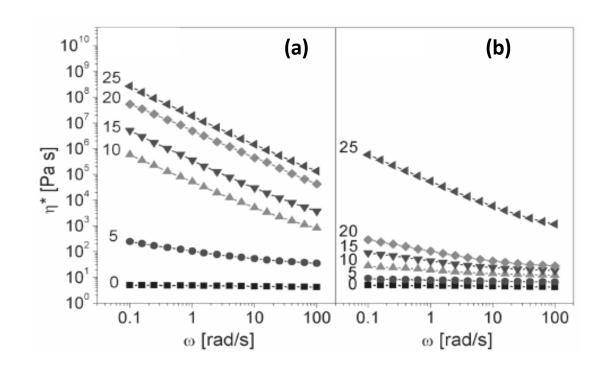
- •High surface functionality → <u>rapid reaction</u>
- Compact spherical morphology (little entanglement)
- → <u>low viscosity even for high M</u>_w
- •Delayed effective gelation → delayed modulus buildup ... *low stress, low shrinkage*



Tailoring interfacial interactions in HPB-silica







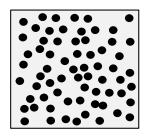
- a) Good dispersion → <u>solid-like behaviour</u>
- b) Reduced interactions with matrix through surface treatment → poorer dispersion but viscous behaviour

It is essential to optimize these interactions!

Ruggerone, Leterrier et al., Macromolecules, 43, 10490-10497 (2010) Geiser, Leterrier et al., Macromolecules, 43, 7705-7712 (2010).



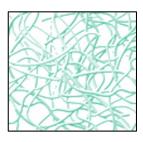
Integrated synthesis of hybrid nancomposites



Particulate composites

solvent assisted ultrasound mixing of resin and solid particles + UV cure

- dispersion of particles is challenging (surface treatment)
- thick paste difficult to process
- fast cure
- hard composite



Sol-gel composites

in-situ synthesis of liquid precursors in resin and dual-cure UV + thermal process

- long process time (condensation)
- low viscosity
- homogeneous nanostructure (transparency)

Geiser, Leterrier et al., Macromol. Mater. Eng., 297, 155-166 (2012)

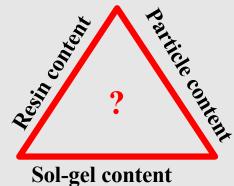


Hybrid composites based on hyperbranched polymers

combination of photopolymerization and sol-gel processes

- + hardness
- + low viscosity
- + low stress
- + transparency
- + rapid processing

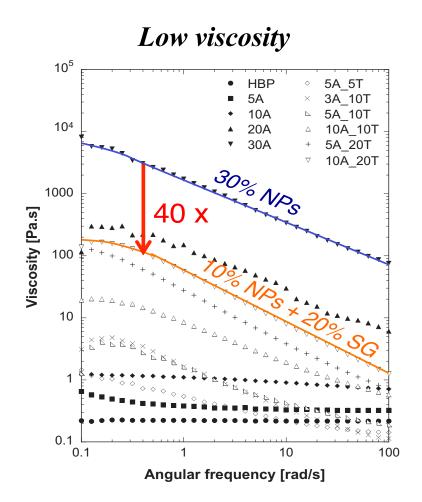








Improved physical response



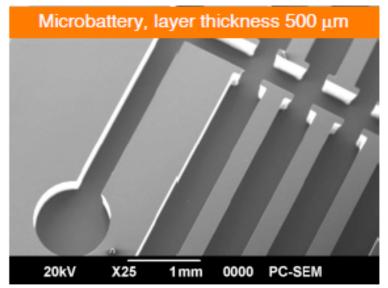
Shrinkage and Stress 30 SU8 25 20 Stress [MPa] Particulate composite Sol-gel 15 (20%vol SiO₂) composite (20%vol SiO₂) **TMPTA** 10 **DPHA** 5 HBP 0 10 5 15

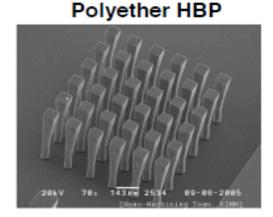
Shrinkage [%]

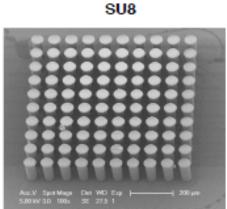
Geiser, Leterrier et al., Macromol. Sympos. 296, 144 (2010) Gonzalez Lazo, Leterrier et al., Polymer 54, 6177 (2013)



Improved applicative properties







FOM = (L x AR) / (Stress x Fab_Time)

Resist	Layer thickness, L (μm)	Aspect ratio, AR	Residual stress (MPa)	Fabrication time (h)	FOM
Polyether HBP	850	7.7	2.4	0.5	5454
Polyester HBP	500	3.3	4.5	0.5	733
SU-8	250	11	25	3	37

Jin Y.-H., J. Micromech. Microeng., 17, 1147-1153 (2007). Schmidt et al., J. Micromech. Microeng. 18, 045022 (2008).

Structures by photolithography



