

# **Advanced materials processing with intelligent systems**

## **Vision Systems**

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# Content

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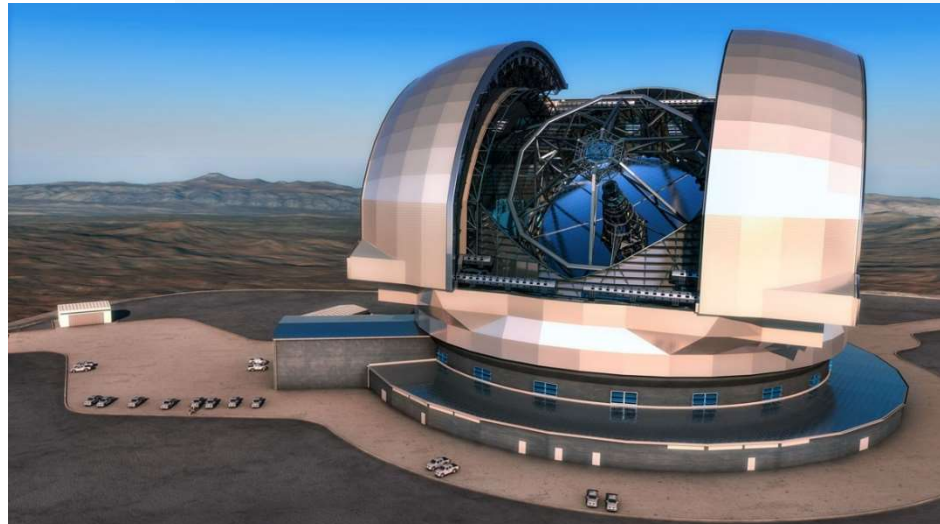
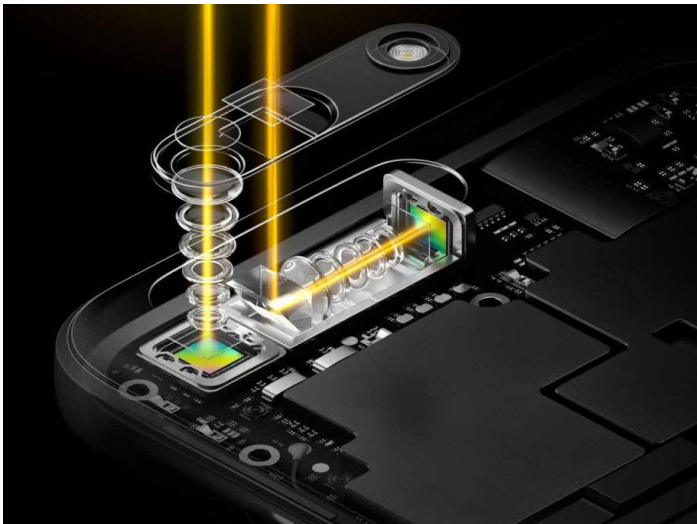
1. Applications of imaging systems
2. Overview of imaging systems
  - Principle
  - Light source
  - Imaging optics
  - Imaging sensor
3. Imaging systems in laser-material processing
  - Laser polishing
  - Laser welding
4. Phase-contrast imaging

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# 1. Applications of vision systems

# Vision system in daily life

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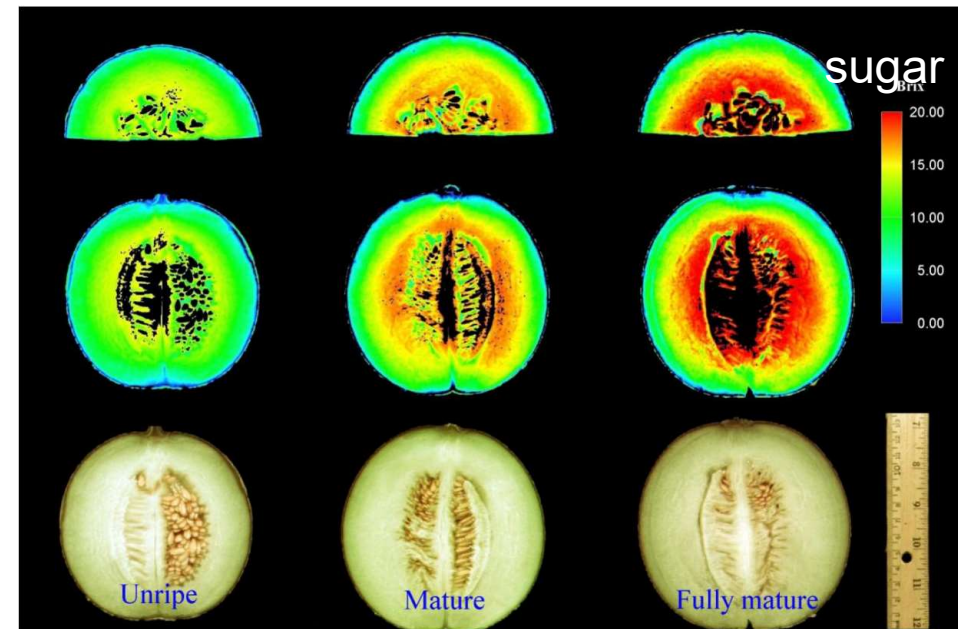
Vision systems exist in all aspects of life



# Extracted information



- Geometrical features (conventional cameras)
- Temperature (thermal camera, hyperspectral camera)
- Composition and chemical distribution (hyperspectral camera)



Hyperspectral view of a melon

# Limit of vision systems

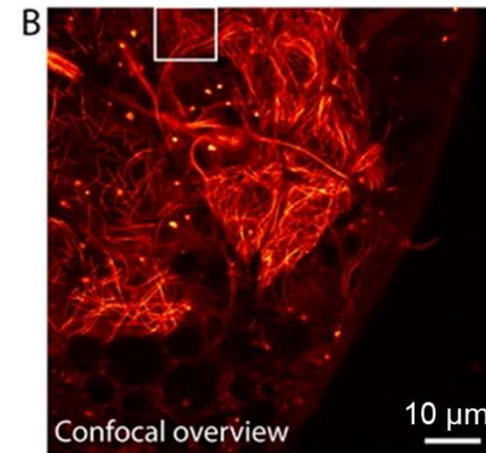
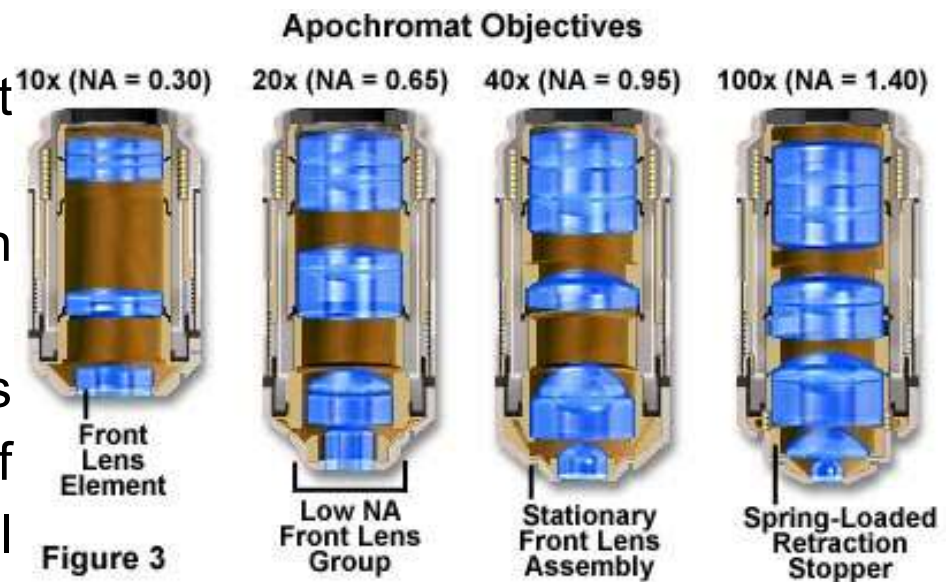


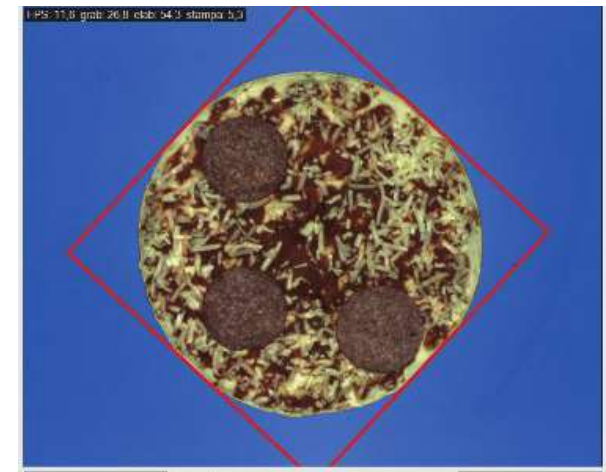
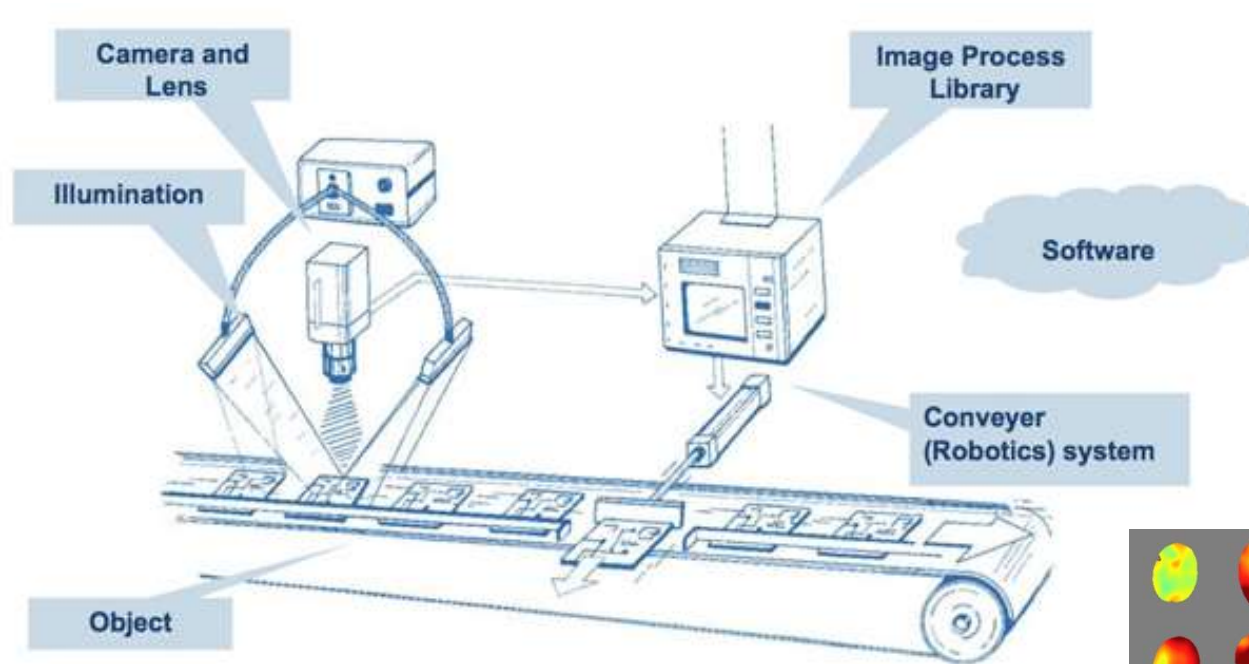
Image of a biological organism

- Field of view up to hundreds of light year
- Spatial resolution down to submicron scale
- Complexity of the system depends heavily on the requirement of imaging resolution and temporal resolution



<https://www.olympus-lifescience.com/fr/microscope-resource/primer/anatomy/objectives/>

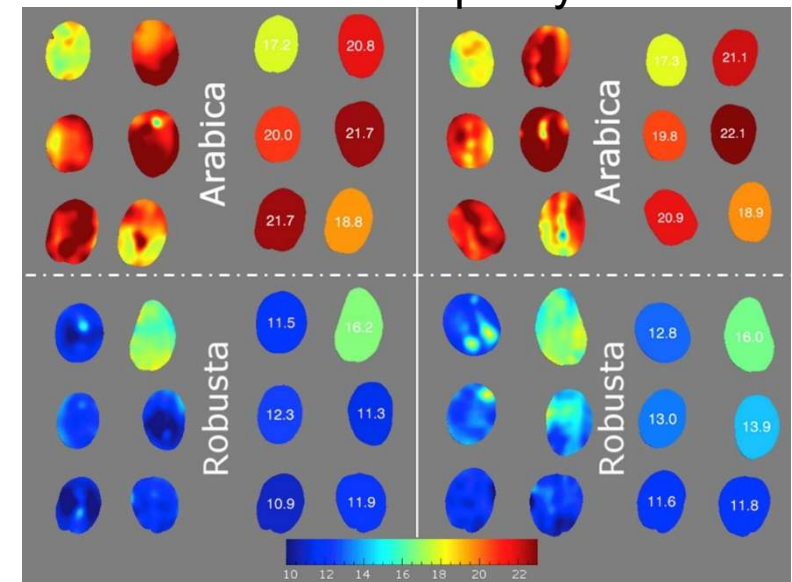
# Machine vision in manufacturing



Pizza quality control

Visualization of specific features in the objects

→ Machine vision for automatic detection of defective objects

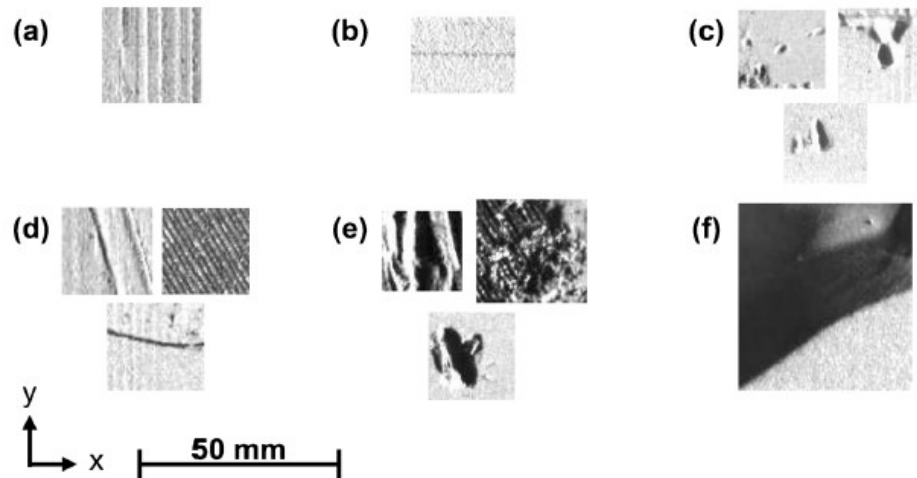
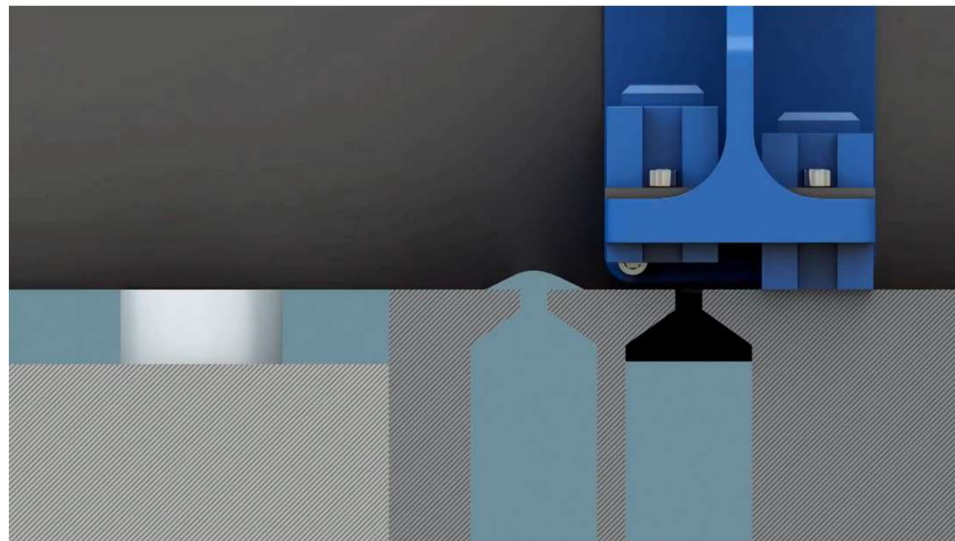


Coffee quality control  
(hyperspectral camera)

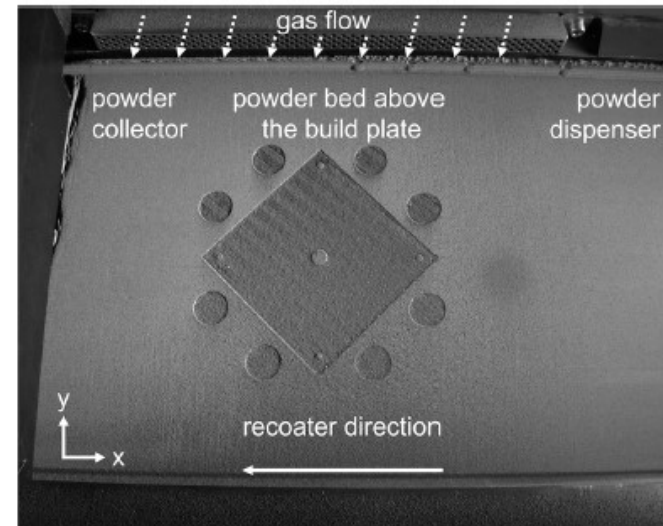
<https://doi.org/10.1016/j.jfoodeng.2018.01.009>



# Machine vision in additive manufacturing



Six different powder bed anomaly (a) *recoater hopping*, (b) *recoater streaking*, (c) *debris*, (d), *super-elevation*, (e) *part damage*, and (f) *incomplete spreading*. <https://doi.org/10.1016/j.addma.2017.11.00>



An image taken from inside of the EOS M290 build chamber using the "powder bed camera". It is oriented such that it is looking down at the powder bed.

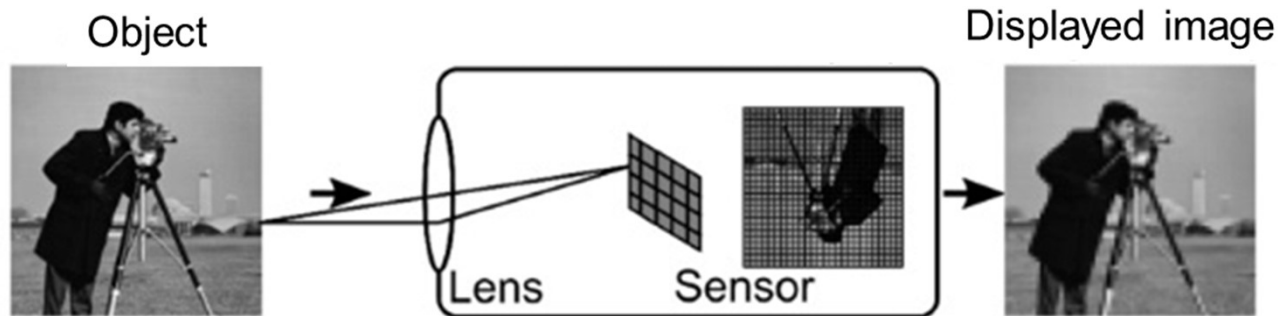


Machine learning  
/ Artificial intelligence

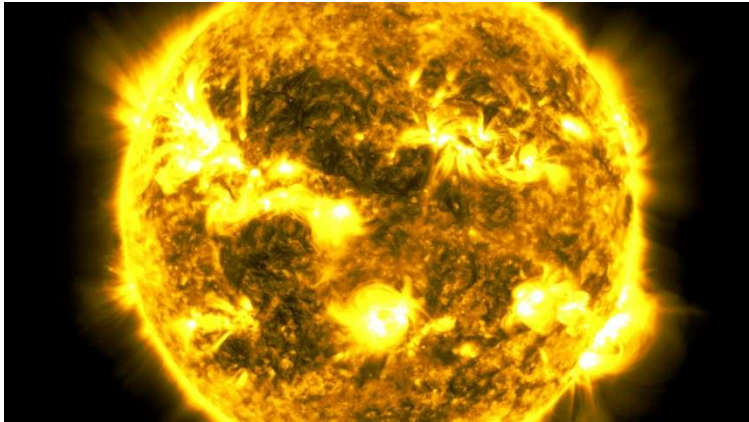
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## 2. Overview of vision system

# Imaging principle



Light originated from the object is collected by imaging optics and projected on a 2D array of photosensitive elements.



Self-illumination



Reflection/scattering of light from external illumination source

# Fast imaging or high-speed photography

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A high-speed camera is a device capable of capturing moving images

- with exposures of **less than 1/1,000 second**
- or **frame rates in excess of 250 frames per second**



Football in slow motion

<https://www.youtube.com/watch?v=XjwO9InuFJk>



Lightning Strike – real-time and at 2,500 fps

[https://www.youtube.com/watch?v=WP9\\_9L20CYM](https://www.youtube.com/watch?v=WP9_9L20CYM)

# Fast imaging or high-speed photography

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A high-speed camera is a device capable of capturing moving images

- with exposures of **less than 1/1,000** second
- or **frame rates in excess of 250 frames per second**

Advantages:

- Visualise events in great detail e.g. melting, solidification, spattering
- Find correlation between sensors signals (e.g. acoustic) and real events
- Confirm hypothesis through visualisation

Disadvantages:

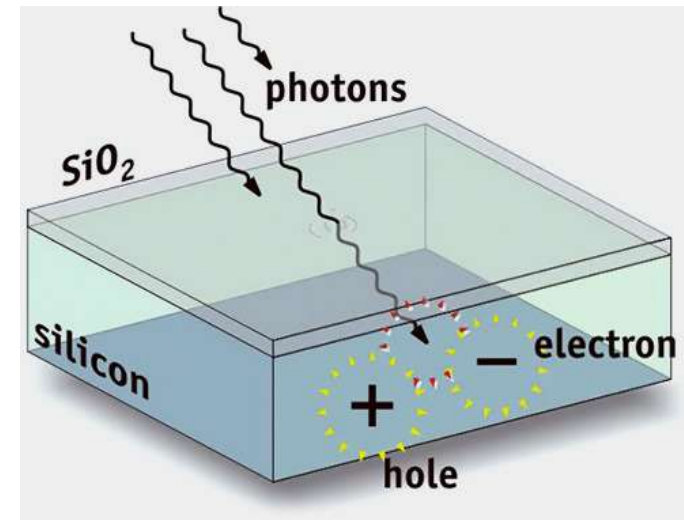
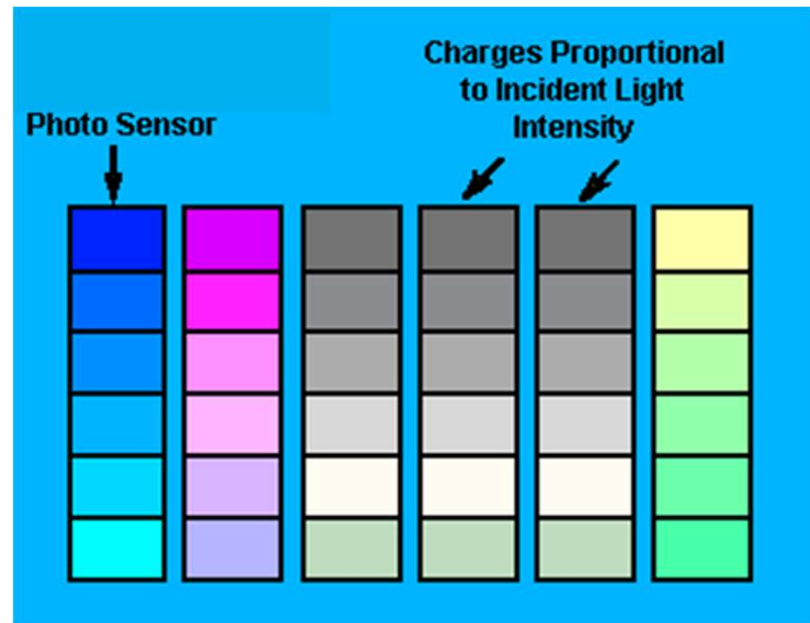
- Accessibility of the information / event
- Cost, good high speed camera are above 100 kCHF  
→ not an wide used industrial solution
- Large amount of data to be treated
- 2D data → requires more storage place and time to be treated as compared to 1D e.g. acoustic



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# Imaging sensors

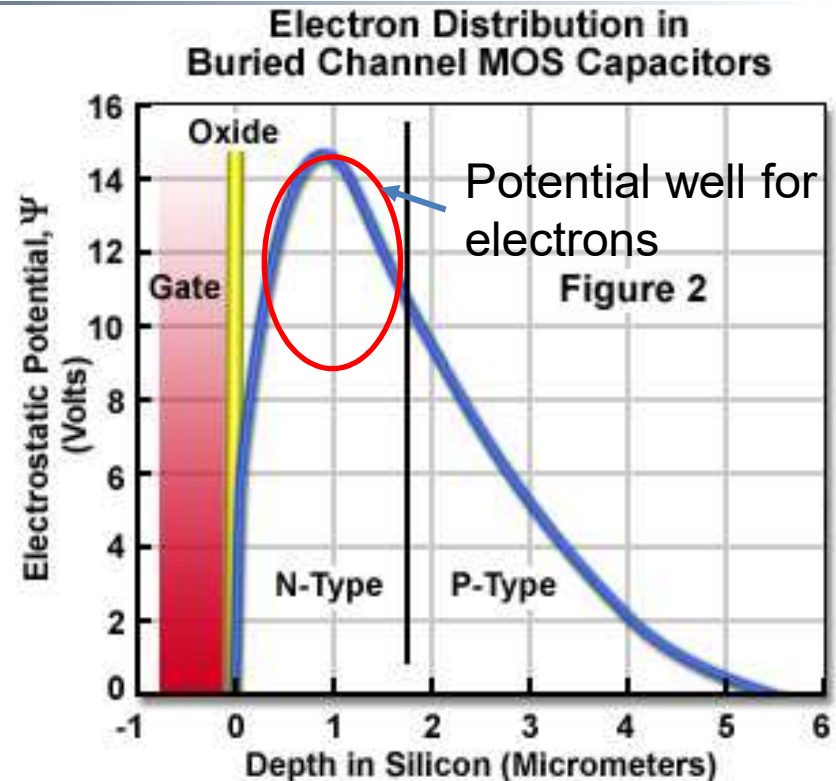
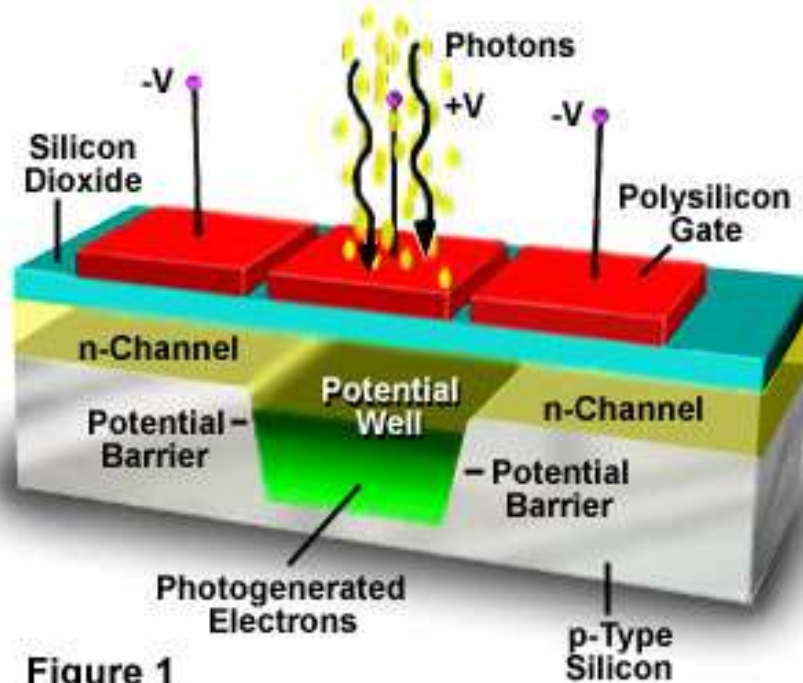
# Imaging sensors



- 2D array of photosensitive elements with output proportional to incident light intensity.
- Two types: Charge-Coupled Device (CCD) and Complementary Metal Oxide Semiconductor (CMOS)
- Light-electricity conversion based on photogeneration of charges in semiconductor

# Metal-Oxide-Semiconductor (MOS)

Metal Oxide Semiconductor (MOS) Capacitor



Potential well is formed directly below the positively biased *gate*.

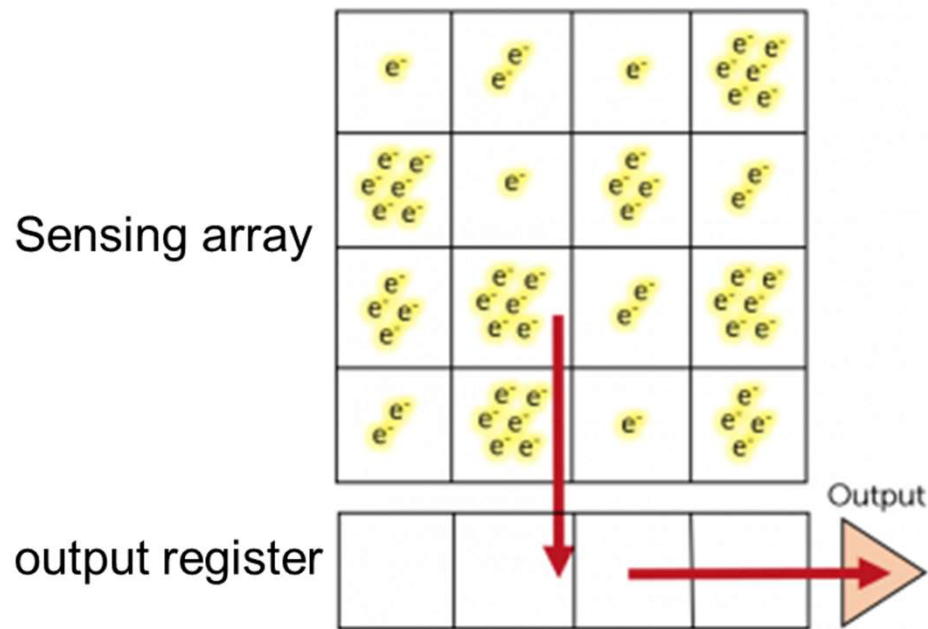
→ The region below each *gate* is one pixel

→ Photogenerated electrons are **accumulated** within the *n*-region, near the *pn* interface

Similar structure for charge generation and accumulation in CCD and CMOS.

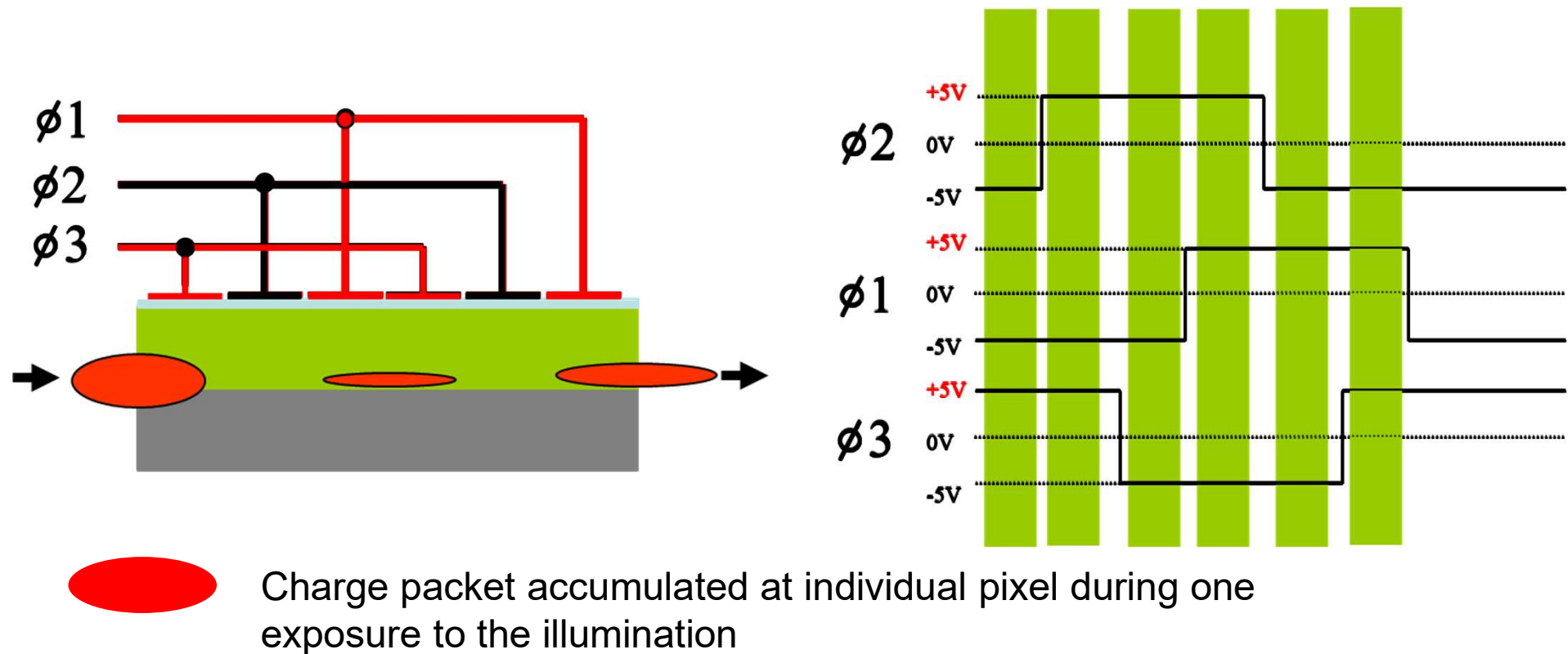
<https://hamamatsu.magnet.fsu.edu/articles/moscapacitor.html>

# CCD operation principle



- During charge transfer, sensing array is shielded to avoid additional exposure  
→ mechanical shutter
- Accumulated charges are transferred vertically to output register, row by row.
- Pixels in output register are shifted horizontally to read out each pixel.
- Charge transfer process is time consuming.

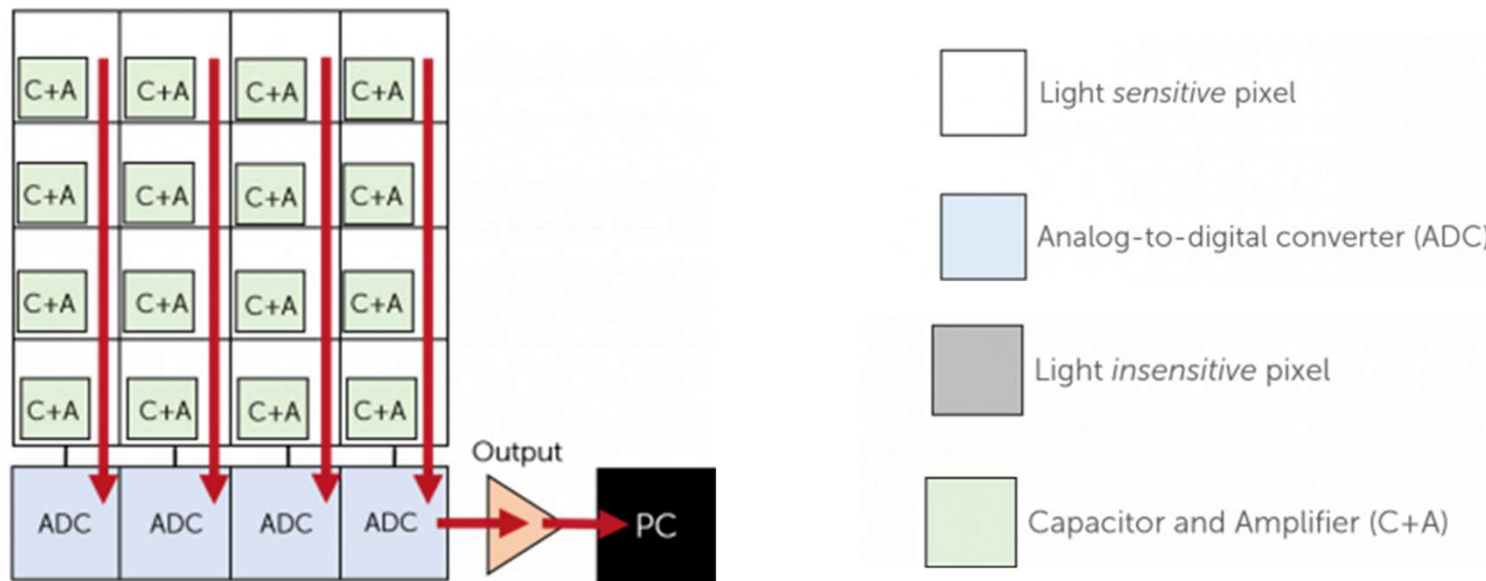
# Charge transfer in CCDs



Accumulated charges shift from left to right by regulating the applied voltages



# CMOS operation principle



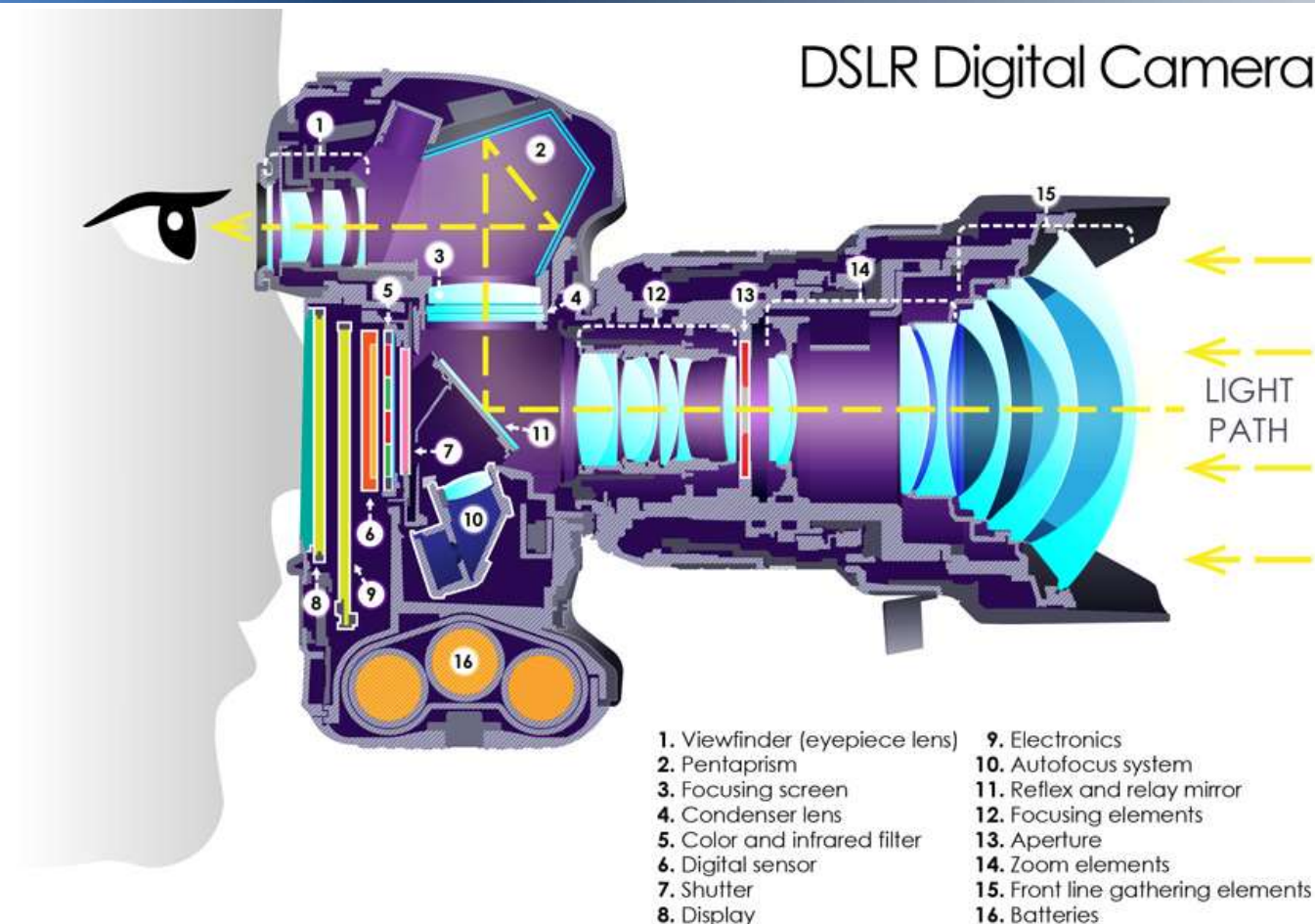
- Pixels include similar MOS structure for photogeneration, together with charge-to-voltage converter, amplifiers, noise-correction, and digitization circuits → smaller area of the photo absorber.
- No physical shifting of charges → faster processing.
- Noises due to the inconsistency in the electronic circuitry in individual pixel.
- Only available for visible imaging

<https://www.princetoninstruments.com/learn/camera-fundamentals/scmos-the-basics>

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# Optical system

# Complexity of the optical system



**Most of the optical components are lenses**

**Many components → too many interfaces → very complex propagation of the light**

<https://www.ephotozine.com/article/this-cutaway-diagram-shows-the-inside-of-a-dslr-30546>

# One of the most complex optical system

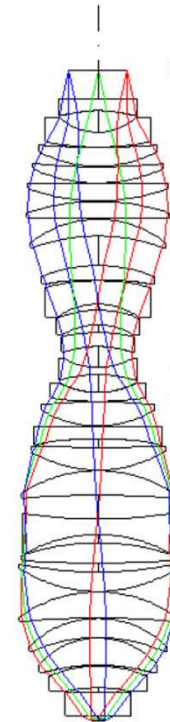
State-of-the-art microstepper with laser and lens



Wavelength 193 nm

| Lens               |            | Field Size | Overlay            | Throughput                                         |
|--------------------|------------|------------|--------------------|----------------------------------------------------|
| NA                 | Resolution | X & Y      | 16-point Alignment | 300 mm Wafers<br>30 mJ/cm <sup>2</sup> (125 shots) |
| Variable 0.85-1.35 | 38 nm      | 26 X 33 mm | 2.5 nm*            | 175 wph                                            |

\* Single machine overlay including chuck dedication



$NA = 0.85$   $y_{imax} = 13.8\text{mm}$ ,  $\lambda = 193\text{nm}$  (ArF) J

A large percentage of high-performance microchips all over the world are now produced using this technology

<https://www.zeiss.com/corporate/int/about-zeiss/history/technological-milestones/lithography-optics.html>

# Geometrical optics

## Two regimes of optics

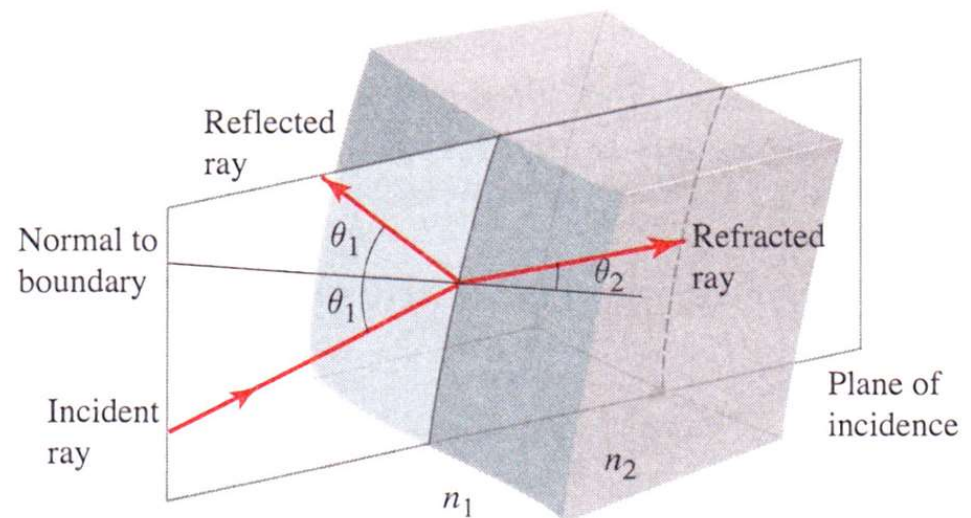
- Wavelength  $\ll D_{objects}$ : geometrical optics → Valid for vision systems
- Wavelength  $> D_{objects}$ : physical optics

## Three basic laws:

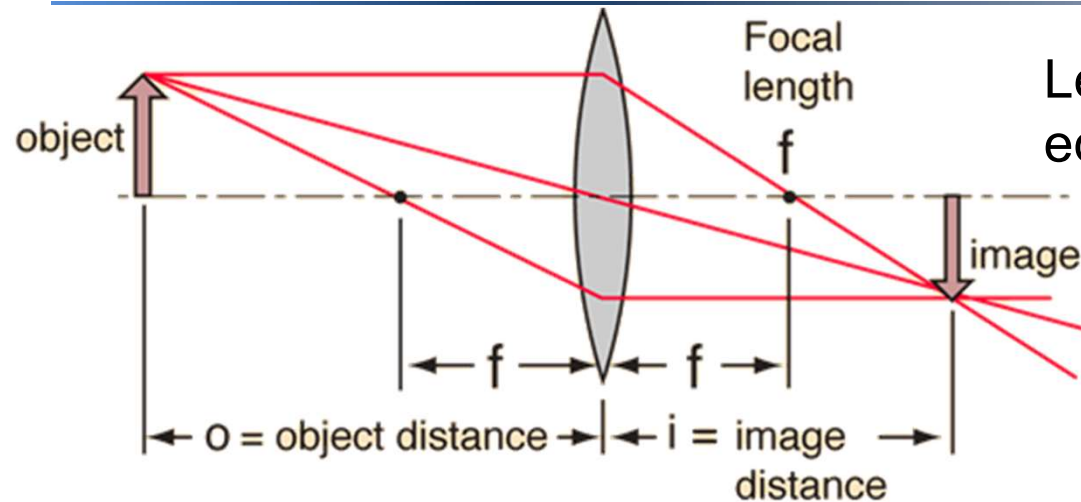
- Rectilinear propagation
- Reflection
- Refraction

## Snell's law:

$$n_1 \sin \theta_1 = n_2 \sin \theta_2$$



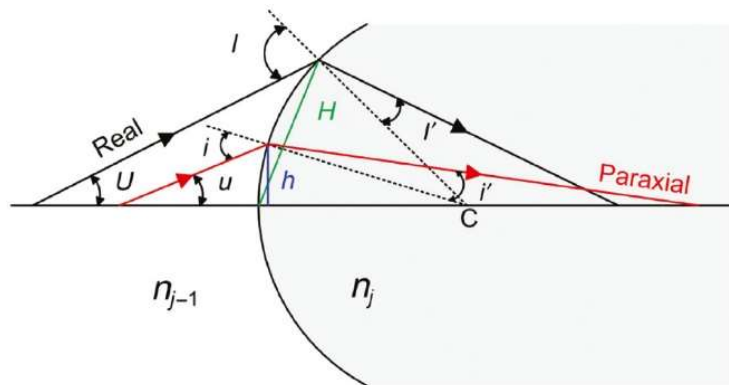
# Single lens equation



Lensmaker's equation  $\frac{1}{f} \approx (n - 1) \left( \frac{1}{R_1} - \frac{1}{R_2} \right)$

$$\frac{1}{f} = \frac{1}{o} + \frac{1}{i}$$

$$M = \left| \frac{i}{o} \right|$$



$f$ : focal length of the lense

$n$ : index of refraction of the lens

$R_1, R_2$ : radius of curvature on two sides of the lense

$o, i$ : distances lense-object and lense-image

$M$ : magnification of the imaging

Taylor series approximation

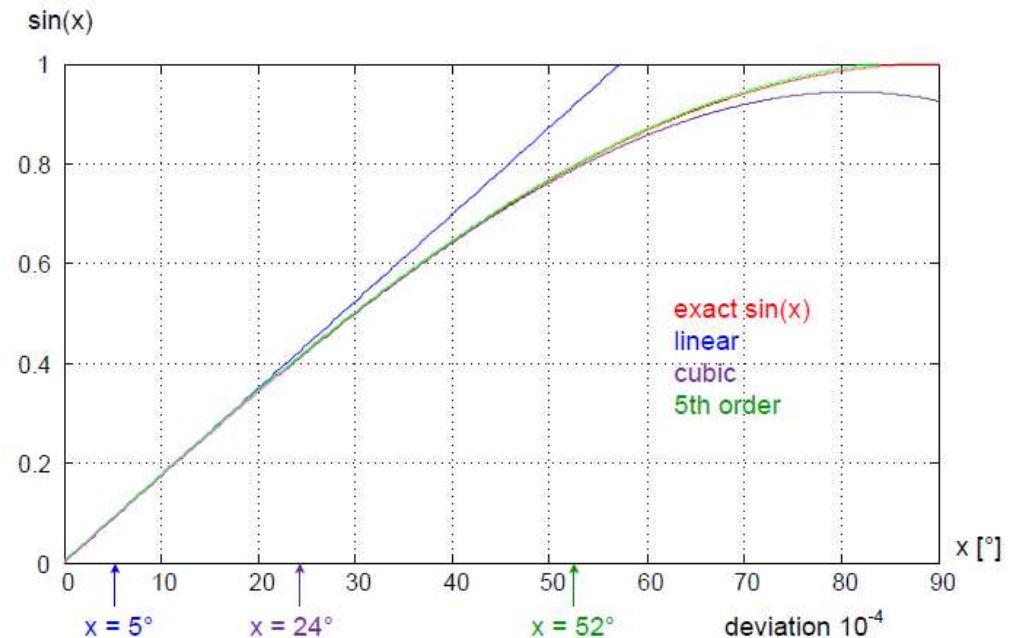
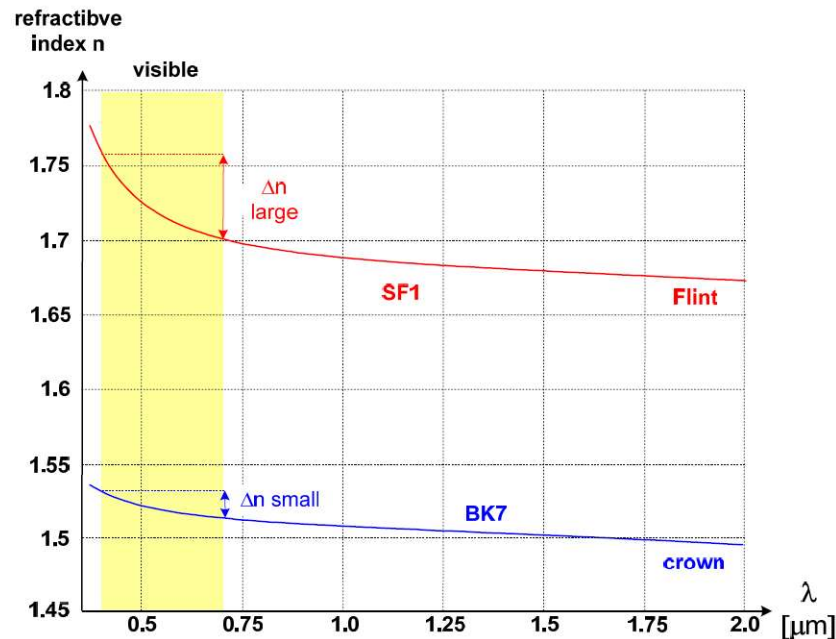
$$\sin(\theta) = \theta - \frac{\theta^3}{3!} + \frac{\theta^5}{5!} - \dots$$

**Assumptions used:**

- Paraxial conditions  $\sin(\theta) \approx \theta$
- Constant refractive index  $n = n(material)$



# Real situation in optical imaging



Curvature of the lense might differ across the lense' surface

Dependence of refractive index on wavelength

Incoming angles are not always small

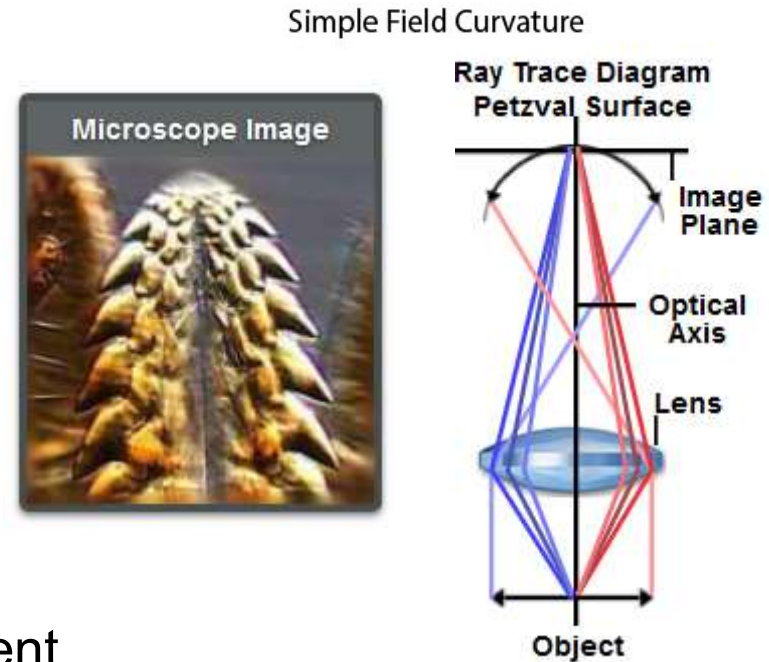
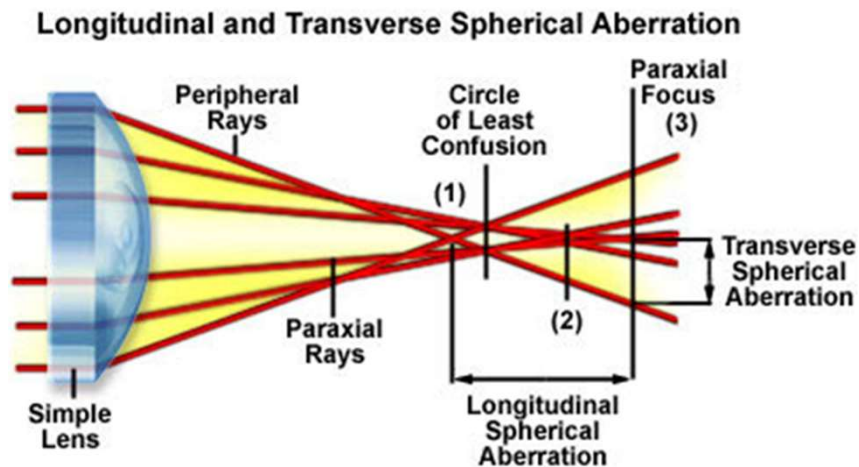


**Each light ray experiences different refraction behaviors**



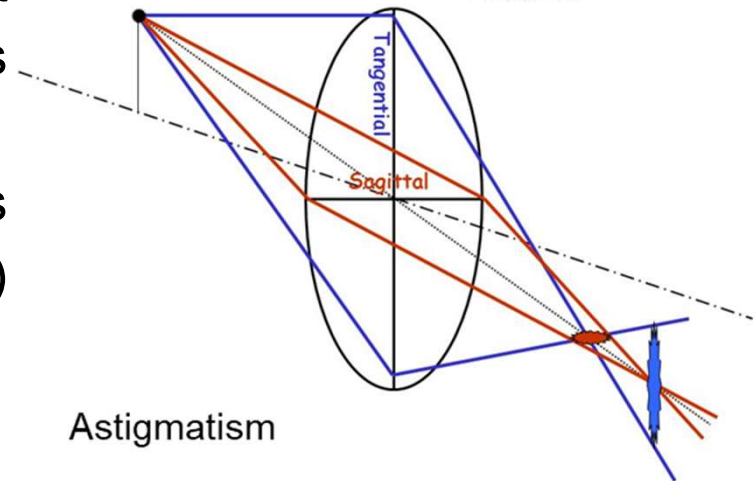
**Light rays do not converge to a single point at the image plane**

# Optical aberration - monochromatic



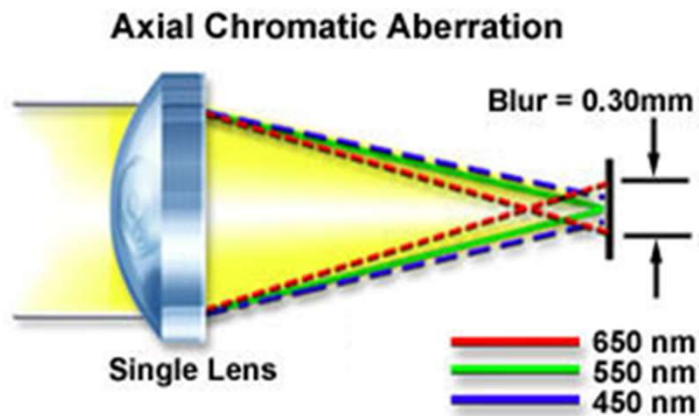
Example of monochromatic aberrations:

- Spherical aberration: refraction is different between peripheral rays and paraxial rays of collimated incoming beam
- Astigmatism: curvature of the lens is different between tangential plane (vertical) and sagittal plane (horizontal)  
→ different focal lengths
- Field curvature, distortion, coma

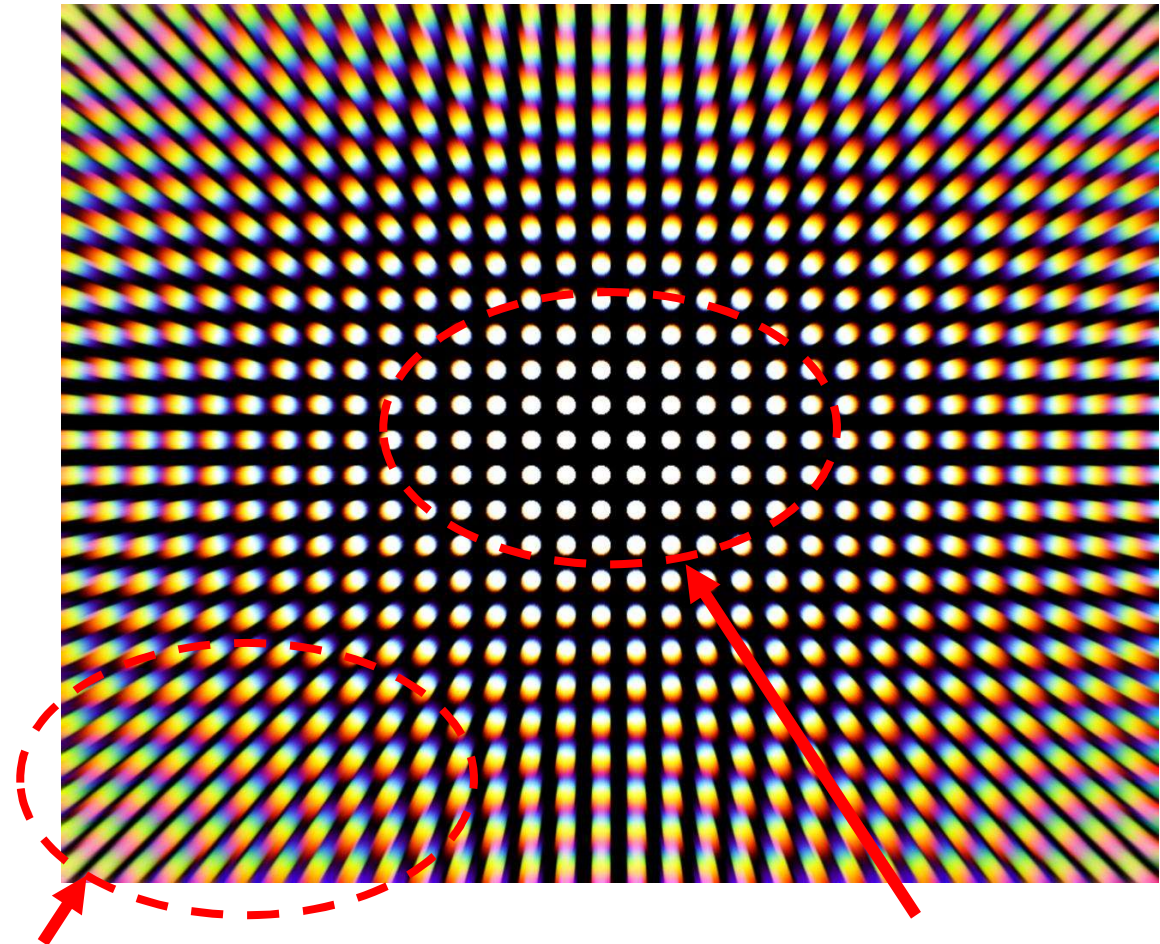


<https://micro.magnet.fsu.edu/primer/anatomy/aberrations.html>

# Chromatic aberration



Chromatic aberration:  
refraction depends on  
wavelength of the light

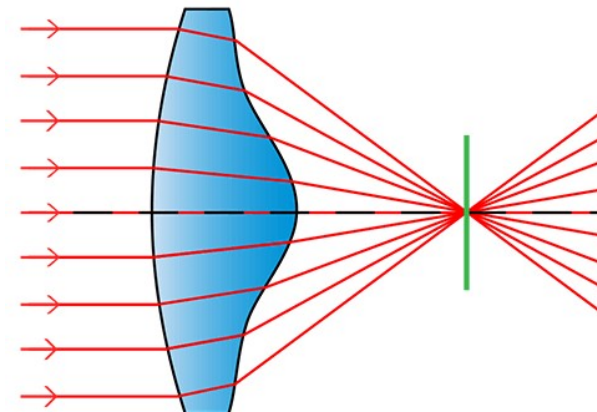
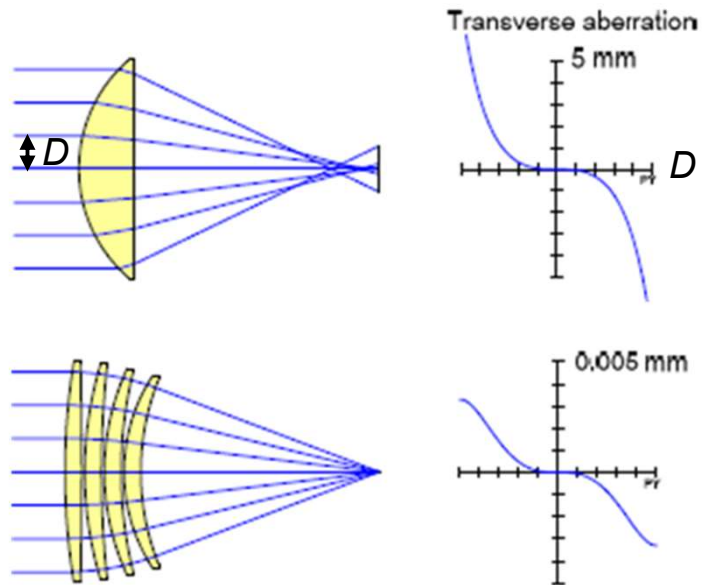


Separation of different wavelengths

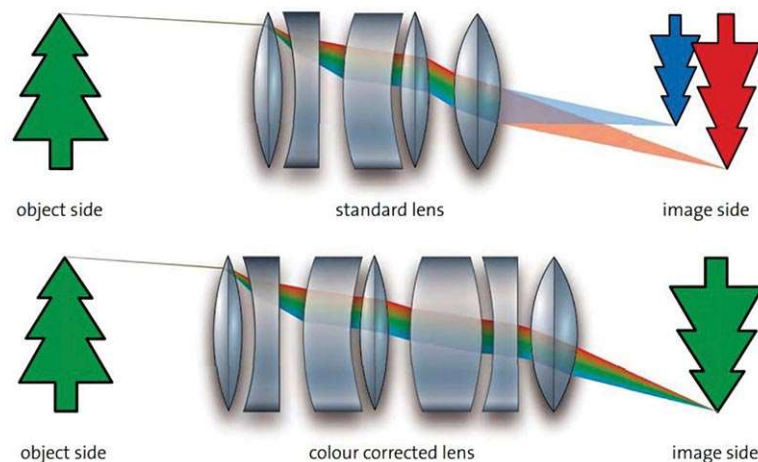
White spot consisting of  
multiple wavelengths



# Corrections of aberrations

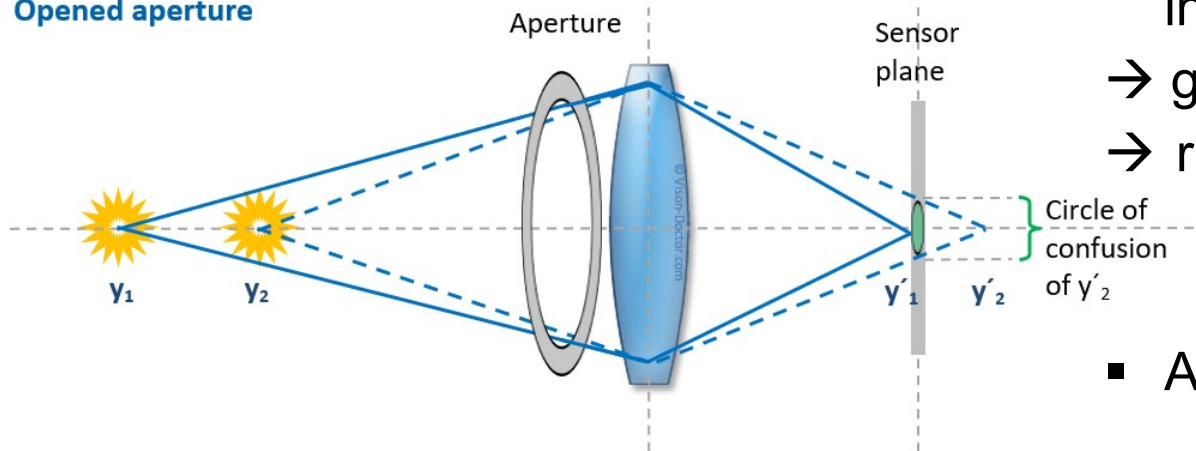


- Customized shape and optical properties of the lenses, this is limited by the thermomechanical properties of the glasses and production methods
- Combination of multiple components to correct the optical aberrations.

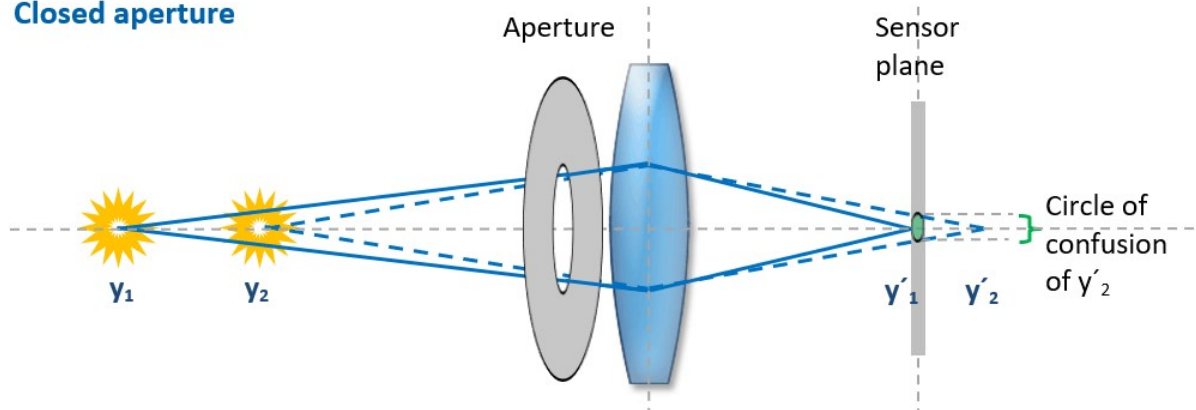


# Aperture in imaging

Opened aperture

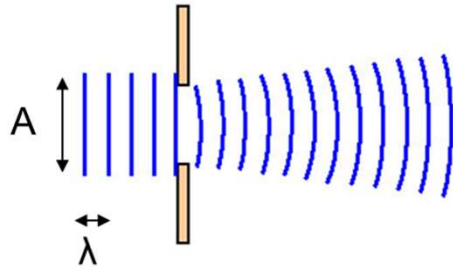


Closed aperture



- Aperture to limit the cone of incoming light
  - go to paraxial conditions
  - reduce optical aberrations
- Aperture also has influence on
  - Depth of field: Large aperture → small depth of field and vice versa
  - Illumination intensity, i.e. exposure time
  - Diffraction limit

# Diffraction caused by aperture



A: aperture

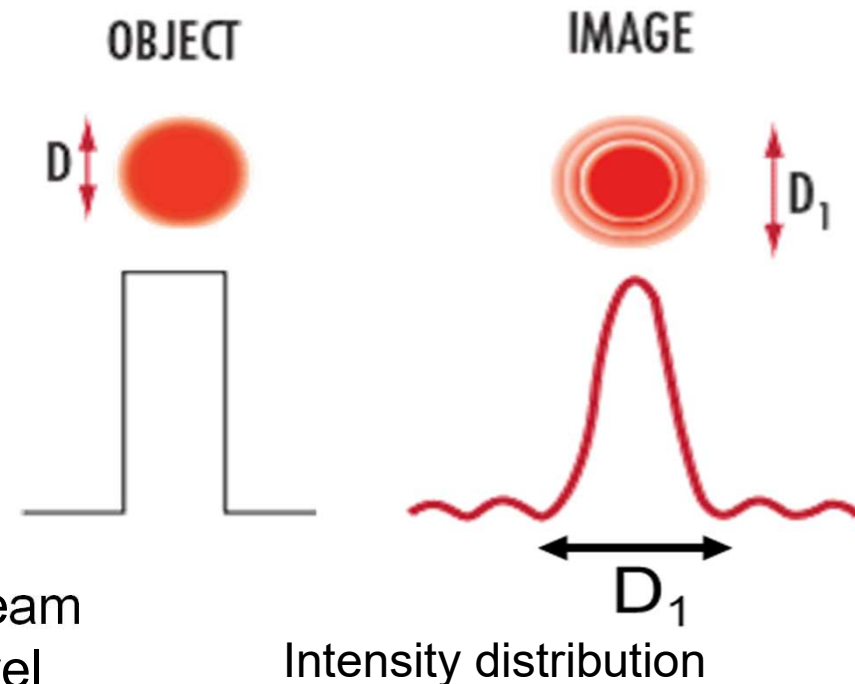
$\lambda$ : wavelength of the light

Aperture causes diffraction of the beam

→ Smaller  $A$  → higher diffraction level

→ Higher  $\lambda$  → higher diffraction level

→ Blurring of the image



For imaging system, the diameter of the image from a point light source ( $D \approx 0$ )

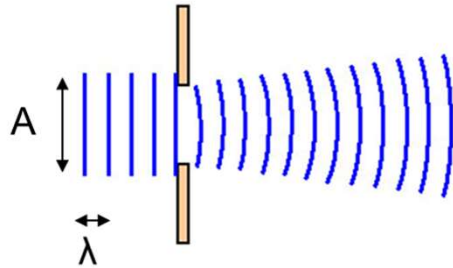
$$D_1 = 1.22 \frac{\lambda \cdot f}{A}$$

$f$ : focal length of the system

<http://ricecatalyst.org/discoveries/2016/10/3-principles-of-super-lensing-overcoming-the-diffraction-limit>

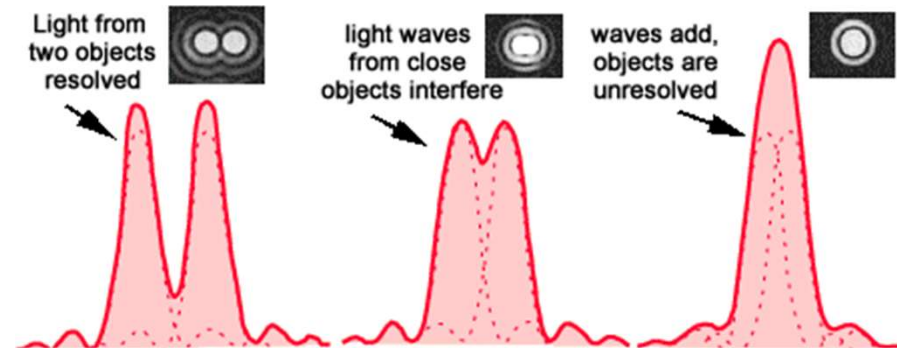


# Diffraction caused by aperture



A: aperture

$\lambda$ : wavelength of the light

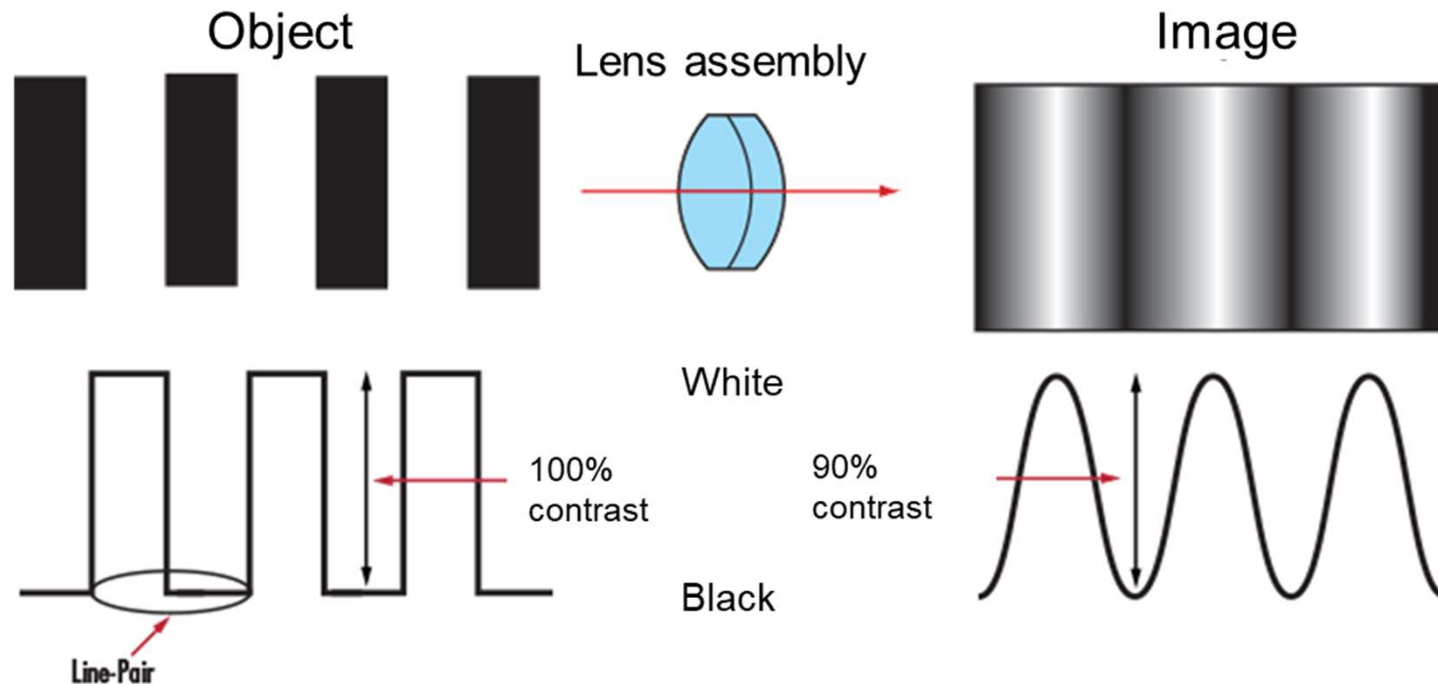


For imaging system, the diameter of the image from a point light source ( $D \approx 0$ )

$$D_1 = 1.22 \frac{\lambda \cdot f}{A} \text{ where } f: \text{focal length of the system}$$

**To distinguish 2 objects, the distance of their images' peak has to be larger than  $D_1/2 \rightarrow D_{\text{objects}} > D_1/2$**

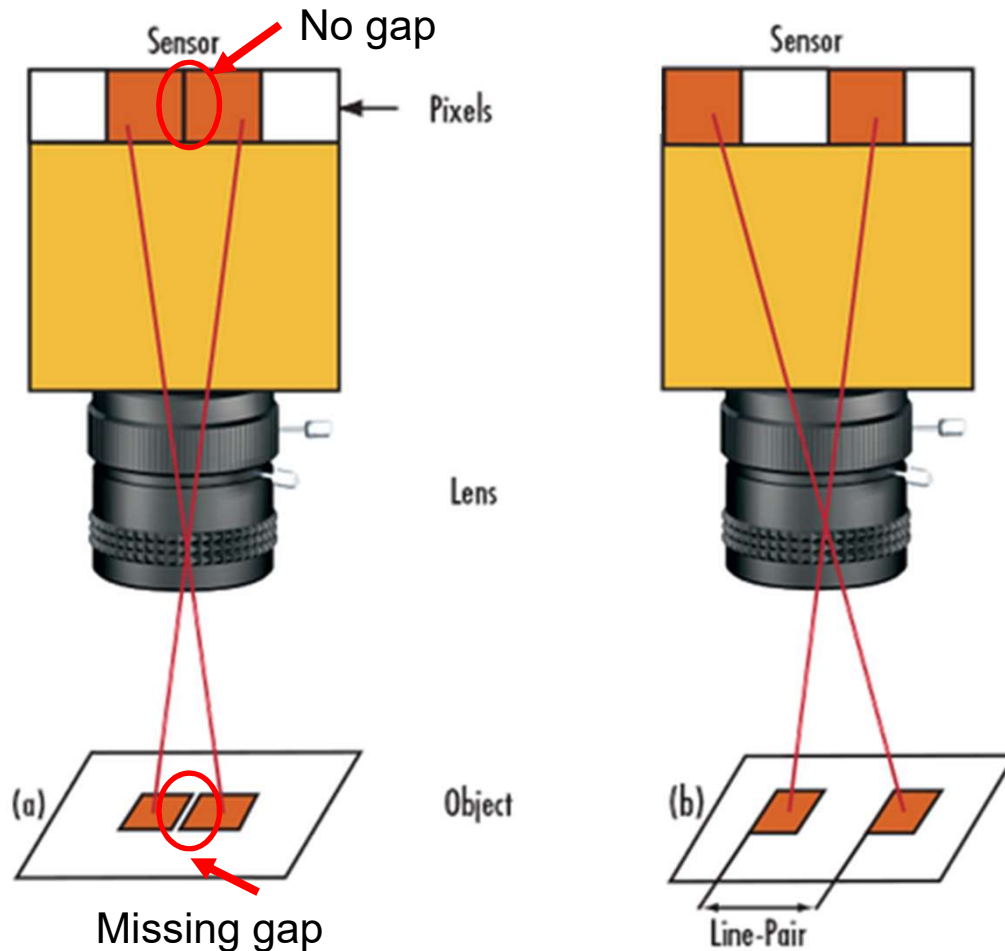
# Imaging resolution



Typical simplification of an object as Line Pairs formed by square waves

**Geometrical features not 100% transferred by imaging optics but blurred due to diffraction → overlapping between neighbouring features**

# Imaging resolution (cont.)

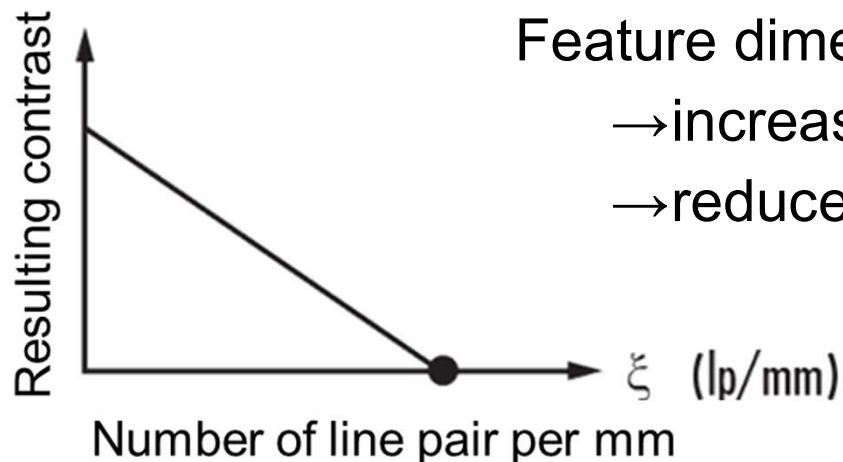
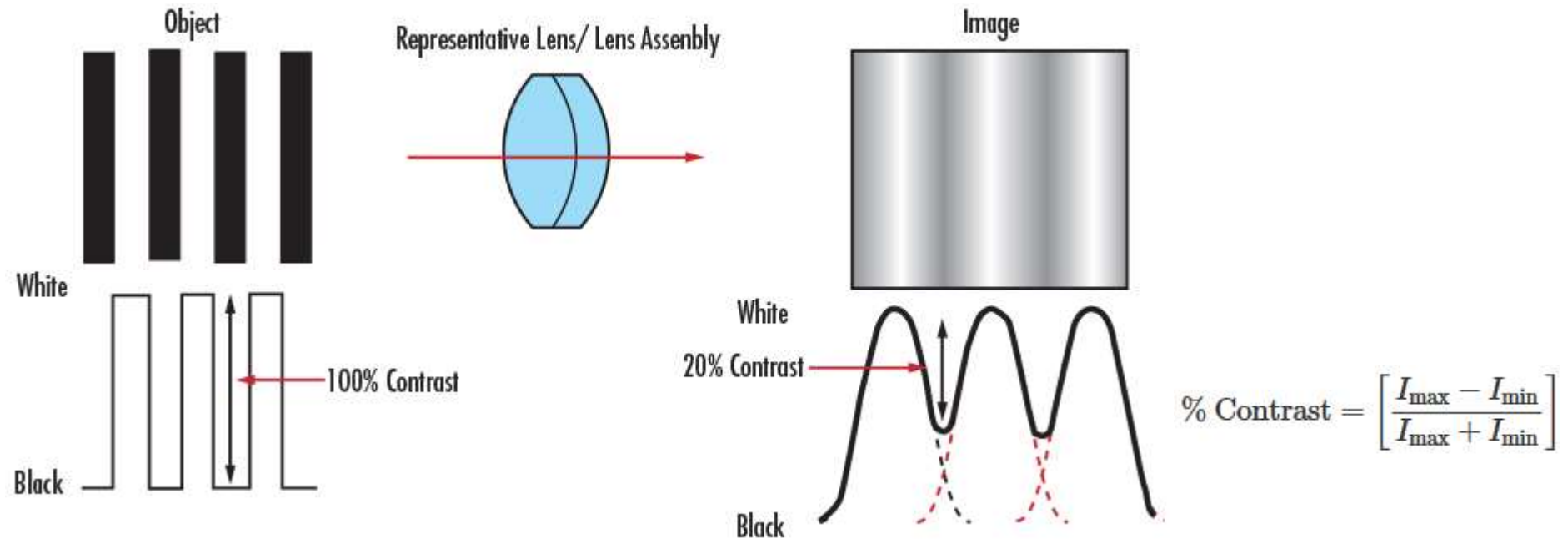


Objects can be resolved if the white and black parts are within two consecutive pixels.

Are the objects resolved?

Objects successfully imaged

# Imaging contrast



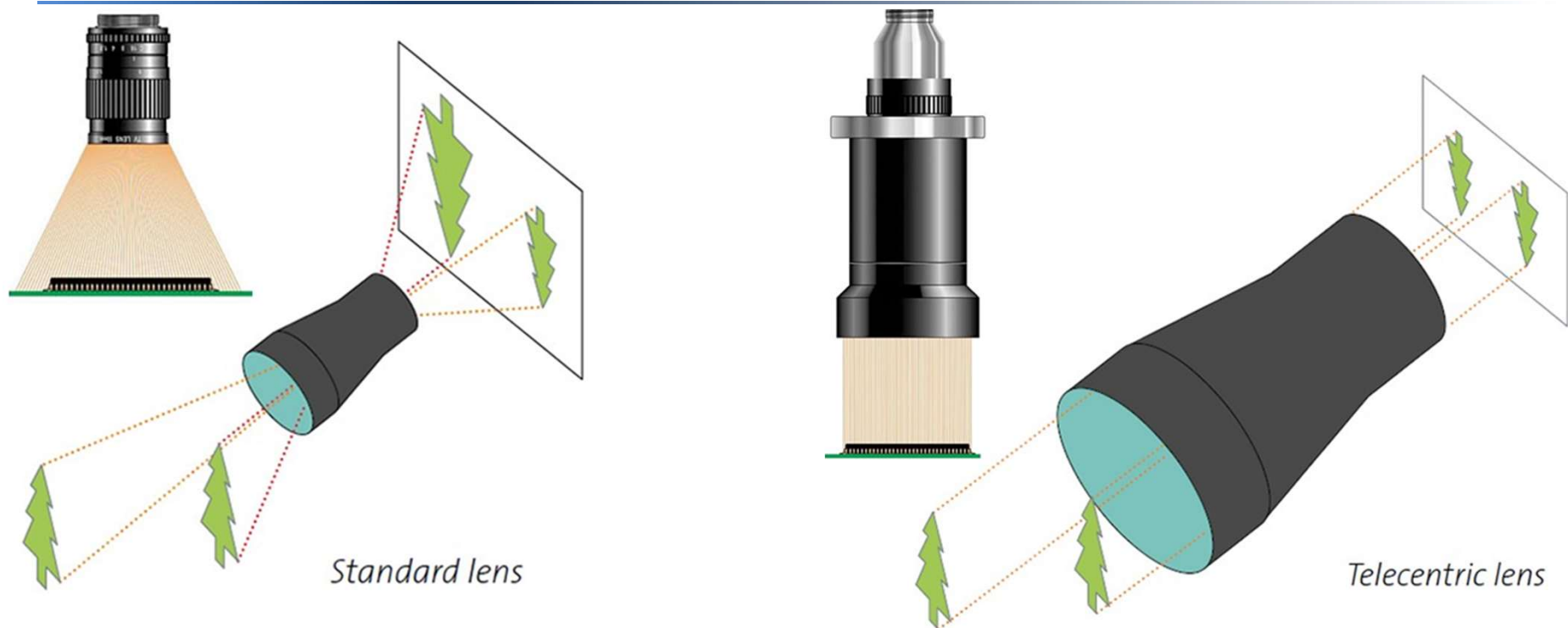
Feature dimension and distances reduce

→ increased overlapping of neighbouring features

→ reduced imaging contrast

<https://www.edmundoptics.com/knowledge-center/application-notes/optics/introduction-to-modulation-transfer-function/>

# Choice of lenses



- Standard lenses (wide angle, macro,...) collect light rays within a cone  
→ magnification depends on distance to lenses.
- Telecentric lenses collect only collimated light rays  
→ all objects in the image have the same magnification irrespective of their distance from the lens

**Choice of lense depends on the purpose**

<https://www.qualitymag.com/articles/94676-optics-for-high-accuracy-machine-vision>



# Telecentric lens

Standard lens



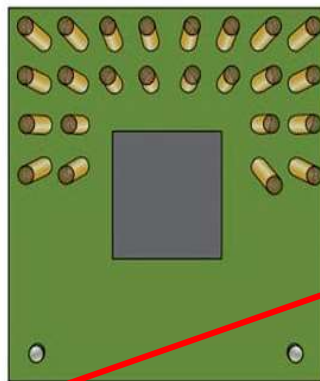
Telecentric lens



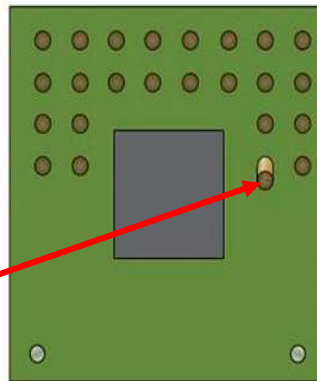
## Pros:

- Easy to measure sizes of features regardless of the distance.
- Easy to detect geometrical distortion in the object.

Standard lens



Telecentric lens



## Cons:

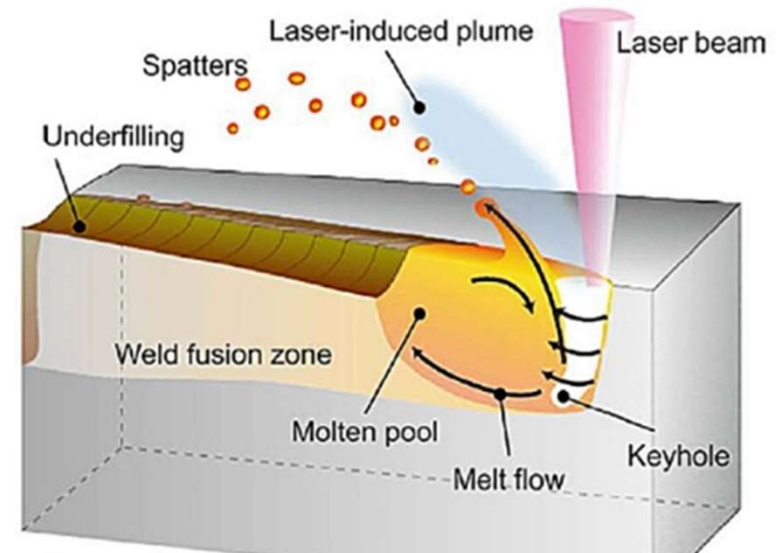
- Limited field of view → limited size of observable objects

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### 3. Vision systems in laser-material processing

# Issues to be considered

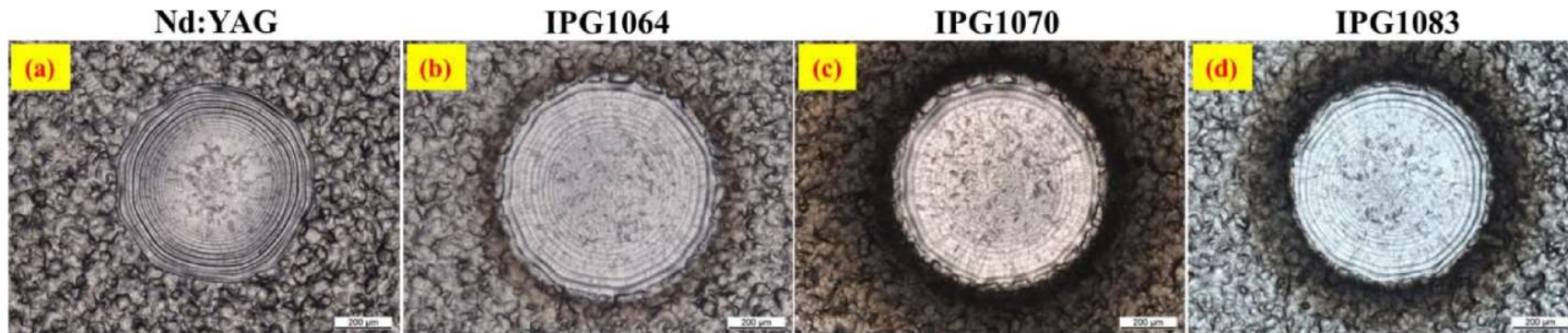
- Object of interest
  - Melt pool
  - Vapor plume
  - Ejected particles
- Properties of the objects
  - Dimension
    - Field of view
    - Type of lens
  - Dynamic behavior
    - Frame rate
    - Exposure time
    - Additional illumination
  - Accessibility
    - Configuration of camera illumination setups.
  - Optical emission/reflection
    - Additional illumination
    - Material for lenses.



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# Plume observation for process development

# Investigation of laser-plume interaction



Application → laser welding of Ti

Approach → move to old Nd:YAG (1064 nm) to new fiber laser

Issue → appearing of **sooth** on the surface of welded titanium when different laser sources are used

Consequences → laser welding quality is questioned

<https://doi.org/10.1016/j.optlaseng.2020.106173>



# Evolution of vapor plumes

1064 nm, 70 W  
3 ms pulse



0 msec

1070 nm, 77 W  
3 ms pulse



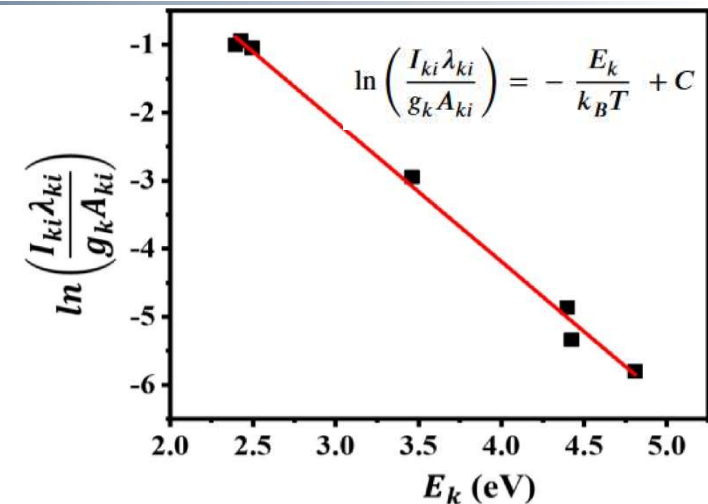
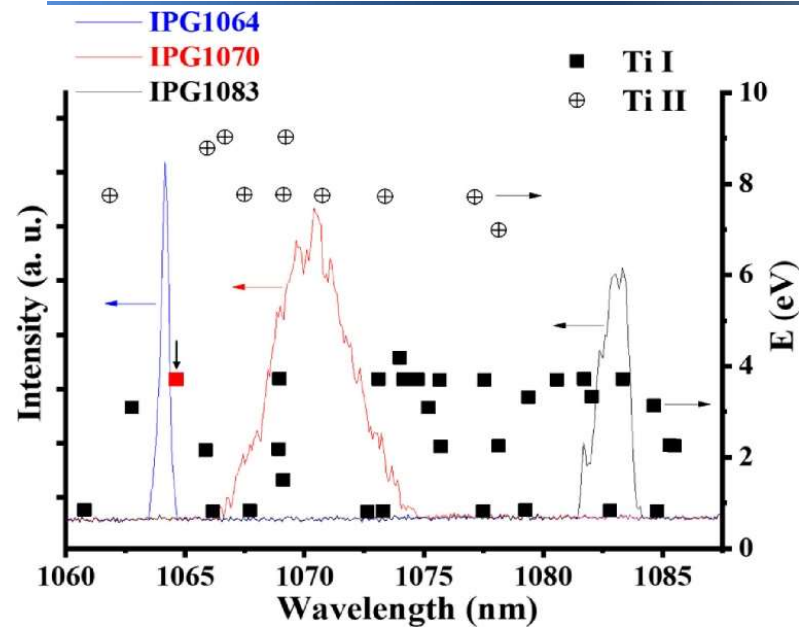
0 msec

- With 1064 nm laser, the plume could travel a larger distance above the surface.
- The plume appears reddish/yellowish for 1064 nm and white for 1070 nm

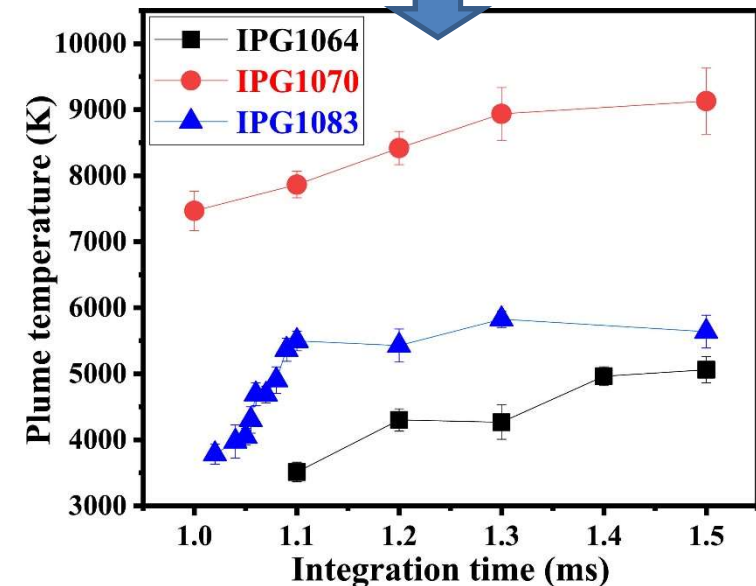


What does it mean  
regarding the temperature ?

# Difference in laser-plume interaction

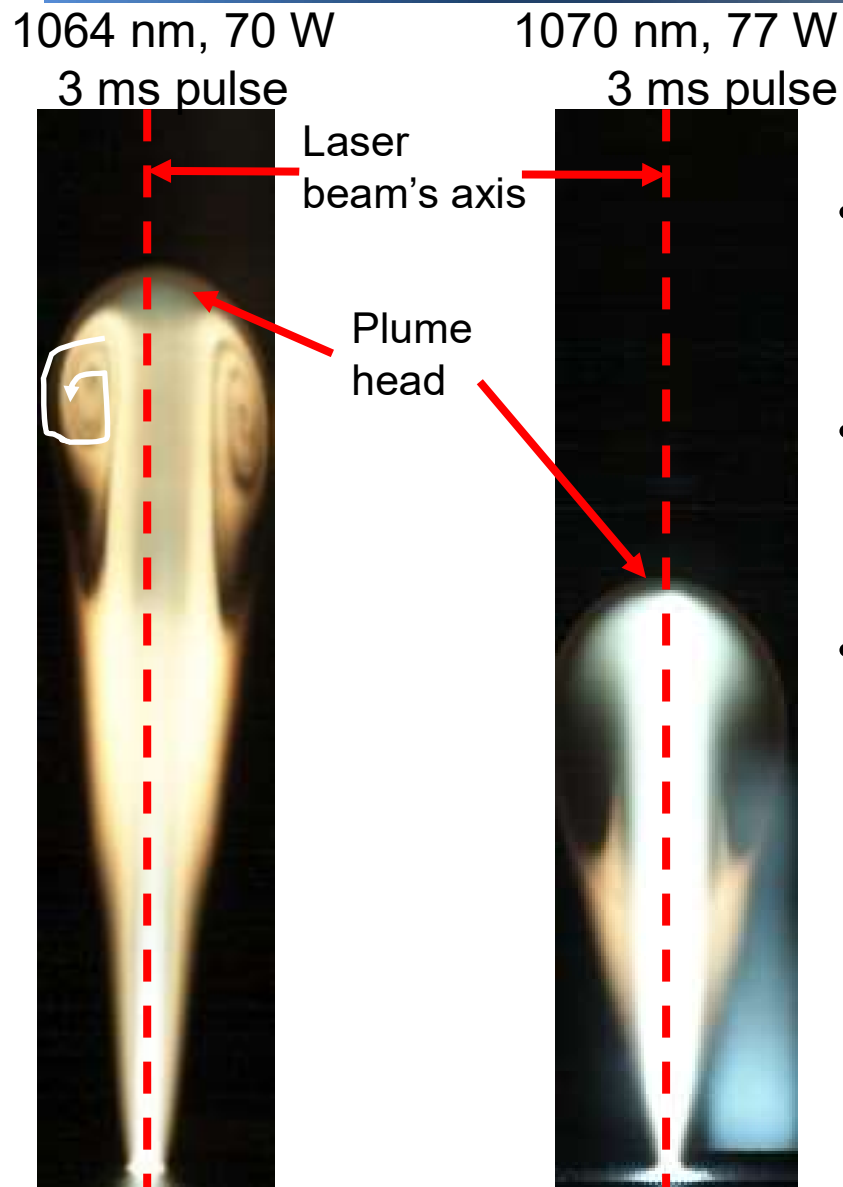


Plume temperature determined using Boltzmann plot method



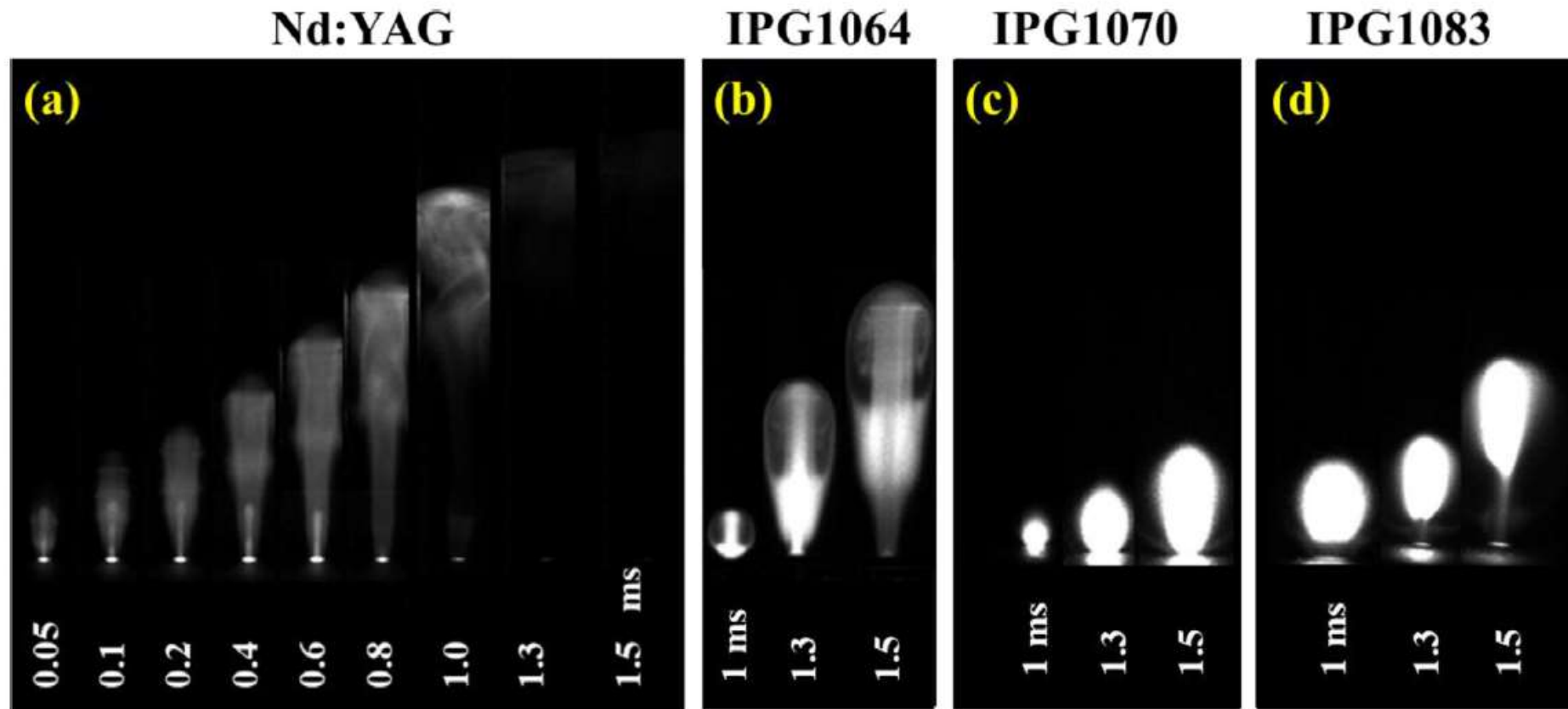
The radiation from IPG1070 and IPG1083 can be easily absorbed by the plume (neutral + single ionized Ti atoms)  
→ The resulting plume has higher temperature

# Difference in laser-plume interaction



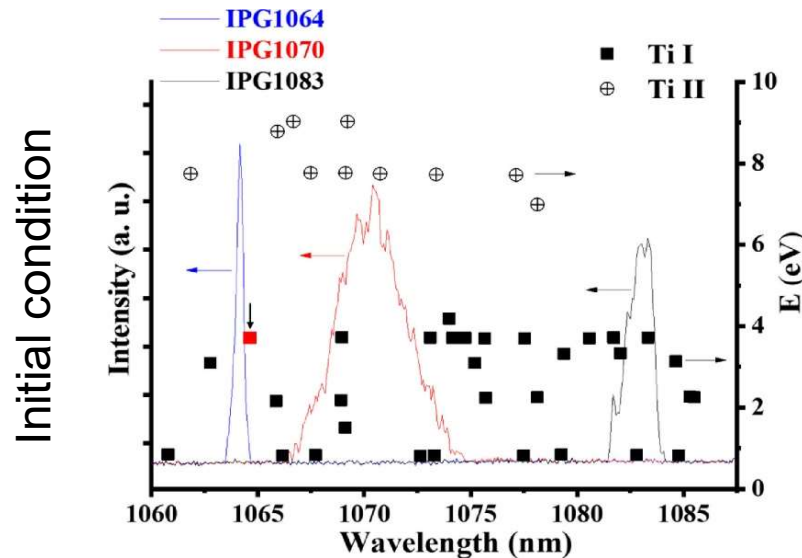
- With 1064 nm laser, plume head has lower temperature due to interaction with cooler atmosphere
- Cooled material in the plume falls down to the side before getting reheated when in contact with the hotter material below
- With 1070 nm, plume head is constantly at high temperature due to the absorption of the incoming laser beam

# Evolution of vapor plumes

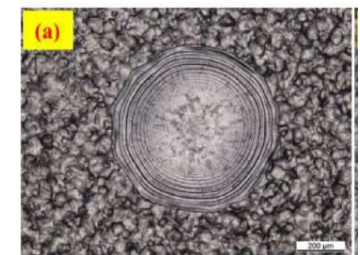
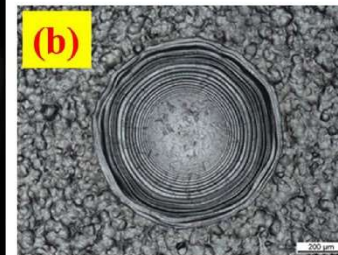
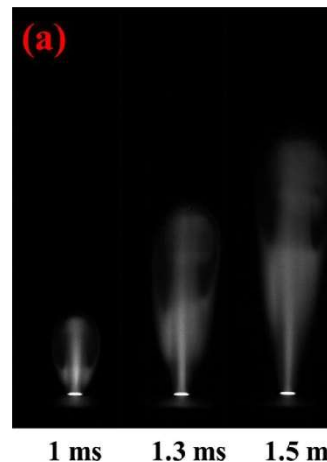
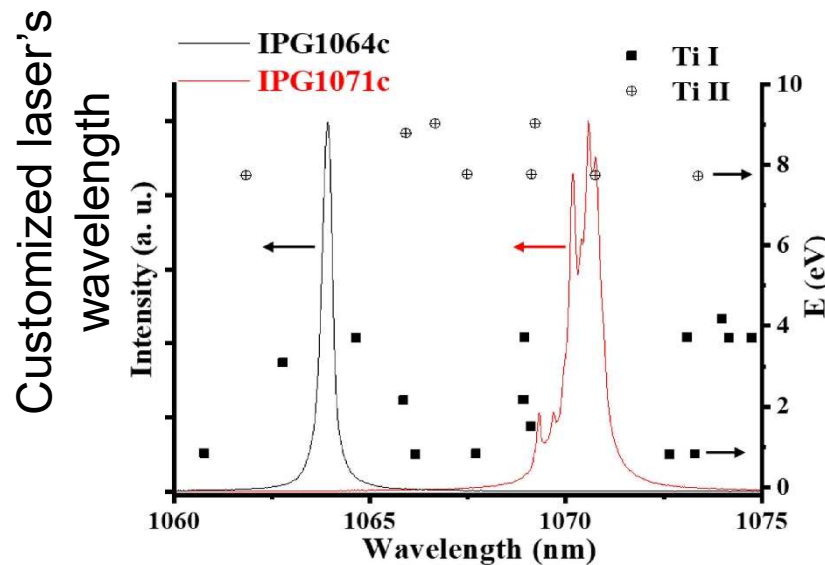


Temporal evolution of the high-speed images of the plume emissions produced by Nd:YAG, IPG1064, IPG1070 and IPG1083 lasers having laser peak power of 1 kW and pulse duration of 1.5 ms from titanium plate

# Influence of laser wavelength (cont.)



New lasers centered at 1064 nm and 1071 nm with smaller distribution  
 → minimal laser absorption by the plume  
 → no soot on the surface.



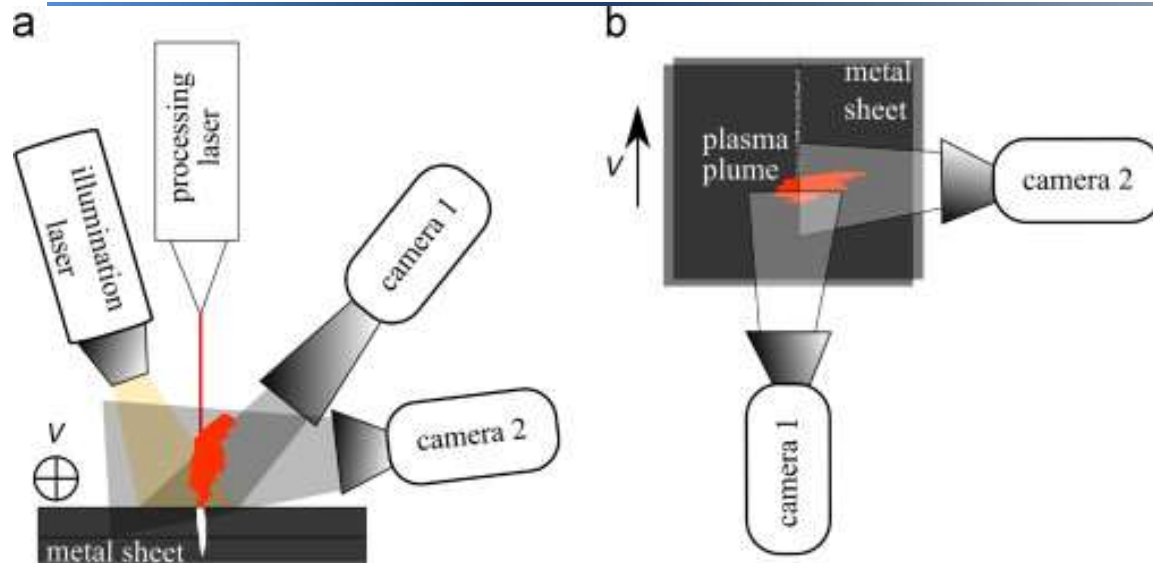
Results of the new 1071 nm and old Nd:YAG

---

# Plume observation for quality monitoring



# Imaging setup

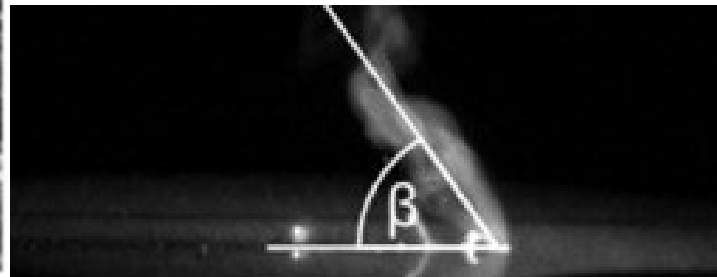
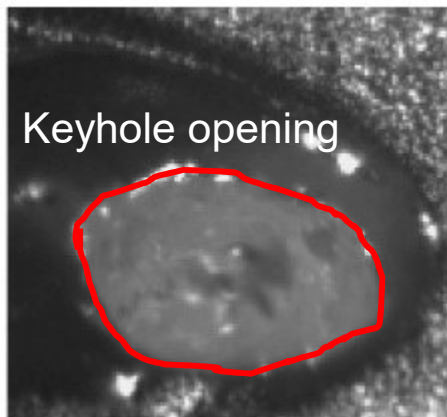


Question:

- Possible to use the plume's visualization to determine process stability?

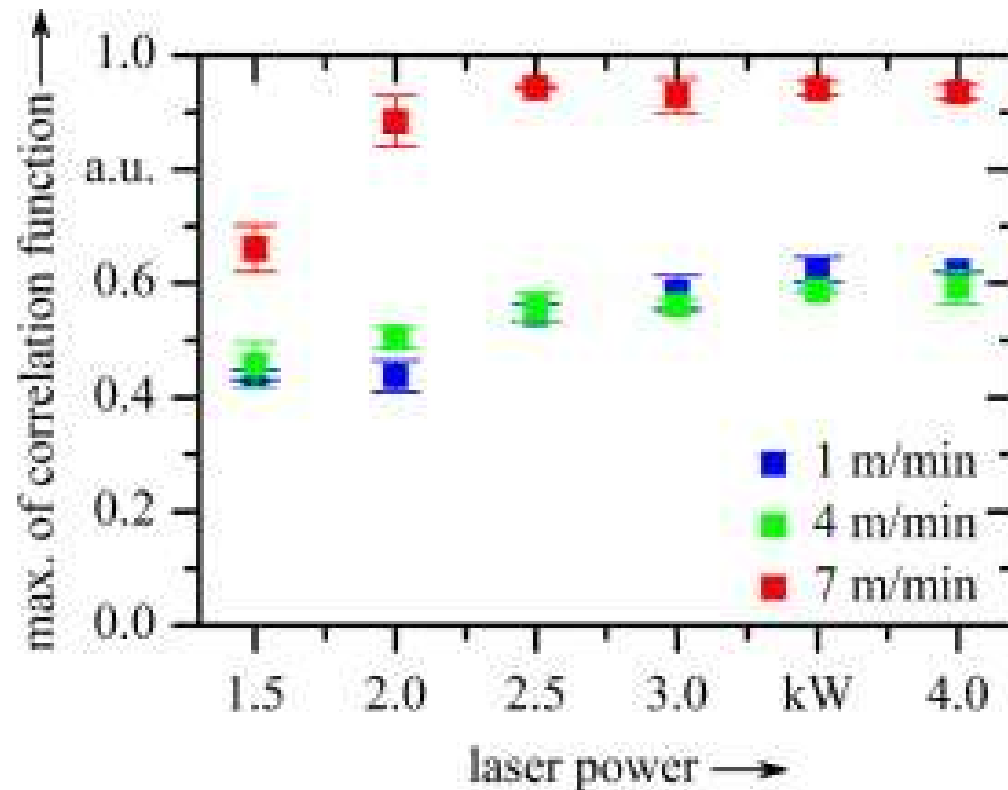
Features of interest:

- surface dimension of the keyhole
- inclination angle of the plume



<https://doi.org/10.1016/j.optlaseng.2014.07.009>

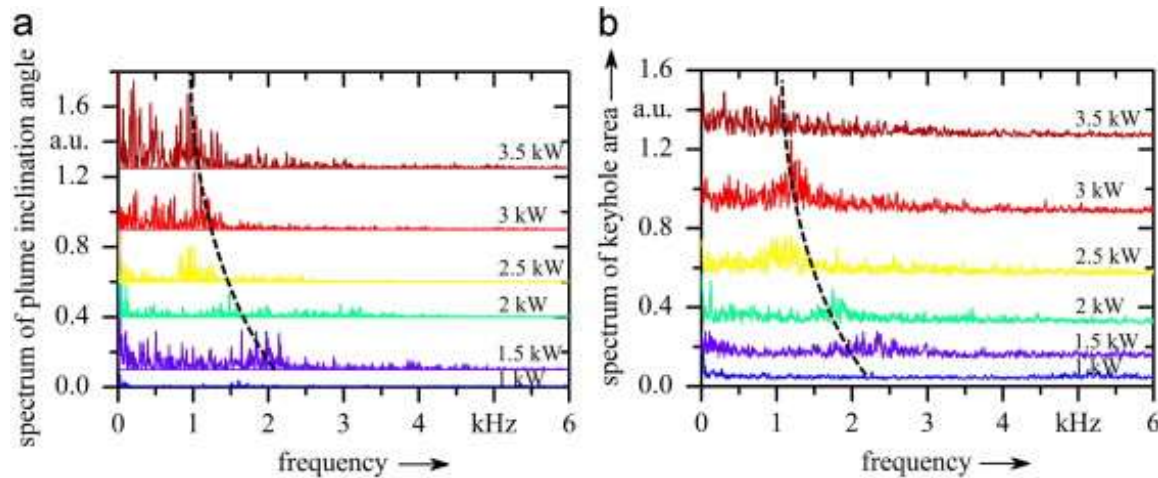
# Correlation between features of interest



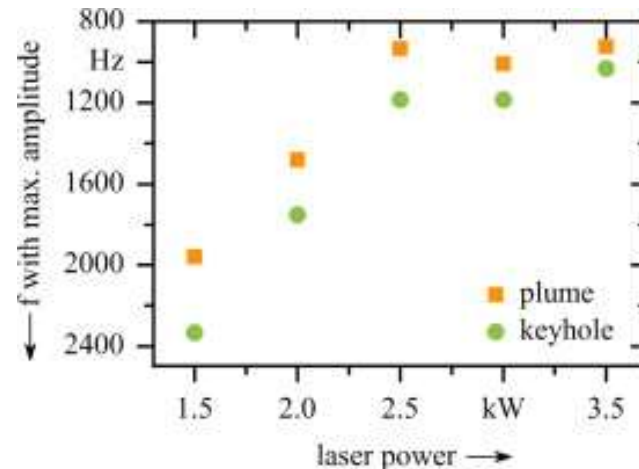
- At 7m/min feed rate, keyhole opening area and plume inclination angle are nicely correlated
- At lower feed rate, keyhole opening area might be also affected by other factors such as flow dynamics of the melt pool

Maximum of the cross-correlation function  
between the keyhole opening area and the plume  
inclination angle for 1, 4 and 7 m/min feed rate

# Stability of the process



(a) FFT spectra of the plume inclination angle and (b) the visible keyhole area for a constant feed rate of 7 m/min. The dashed line indicates the trend of the dominating frequencies (no dominating frequency visible for 1 kW).



- Interestingly, the FFT contents of plume inclination angle and keyhole area have similar dependencies on the laser power and fluctuates at similar dominating frequency contents

- It seems that higher laser power leads to lower frequency of the dominant content.

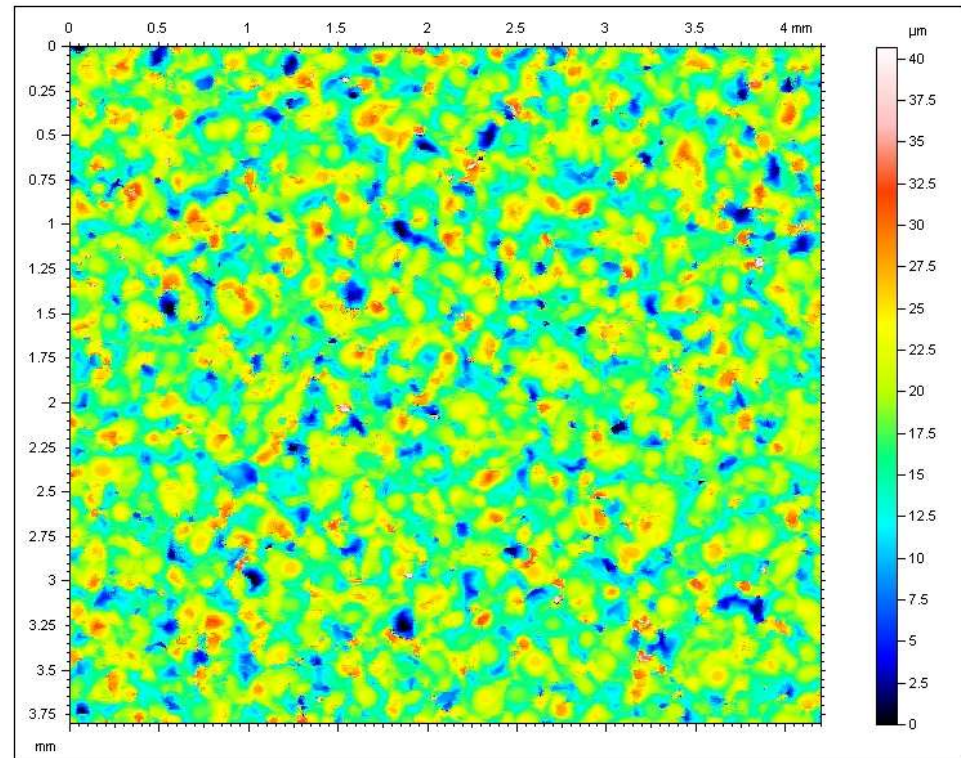
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# Melt pool observation for process development

# Laser polishing of tool steel

**Aim:** Polishing of hardened tool steel for the mould industry, from electrical discharge machined (EDM) rough surface ( $R_a \approx 3.2 \mu\text{m}$ ) to  $R_a \approx 0.3 \mu\text{m}$  → a decrease by a factor of 10

Die sink EDM



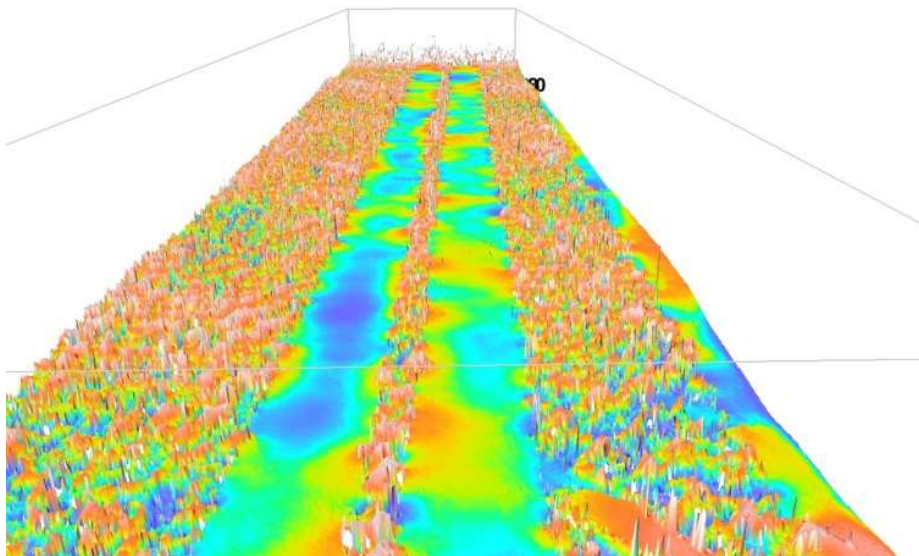
Topographical map of tool steel treated with EDM.

# Laser polishing of tool steel

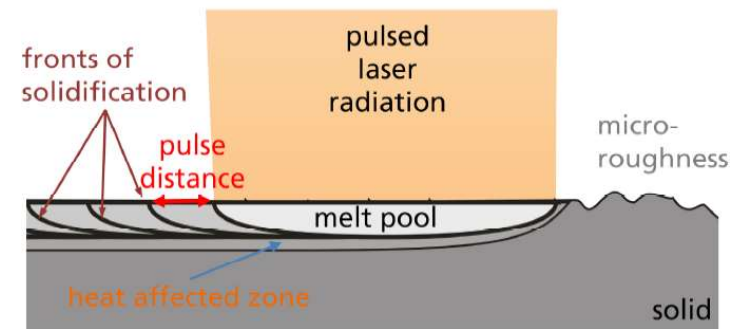
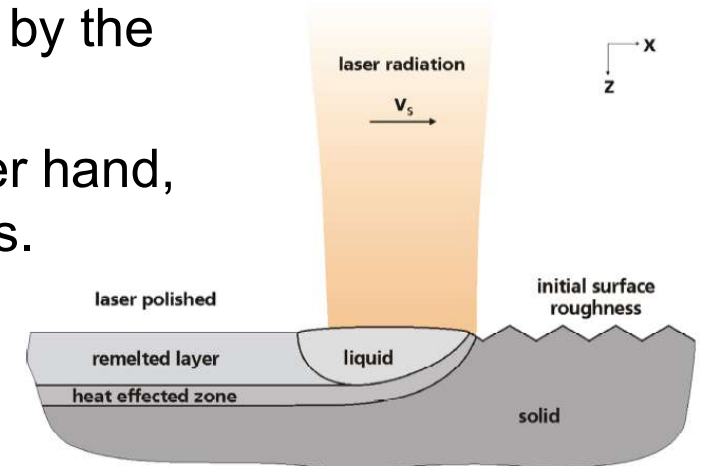
**Surface re-melting** is a part of the laser polishing process

The rough surface of the material is melted by laser radiation. In the liquid state the surface is flattened by the influence of surface tension.

Convective flow or Marangoni effect, on the other hand, can lead to an increase of the surface roughness.



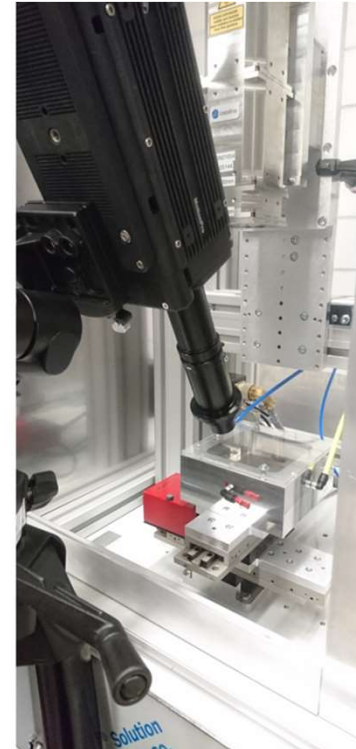
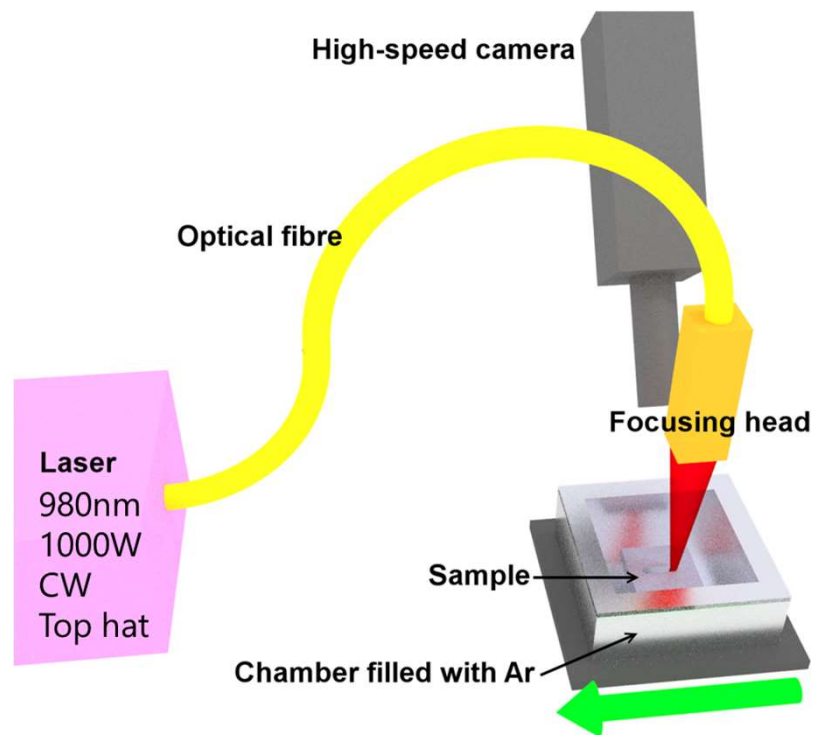
*Surface topography with 2 re-melted lines, in the center*



Temmler A, Willenborg E, Wissenbach K. Laser polishing  
[10.1117/12.906001](https://doi.org/10.1117/12.906001)



# Experimental setup



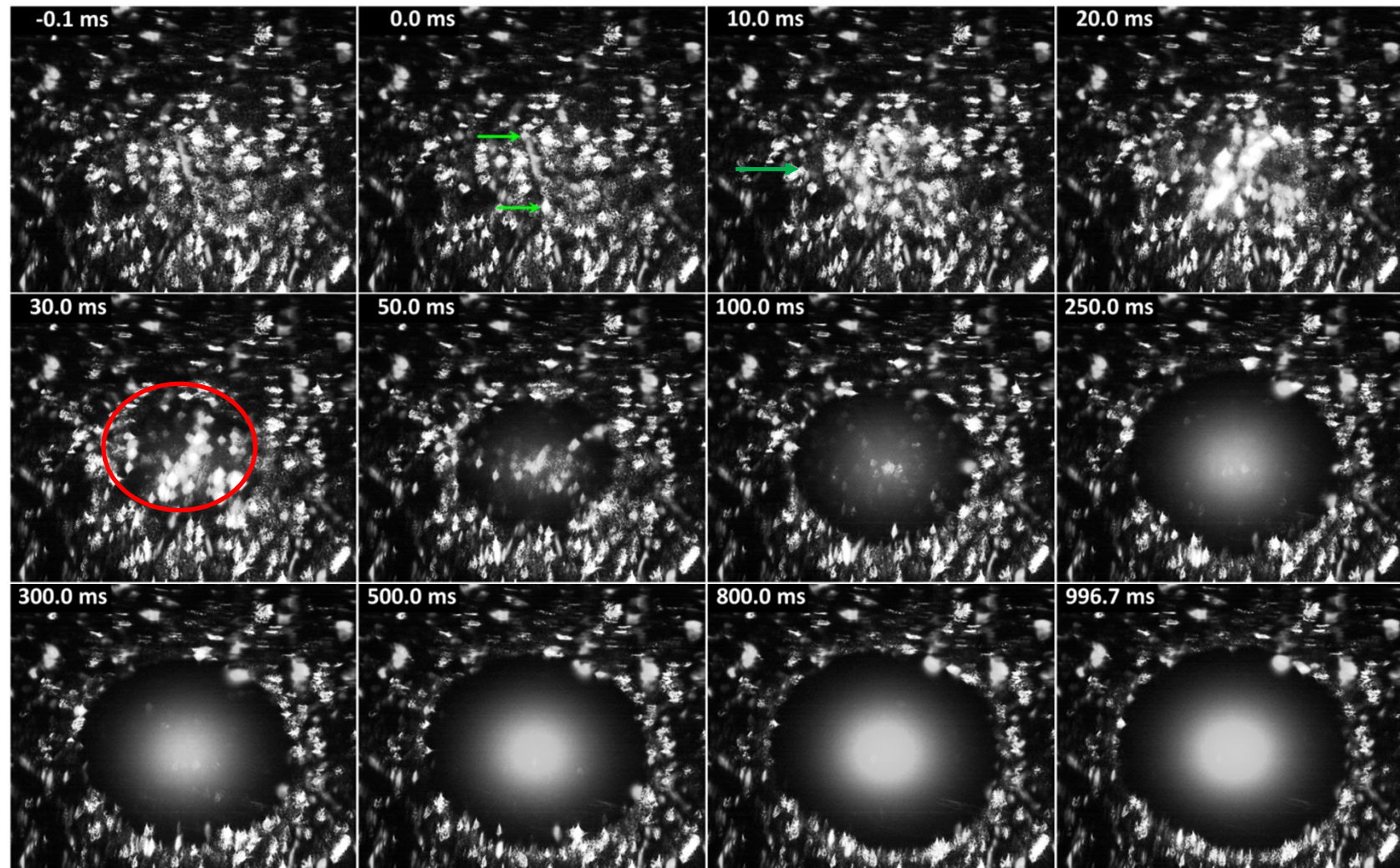
- Observation:
  - High speed camera at 10 kHz
  - A telecentric objective Moritex ML-Z07545 used at 4.5x magnification
  - Low pass filter at 800 nm to cut laser light
  - External illumination by a 532 nm laser

# Evolution of the melt pool for a fixed illumination

- Laser conditions :
  - Wavelength NIR
  - Spot size  $\approx 1$  mm
  - Power  $\approx 300$  W
  - Velocity 0 mm/s
  - Illumination  $\approx 1$  s.
- Observation:
  - High speed camera at 10 kHz
  - With a telecentric objective Moritex ML-Z07545 0.75-4.5x used at the highest magnification (4,5x)
  - Low pass filter at 800 nm to cut laser light
  - External illumination by a 532 nm laser



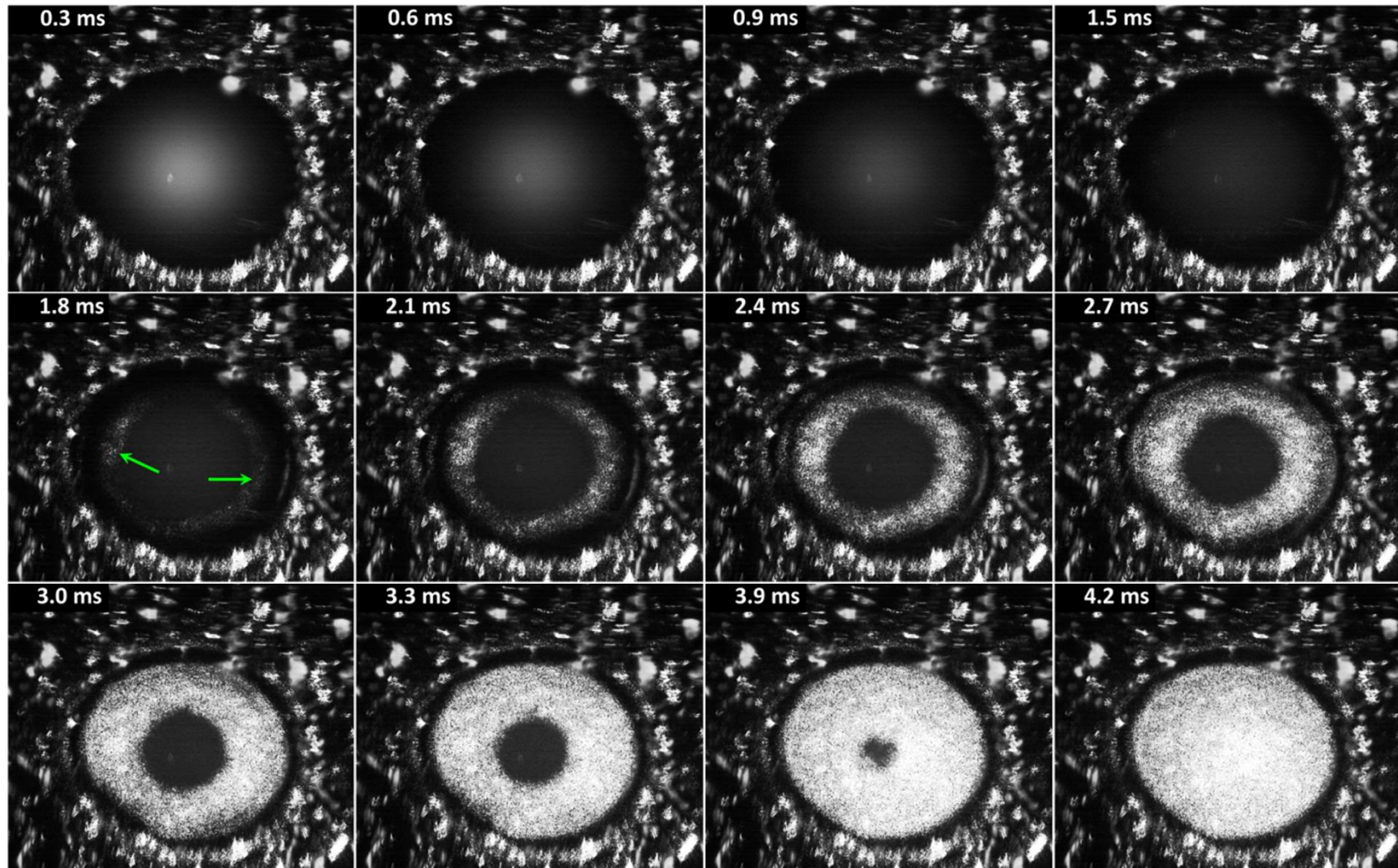
# Evolution of the melt pool for a fixed illumination



Evolution of the melt pool during a static experiment, with a power of 317 W for a duration of 997 ms.

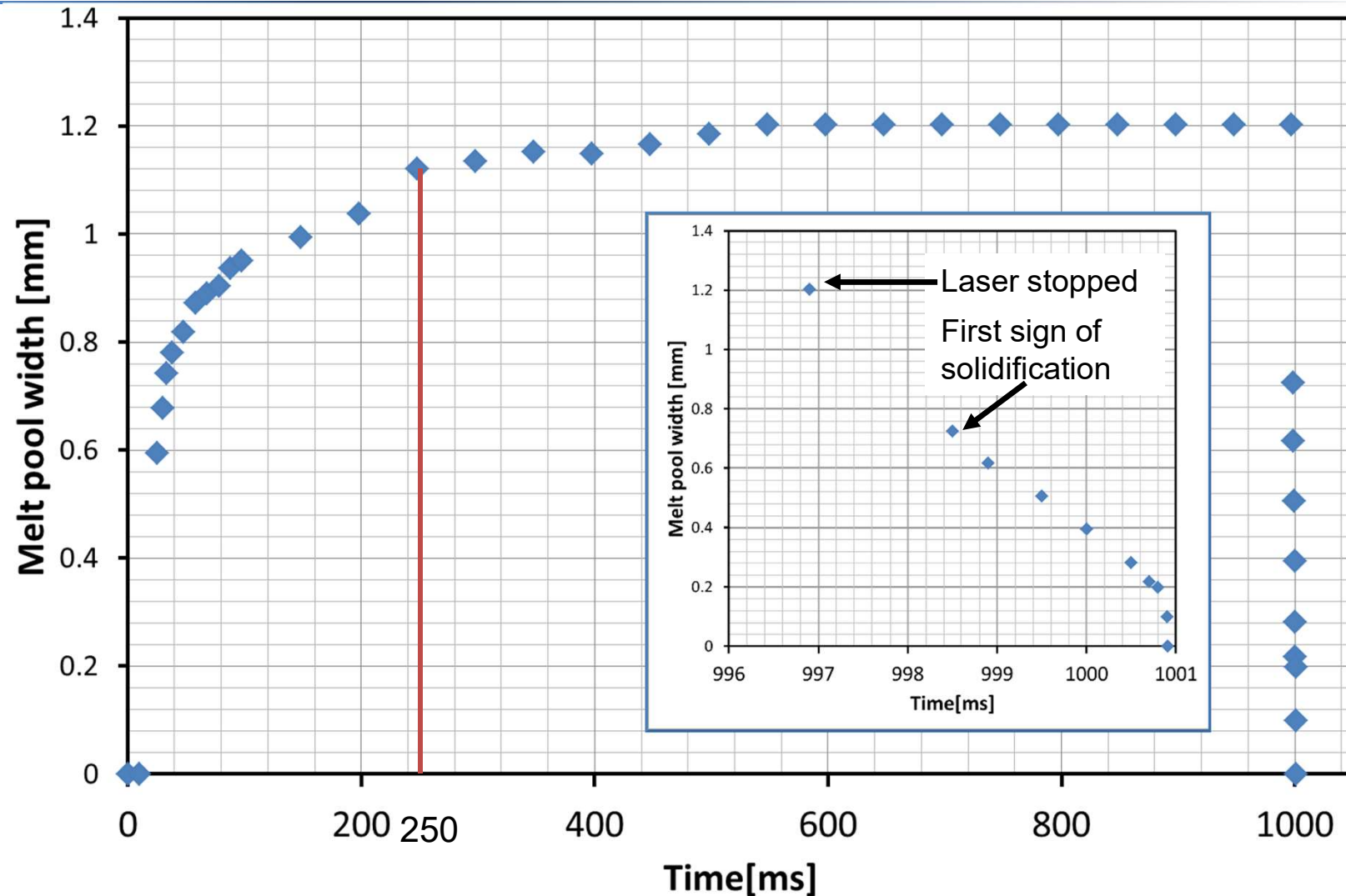


# Evolution of the melt pool for a fixed illumination



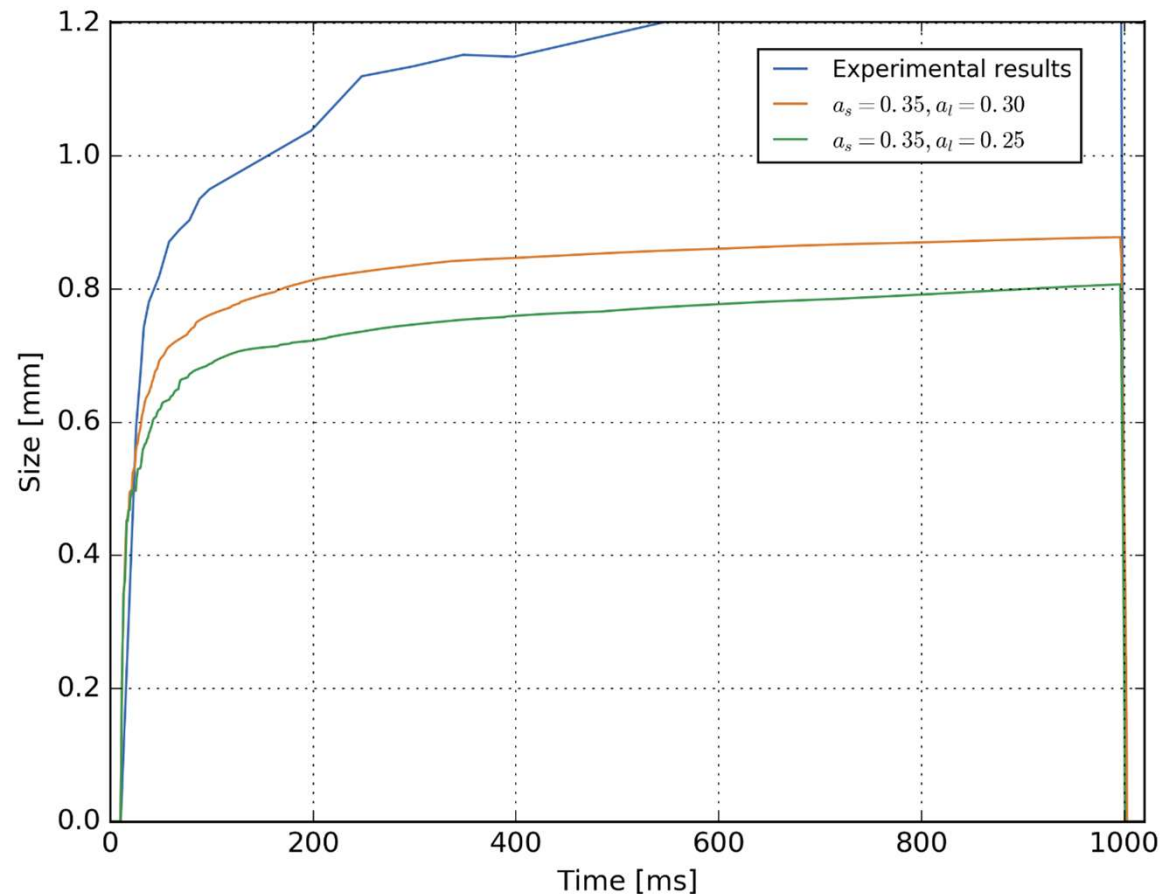
Solidification sequence for the same experiment as in the previous slide. Time stamps are from the end of laser illumination.

# Evolution of the melt pool for a fixed illumination



Evolution of the melt pool with time. Bleu diamonds are the measured data from the high speed images. The inset shows the detail of the solidification.

# Evolution of the melt pool for a fixed illumination simulation vs experiment



Time evolution of the melt pool width. The inset shows the detail of the solidification.  $a_s$  and  $a_l$  are the absorption coefficients in solid and liquid, respectively



# Evolution of the melt pool for a moving sample

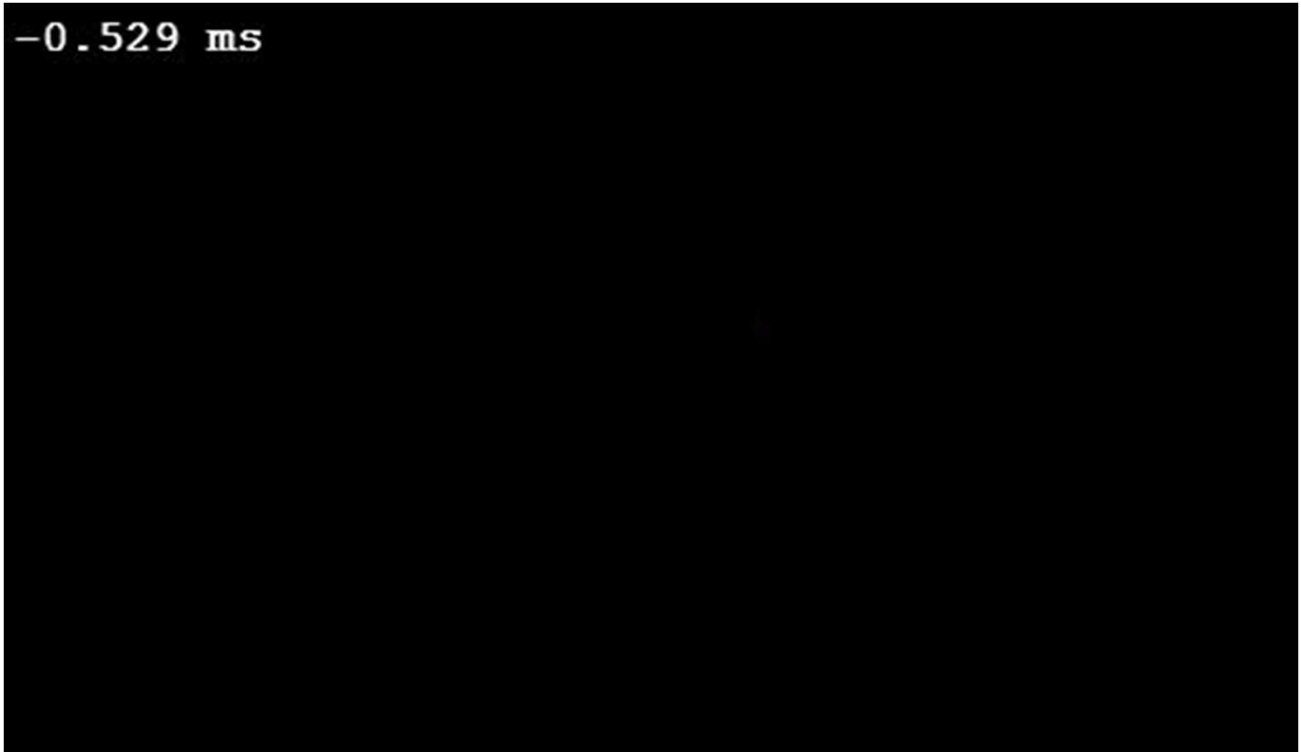
- Laser conditions :

- Wavelength NIR
- Spot size  $\approx 1$  mm
- Power  $\approx 450$  W
- Velocity 50 mm/s
- Illumination  $\approx 1$  s.

- Observation:

- High speed camera at 10 kHz
- With a telecentric objective Moritex ML-Z07545 0.75-4.5x used at the highest magnification (4,5x)
- Red filter (0.3% pass in NIR)

-0.529 ms



# Evolution of the melt pool for a moving sample – return with 90% overlap

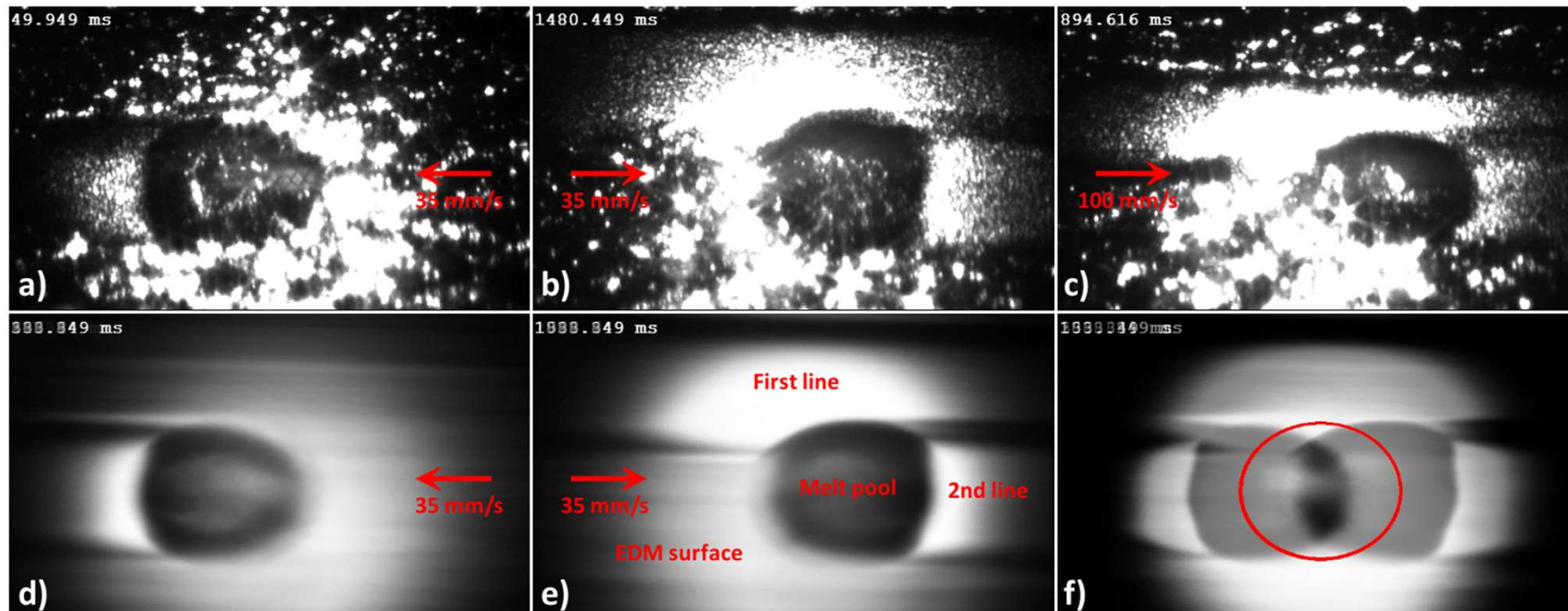
- Laser conditions :
  - Wavelength NIR
  - Spot size  $\approx 1$  mm
  - Power  $\approx 450$  W
  - Velocity 50 mm/s
  - Illumination  $\approx 1$  s.

- Observation:
  - High speed camera at 10 kHz
  - With a telecentric objective Moritex ML-Z07545 0.75-4.5x used at the highest magnification (4,5x)
  - Red filter (0.3% pass in NIR)

914.471 ms

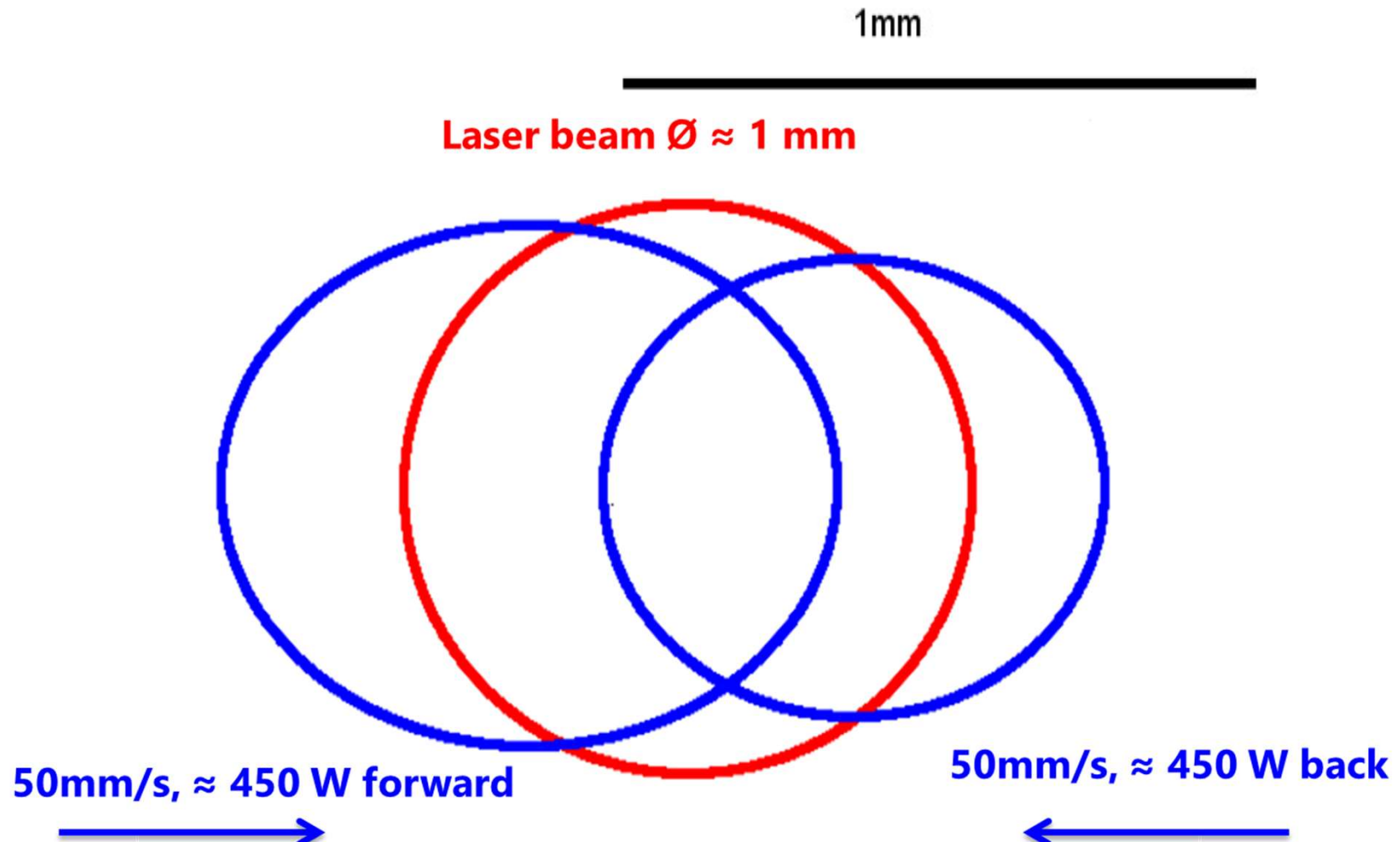


# Evolution of the melt pool for a moving sample

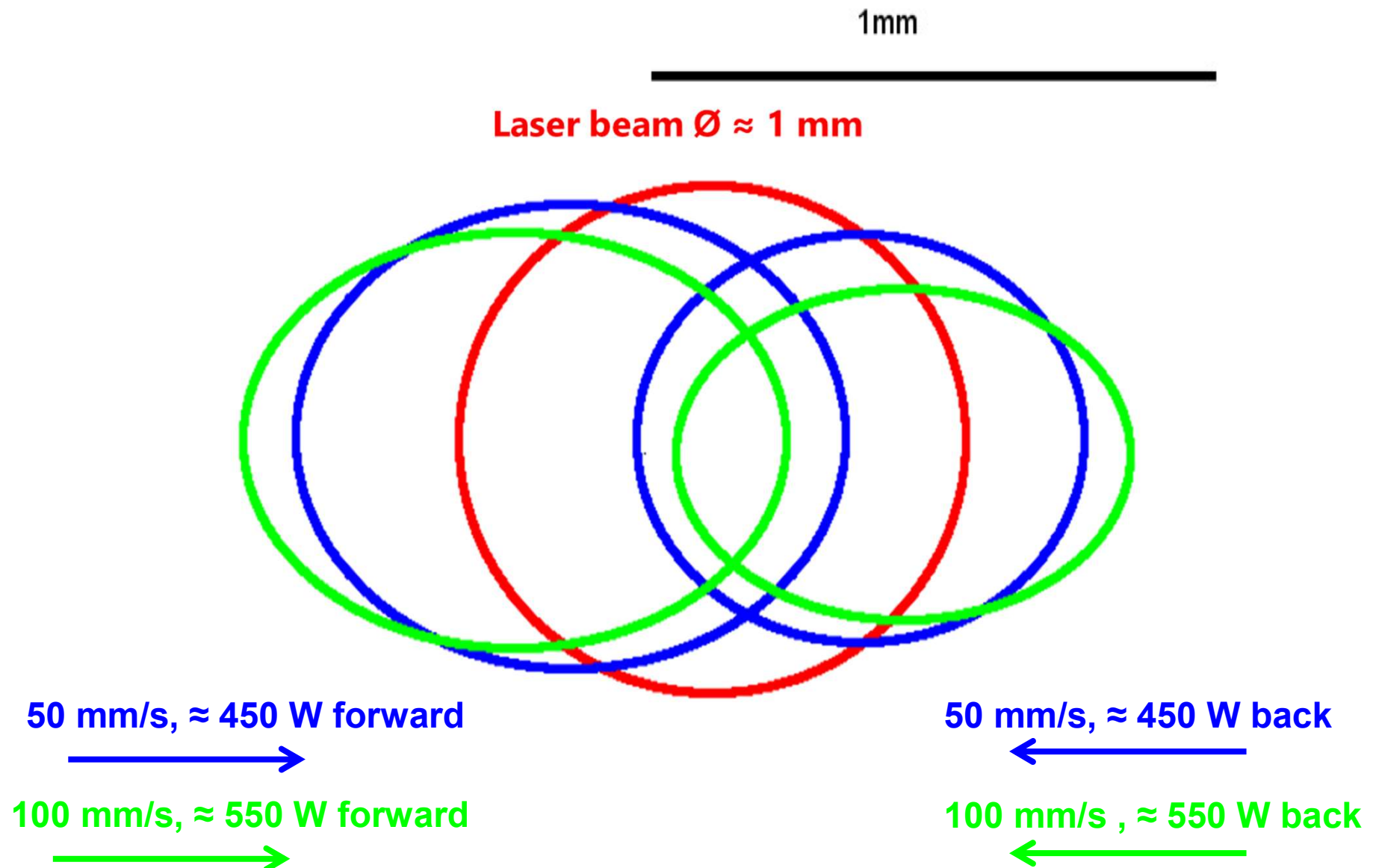


a) First line at 35 mm/s and 415 W. b) Second line with an overlap of 30% also at 35 mm/s and 415 W. c) Second line at 100 mm/s and 561 W. d) Average of the light intensity of all image for the first line at 35 mm/s and 415 W. e) Average of the light intensity of all image for the second line at 35 mm/s and 415 W. f) Combination of 50% d) and 50% e). For a scale indication, the ellipses in *f* represent the spot diameter of 0.9 mm and so main axes gives the scale in *x* and *y*-directions. All images have the same scale.

# Evolution of the melt pool for a moving sample

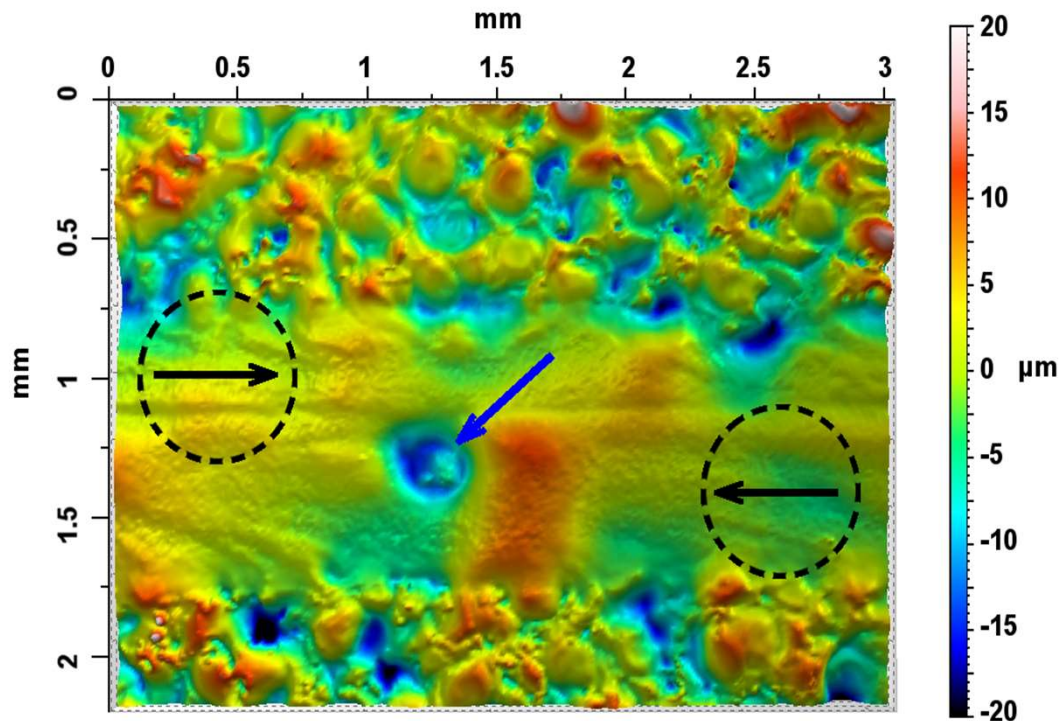


# Evolution of the melt pool for a moving sample





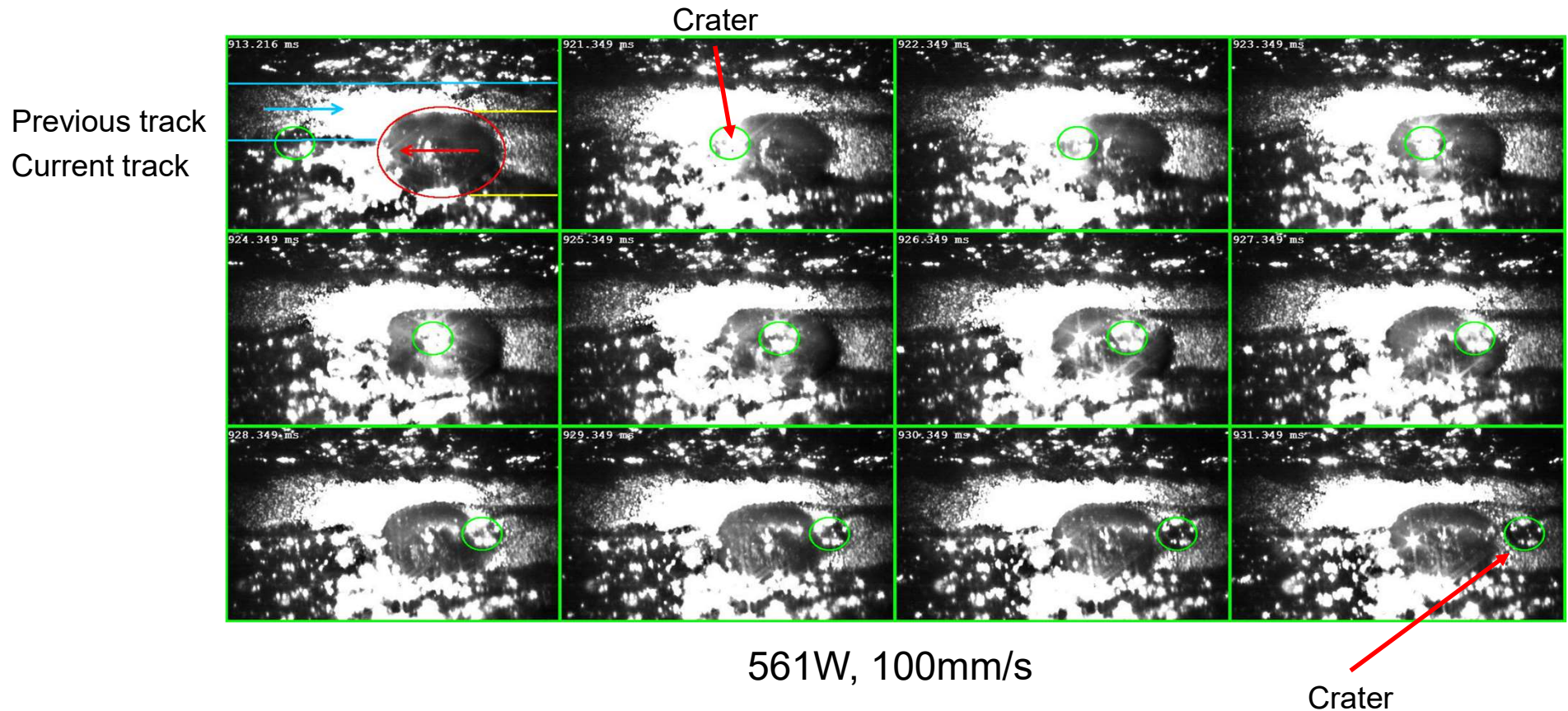
# Issues with laser polishing of EDM surfaces



- Presence of craters on the laser polished surface
- The craters cannot be removed by the melting process

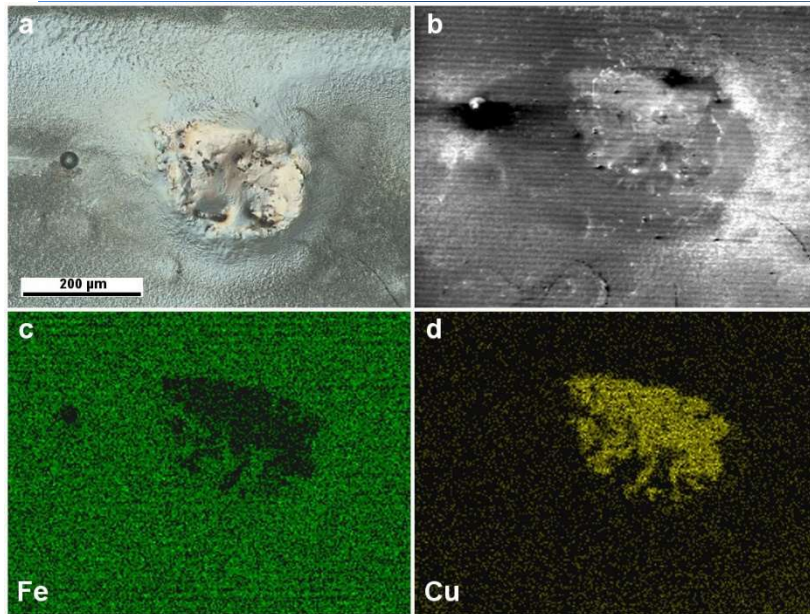
Topographical map of a crater (indicated by blue arrow) observed on sample treated at a speed of 100 mm/s and laser power of 561 W. The melt track was made by two consecutive laser scans, whose directions are indicated by the arrows. The dashed circles approximate the dimension of the melt pool.

# Interaction between the crater and the melt pool



- The crater seems not melted during the interaction with the melt pool.
- The crater shows high optical reflectance.
- Size of the melt pool slightly decreased when the crater is within the melt pool.

# Origin of the crater



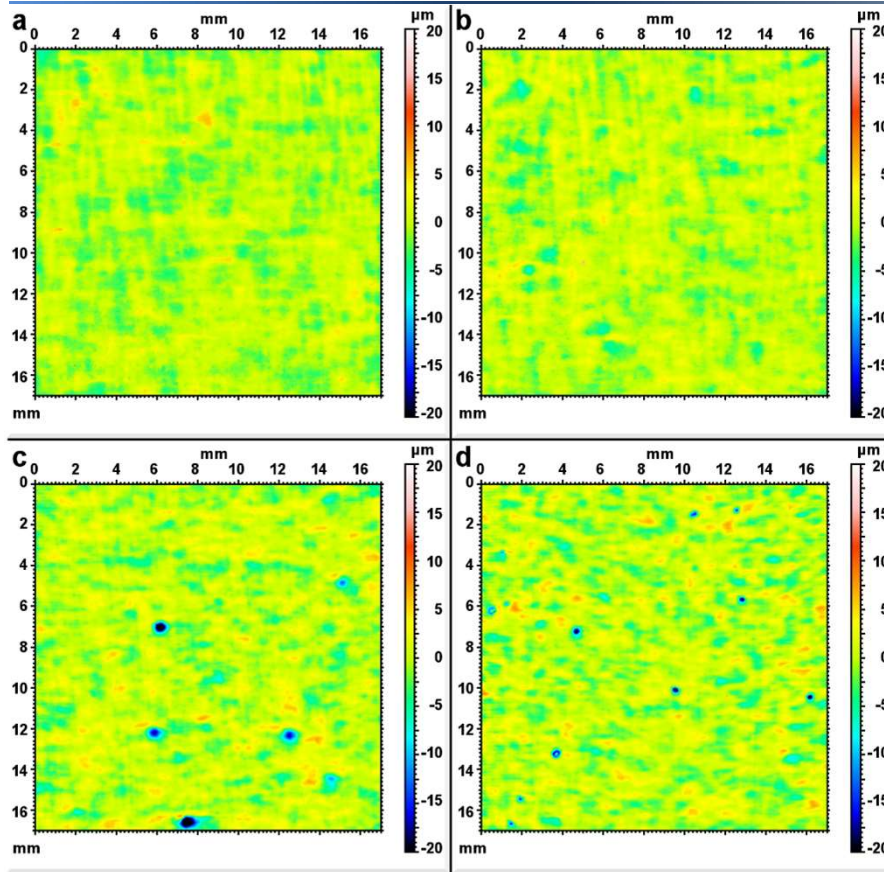
- Copper (Cu) detected at the craters.
- Cu likely came from the electrodes used in the EDM process.
- Cu has very high reflectance ( $> 90\%$ ) →
  - Likely to be melted by heat transfer from the molten stainless steel.
  - Can reduce the total absorbed laser energy → reduce melt pool temperature and size.

(a) Light microscope, (b) SEM, (c) and (d) SEM+EDX

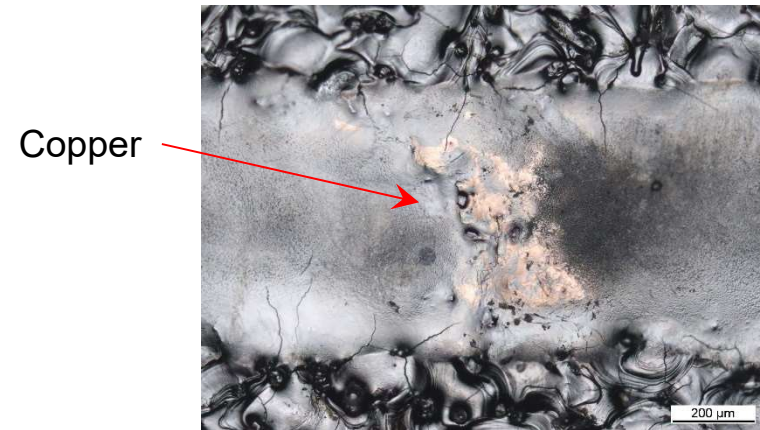
| Surface treatment | C<br>(at.%) | Si<br>(at.%) | Mn<br>(at.%) | Cr<br>(at.%) | Mo<br>(at.%) | Ni<br>(at.%) | Cu<br>(at.%) | Fe<br>(at.%) |
|-------------------|-------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| EDM               | 1.680       | 0.901        | 0.273        | 4.847        | 1.274        | 0.206        | 1.440        | 88.630       |
| Mechanical        | 0.417       | 0.849        | 0.333        | 5.007        | 1.253        | 0.227        | 0.066        | 91.150       |



# Influence of scanning velocity



Topographical maps of 17x17mm<sup>2</sup> realized on the same sample for (a) 415 W, 35 mm/s, (b) 454 W, 50 mm/s, (c) 561 W, 100 mm/s and (d) 651 W, 150 mm/s with a spacing between the lines of 90  $\mu$ m.



454 W, 50mm/s

How to remove the crater?

- Use very high laser power → ?
- Change laser => green laser → ?
- Change scanning velocity → ?
- At low velocity, no crater was observed and the copper trace seems to be melted
- At velocity above 50 mm/s  
→ increased amount of craters

# Challenges in imaging of melt pool



Speckle

Melting start

Melt pool

High-speed images during laser melting; 532 nm laser as illumination source  
Melt pool > 1 mm in diameter

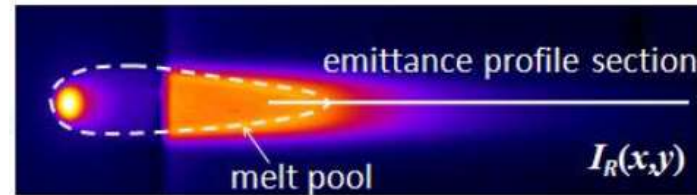
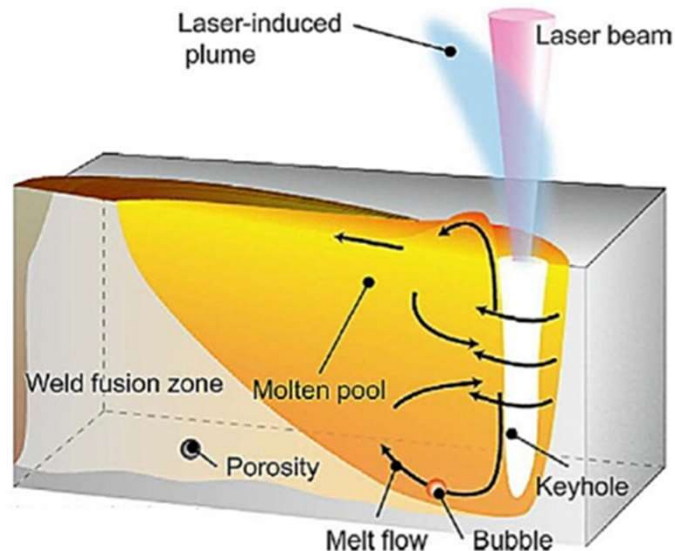
- Speckle pattern within the illuminated spot
- Speckle due to the interference on the image plane of the laser light scattered/reflected from the surface
- Speckle pattern depends on illumination wavelength, viewing angle, roughness of the surface....



**Speckle is significant when observing small melt pool, i.e. 30–100  $\mu\text{m}$**



# Challenges in imaging of melt pool

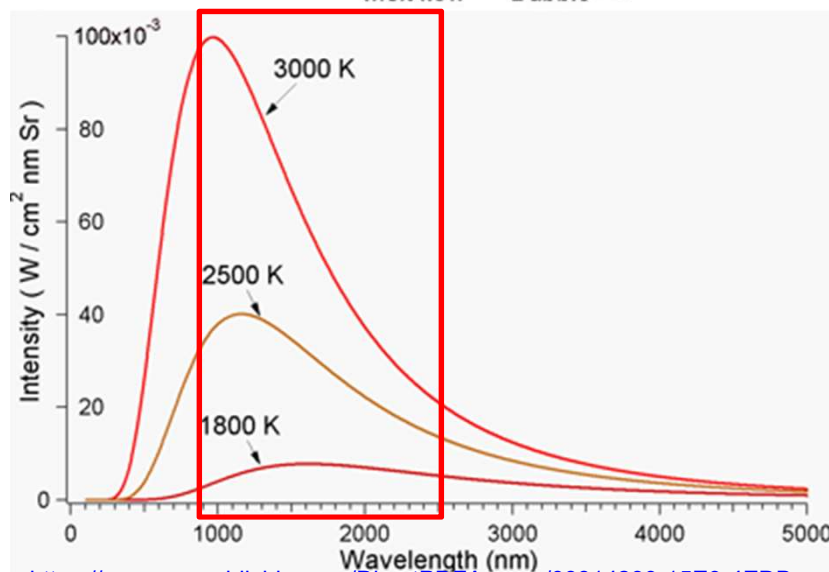


Black-body radiation as light source:

- Limited only to the hottest part of the melt pool
- Possible optical chromatic aberration due to the broad spectral range of emission
- Low imaging resolution if only NIR wavelength is used (thermal camera)
- Visual accessibility affected by the irradiating plume

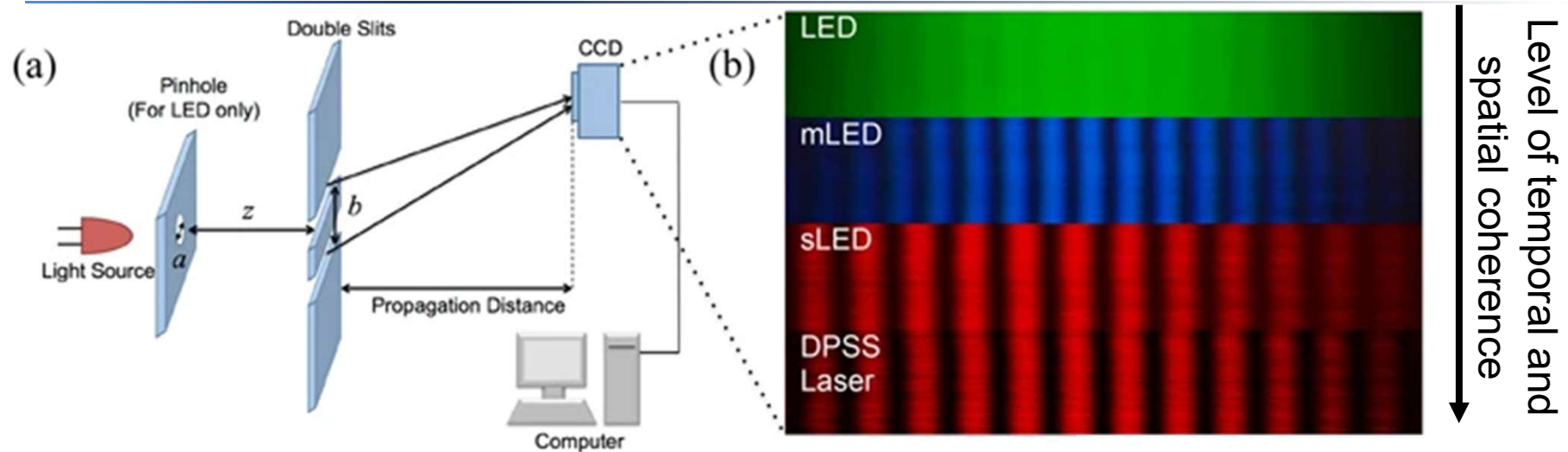


**Powerful external illumination source**



[https://www.osapublishing.org/DirectPDFAccess/03814239-15E9-4EDB-BA9FB0FE86FF90DA\\_367322/oe-25-12-13539.pdf?da=1&id=367322&seq=0&mobile=no](https://www.osapublishing.org/DirectPDFAccess/03814239-15E9-4EDB-BA9FB0FE86FF90DA_367322/oe-25-12-13539.pdf?da=1&id=367322&seq=0&mobile=no)

# Choice of illumination source



Interference is more significant with increasing level of coherence in light source.

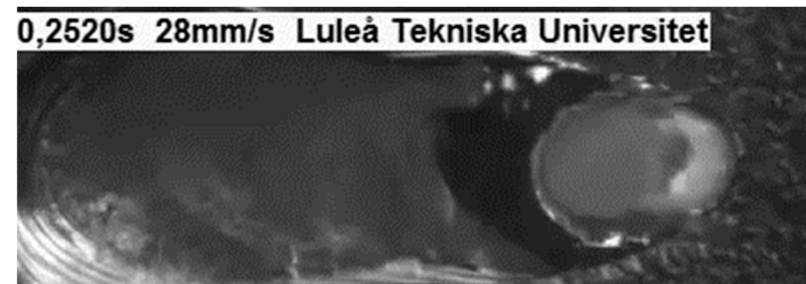
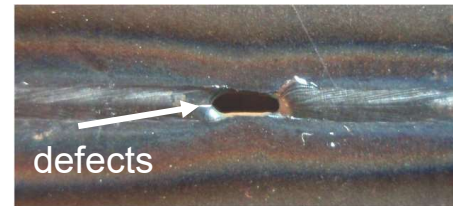


**Use of incoherent light source**

# High speed imaging of melt pool



Keyhole observation



Defect formation in  
laser welding

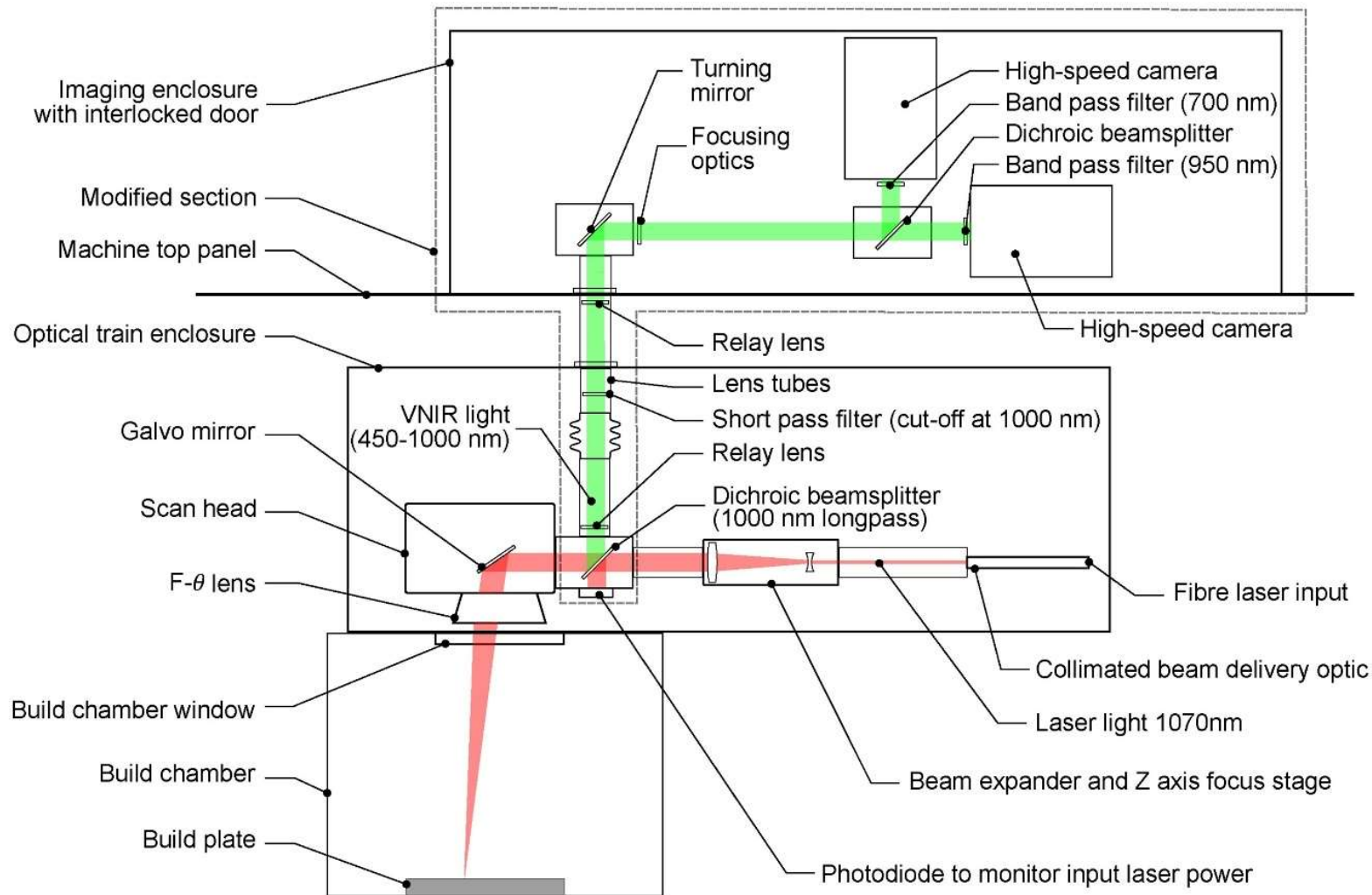
Visualization at much higher frame rate  
and better spatial resolution thanks to  
the powerful incoherent illumination  
source.



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# Thermal imaging for process development and monitoring

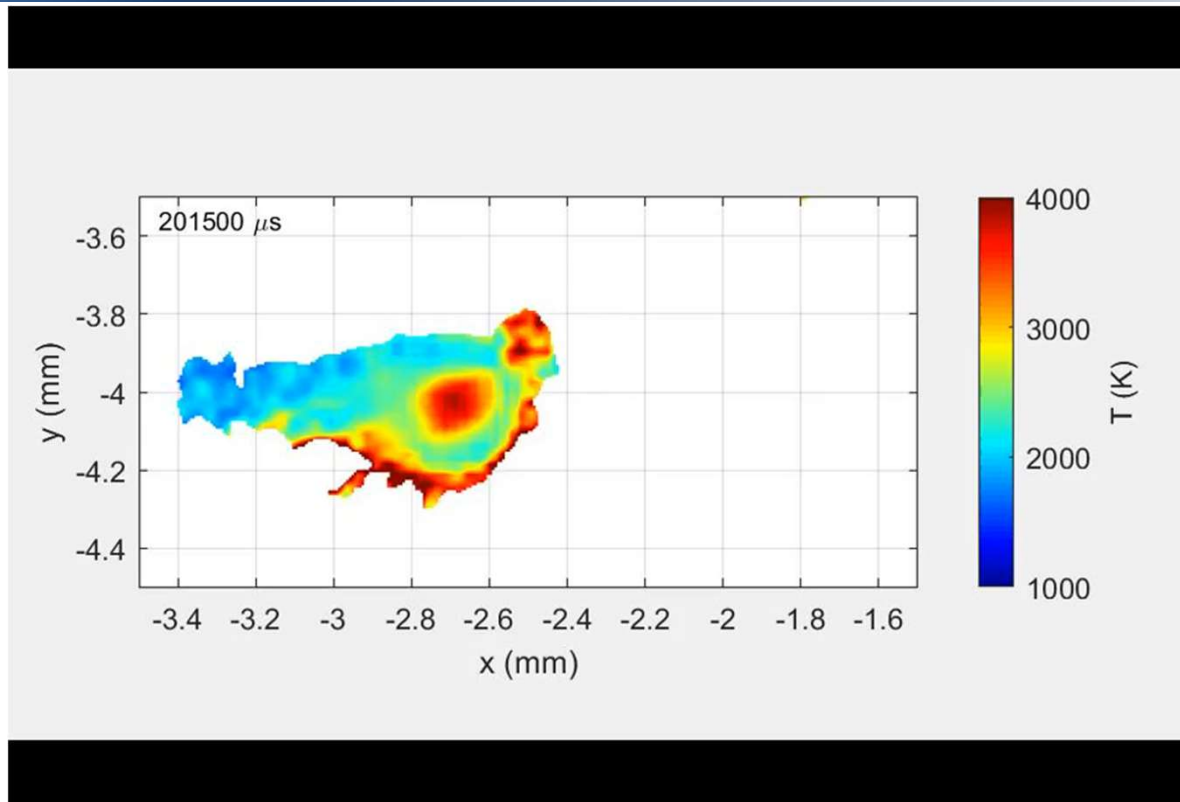
# Thermal imaging setup for powder bed fusion



<https://www.sciencedirect.com/science/article/pii/S221486041830188X>



# Thermal imaging of the process zone



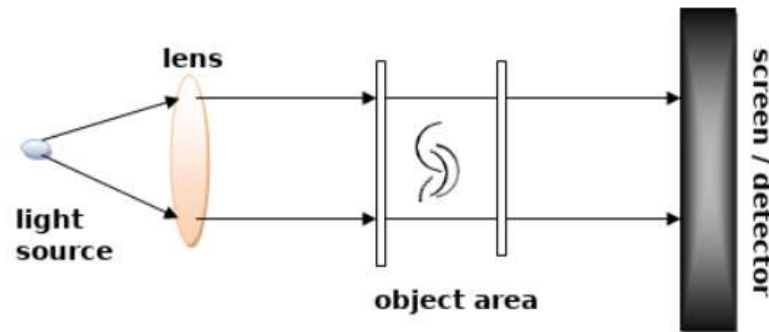
- Obtained information: temperature distribution in the melt pool, profile of the melt pool, cooling rate, spatters, ejections
- Limitations: uncertainty in emissivity value, possibility of vapor plume and spatters hindering the observation of the melt pool.

<https://www.sciencedirect.com/science/article/pii/S221486041830188X>

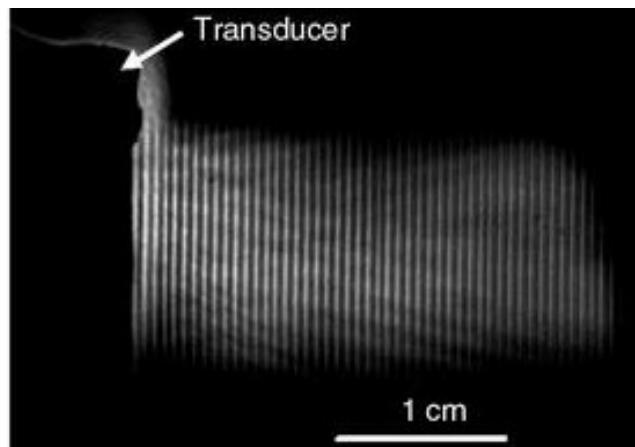
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## 4. Phase-contrast imaging

# Phase-contrast imaging



- Based on the differences in optical properties of the object as compared to the surrounding.
- Objects: vapor plume, processed zone, ejected materials and airborne shockwave.
- Information about the volumetric behaviors.

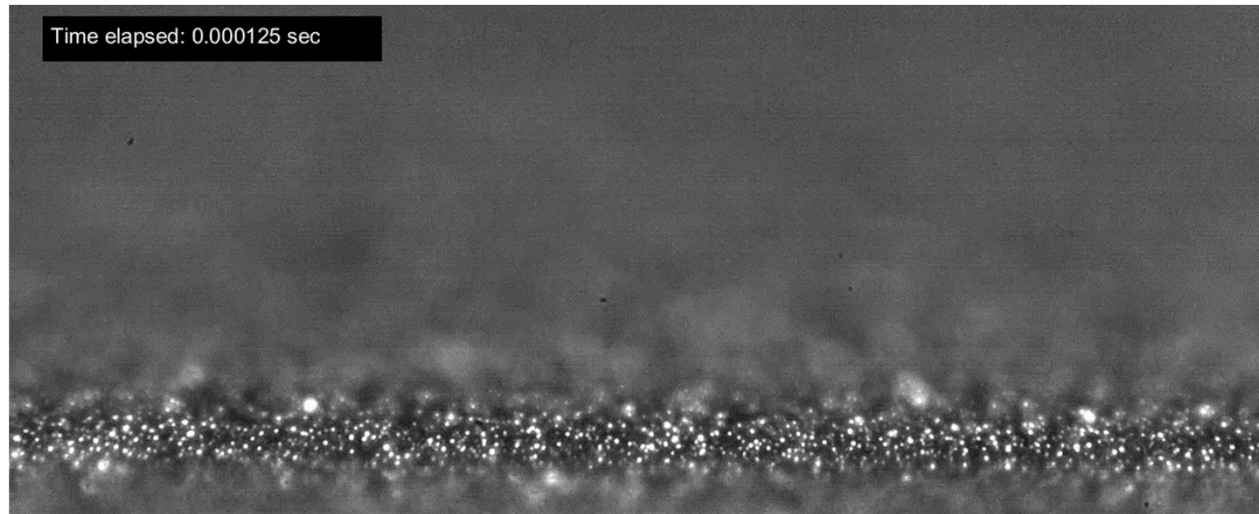


[https://ecap.nat.fau.de/wp-content/uploads/2019/02/2019\\_Akstaller\\_MA.pdf](https://ecap.nat.fau.de/wp-content/uploads/2019/02/2019_Akstaller_MA.pdf)

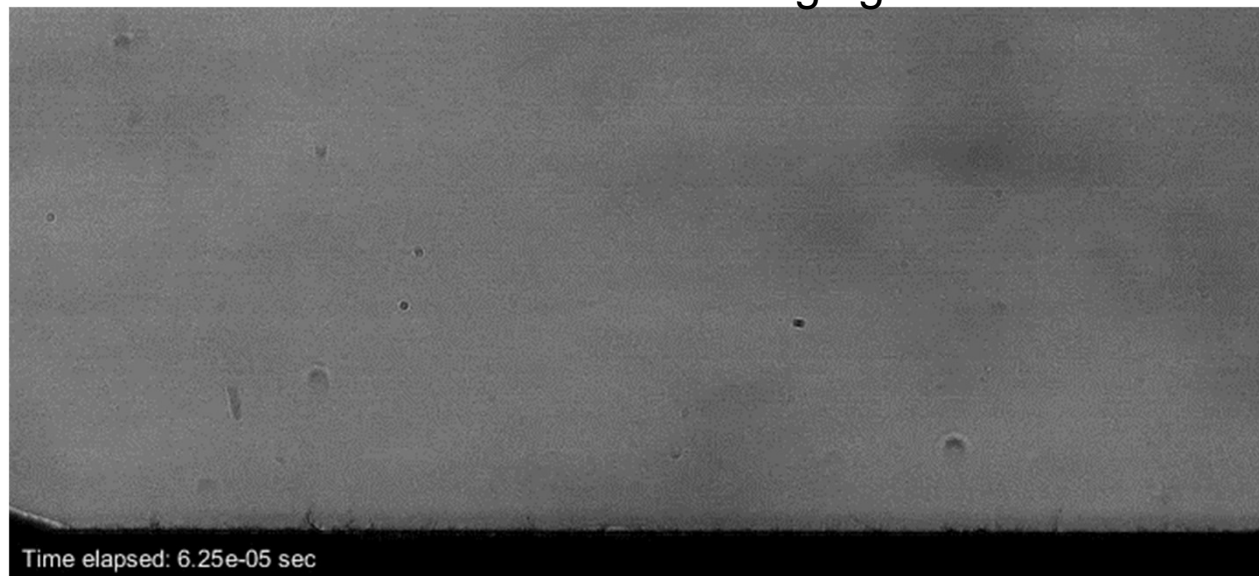


<https://gfycat.com/discover/schlieren-gifs>

# Conventional vs phase-contrast imaging



Conventional imaging

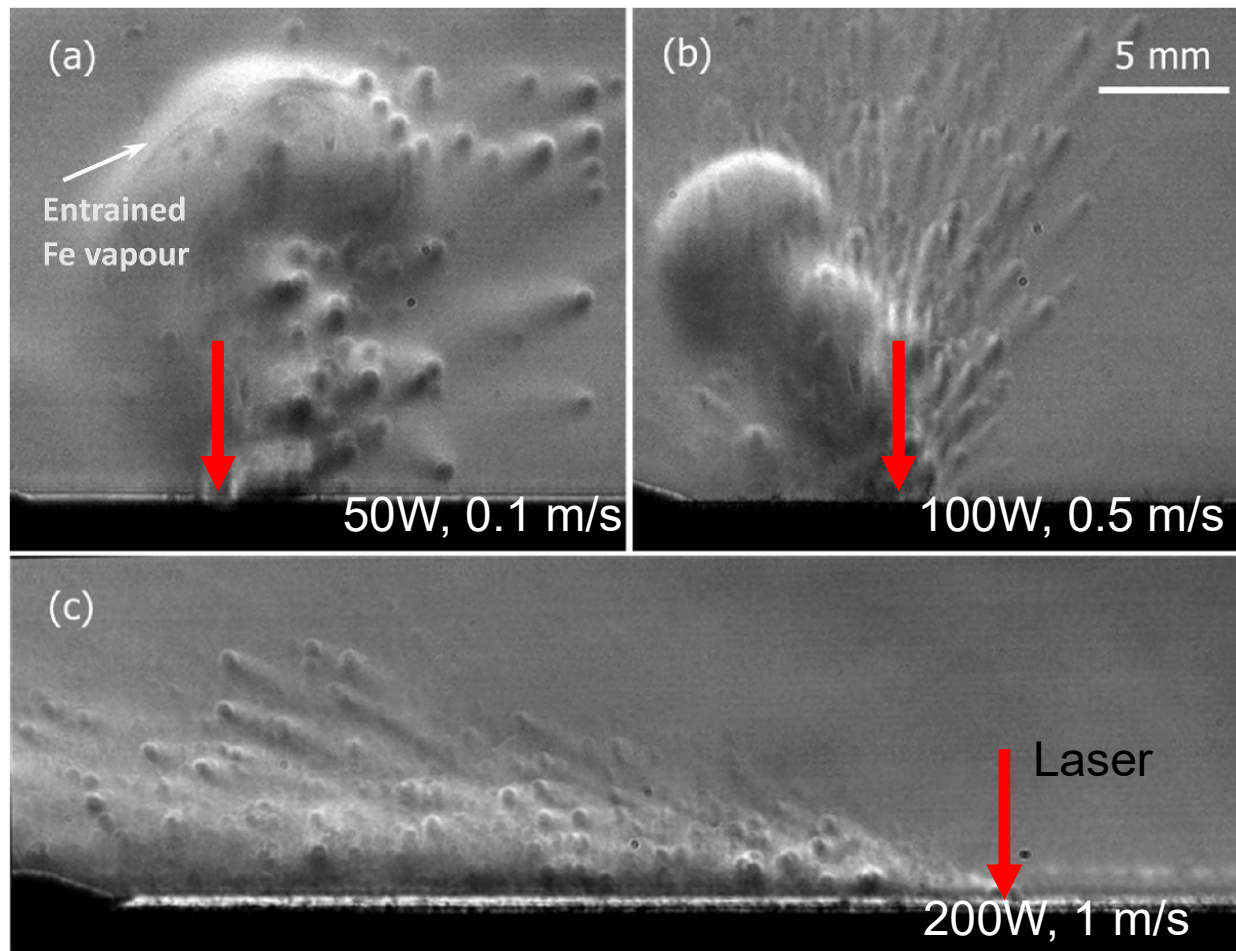


Phase-contrast imaging

- Phase-contrast imaging provides better visualization of the atmospheric regions with changes in refractive index.

<https://doi.org/10.1016/j.actamat.2017.09.051>

# Influence of process conditions on gas flow

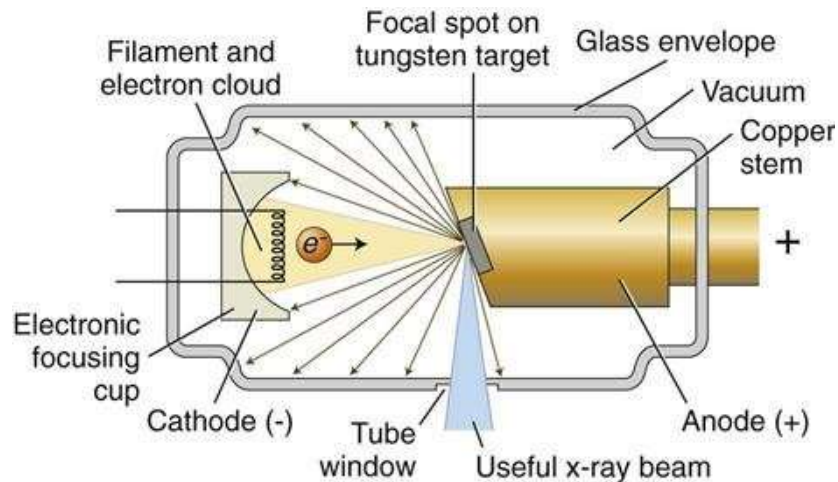


- With the same energy density, high scanning speed is preferable to reduce the influence from the vapor plume and the hot gas zones.



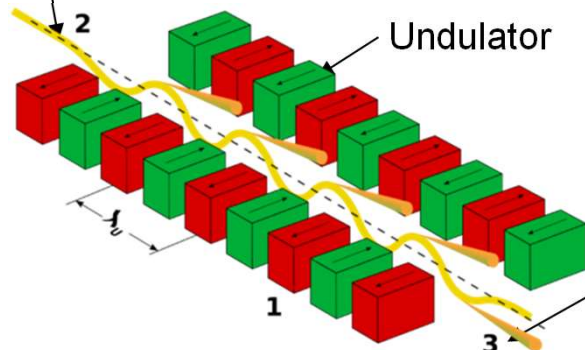
# Phase-contrast X-ray imaging

Object of interest: a very wide range due to the good penetration of X-ray



X-ray tube

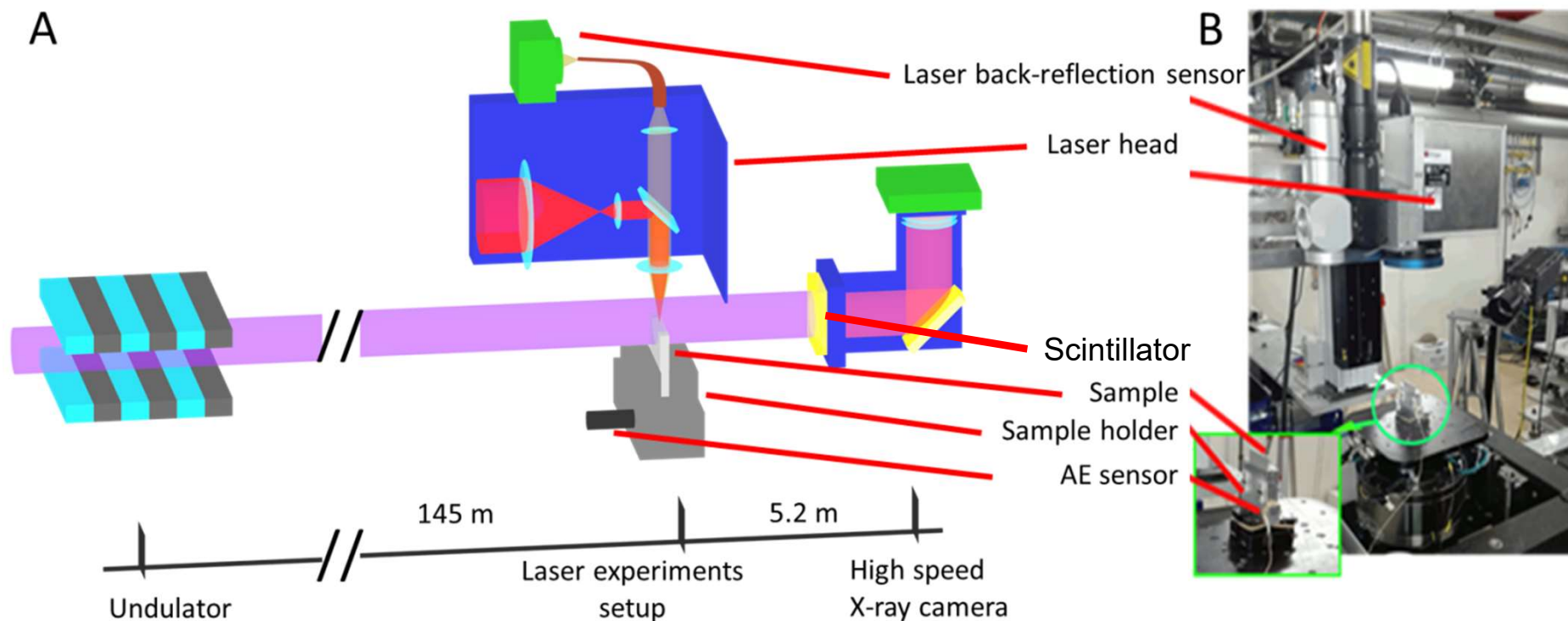
Highly accelerated electrons



Emitted X-ray beam

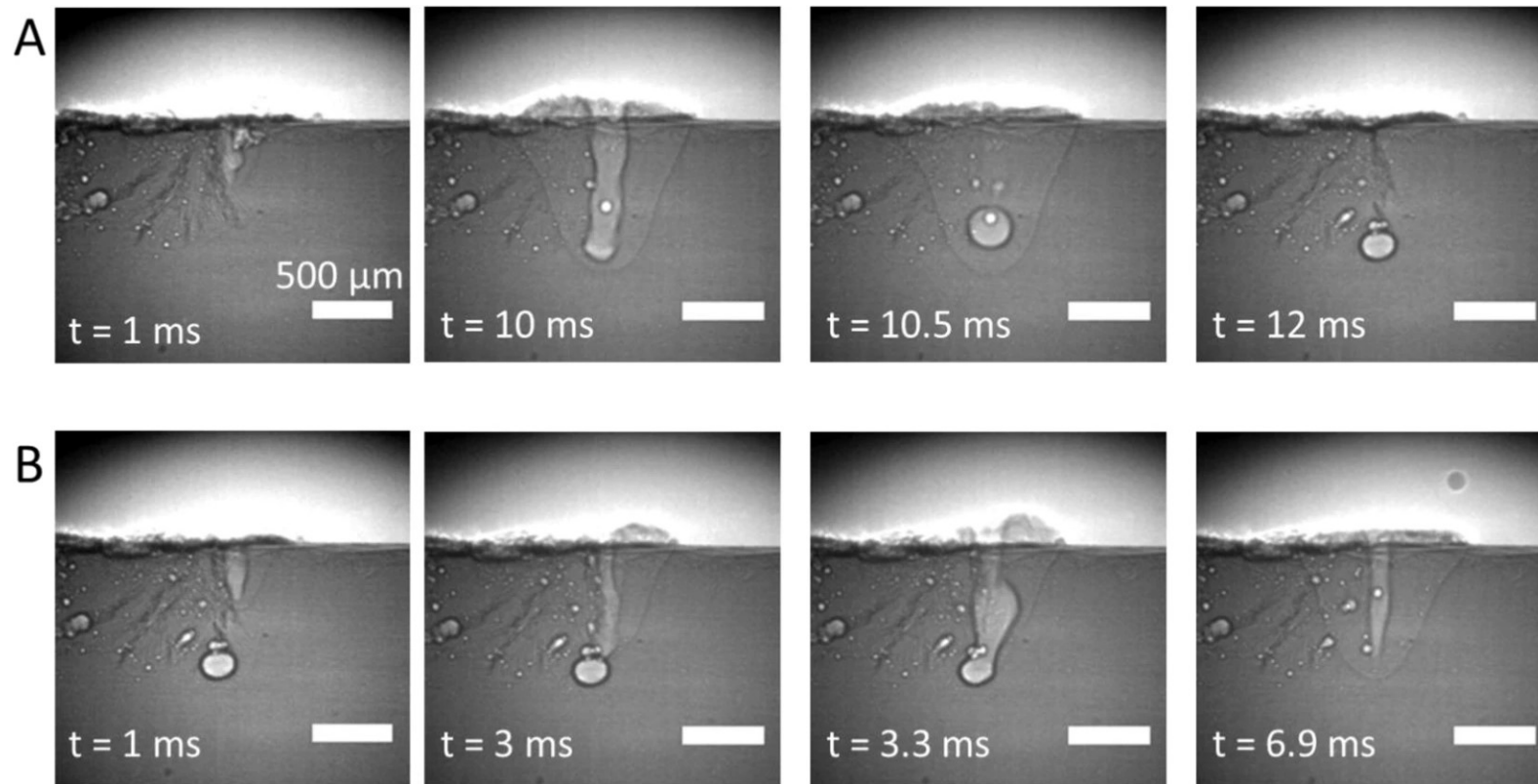
Synchrotron source

# Process dynamic visualization



(A) Schematic of the experimental setup for in-situ X-ray radiography of the laser welds. The bar below defines the key nodes of the setup and their mutual positions; (B) Picture of the welding experimental station.

# Process dynamic visualization



Visualization of sub-surface events, e.g. the removal of pores during laser welding.

# Summary

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- Visualization can provide significantly more information about the process.
- Main limitations: temporal and spatial resolutions, cost of implementation.

# Thank you for your attention

