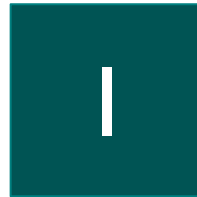


Systemic usage of water in industrial processes

PART



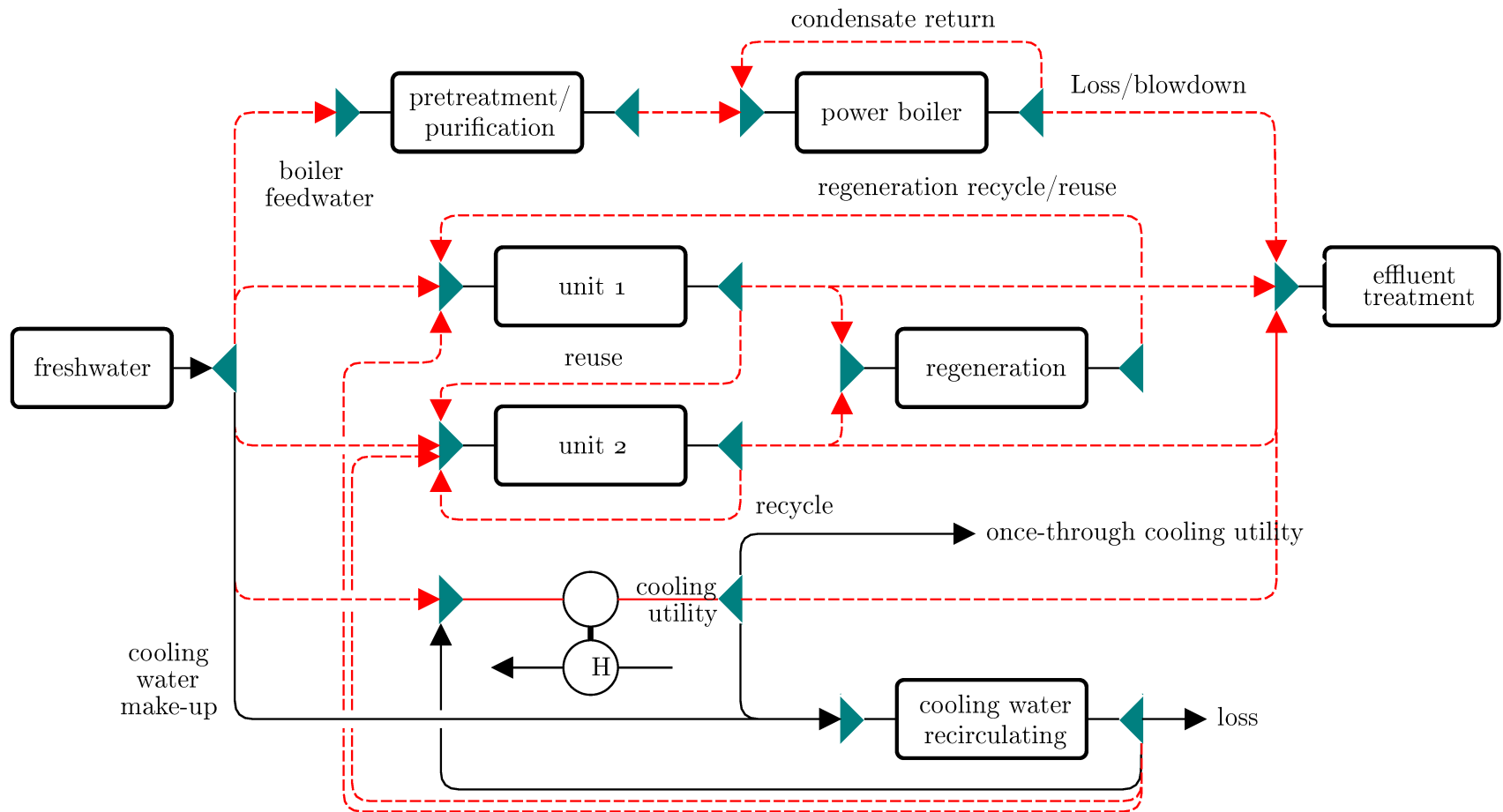
HEAT-INTEGRATED WATER ALLOCATION NETWORK

How can heat and water exchanges be systematically managed within industrial processes? How can industrial specificities be addressed in the solution strategy? What are the main criteria in optimizing such systems? What approach can be used to generate a set of energy and water saving opportunities?

- background and context
- a comprehensive literature survey:
- an **iterative sequential** solution strategy
- generating a set of promising solutions → integer-cut constraint (ICC)

Kermani, M., Kantor, I.D., Maréchal, F., 2018. Synthesis of heat-integrated water allocation networks: a meta-analysis of solution strategies and network features. *Energies*, 11, 1158

Kermani, M., Périn-Levasseur, Z., Benali, M., Savulescu, L., Maréchal, F., 2017. A novel MILP approach for simultaneous optimization of water and energy: application to a Canadian softwood kraft pulping mill. *Computers & Chemical Engineering. Sustainability & Energy Systems* 102, 238–257.



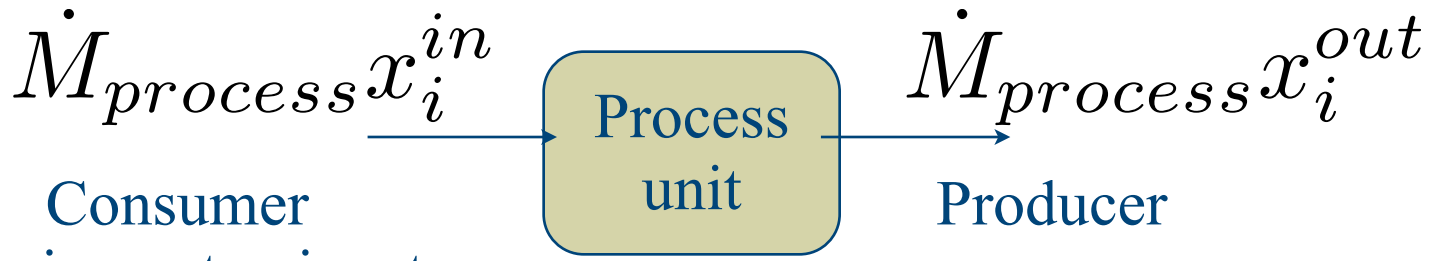
water flows subject to thermal duties

Process integration techniques for rational use of water

◆ Analogy

- Temperature = concentration
- Heat flow = flowrate
- Hot stream : producers
- Cold streams : consumers

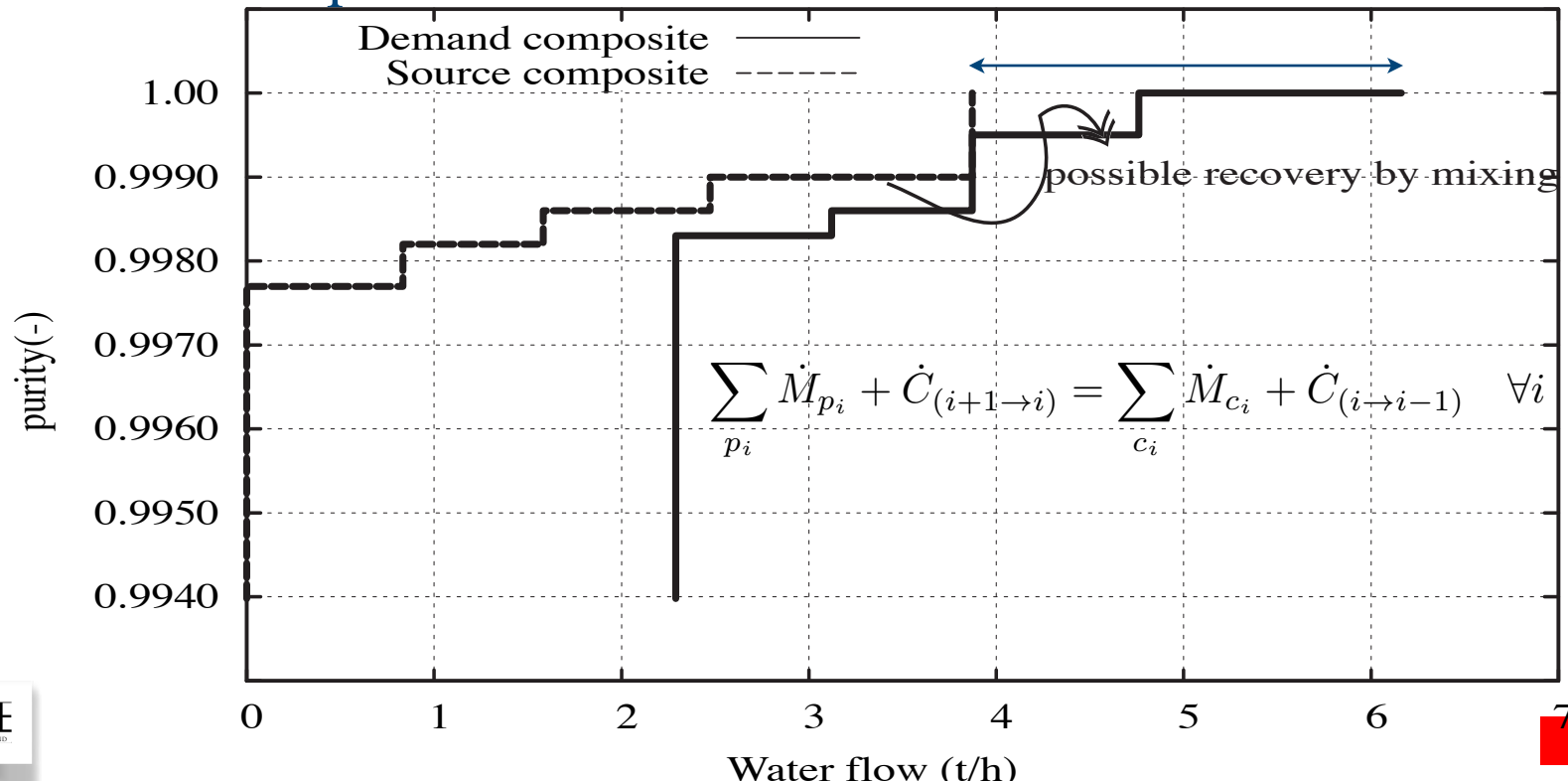
Source and demands



i : contaminant

Minimum fresh water requirement

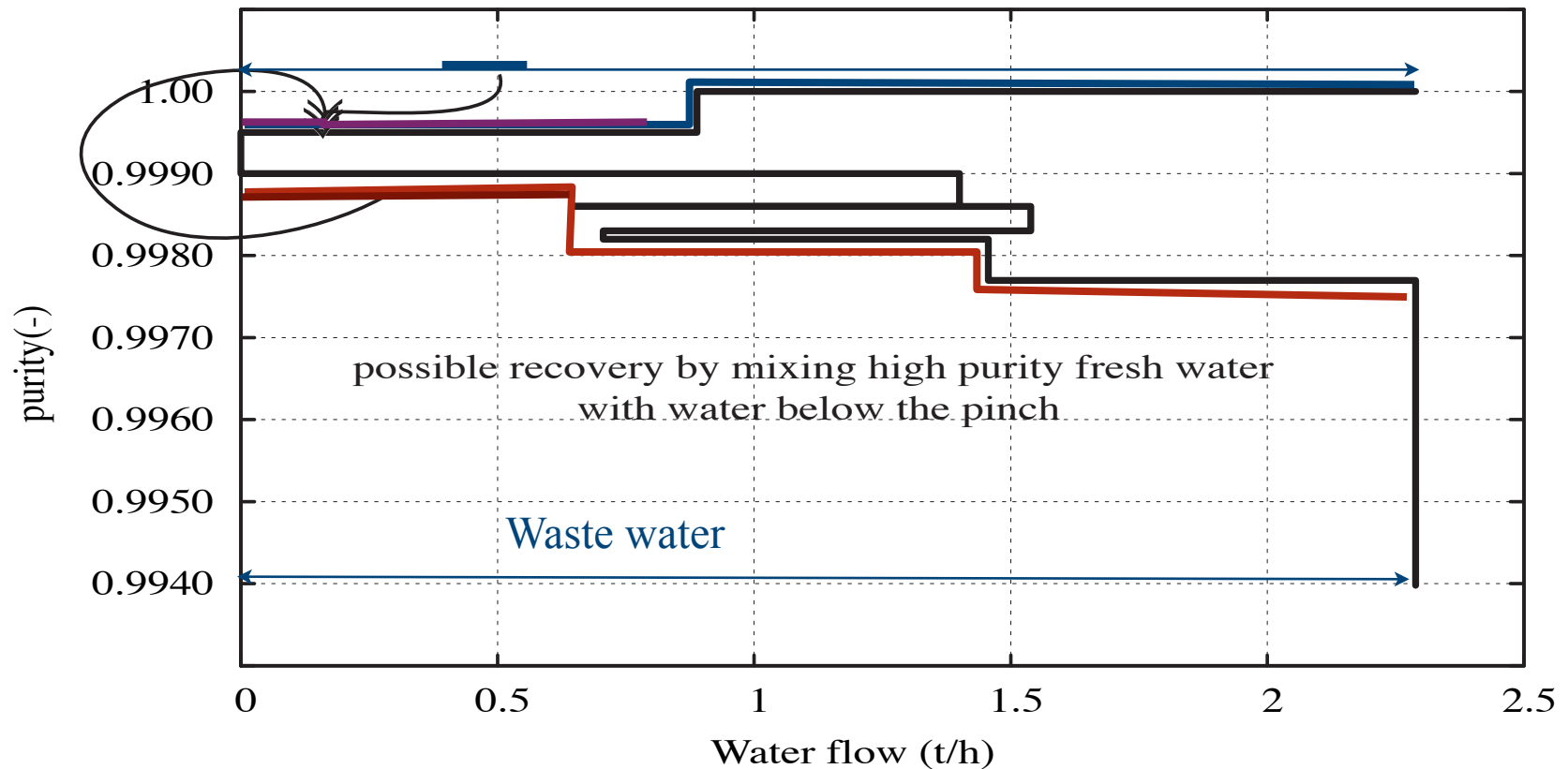
Composite curve



Water surplus composite

Grand composite

Minimum fresh water requirement



Integrated water management

- ◆ Waste water streams from the process

- i contaminants : x_i

- Water flow

$$\dot{M}_{support} \quad x_i^{in} \rightarrow x_i^{target} \Rightarrow \dot{M}_i = \dot{M}_{support}(x_i^{in} - x_i^{target})$$

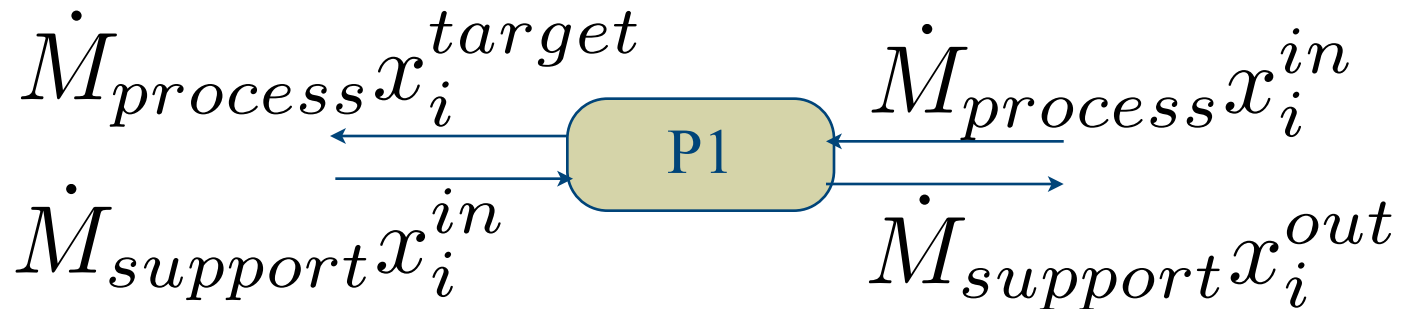
- Hot stream

Water treatment units

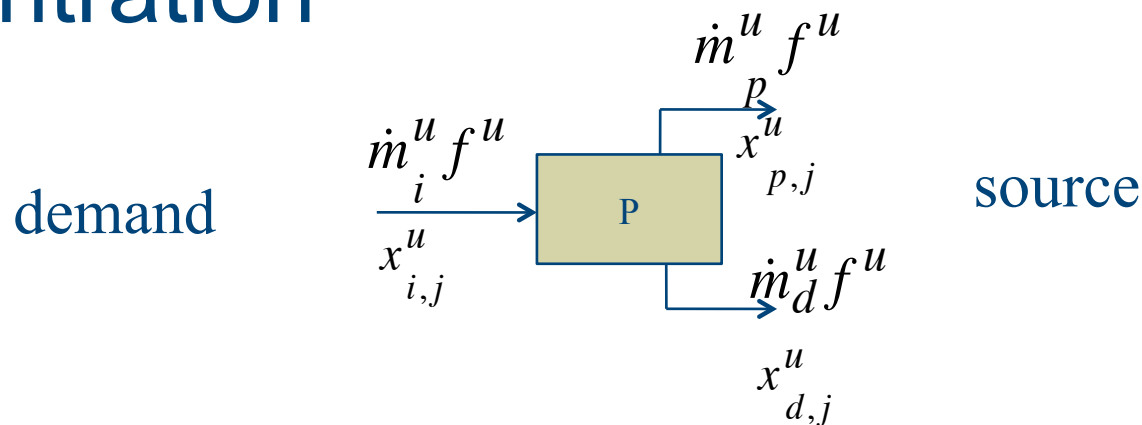
◆ Destruction of pollutant



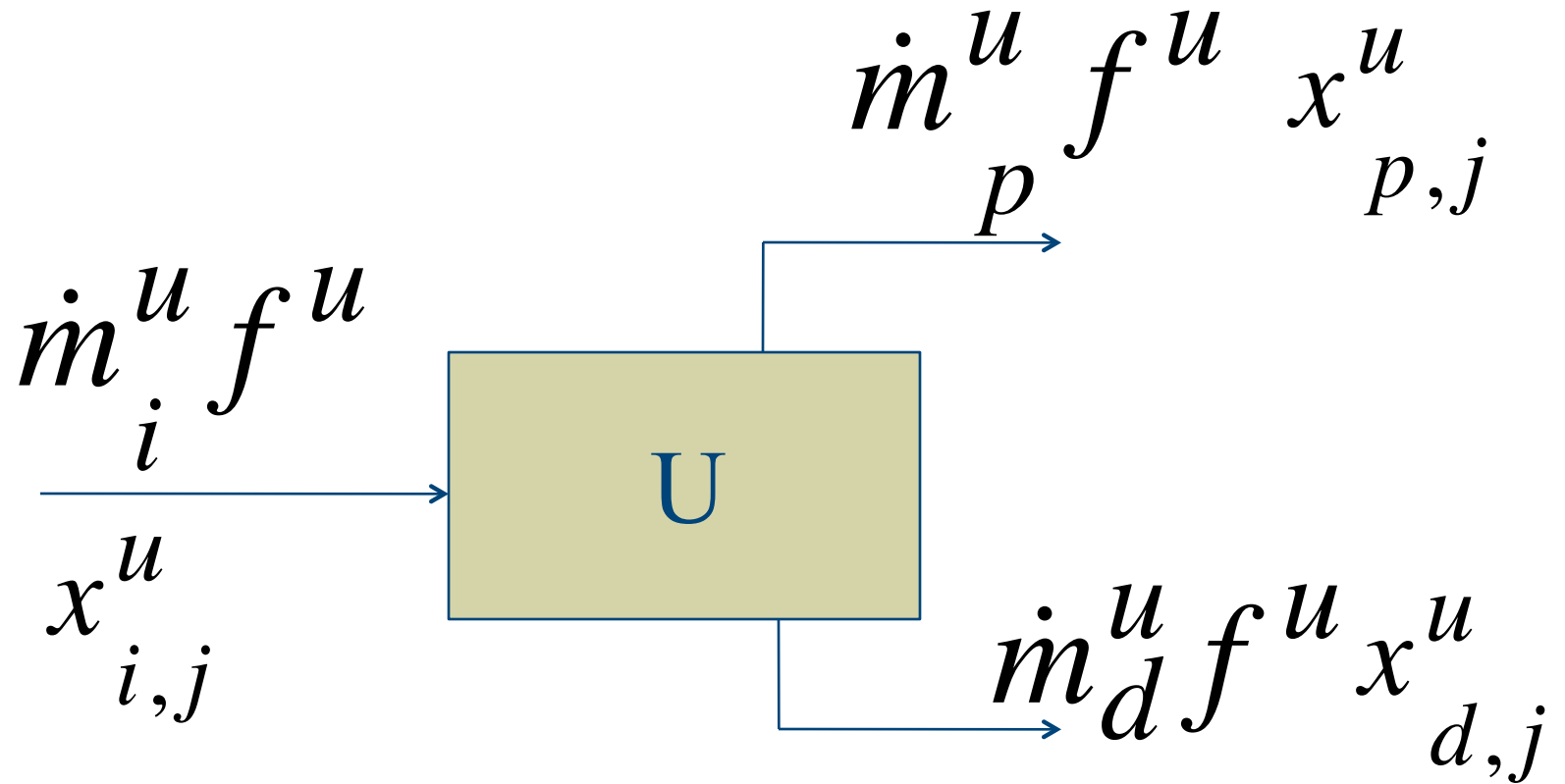
◆ Extraction



◆ Concentration



Generic formulation

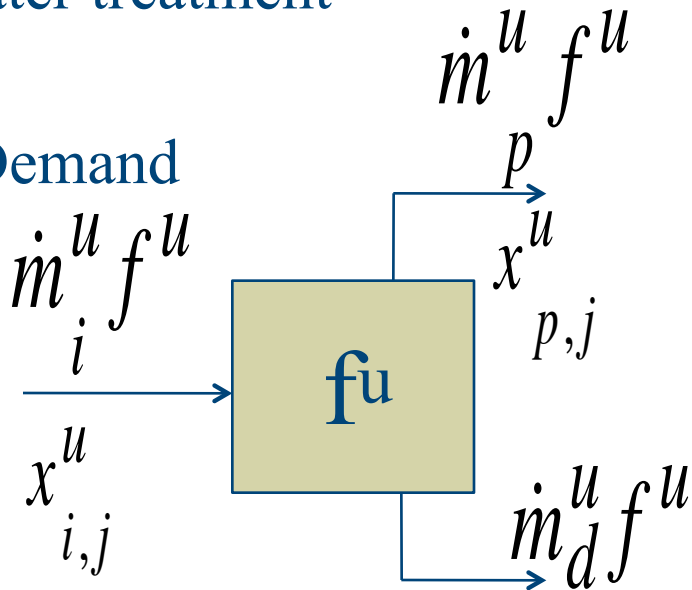


Unit U : operation model : $\text{out} = f(\text{in})$

consumers/producers

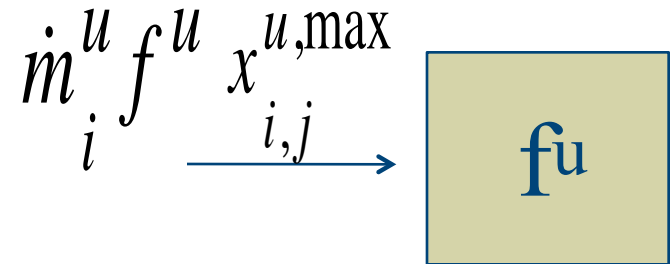
Water treatment

Demand

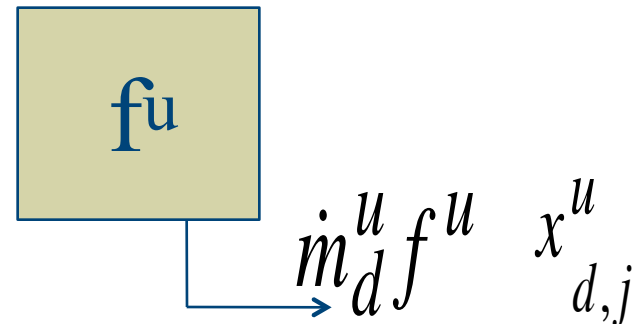


$f^u = const$ for process units

Demand



*Waste water with unknown flow but cost



Sources

*Fresh water source with unknown flow but cost

Problem formulation

s : supplier

d : demand

$$\min_{c_{s,d}, y_u} \sum_{u=1}^{n_u} (C_u^2 * f_u + C_u^1 * y_u)$$

Cost => use of the units
Inc. fresh water

$$\sum_{s=1}^{n_s} c_{s,d} - \dot{m}_d * f_u(d) = 0 \quad \forall d = 1, \dots, n_{demande}$$

$$\dot{m}_s * f_u(s) - \sum_{d=1}^{n_d} c_{s,d} \geq 0 \quad \forall s = 1, \dots, n_{sources}$$

Mixer

$$\sum_{s=1}^{n_s} \frac{c_{s,d}}{X_s} * x_{s,j} \leq \frac{\dot{m}_d}{X_d} * f_u(d) * x_{d,j}^{\max} \quad \forall j = 1, n_{impureté} \quad \forall d = 1, n_d$$

$$\sum_{s=1}^{n_s} \frac{c_{s,d}}{X_s} * (1 - X_s) \leq \frac{\dot{m}_d}{X_d} * f_u(d) * (1 - X_d^{\max}) \quad \forall d = 1, n_d$$

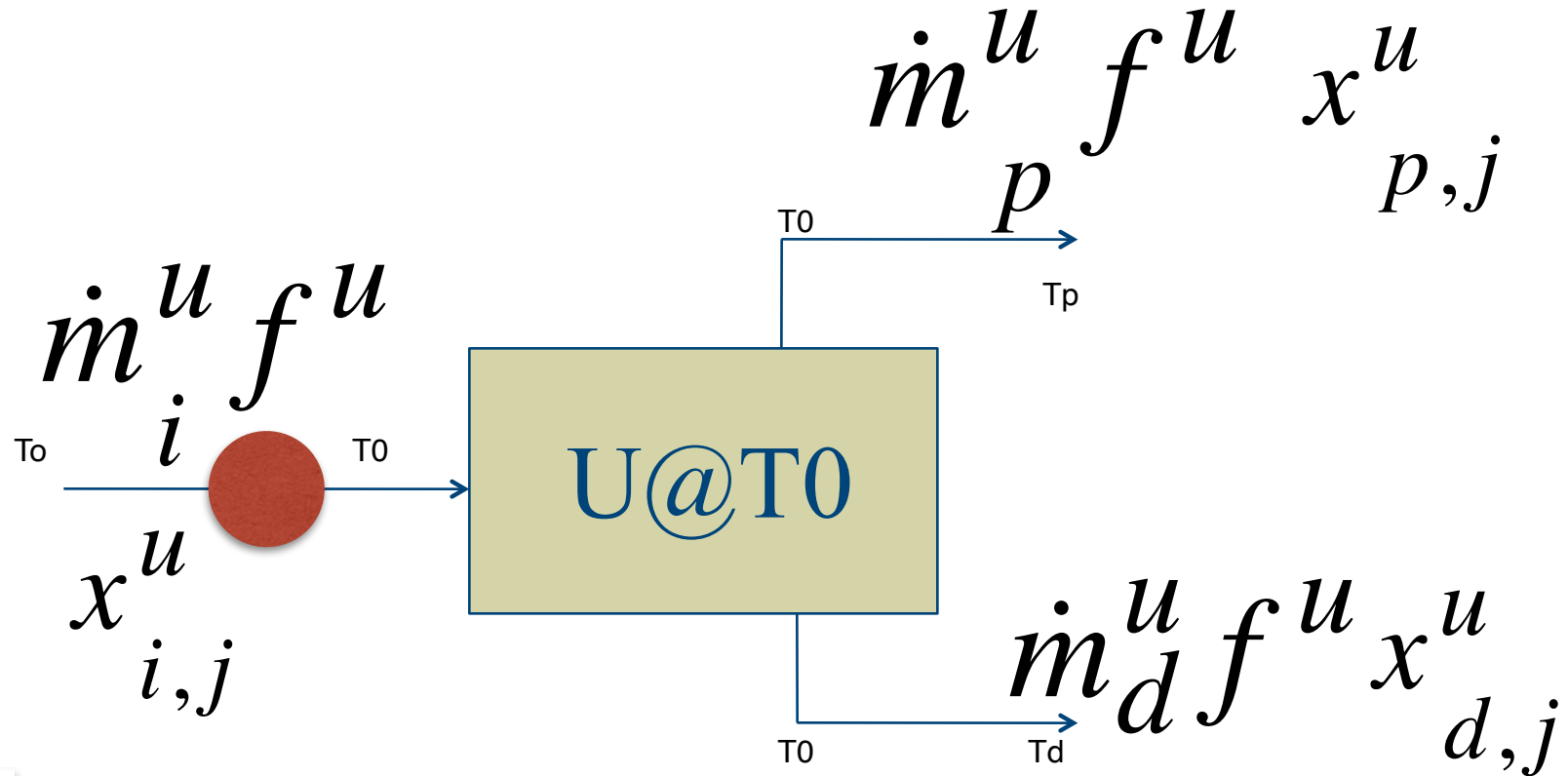
$$X_i = 1 - \sum_{j=1}^{n_{impureté}} x_{i,j} \quad f_u = 1 \quad \forall u = 1, \dots, n_{u, procédé}$$

$$f_u^{\min} * y_u \leq f_u \leq f_u^{\max} * y_u \quad \forall u = 1, \dots, n_{util}$$

$$y_u \in \{0, 1\}$$

Combined heat and mass integration

- ◆ 1st approach
 - realise the mass integration at ambient temperature

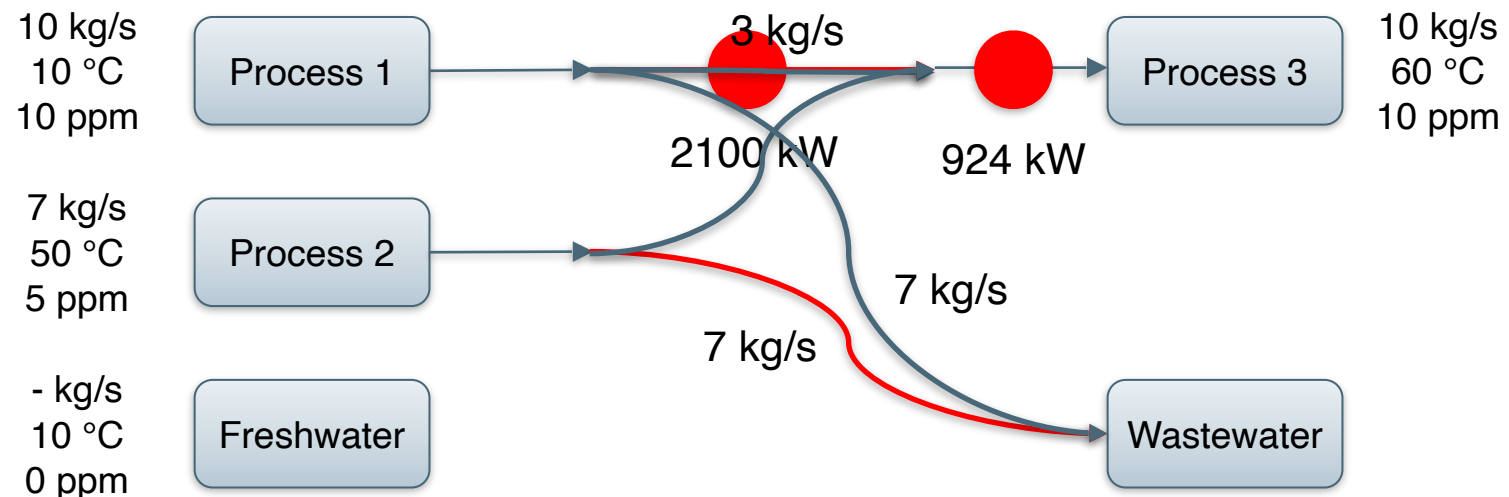


Why combined mass and energy integration?

Sequential approach:

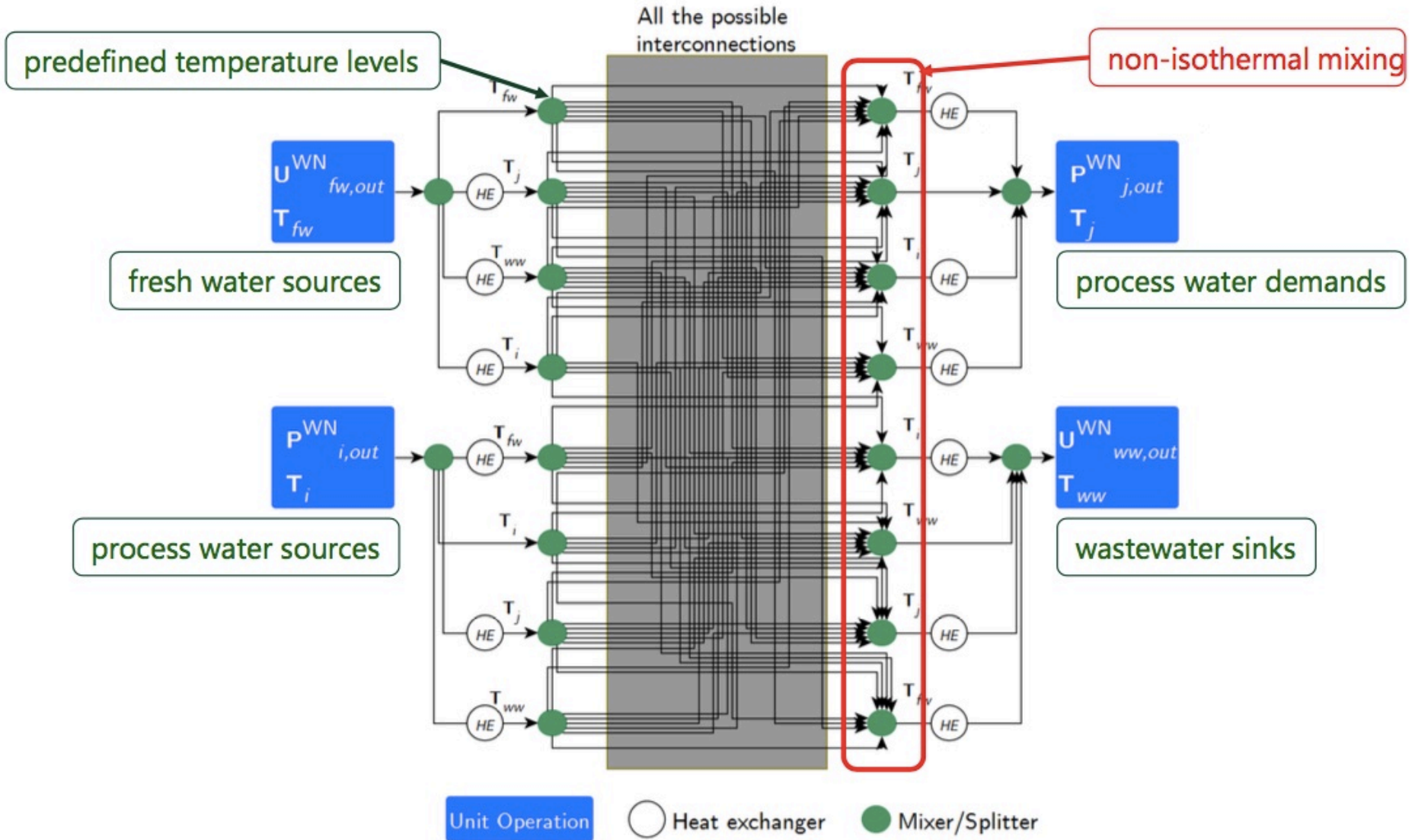
- 1 - Design of water network
- 2 - Design of heat exchange network

Drawback: Not considering energy implication and heat integration aspects in water network design.



	Sequential	Simultaneous
Fresh water consumption (kg/s)	0	0
Wastewater production (kg/s)	7	7
Hot utility (kW)	2100	924

Detailed super-structure



Objective function: minimize the total cost of the network

$$\min \left\{ \begin{aligned} & \left(\sum_{fw \in U_{out}^{WN}} m_{fw} \cdot C_{fw} + \sum_{ww \in U_{in}^{WN}} m_{ww} \cdot C_{ww} \right) \cdot t_{operating} \\ & + \left(\sum_{u \in U^H} f_u^H \cdot q_u^H + \sum_{u \in U^C} f_u^C \cdot q_u^C \right) \cdot t_{operating} \\ & + \frac{i \cdot (1+i)^{n_{year}}}{(1+i)^{n_{year}} - 1} \cdot \left(\sum_{u \in U^H} (y_u^H \cdot I_{f,u}^H + f_u^H \cdot I_{p,u}^H) \right. \\ & \quad \left. + \sum_{u \in U^C} (y_u^C \cdot I_{f,u}^C + f_u^C \cdot I_{p,u}^C) \right) \\ & + \frac{i \cdot (1+i)^{n_{year}}}{(1+i)^{n_{year}} - 1} \cdot \left(\sum_{i \in p^{WN} \cup U^{WN}} \left(\sum_{t \in T, t \neq i} m_{i,t} \cdot I_{p,i,t}^{WN} \right) \right) \end{aligned} \right\}$$

cost of fresh water and wastewater

cost of hot and cold utilities

investment cost of thermal utilities

Subjected to:

- Existence of a system (e.g. utility of fresh water, sub-units, hot utility);
- Heat cascade model (Maréchal and Kalitventzeff, 1996);
- Mass balance;
- Temperature and contamination constraints;

mathematical formulation and superstructure generation

$$\mathbf{P1} : \min C^{\text{tac}} = C^{\text{op}} + C^{\text{inv}}$$

$$= \left[\sum_{fw \in \mathbf{U}_{out}^{\text{WAN}}} \dot{m}_{fw} C_{fw} + \sum_{ww \in \mathbf{U}_{in}^{\text{WAN}}} \dot{m}_{ww} C_{ww} + \sum_{u \in \mathbf{U}^H} \dot{f}_u^H q_u^H C_u^H + \sum_{u \in \mathbf{U}^C} \dot{f}_u^C q_u^C C_u^C \right] \cdot t^{\text{op}}$$

resource consumption

$$+ \frac{\text{irr}(1 + \text{irr})^{\text{year}}}{(1 + \text{irr})^{\text{year}}} \left[\sum_{u \in \mathbf{U}^H} (y_u^H I_{f,u}^H + \dot{m}_{f,u}^H) + \sum_{u \in \mathbf{U}^C} (C_u C_u + \dot{m}_{p,u}^C) \right]$$

investment cost

$$+ \frac{\text{irr}(1 + \text{irr})^{\text{year}}}{(1 + \text{irr})^{\text{year}}} \left[\sum_{i \in \mathbf{WAN}} \left(\sum_{T \in \mathbf{T}_i^{\text{WAN}}} (y_{i,T} \cdot I_{f,i,T}^{\text{WAN}} + \dot{m}_{i,T} \cdot I_{p,i,T}^{\text{WAN}}) \right) \right]$$

penalty cost

subject to:

- mass balance
- contamination constraint [75]

$$\sum_{i \in \mathbf{WAN}_{out}} \sum_{T' \in \mathbf{T}_i^{\text{WAN}}} \sum_{T \in \mathbf{T}_j^{\text{WAN}}} \dot{m}_{i,j,T',T} \cdot C_i^{k,max} = \dot{m}_{j,T} \cdot C_j^{k,max} \quad \forall j \in \mathbf{WAN}_{in}, \quad \forall T \in \mathbf{T}_j^{\text{WAN}}$$

nonlinear equality

$$\sum_{i \in \mathbf{WAN}_{out}} \sum_{T' \in \mathbf{T}_i^{\text{WAN}}} \sum_{T \in \mathbf{T}_j^{\text{WAN}}} \dot{m}_{i,j,T',T} \cdot C_i^{k,max} \leq \dot{m}_{j,T} \cdot C_j^{k,max} \quad \forall j \in \mathbf{WAN}_{in}, \quad \forall T \in \mathbf{T}_j^{\text{WAN}}$$

linear inequality

- energy balance (neat cascade model) [84]
- fixed-load vs fixed-flow formulations

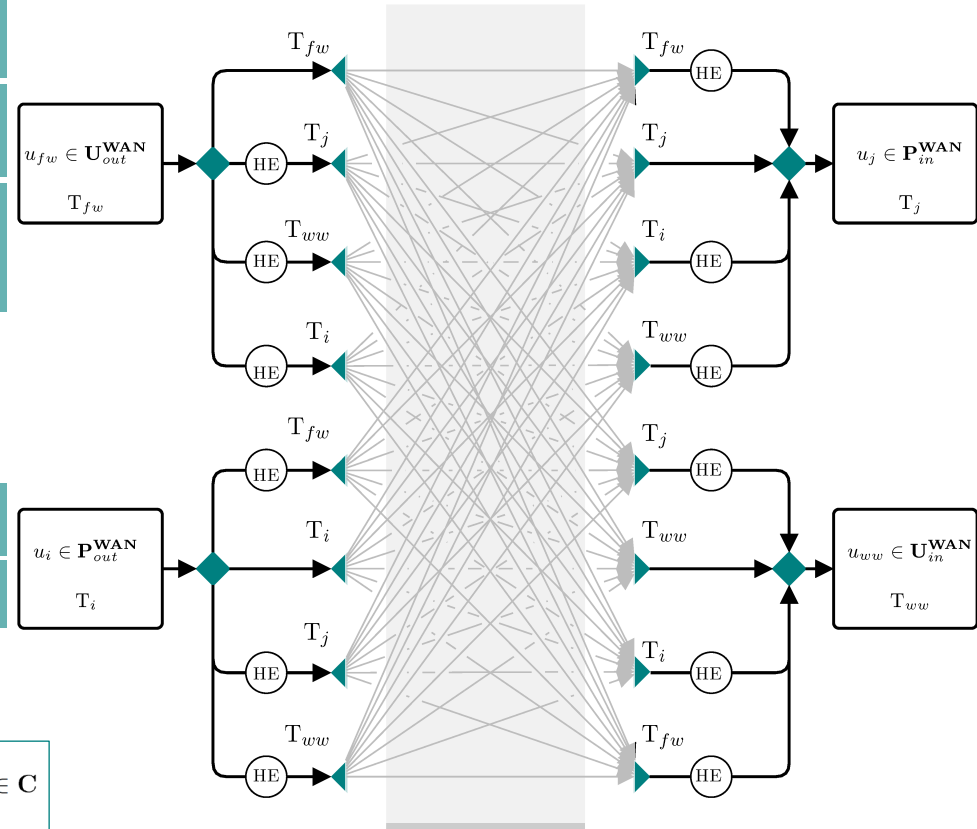
$$\dot{m}_u = \frac{L_u^k}{(c_u^{k,out} - c_u^{k,in})} \quad \Leftrightarrow \quad \dot{m}_u \cdot c_u^{k,in} + L_u^k = \dot{m}_u \cdot c_u^{k,out} \quad \forall k \in \mathbf{C}$$

$$m_u^{\min} = \frac{L_u^k}{c_u^{k,out,max}}$$

$$m_u^{\max} = \frac{L_u^k}{(c_u^{k,out,max} - c_u^{k,in,max})}$$

$$\sum_{i \in \mathbf{WAN}_{out}} \sum_{T' \in \mathbf{T}_i^{\text{WAN}}} \dot{m}_{i,j,T',T} \cdot T' = \dot{m}_{j,T} \cdot T \quad \forall j \in \mathbf{WAN}_{in}, \quad \forall T \in \mathbf{T}_j^{\text{WAN}}$$

all possible interconnections



unit operation

○ heat exchanger

◆ final mixer/initial splitter

◀ intermediary splitter

▶ intermediary mixer

Simultaneous optimisation of water and energy

Embedded concepts in SOWE

Restricted matches

- Addressing contamination constraints (lack of data)
- Addressing heat and mass exchange restriction

Water tanks

- Influence of tank temperature on water network design
- Seasonal variations in the temperature of water

Process-specific constraints

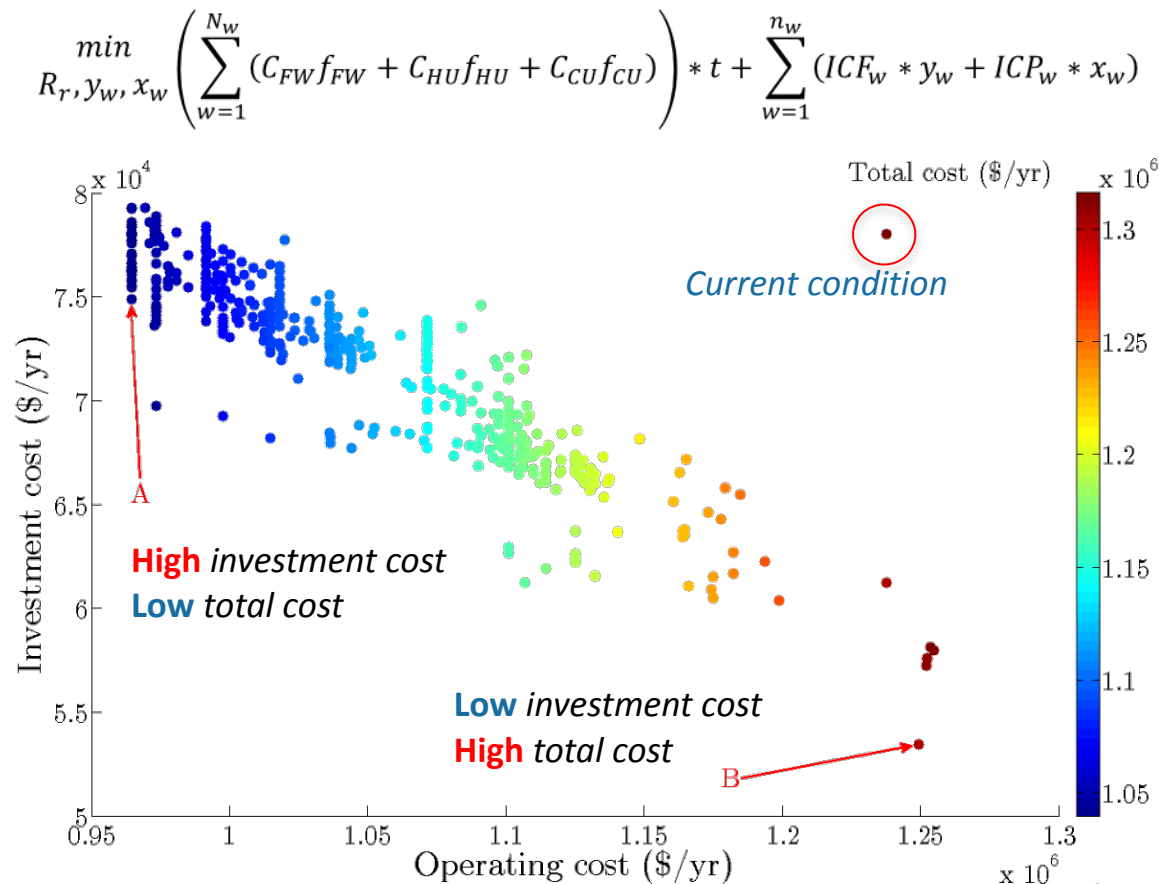
- Uncertainties (or unavailability) of measurements
 - Heat exchangers replaced by water-using units
- Economic, topological and any practical constraint in the mill:
 - Geographical allocation of process operations
 - Cost of piping

(Kermani et al. 2014)

Simultaneous optimisation of water and energy

Mathematical techniques: Integer-Cut Constraint (ICC)

- Finding ordered set of solutions for the same problem.
- Finding the most attractive solution considering other criteria.



(Kermani et al. 2014)

Industrial application

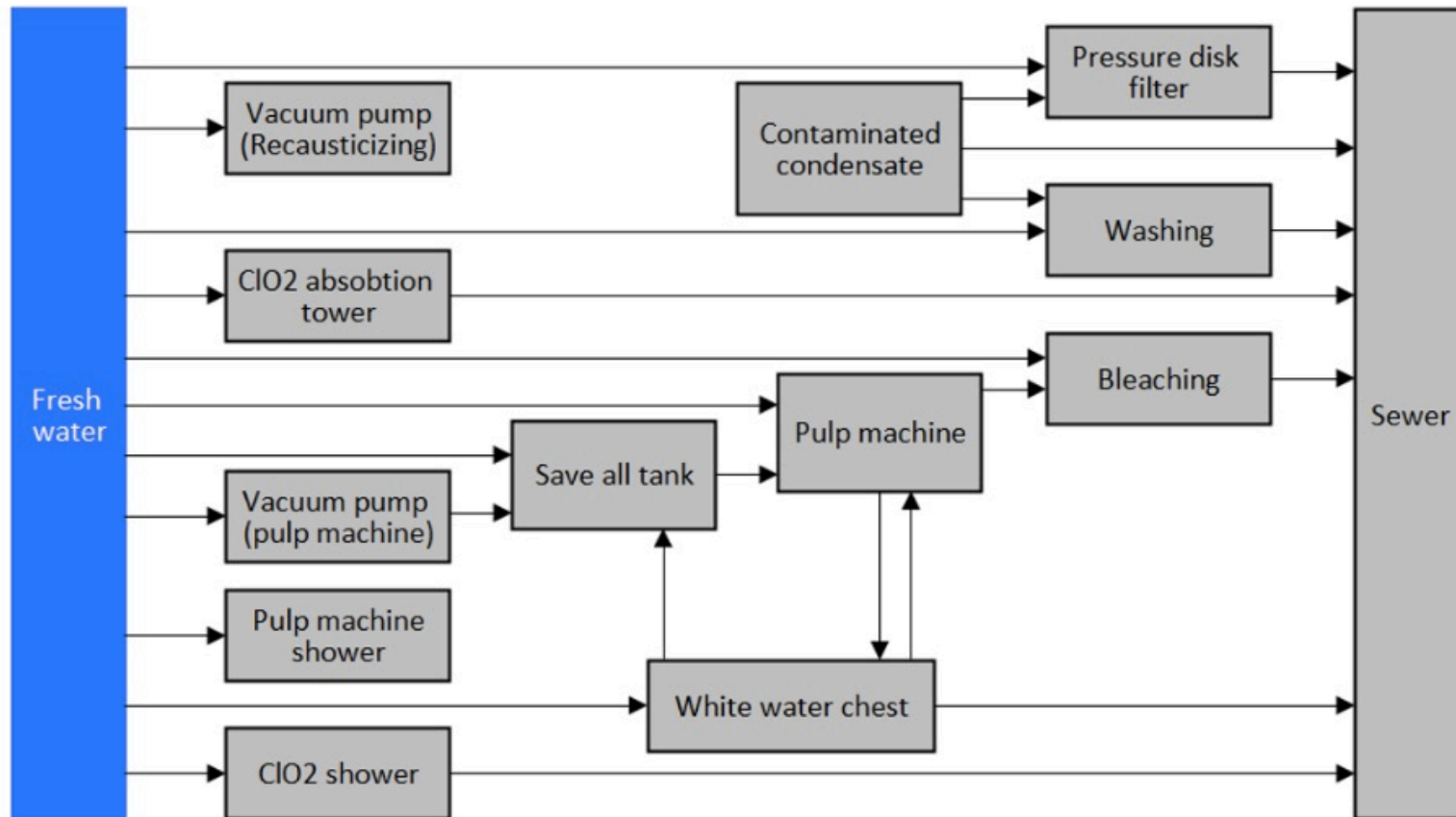
Pulp and paper process

- 1,000 adt pulp /d

			Current condition of the mill
Steam Consumption	# 60 ⁽¹⁾	MW	136
	# 160 ⁽²⁾	MW	41
Total hot utility		MW	177
Water consumption		kg/s	592

⁽¹⁾ 413 kPa (g)

⁽²⁾ 1100 kPa (g)

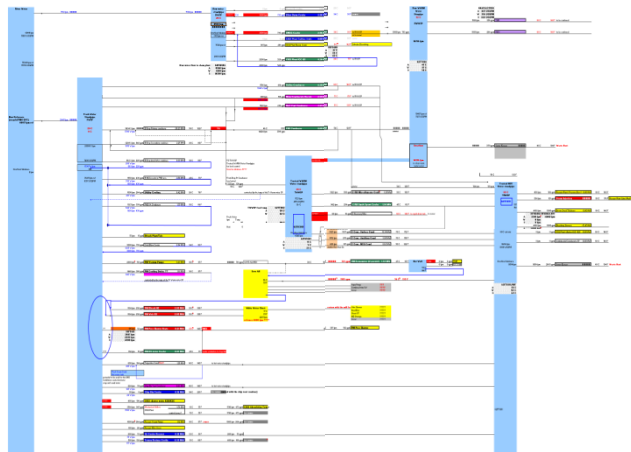


Simultaneous optimisation of water and energy

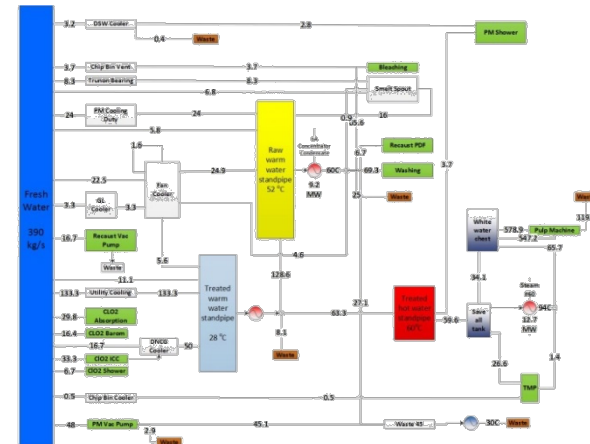
Industrial case study - results

- **Pulp and paper industry producing 1,000 adt/d of pulp:**
 - Number of thermal streams: **37**
 - Number of tanks: **3**
 - Number of water-using operations: **12**

From current water network



To optimized water network



Current condition of the mill				SOWE
Steam Consumption	# 60 ⁽¹⁾	MW	136	131 (-3.6 %)
	# 160 ⁽²⁾	MW	41	8.7
Total hot utility		MW	177	139.7 (-21%)
Water consumption		kg/s	592	390 (-34%)

⁽¹⁾ 413 kPa (g)

⁽²⁾ 1100 kPa (g)

(Kermani et al. 2014)

