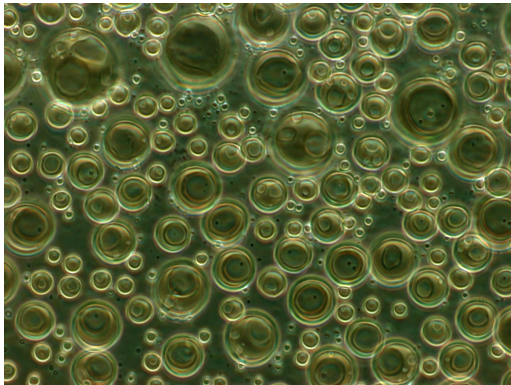
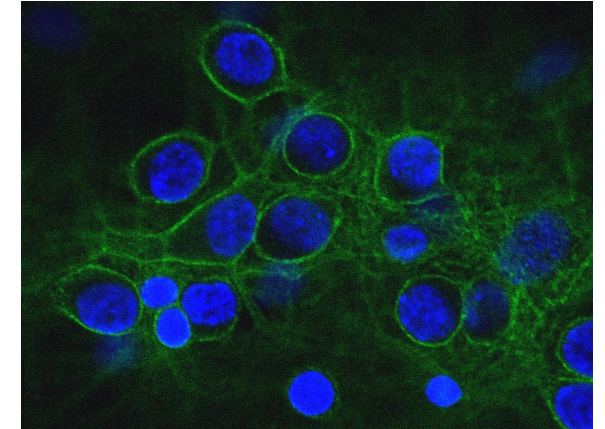
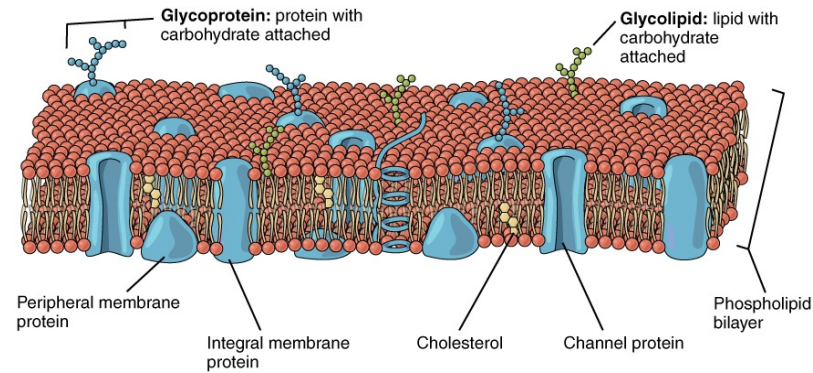
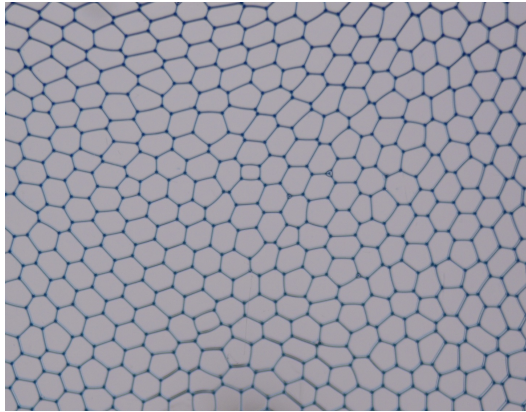


ME470: Mechanics of Soft and Biological Matter

Lecture3: 1D Elements

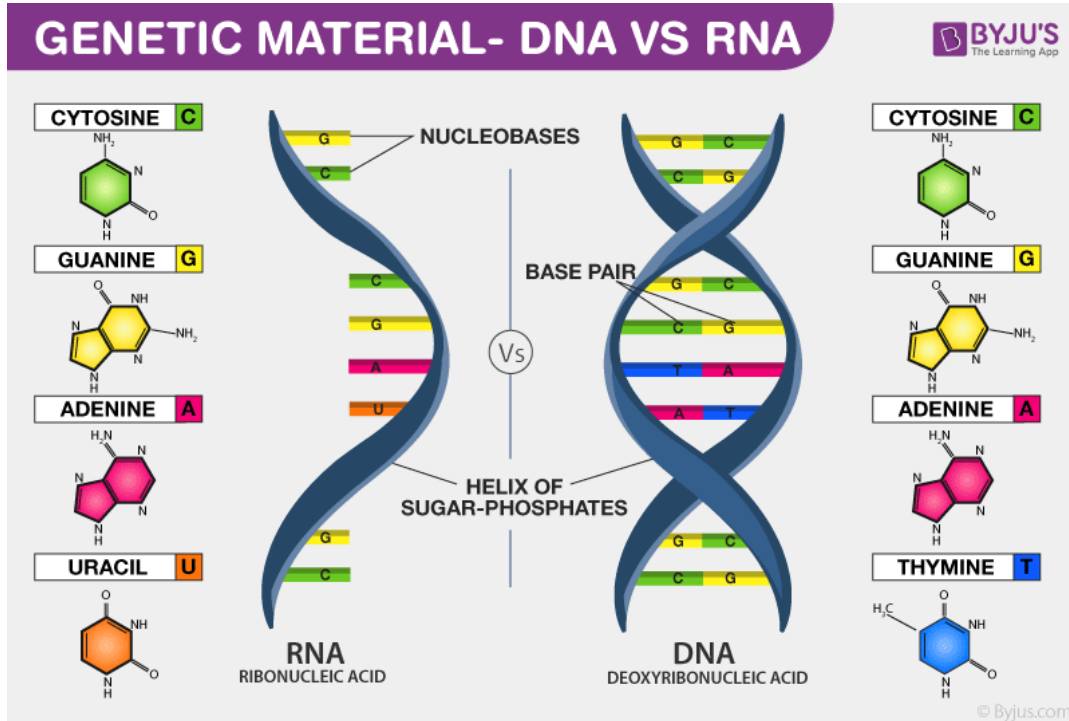


Sangwoo Kim

MESOBIO – IGM – STI – EPFL

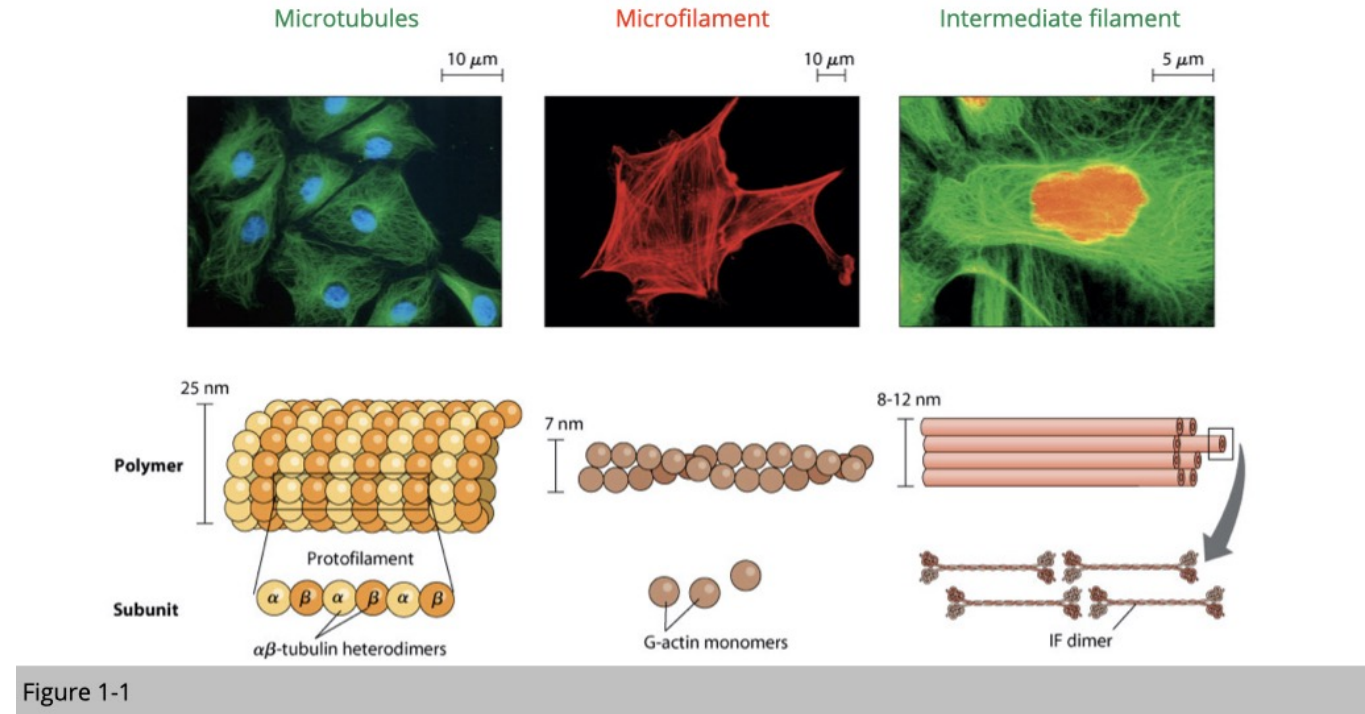
Red Blood Cells

Genetic materials



(<https://byjus.com/biology/genetic-material-dna-rna/>)

Cytoskeleton



(https://medicine.nus.edu.sg/phys/lab/TsaiSY_Lab/LSM4232-L1.html)

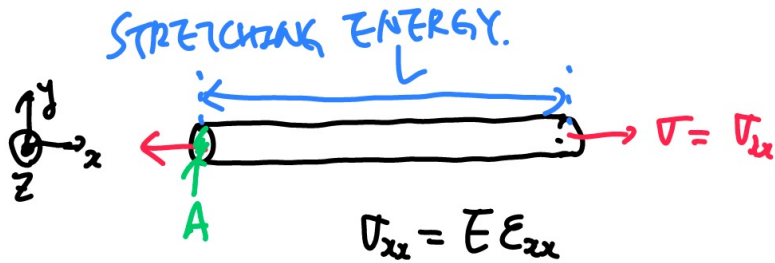
Goal: How can we describe mechanics of one-dimensional filaments?

Biopolymer is one of the most important structural elements for cells

- DNA, RNA: Nucleotides
- Microfilament (actin filament): actin
- Microtubule: tubulin dimers
- Intermediate filament: diverse composition (keratins, vimentins)

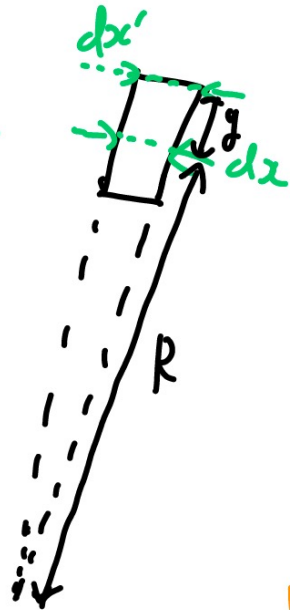
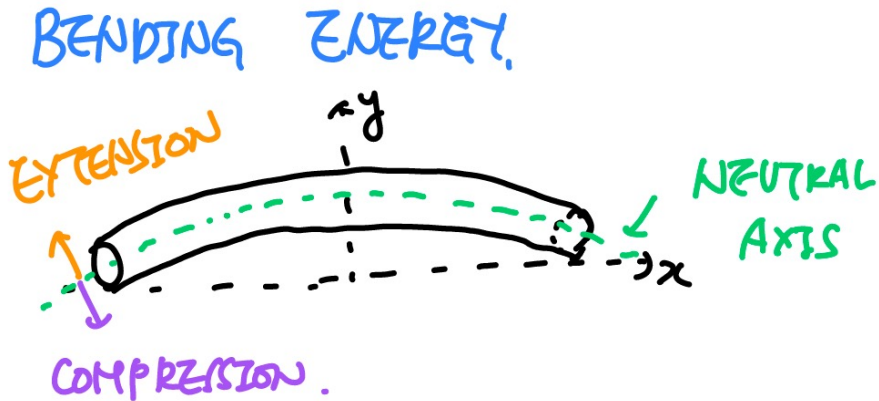
1D elements (filaments, fibers, springs) can contribute to soft behaviors by

- Elastic response (bending dominant)
- Entropic response



$$U_{stretch} = \int u dV = V \int \sigma_{xx} d\epsilon_{xx} = LAE \int \epsilon_{xx} d\epsilon_{xx} = \frac{1}{2} LAE \epsilon^2$$

Typical energy to stretch by $\epsilon = \frac{\Delta L}{L}$



$$\frac{dx'}{dx} = \frac{R+y}{R} \quad \Rightarrow \quad \frac{dx' - dx}{dx} = \frac{y}{R} = \epsilon_{xx}$$

$$U_{bend} = \int \frac{1}{2} E \left(\frac{y}{R} \right)^2 dV = \frac{1}{2} EL \int \frac{y^2}{R^2} dV \quad \text{(uniform along x axis)}$$

$$= \frac{1}{2} E \frac{L}{R^2} \int y^2 dV \quad \text{(uniform curvature)}$$

Area moment of inertia, I

EPFL Elastic response: stretching vs bending

5

If relevant length scale of beam is $\sim d$ in y and z , $I \sim d^4$

(e.g. circular cross section with diameter, d , $I = \frac{\pi}{64} d^4$)

For large bending deformation, $R \sim L$


$$U_{bend} \sim \frac{1}{2} E \frac{1}{L} d^4 \sim \frac{1}{2} L E A \left(\frac{d^2}{L^2} \right) \quad (A \sim d^2)$$

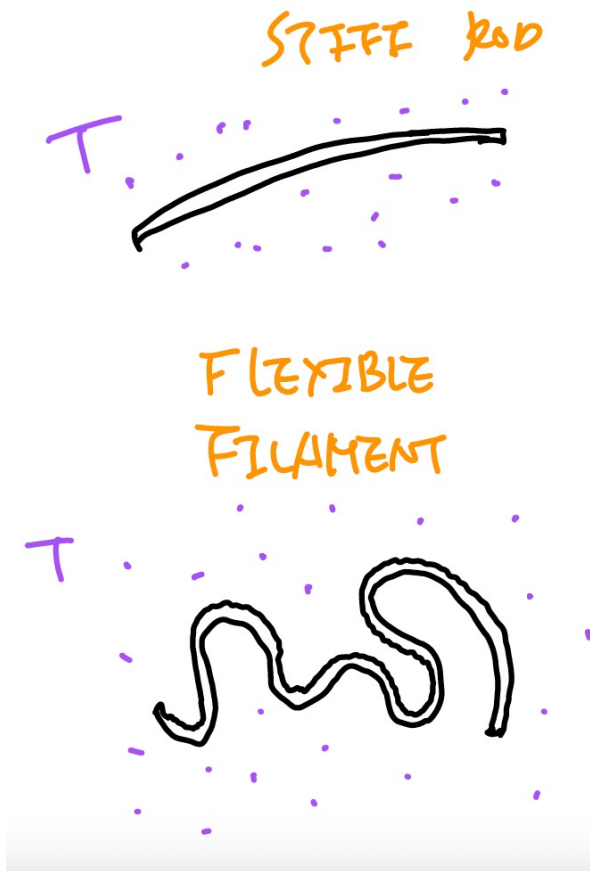
Compare with strong stretching ($\varepsilon \sim 1$)


$$\frac{U_{stretch}}{U_{bend}} \sim \frac{d^2}{L^2} \ll 1$$

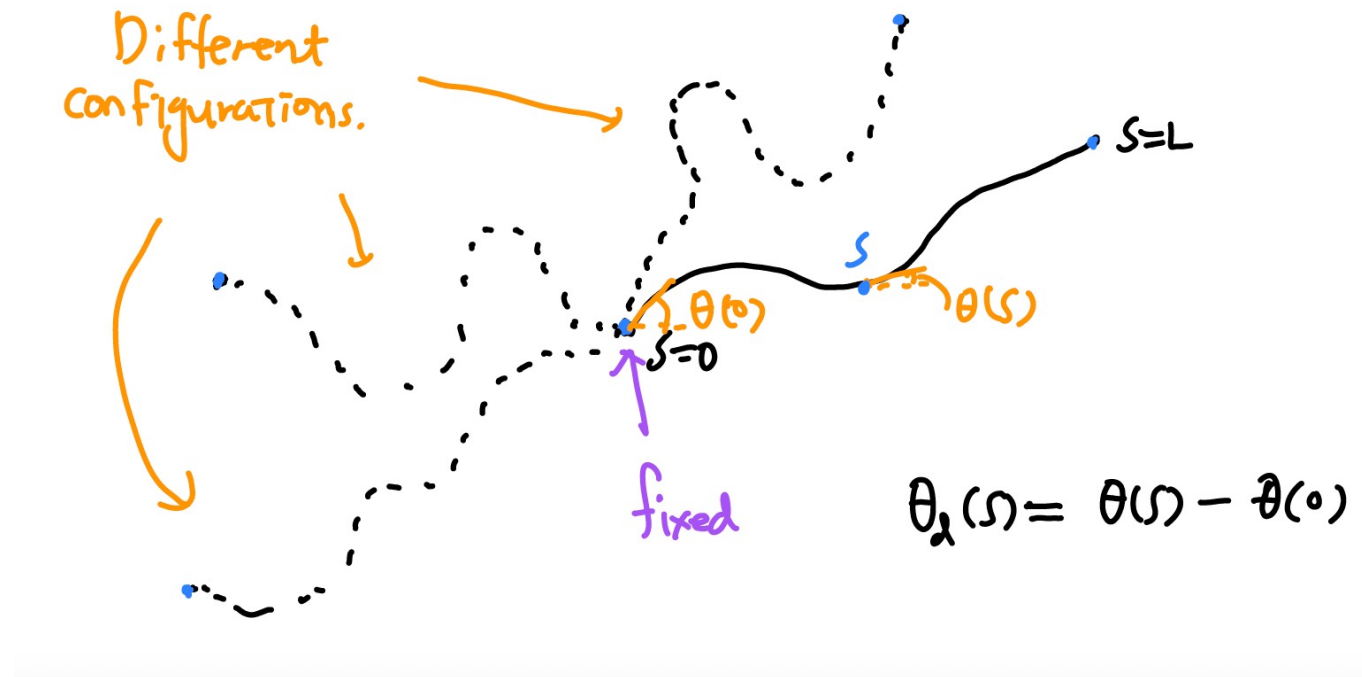
Inextensible assumption is good for 1D element! (e.g. fixed contour length)

Q: what determines equilibrium configuration of 1D element?

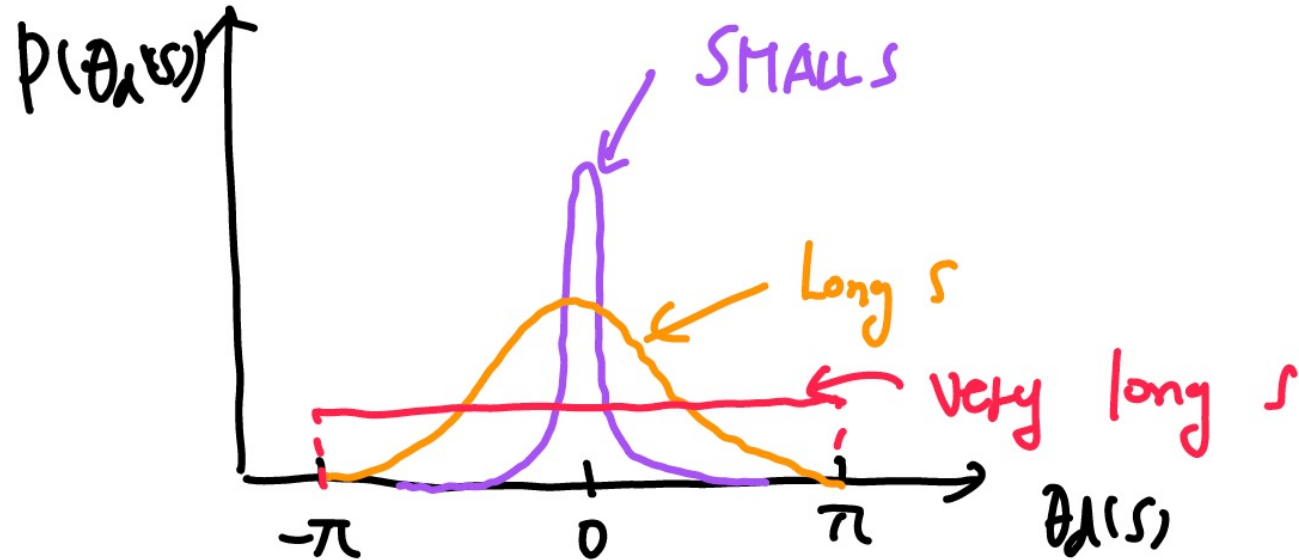
A: competition between **energetic influence** (bending) and **entropic influence** (thermal fluctuations)



Measure flexibility of 1D element



$\theta_d(s)$ exhibit distinct distributions



Define $f(s) = \langle \cos(\theta_d(s)) \rangle$: orientation correlation function ($\langle \cdot \rangle$ means average over multiple configurations)

$$\frac{df}{ds} \approx \frac{f(s + \Delta s) - f(s)}{\Delta s} = \frac{\langle \cos(\theta_d(s + \Delta s)) \rangle - \langle \cos(\theta_d(s)) \rangle}{\Delta s}$$

Here
$$\theta_d(s + \Delta s) \approx \theta_d(s) + \frac{d\theta_d(s)}{ds} \Delta s = \theta_d(s) + \Delta\theta_d(s)$$

⇒
$$\frac{df(s)}{ds} \approx \frac{\langle \cos(\theta_d(s) + \Delta\theta_d(s)) \rangle - \langle \cos(\theta_d(s)) \rangle}{\Delta s} = \frac{\langle \cos(\theta_d(s)) \rangle \langle \cos(\Delta\theta_d(s)) \rangle - \langle \cos(\theta_d(s)) \rangle}{\Delta s}$$

$$\frac{df(s)}{ds} \approx \left(\frac{\langle \cos(\Delta\theta_d(s)) \rangle - 1}{\Delta s} \right) f(s) = -c f(s)$$

Independent of s, constant

Solution: $f(s) = e^{-cs} = e^{-\frac{s}{l_p}}$ Persistence length

Persistence length gives a characteristic length scale over which the orientation of a thermally undulating polymer become mostly uncorrelated

Consider 3D elastic beam with bending stiffness (flexural rigidity), EI

$$U_b = \frac{1}{2}EI \frac{s}{R^2} = \frac{1}{2}EI \frac{\theta^2}{s} \quad \leftarrow \quad \theta = \frac{s}{R}$$



Use canonical ensemble (constant T , Boltzmann distribution)

$$P(\theta) = \frac{1}{Z} \exp\left(-\frac{U_b(\theta)}{k_B T}\right)$$

$$Z = \int_0^{2\pi} \int_0^\pi \exp\left(-\frac{U_b(\theta)}{k_B T}\right) \sin \theta \, d\theta \, d\phi$$

(Use spherical coordinate, consider all possible angle in 3D)

$$\langle \theta^2 \rangle = \frac{1}{Z} \int_0^{2\pi} \int_0^\pi \theta^2 P(\theta) \sin \theta \, d\theta \, d\phi = \frac{2k_B T s}{EI}$$

Exercise

We also know that for small $\theta_d(s)$,

$$\langle \cos(\theta_d(s)) \rangle \approx \left\langle 1 - \frac{\theta_d^2(s)}{2} \right\rangle = 1 - \left\langle \frac{\theta_d^2(s)}{2} \right\rangle = 1 - \frac{k_B T}{EI} s$$

Also,

$$\langle \cos(\theta_d(s)) \rangle = e^{-s/l_p} \approx 1 - \frac{s}{l_p}$$



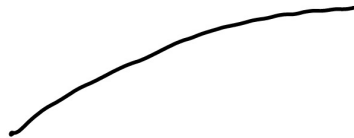
$$l_p = \frac{EI}{k_B T}$$

	F-actin	Microtubule	Intermediate filament	DNA
l_p	$10\mu m$	$6\mu m$	$1\mu m$	$53nm$
L	$1 - 20\mu m$	$1 - 20\mu m$	$1 - 20\mu m$	$0.34N_{bp}nm$
	Semi-flexible	Stiff	Usually flexible	Flexible for large enough N_{bp}

STIFF

SEMI-FLEXIBLE

FLEXIBLE



BENDING ENERGY DOMINANT



ENTROPY DOMINANT

