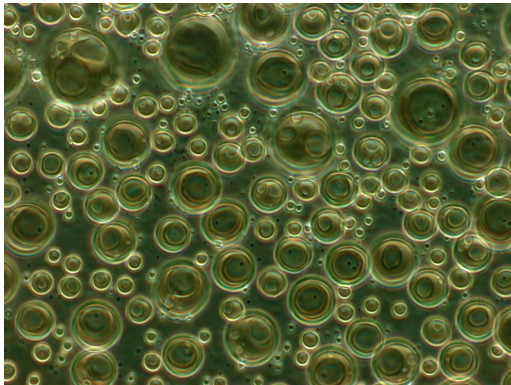
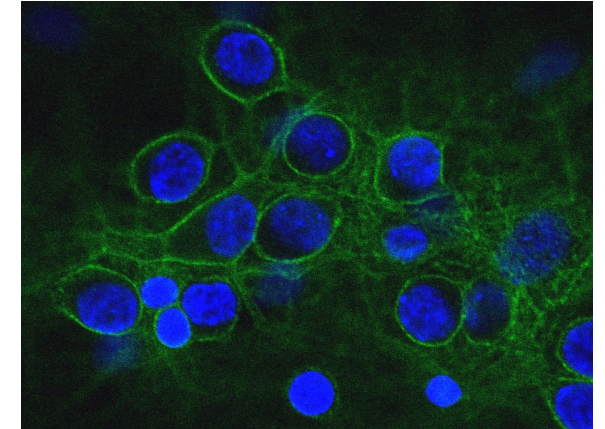
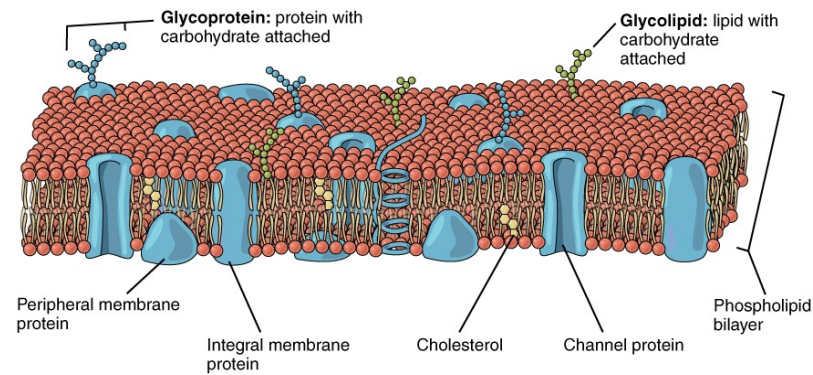
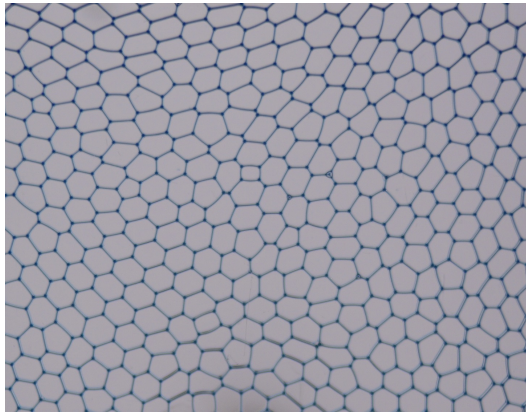


ME470: Mechanics of Soft and Biological Matter

Lecture 14: Review



Sangwoo Kim

MESOBIO – IGM – STI – EPFL

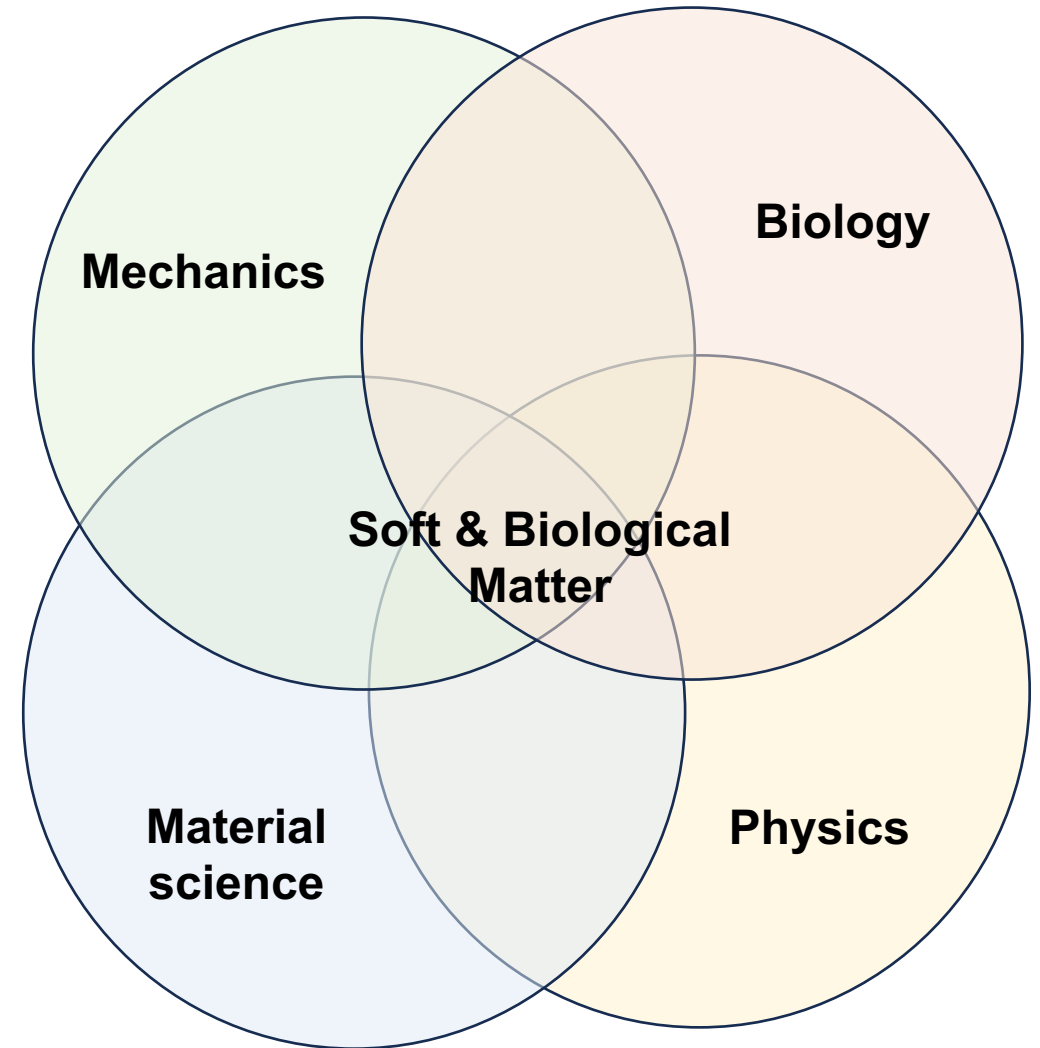
Red Blood Cells

Soft and Biological Matter

- Polymer melts/solutions
- Foams, emulsions, suspensions
- Granular materials
- Rubber
- Cells
- Tissues, Organs
- Membrane, vesicles

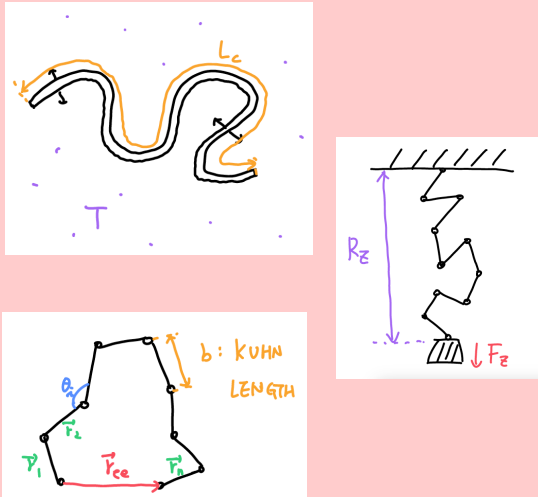
Many, but not all, soft and biological matter

- Are viscoelastic/viscoplastic
- Are self-organized
- Show “slow” relaxation of strain
- Show entropic effects (thermal fluctuations)



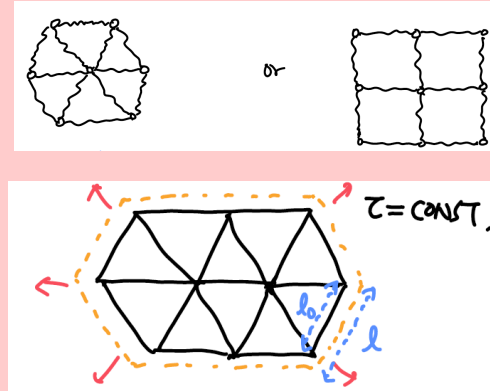
Objective: a comprehensive understanding of theoretical (and computational) modeling of soft and biological matter, emphasis on biological system

Part 1



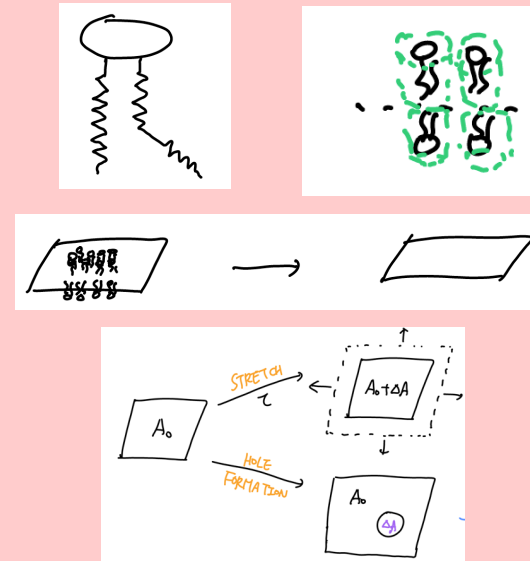
Mechanics of 1D elements

Part 2



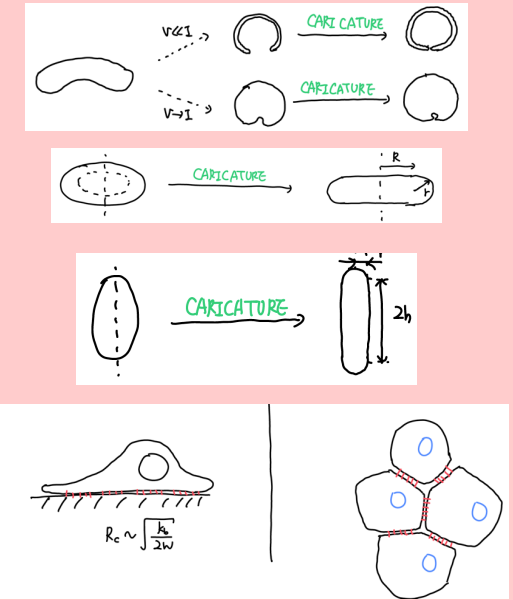
Mechanics of 2D network

Part 3



Mechanics of membranes

Part 4



Mechanics of cells and tissues

Relation between external load and deformation

3D homogeneous isotropic linear elastic materials

$$\sigma_{ik} = 2\mu \left(\varepsilon_{ik} - \frac{1}{3} \varepsilon_{ll} \delta_{ik} \right) + K \varepsilon_{ll} \delta_{ik}$$

Shear modulus

Bulk modulus

2D homogeneous isotropic linear elastic materials

$$\tau_{ij} = 2\mu_A \left(\varepsilon_{ij} - \frac{1}{2} \varepsilon_{ll} \delta_{ij} \right) + K_A \varepsilon_{ll} \delta_{ij}$$

Area shear modulus

Area stretch modulus



We mainly used strain energy formalism

$$u = \frac{1}{2} \sigma_{ik} \varepsilon_{ik}$$

Use different energy functionals

u is minimal for $ds = 0, d\varepsilon_{ik} = 0$

h is minimal for $ds = 0, d\sigma_{ik} = 0$ $h = u - \sigma_{ik}\varepsilon_{ik}$

f is minimal for $dT = 0, d\varepsilon_{ik} = 0$ $f = u - Ts$

g is minimal for $dT = 0, d\sigma_{ik} = 0$ $g = u - Ts - \sigma_{ik}\varepsilon_{ik}$

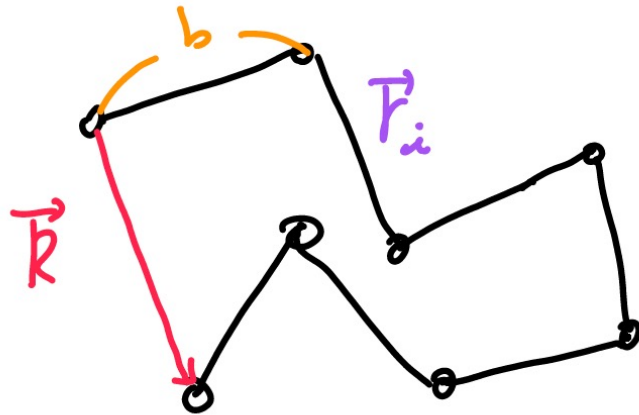
Statistical Mechanics

Entropy: $S = k_b \ln \Omega$

Canonical ensemble: $Prob(E_A) = \frac{1}{Z} e^{-\beta E_A}$ $Z = \sum_{E_A} e^{-\beta E_A}$

- Stretching vs bending $\rightarrow$ Inextensible assumption
- Persistence length: $l_p = EI/k_B T$
 - competition between energetic influence and entropic influence
 - Stiff rod vs flexible filament

Ideal chain: polymer model in the flexible limit



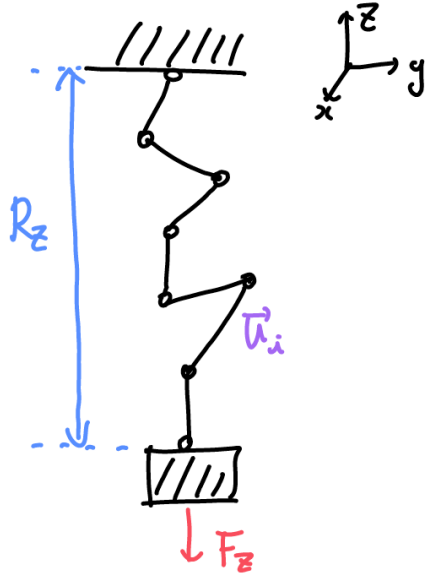
$$\langle \vec{R} \rangle = 0 \quad \langle R^2 \rangle = \langle \vec{R} \cdot \vec{R} \rangle = nb^2$$

- n inextensible segments are joined by frictionless hinge
- Same as random walk $\rightarrow$ Gaussian distribution

$$F = \left(\frac{3k_B T}{nb^2} \right) R$$

k_{sp} : spring constant

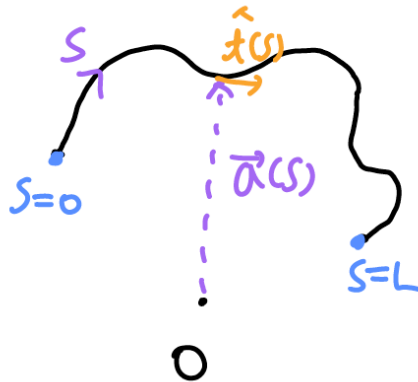
Freely jointed chain: realistic description at $R \sim L$



- n inextensible segments are joined by frictionless hinge with weight attached at the end
- Use canonical ensemble
- IC recovered for small F_z

$$\langle R_z \rangle = nb \left[\coth \left(\frac{bF_z}{k_B T} \right) - \frac{k_B T}{bF_z} \right]$$

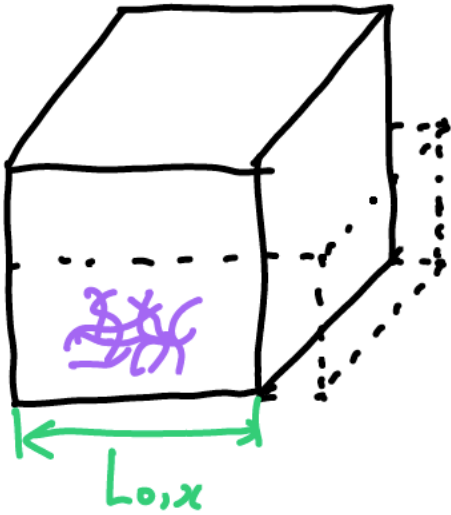
Worm-like chain: continuous elastic curve in 3D



$$F_z = \frac{k_B T}{l_p} \left[\frac{1}{4} \left(1 - \frac{\langle R_z \rangle}{L} \right)^{-2} - \frac{1}{4} + \frac{\langle R_z \rangle}{L} \right]$$

$$b = 2l_p$$

Bulk entropic materials: entangled entropic springs (disordered)



- Use affine deformation assumption
 - microscopic deformation=macroscopic deformation
- Consider free energy change for stretching

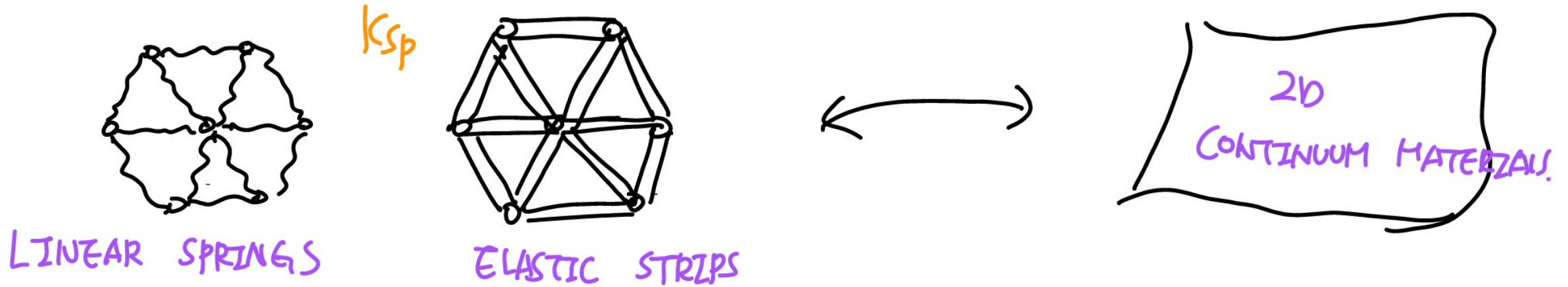
$$\langle \Delta \Psi \rangle = \frac{k_B T}{2} \left(\lambda^2 + \frac{2}{\lambda^2} - 3 \right) \quad (\text{uniaxial stretching})$$

$$\sigma_{xx} = \frac{F_x}{A} = \frac{N}{AL_{0,x}} k_B T \left(\lambda - \frac{2}{\lambda^2} \right) = \rho_c k_B T \left(\lambda - \frac{2}{\lambda^2} \right)$$

Chain volume density



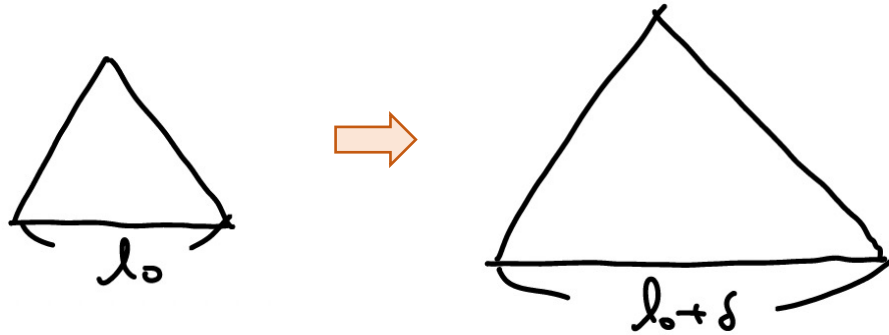
$$E = 3\rho_c k_B T$$



Constitutive relation (2D linear elastic): $\tau_{ij} = C_{ijkl} \varepsilon_{kl} \quad i, j, k, l \in \{x, y\}$

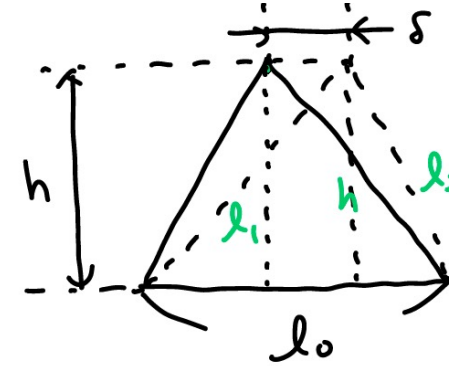
- ⇒ Symmetry and thermodynamics reduces coefficients from 16 to 6
- ⇒ 6-fold symmetry only leaves 2 independent coefficients
- ⇒ Regular triangular spring network as 2D isotropic homogeneous elastic materials!

Bulk modulus



$$K_A = \frac{\sqrt{3}}{2} k_{sp}$$

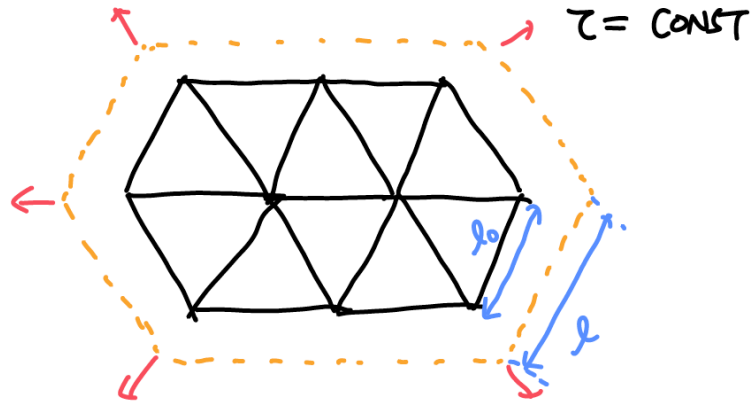
Shear modulus



$$\mu_A = \frac{\sqrt{3}}{4} k_{sp}$$

Network under external stress

extension



$$l = \frac{l_0}{1 - \tau/\tau_b}$$

$$\tau_b = \sqrt{3}k_{sp}$$

Compression

Mode1: uniform contraction

$$\tau_c < \tau < 0$$

Uniform contraction

Mode2: collapse

$$\tau < \tau_c$$

Collapse



$$\tau_c = \frac{1}{8}\tau_b$$

Prestressed network

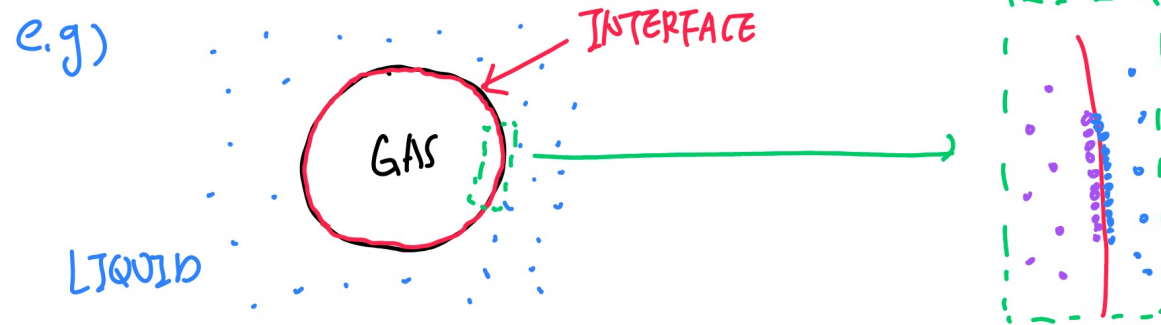
$$K_A = \frac{\sqrt{3}}{2} k_{sp} \left(1 - \frac{\tau}{\sqrt{3} k_{sp}} \right)$$

$$\mu_A = \frac{\sqrt{3}}{4} k_{sp} \left(1 + \frac{\sqrt{3} \tau}{k_{sp}} \right)$$

Numerical simulation of 2D network

- Rigidity percolation transition
- Entropic effects (finite temperature)
- Disordered network structure (diluted triangular lattice, Mikado network, packing inspired network)

Simple interface: surface tension



Young-Laplace law

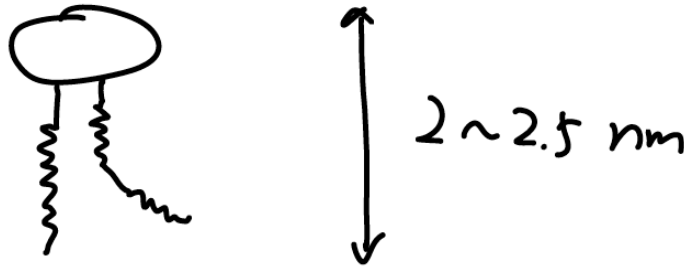
$$\Delta P = P_g - P_l = \gamma \frac{dA}{dV}$$

Surfactants: makes interface become elastic

Phospholipids (e.g. DOPC)

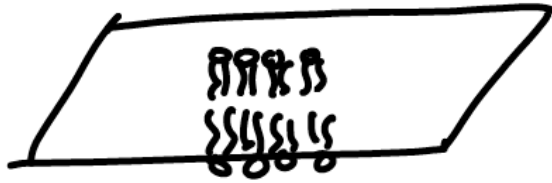
Hydrophilic head

Hydrophobic tail



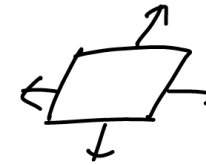
- Critical concentration n_{agg} , where interface gets preferentially populated!
- Monolayer: $K_A = (k + 1)$

Bilayer

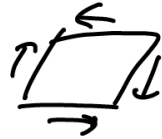


Membrane as 2D continuum materials

(1) stretch/compression: $K_A^{bl} = 2(k + 1)\gamma \sim 0.1 - 0.2 \text{ J/m}^2$



(2) shear: liquid in plane



(3) bending



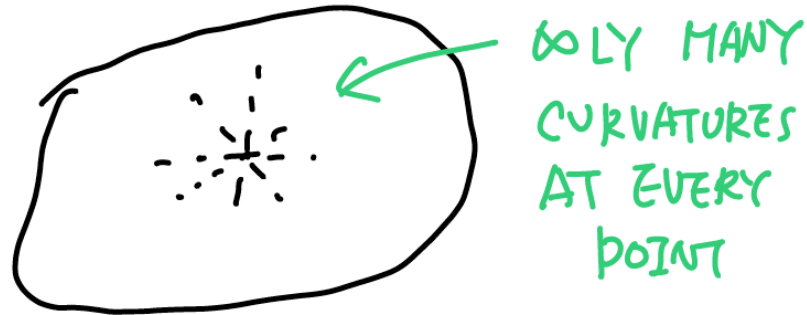
- Plate bending in one direction: $k_b = \frac{1}{12} h^2 K_A$
- 3D thin plate: $U_{b,plate} = \frac{1}{2} \left(\frac{Eh^3}{12(1-\nu^2)} \right) \iint \left[(\epsilon_{xx} + \epsilon_{yy})^2 + 2(1-\nu)(\epsilon_{xy}^2 - \epsilon_{xx}\epsilon_{yy}) \right] dx dy$

$$U = \frac{1}{2} k_b \iint (2H)^2 dA + k_G \iint K_G dA$$

Helfrich free energy

Differential geometry

More general definition of mean and Gaussian curvature:



$$H = \frac{1}{2}(C_1 + C_2) = \frac{1}{2}\left(\frac{1}{R_1} + \frac{1}{R_2}\right)$$

$$K_G = C_1 C_2 = \frac{1}{R_1 R_2}$$

Gauss-Bonnet Theorem: for closed surface

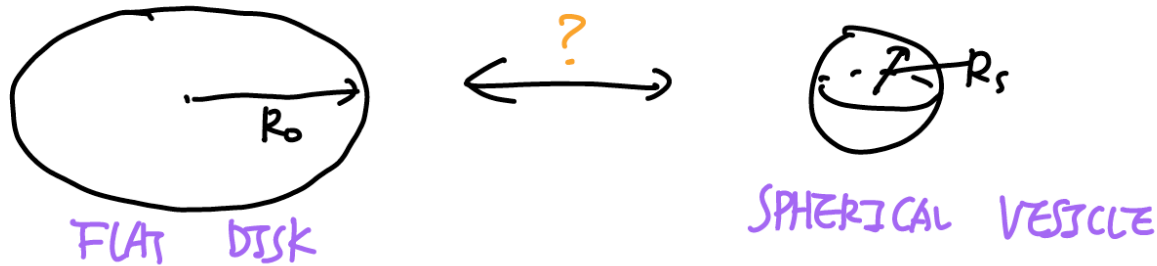
$$\iint K_G dA = \oint K_G dA = 4\pi(1 - g)$$

General differential geometric formalism to compute H and K_G :

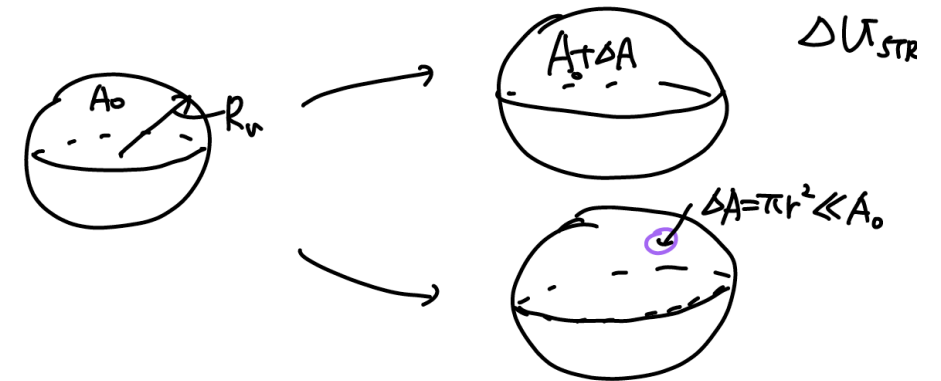
$$H = \frac{eG - 2fF + gE}{2(EG - F^2)}$$

$$K_G = \frac{eg - f^2}{EG - F^2}$$

Vesicle formation: competition between line tension and bending energy



Rupture: competition between line tension and stretching energy



$$U = \frac{1}{2} k_b \iint (2H)^2 dA + k_G \iint K_G dA + \int_{\partial A} \lambda ds + \frac{1}{2} K_A \iint \varepsilon_{II}^2 dA$$

Bending

Bending

Line
tension

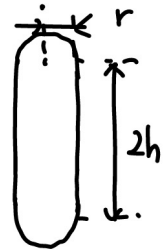
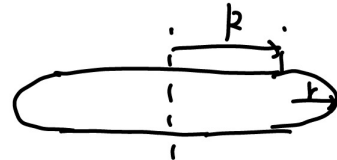
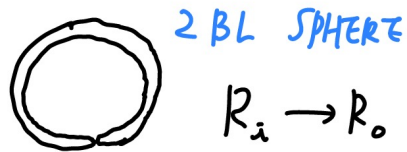
stretching

Refined membrane bending model

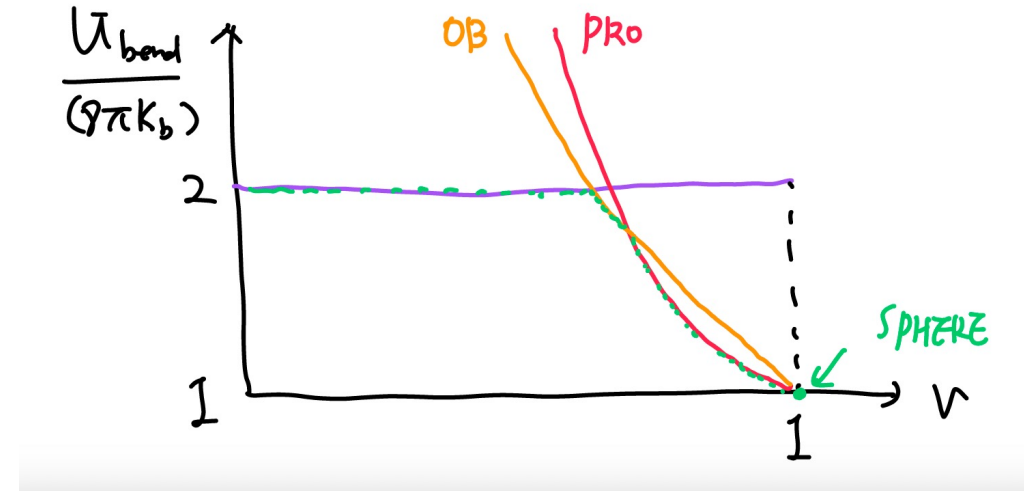
- Spontaneous curvature
- Area – difference elasticity model (ADE model)

Vesicle shapes using the minimal model:

(1) Mode analysis



SPHERE CYLINDER



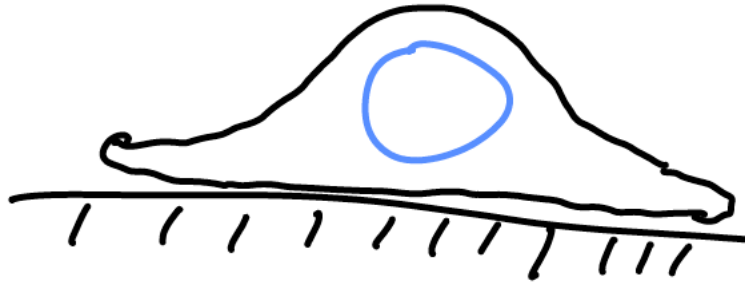
(2) Numerical computation: discretizing vesicle shape into triangulation

(3) Variational calculus: analytic approach to minimize a functional

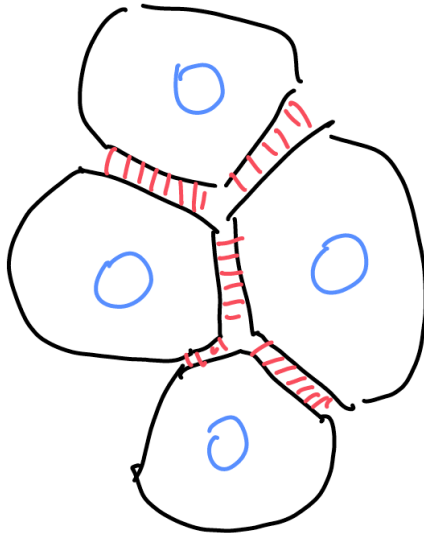
$$k_b \vec{\nabla}^4 \zeta - \sigma = 0$$

Plate equation!

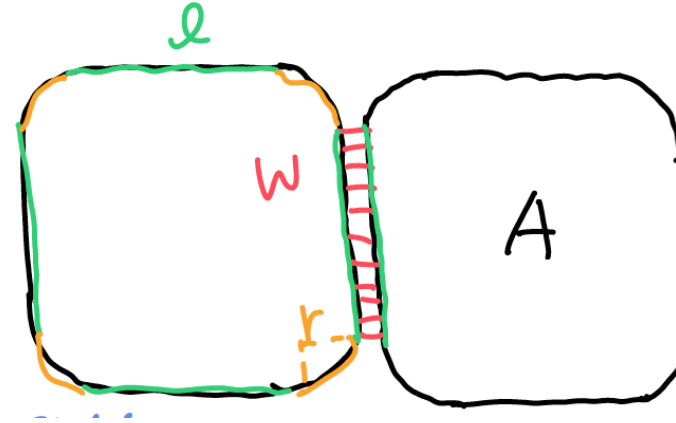
Cell-substrate adhesion



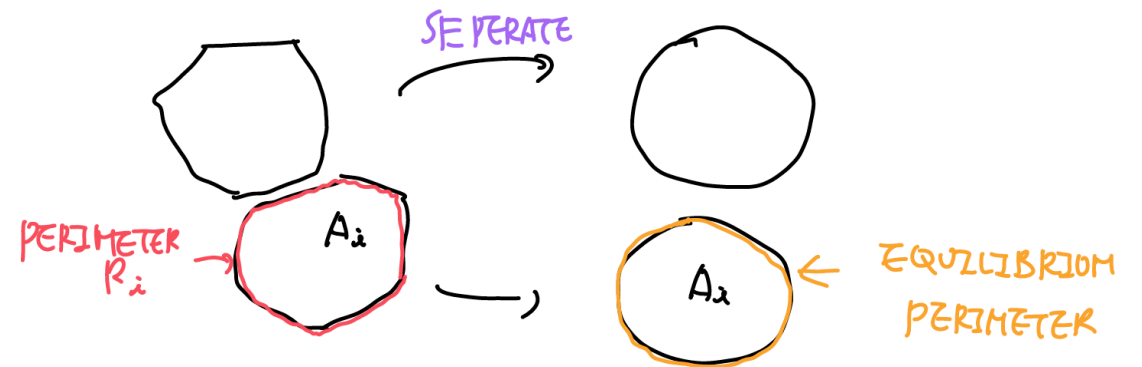
Cell-substrate adhesion



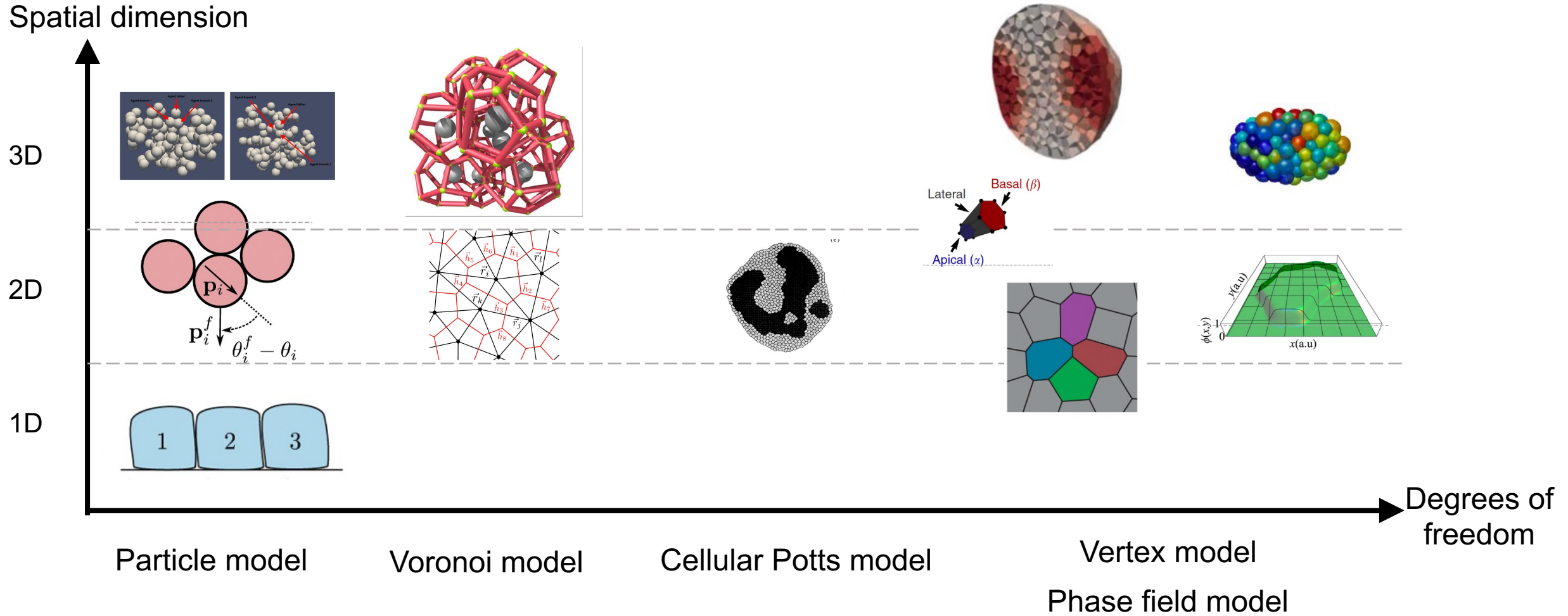
Competition between adhesion & bending



Competition between adhesion & stretching



Cell-based discrete model



EPFL Final exam

- 2:15pm – 5:15pm (3hours), December 19th, 2024, CE15
- You must bring your **STUDENT ID** and **CALCULATOR**
- A formula sheet and scratch papers will be provided.
- Format
 - 10 short questions
 - 3 quantitative analysis questions