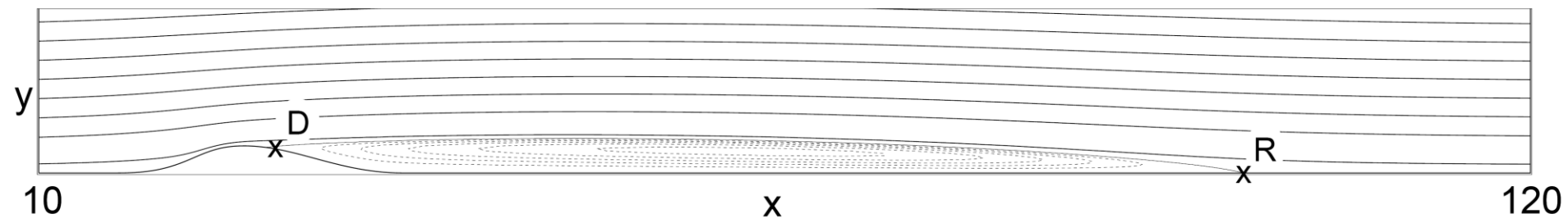
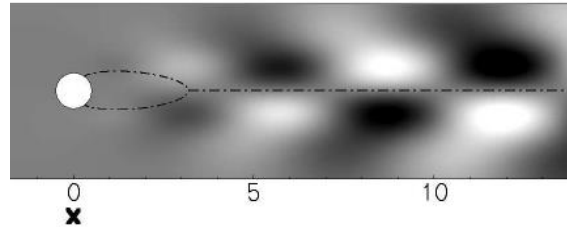


Global linear instability of flows



Global linear instability of flows



*Stability of viscous flow past
a circular cylinder*
A. Zebib



1971

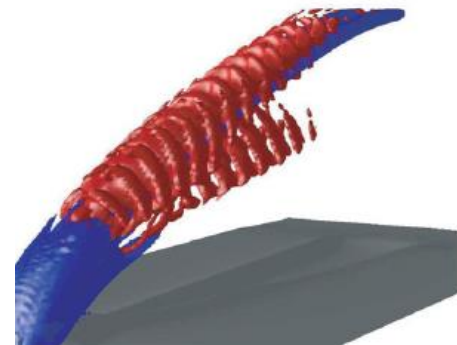
2 D

2009

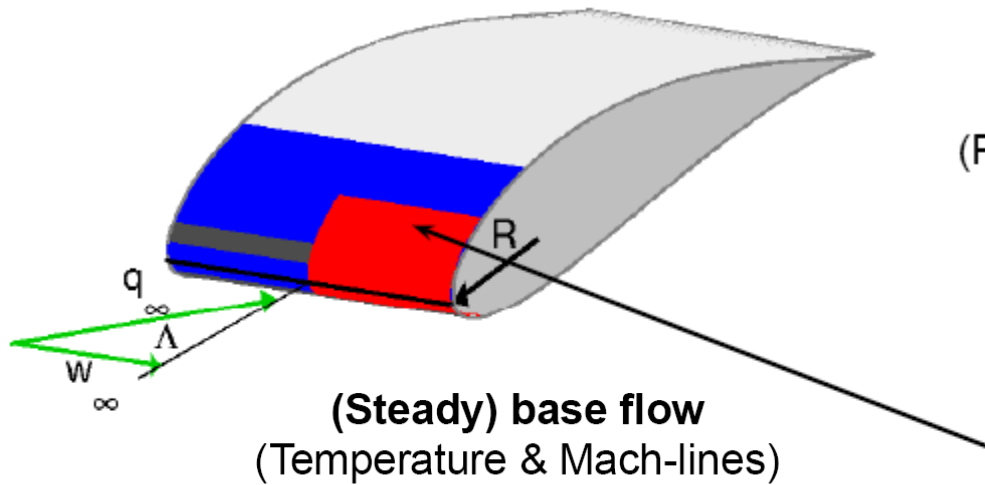
3 D

*Accurate solution of the Orr–
Sommerfeld stability equation*
S. A. Orszag

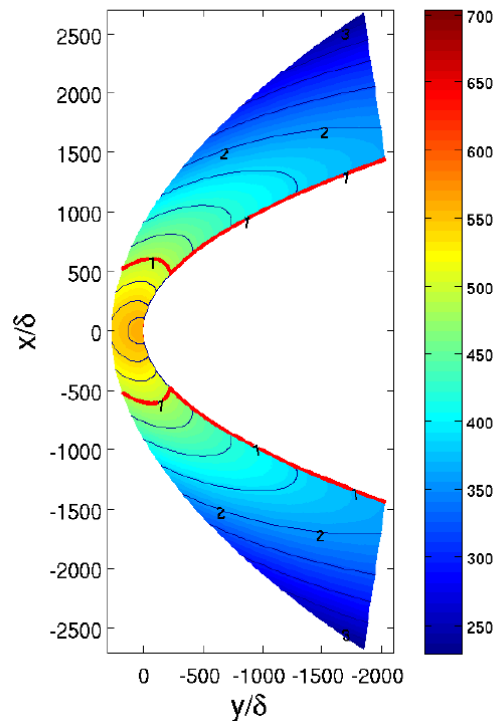
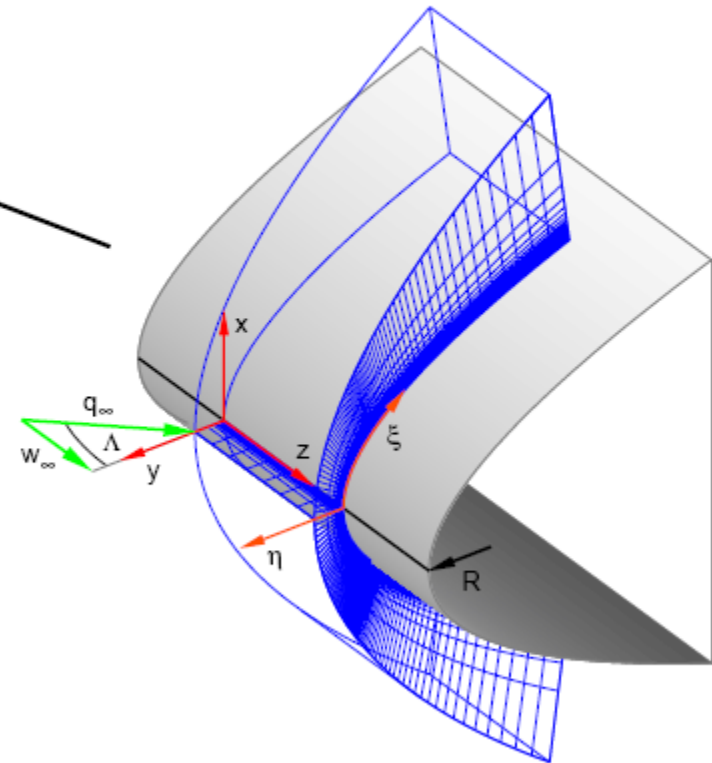
*Global stability of a jet
in crossflow*
S. Bagheri



Global linear instability of flows in complex geometry

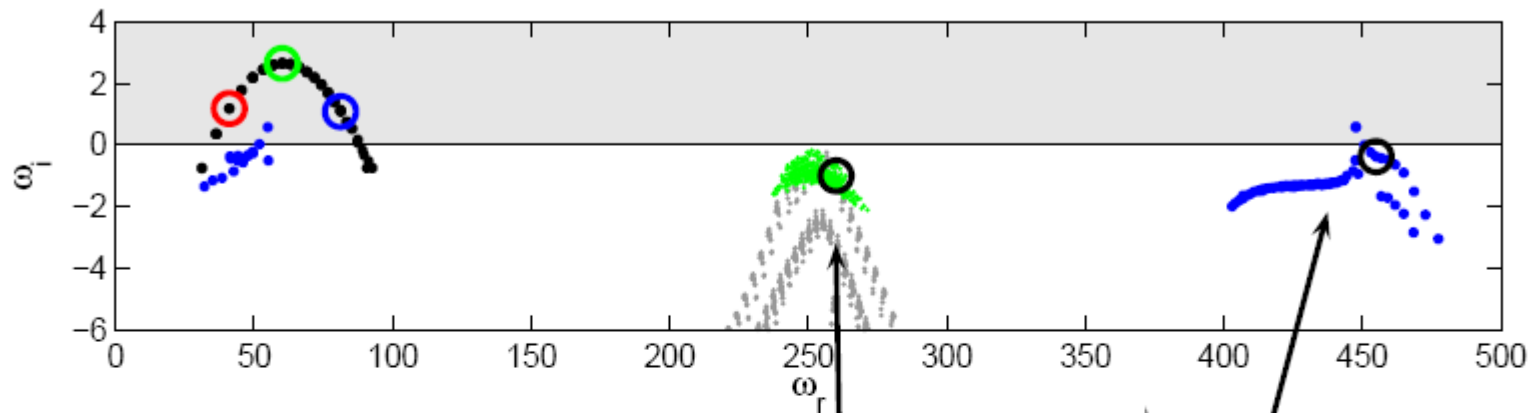


Leading-edge region
(Parabolic body of infinite span)

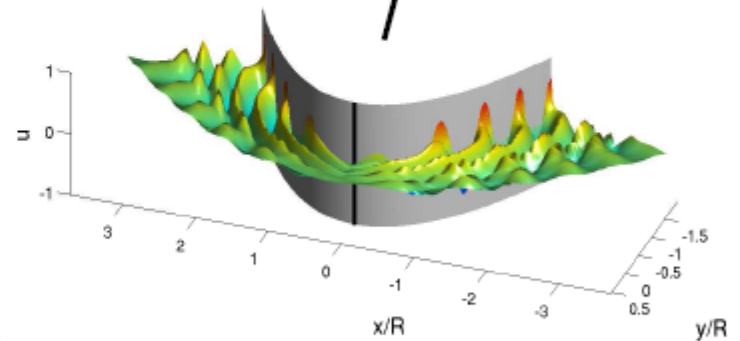
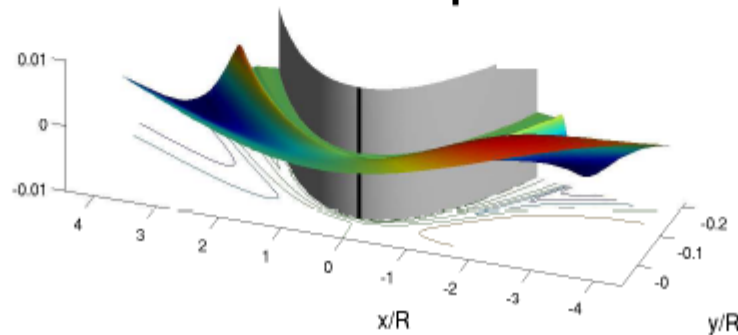
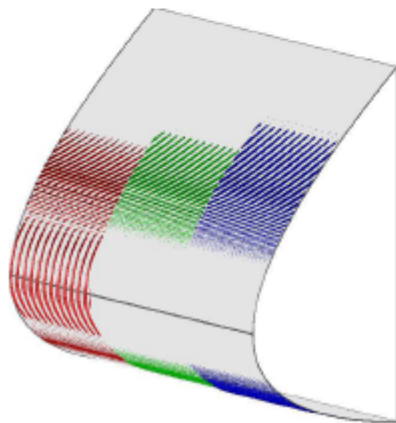


Mack and Schmid 2010

Global spectrum: $\phi'(x, y, z, t) = \tilde{\phi}(x, y)e^{i(\beta z - \omega t)}$ with $\omega = \omega_r + i\omega_i$



Associated global modes $\tilde{v}(x, y, z)$



Mack and Schmid 2010

Discretization methods

All standard methods

- Spectral methods (memory saving)
 - Finite elements
 - Finite volumes
 - Finite differences
- } Sparse and parallelizable

Very few compressible studies

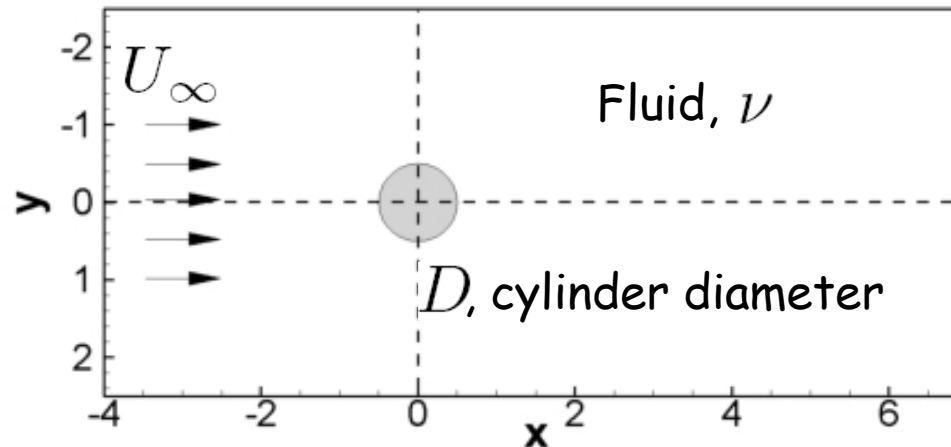
Apparently no use of « non-standard » methods:

- particle methods, vortex methods,...
- Lattice-Boltzmann

Global linear instability of flows in complex geometry

1. Global instability of a classical 2D flow
2. Less classical unstable flows
3. Stable flows

Wake behind cylinder flow



$$Re = \frac{U_\infty D}{\nu}$$

Incompressible 2D flow described by

(u, p)

Velocity

Pressure

Navier-Stokes equations

$$\partial_t u + \nabla u \cdot u = -\nabla p + Re^{-1} \nabla^2 u,$$

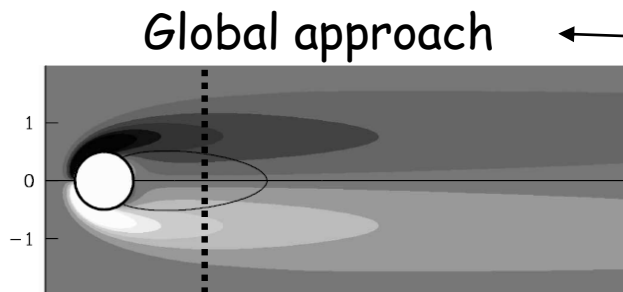
$$\nabla \cdot u = 0$$

Stability analysis

Perturbation expansion

$$(u, p) = (U, P) + (u', p') \quad \text{Perturbations}$$

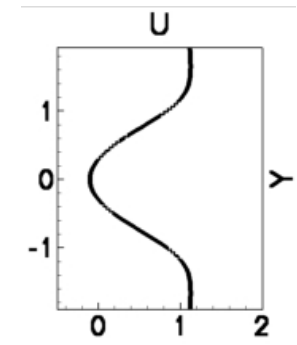
Stationary base flow



$$\leftarrow U(x, y) \quad U(y) \longrightarrow$$

Local approach

Huerre & Monkewitz (1990)



Base flow equations

$$\begin{aligned} \nabla U \cdot U &= -\nabla P + Re^{-1} \nabla^2 U, \\ \nabla \cdot U &= 0 \end{aligned}$$

Zebib, Jackson (1987)

Linearized perturbation equations

$$\begin{aligned} \partial_t u' + \nabla U \cdot u' + \nabla u' \cdot U + \cancel{\nabla u' \cdot u'} &= -\nabla p' + Re^{-1} \nabla^2 u', \\ \nabla \cdot u' &= 0 \end{aligned}$$

Analyse de stabilité globale

$$U(x, y)$$



$$(\mathbf{u}', p')(x, y, t) = (\hat{\mathbf{u}}, \hat{p})(x, y) \exp[\sigma t]$$

Global mode(complex)

Growth-rate

$$\sigma = \lambda + i\omega$$

frequency

$$St = \frac{\omega}{2\pi}$$

Global stability equations

$$\sigma \hat{u} + \nabla \hat{u} \cdot U + \nabla U \cdot \hat{u} = -\nabla \hat{p} + Re^{-1} \nabla^2 \hat{u},$$

$$\nabla \cdot \hat{u} = 0,$$

Global stability analysis solvers

For a given value of Re , numerically solve

- non linear equations,

$$\nabla U \cdot U = -\nabla P + Re^{-1} \nabla^2 U,$$

(Newton method)

- Eigenvalue problem

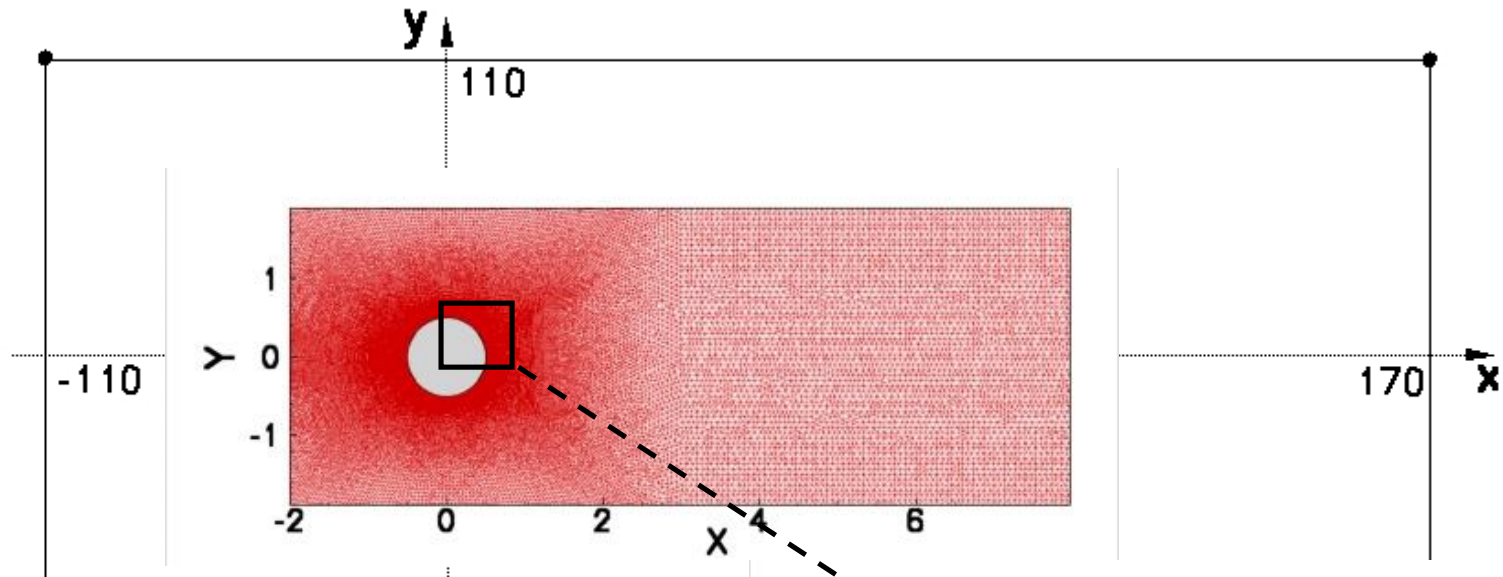
$$\sigma \hat{u} + \nabla \hat{u} \cdot U + \nabla U \cdot \hat{u} = -\nabla \hat{p} + Re^{-1} \nabla^2 \hat{u},$$

(Krylov-Arnoldi method)

Spatial discretization = finite element methods

(FreeFem++ freeware)

Computational model and mesh



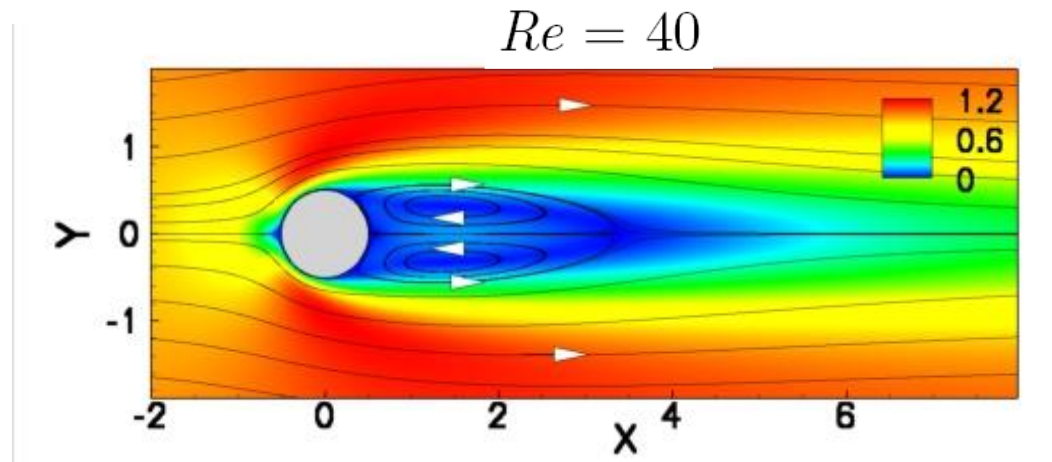
Triangular mesh

Number of triangles ~ 375 000

Number of nodes ~ 190 000

Taylor-Hood finite elements (P2,P2,P1) → number of degrees of freedom ~ $1.6 \cdot 10^6$

Base flow



Drag coefficient

$$C_D = \frac{F_D}{0.5 D U_\infty^2}$$

C_D	$Re = 20$	$Re = 40$
Dennis & Chang (1970)	2.05	1.52
Fornberg (1980)	2.00	1.50
Ye et al. (1999)	2.03	1.52
Giannetti & Luchini (2007)	2.05	1.54
Marquet et al. (2008)	2.00	1.50

Valeur propre et mode global dominants

$$\Re\{\hat{u}\} \quad (\hat{u}, \hat{p}) \exp[\sigma t] \quad \sigma = \lambda + i\omega$$

Leading eigenvalue:

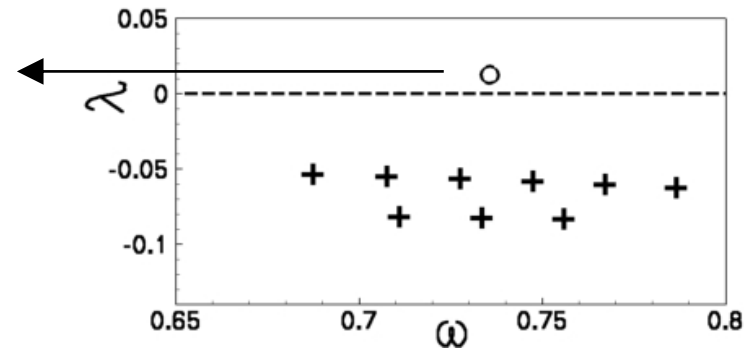
λ_{max}

if $\lambda_{max} < 0 \rightarrow$ Stable flow

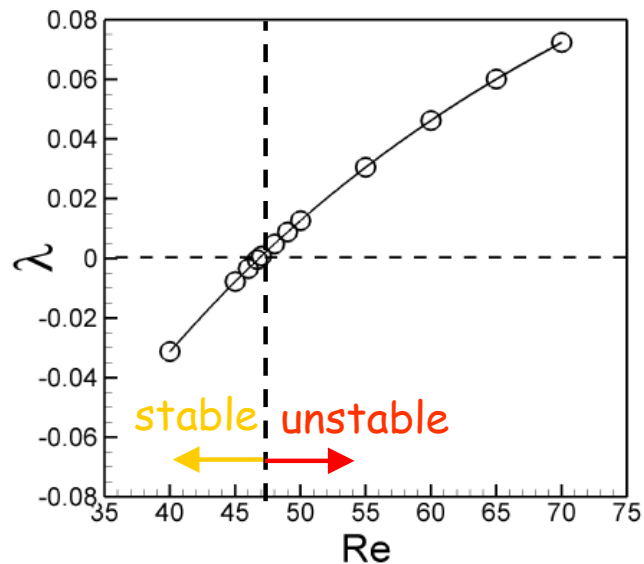
if $\lambda_{max} > 0 \rightarrow$ Unstable flow

Leading global mode

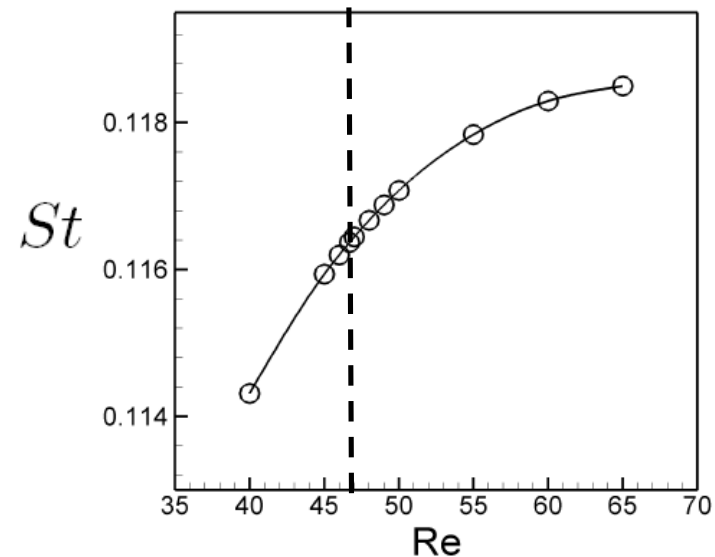
Spectrum at $Re = 50$



Evolution as a function of the Reynolds number



$$Re_c = 46.7(\pm 0.1)$$



$$St_c = 0.116$$

To keep in mind

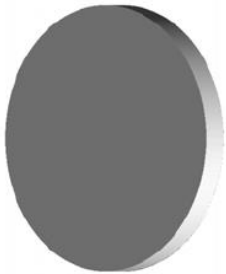
Global stability analysis=
Nonlinear problem (base flow) +
Eigenvalue problem

Global linear instability of flows in complex geometry

1. Global instability of a classical 2D flow
2. Less classical unstable flows
3. Stable flows

Prototype flows

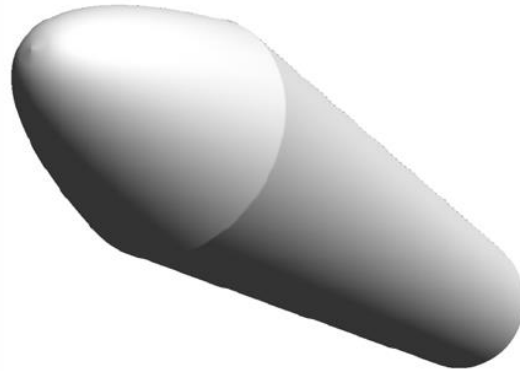
Axisymmetric wakes



Disk



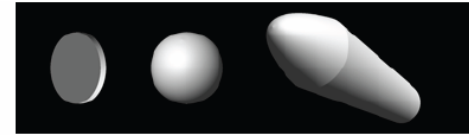
Sphere



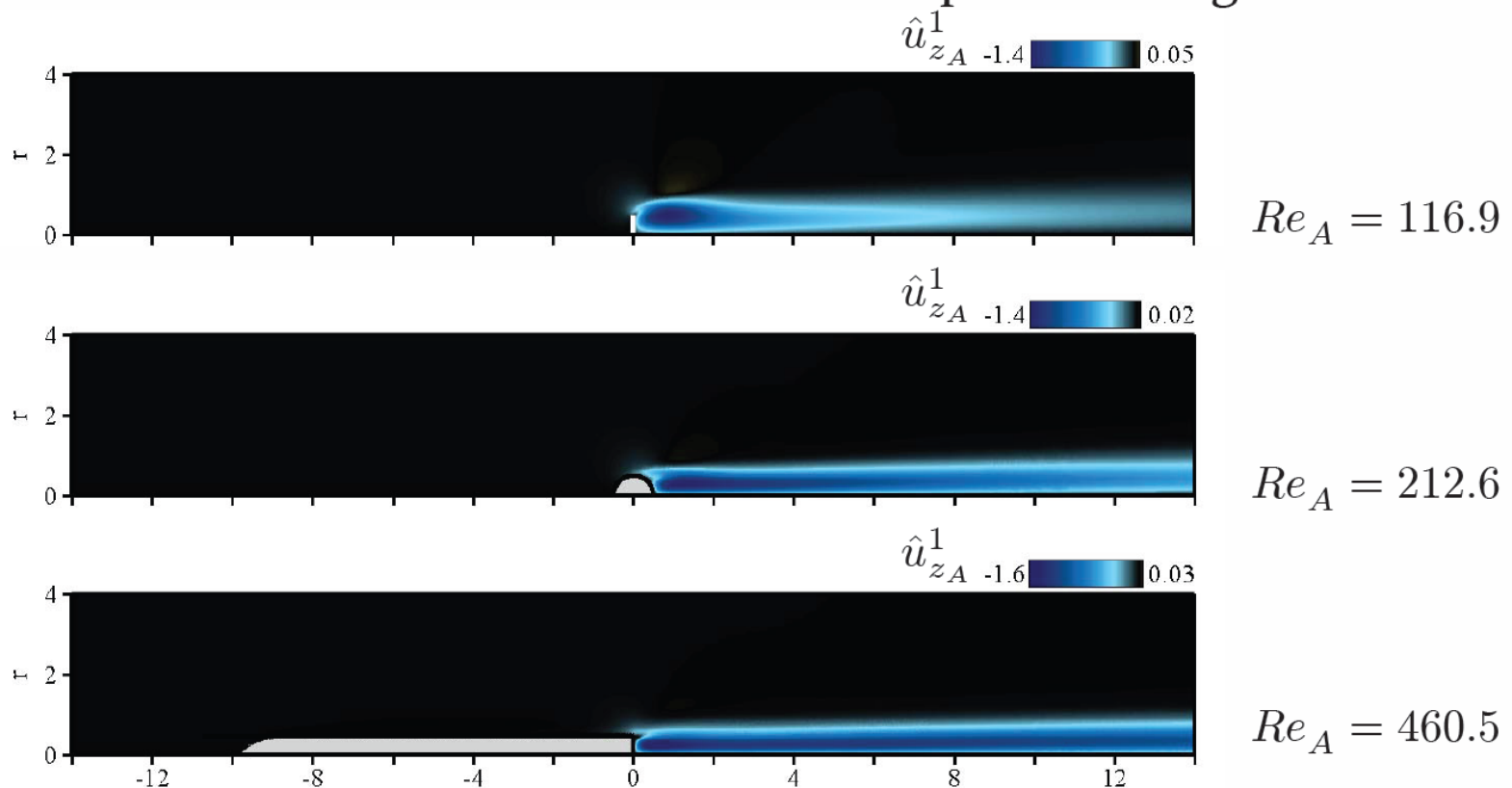
Blunt base

Meliga et al. 2008,2009,2010

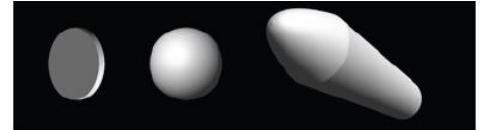
Leading global modes



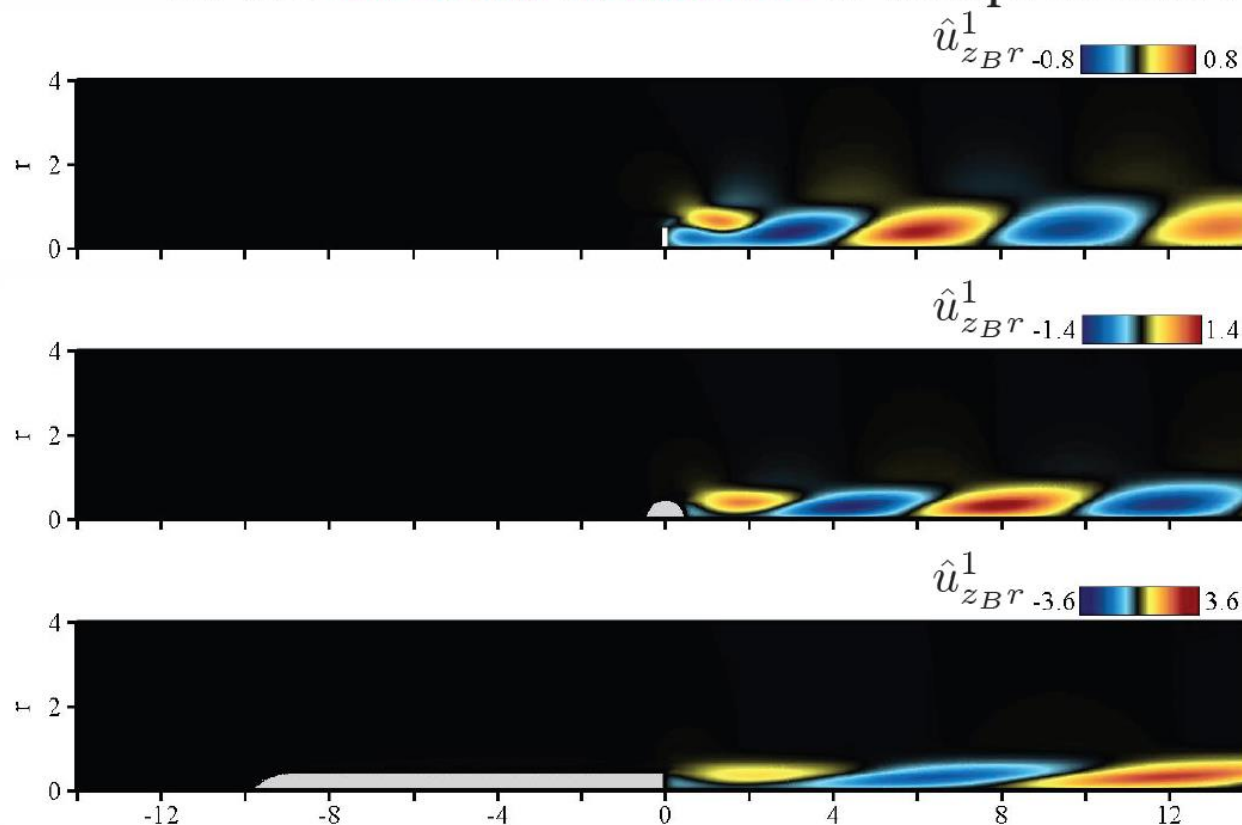
Same bifurcation sequence for all prototype flows,
in the **INCOMPRESSIBLE** & compressible regimes



Leading global modes



Same bifurcation sequence for all prototype flows,
in the **INCOMPRESSIBLE** & compressible regimes



$$Re_B = 125.8$$

$$St = 0.12$$

$$Re_B = 280.7$$

$$St = 0.11$$

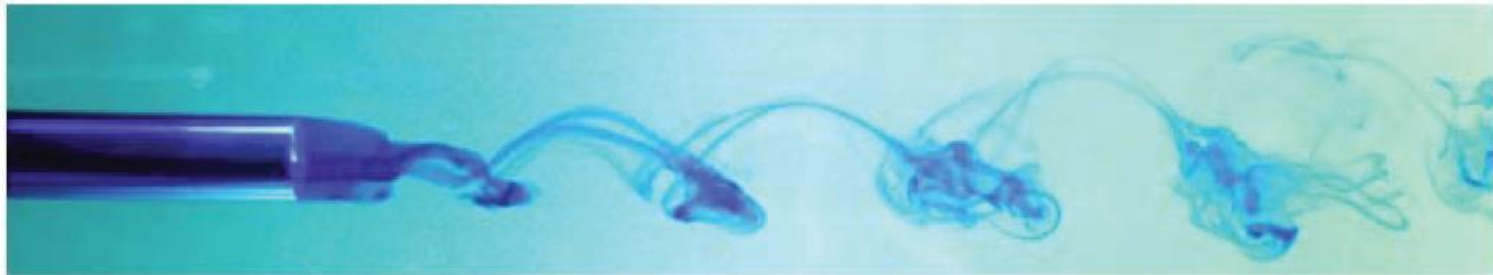
$$Re_B = 909.1$$

$$St = 0.07$$

How do these theoretical considerations compare with experiments



Sphere – Johnson & Patel (1999)

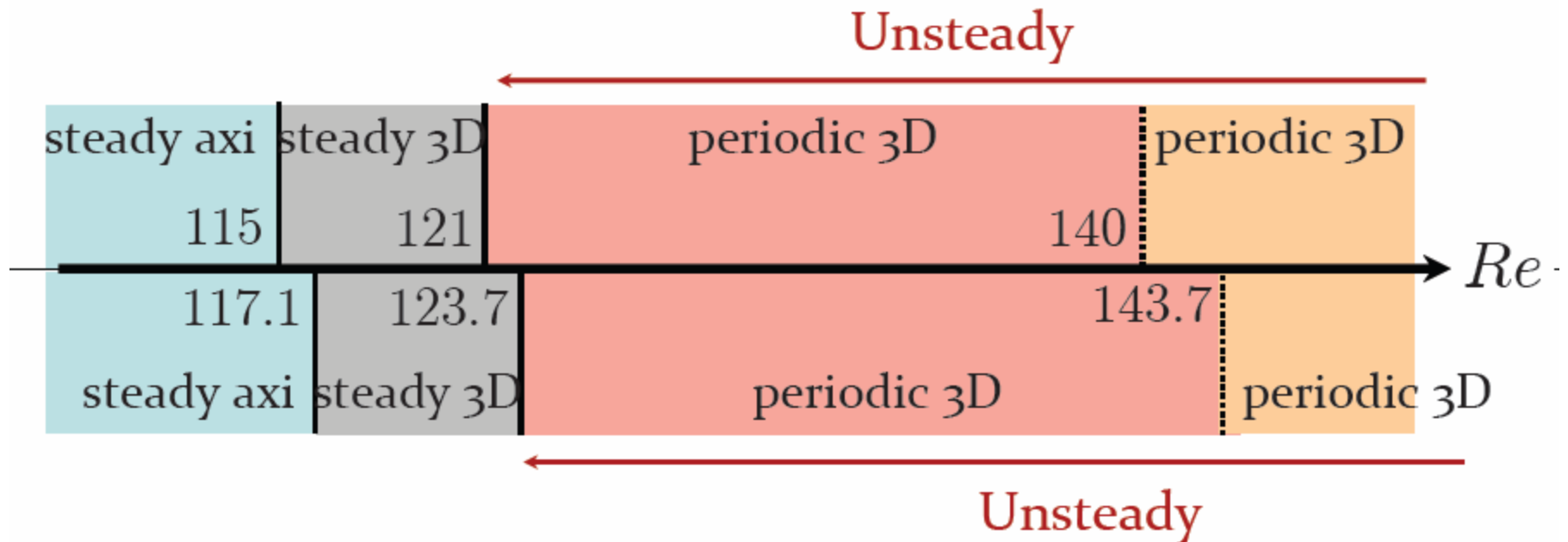


Blunt base – Siegel et al. (2008)

Remarkable predictions of successive symmetry breakings and thresholds

Direct numerical simulation of the 3D flow

Fabre et al. (2008)

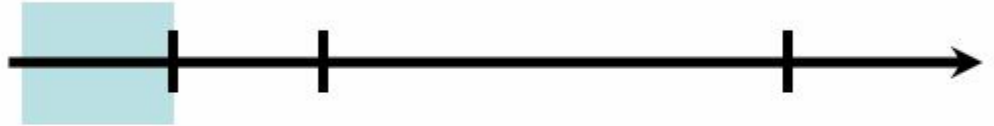


Weakly nonlinear global stability

Meliga et al. 2009

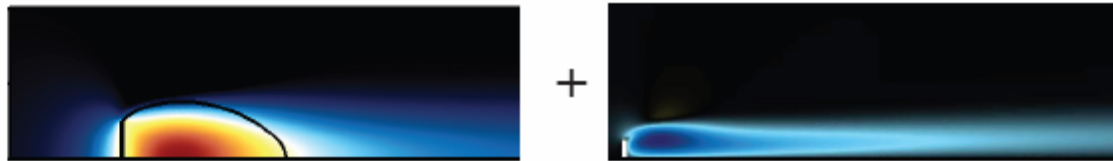
Stable solutions

- Steady axi



Stable solutions

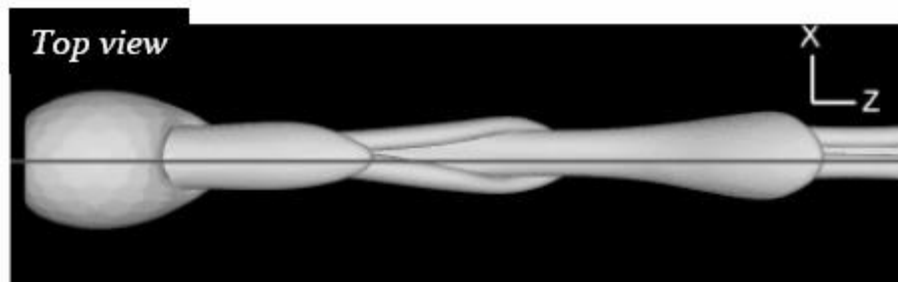
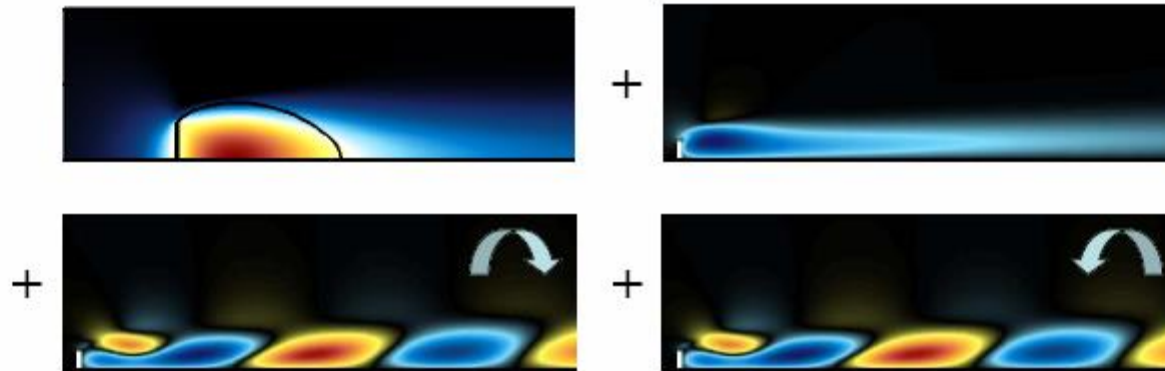
- Steady 3D + planar sym.



Numerical dye lines

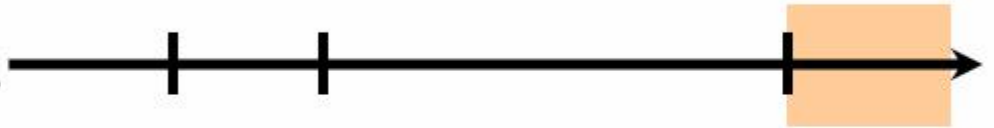
Stable solutions

- Periodic 3D, no sym.



Stable solutions

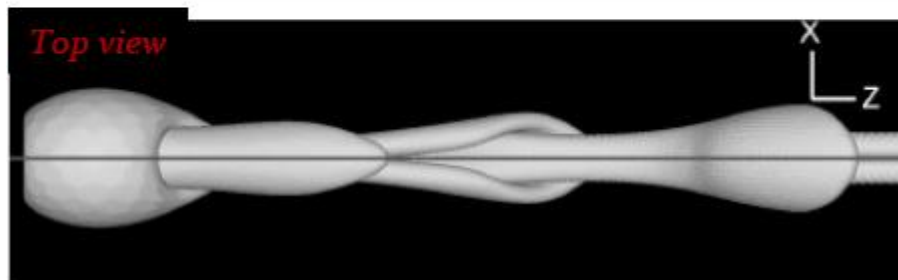
- Periodic 3D + planar sym.



+



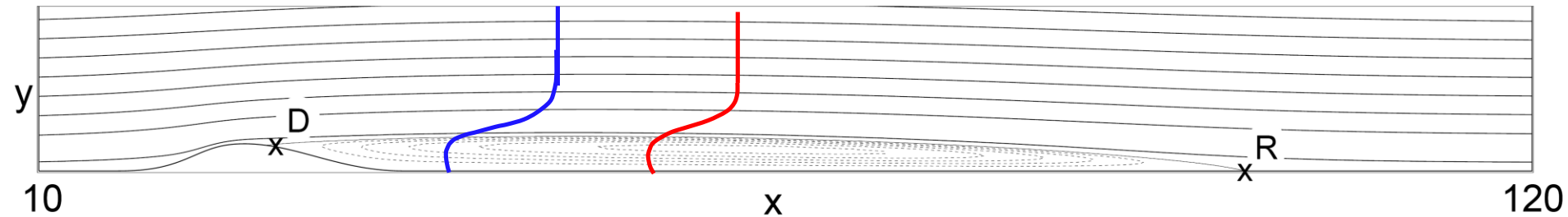
+



Global linear instability of flows in complex geometry

1. Global instability of a classical 2D flow
2. Less classical unstable flows
3. Stable flows

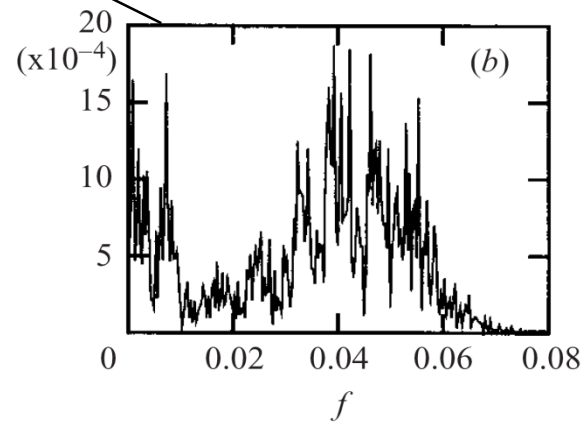
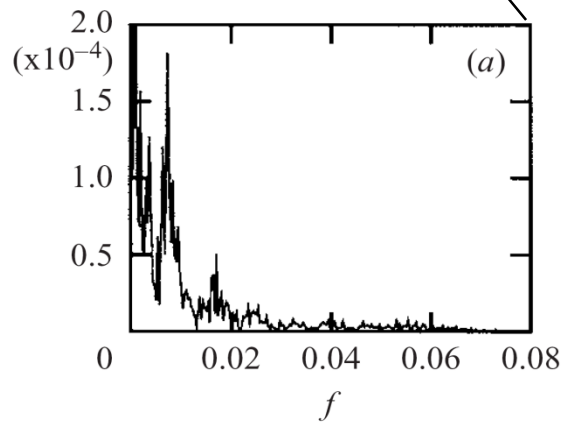
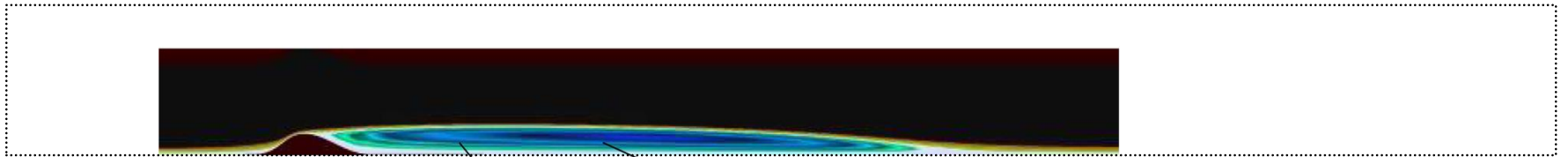
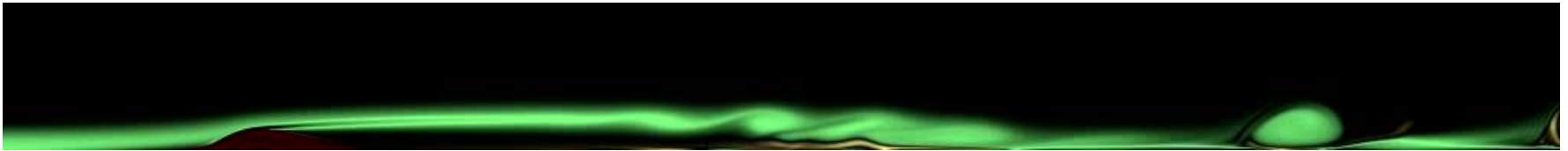
Global low frequency oscillations in a detached boundary layer



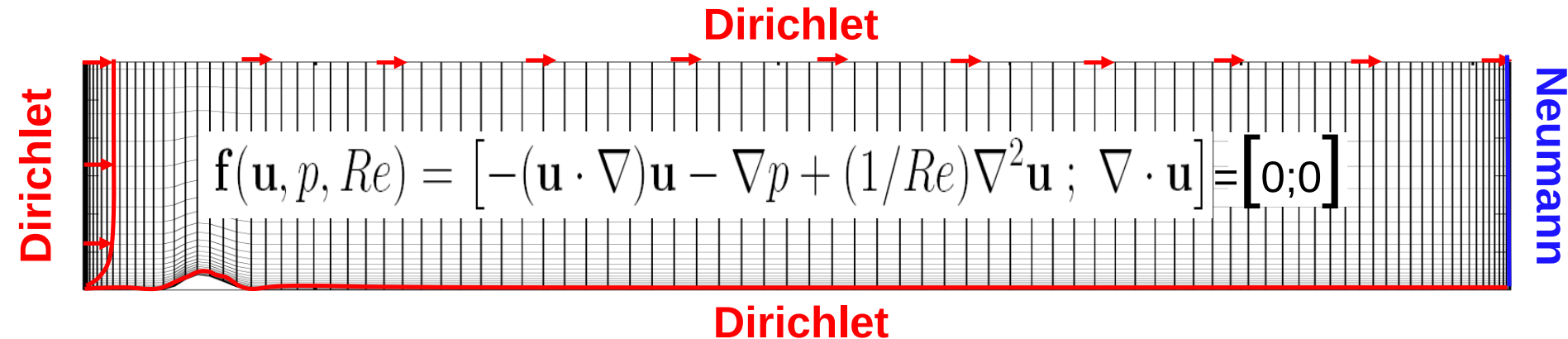
Locally parallel 1D instability fails!

Marquillie and Ehrenstein (2003)

Flapping in the DNS



Navier-Stokes steady states



Mapping and chebyshev-collocation in both streamwise x and normal y coordinates

Chebyshev discretization in a square: spurious pressure modes

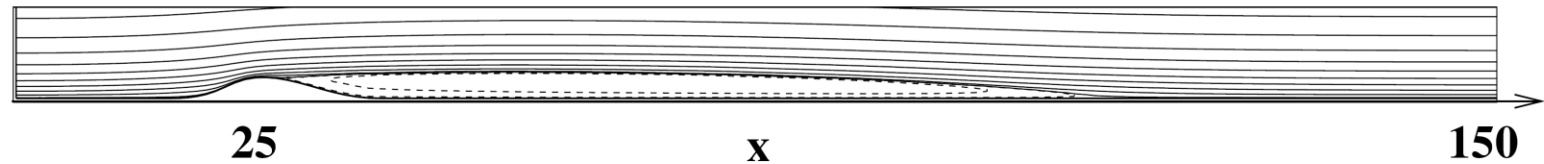
4 corners, $p_i = 0$ and $\nabla p_i = 0$

8 extra conditions: continuity of normal derivative for p at the corners and $p_i = 0$.

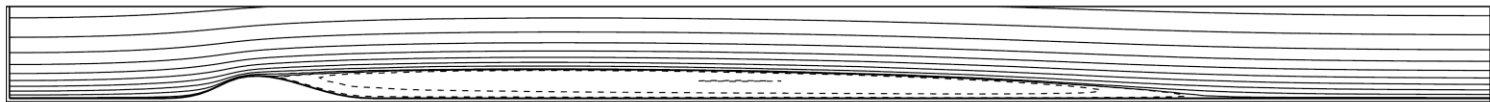
Domain length $L=300$, $H=30$, 250×40 collocation points

Continuation procedure to obtain unstable steady states

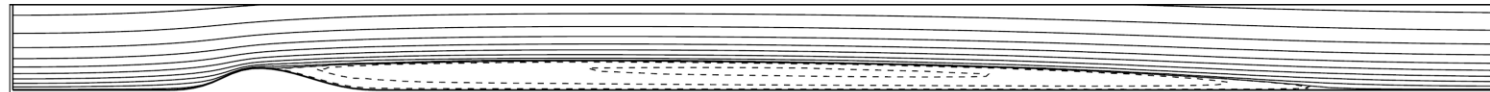
$h = 1.8$



$h = 1.9$



$h = 2, \text{Re} = 590$



$h = 2, \text{Re} = 680$

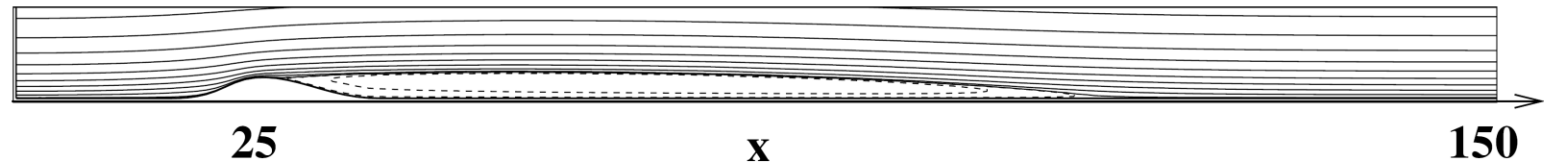


Ehrenstein and Gallaire (2008)

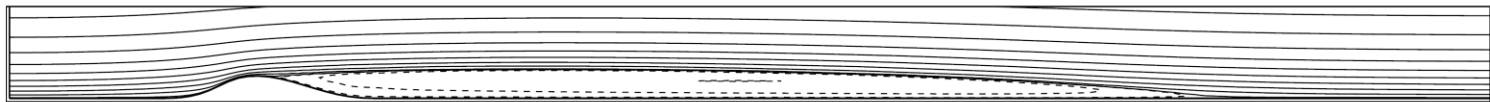
No topology change

Continuation procedure to obtain unstable steady states

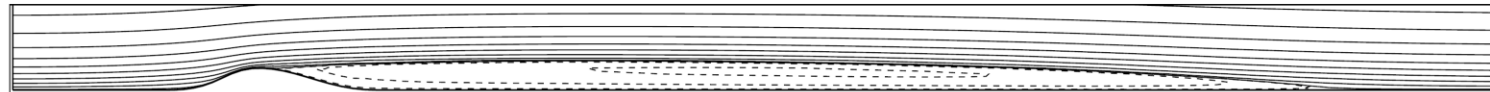
$h = 1.8$



$h = 1.9$



$h = 2, \text{Re} = 590$



$h = 2, \text{Re} = 680$



Ehrenstein and Gallaire (2008)

Reattachment increasingly difficult to capture

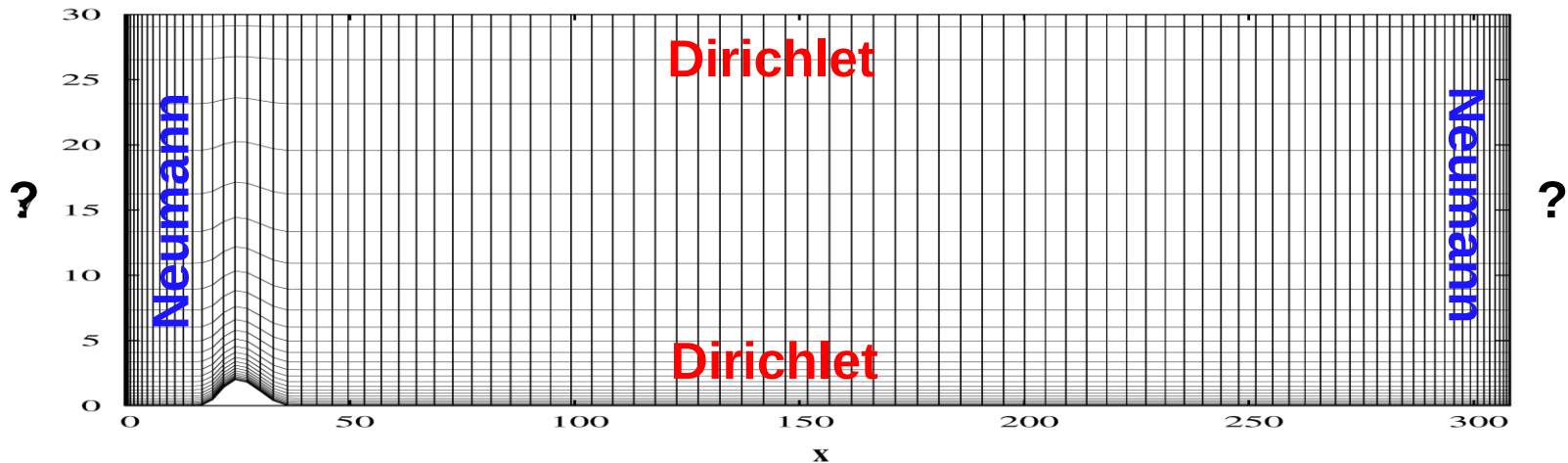
2D temporal global modes

$$\frac{\partial \mathbf{u}}{\partial t} = - \underbrace{(\underbrace{\mathbf{U}}_{\text{Base flow}} \cdot \nabla)}_{\text{Perturbation}} \mathbf{u} - (\mathbf{u} \cdot \nabla) \mathbf{U} - \nabla p + \frac{1}{Re} \nabla^2 \mathbf{u},$$

$$\nabla \cdot \mathbf{u} = 0,$$

$$[\mathbf{u}(x, y, z, t), p(x, y, z, t)] = [\hat{\mathbf{u}}(x, y), \hat{p}(x, y)] e^{\sigma t}$$

σ : growth rate

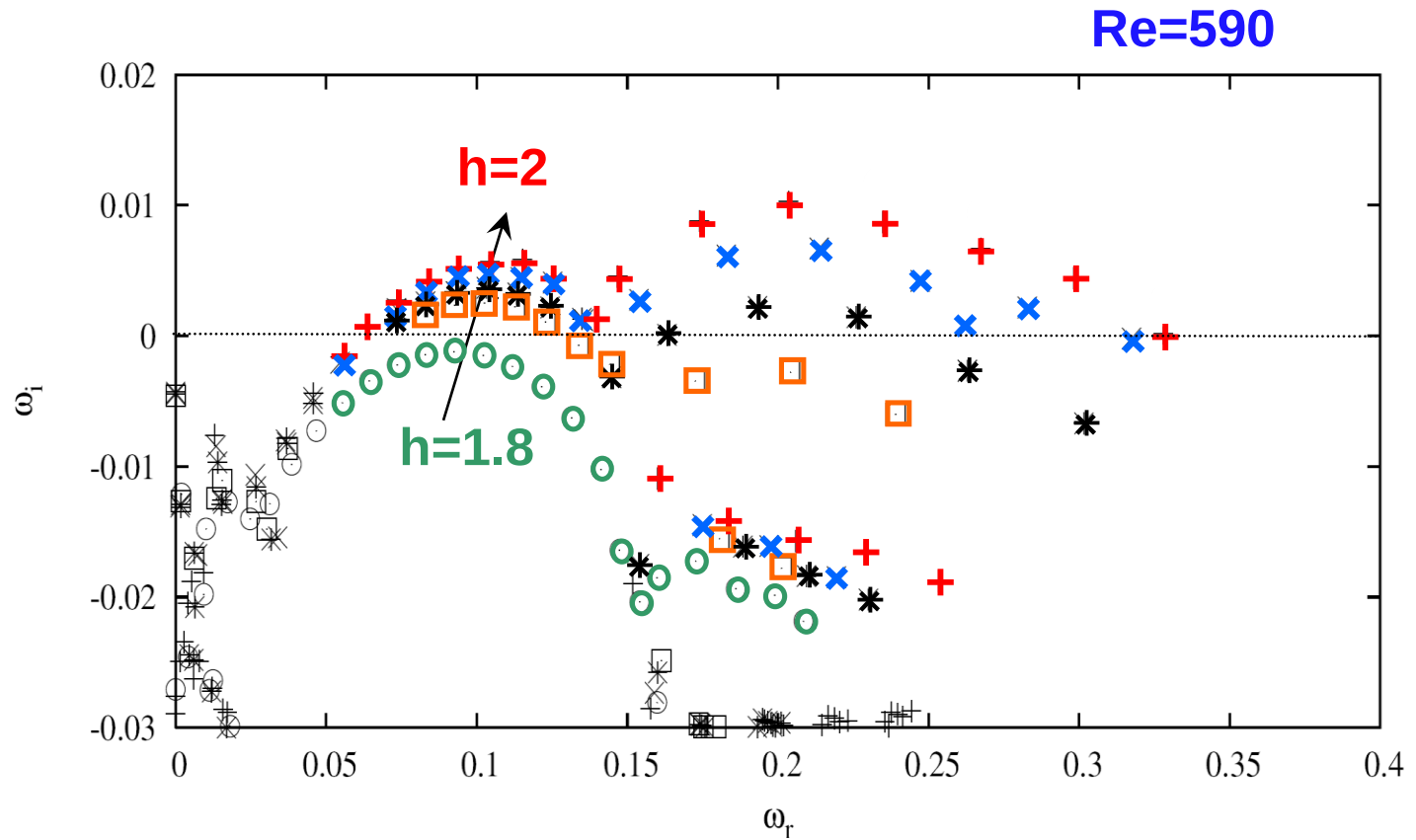


Generalized eigenvalue problem

$$\mathbf{A} \hat{\mathbf{v}} = \sigma \mathbf{B} \hat{\mathbf{v}}$$

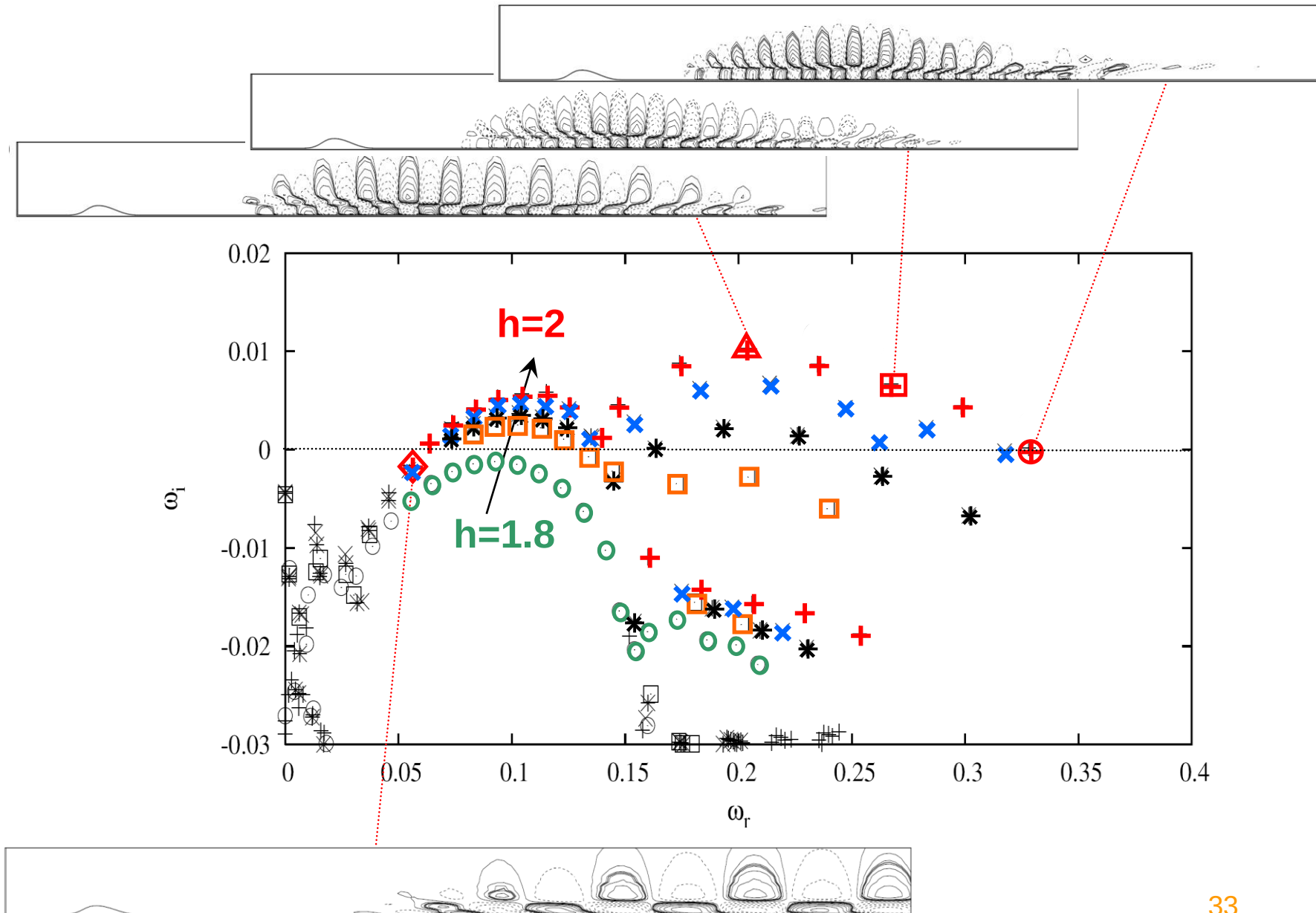
Inverse Krylov-Arnoldi method

Unstable spectrum

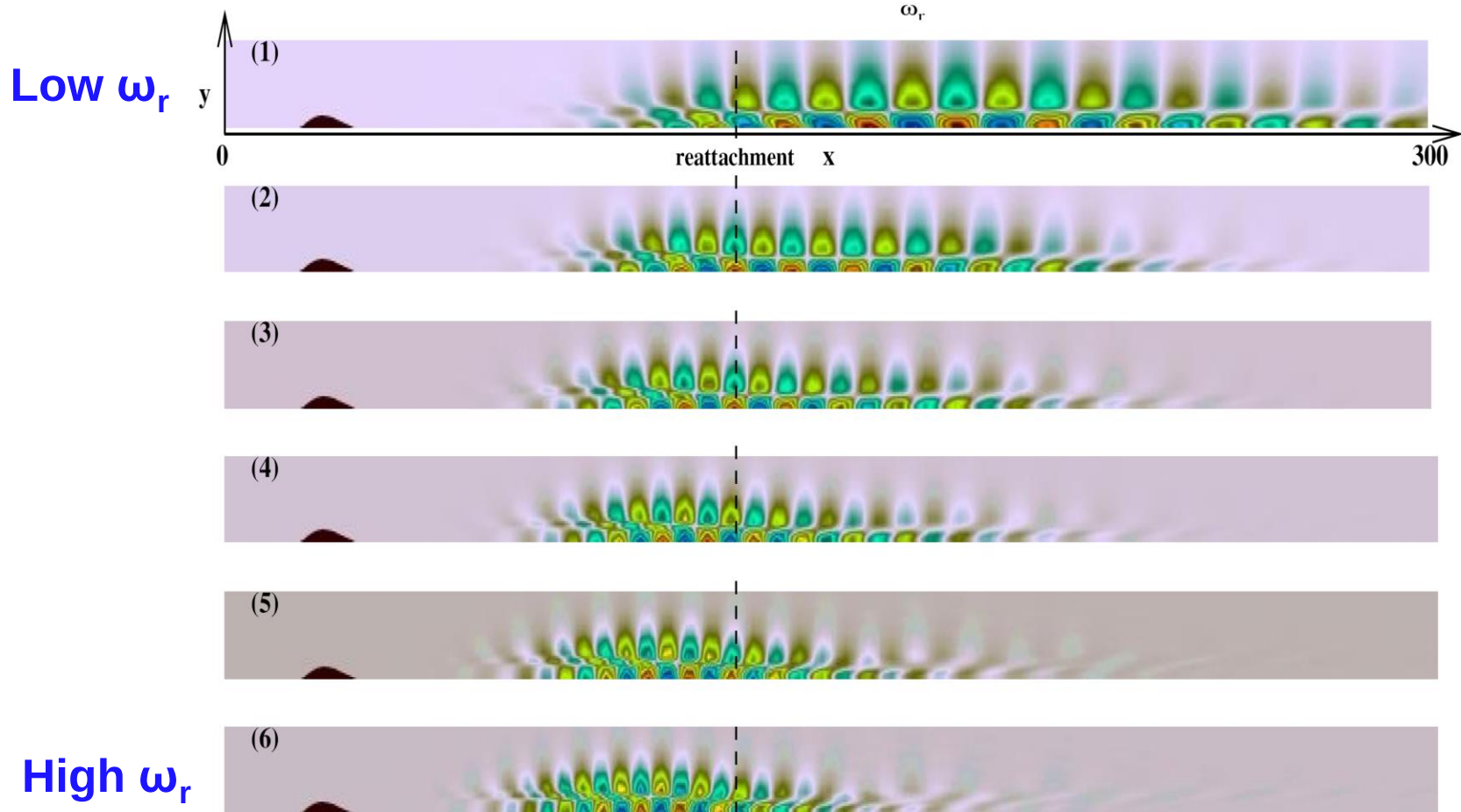


Ehrenstein and Gallaire(2007)

Eigenmodes

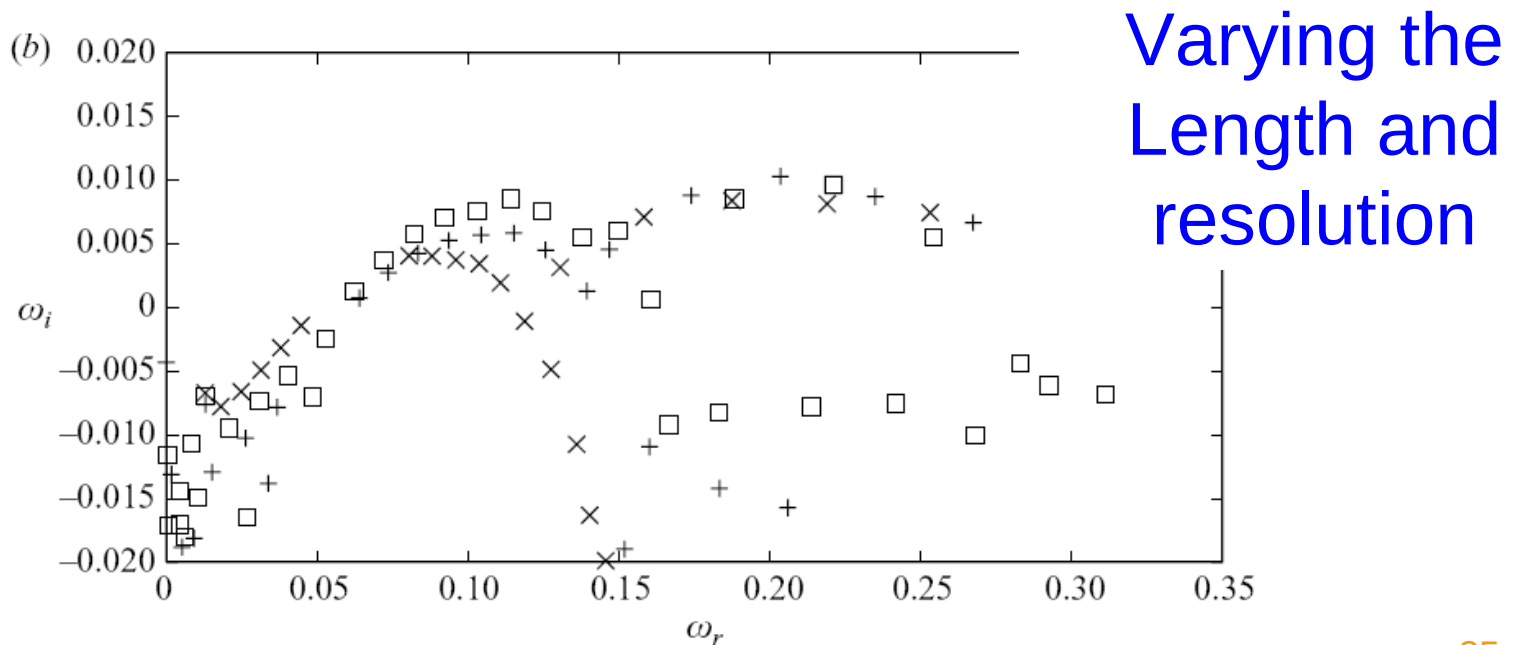
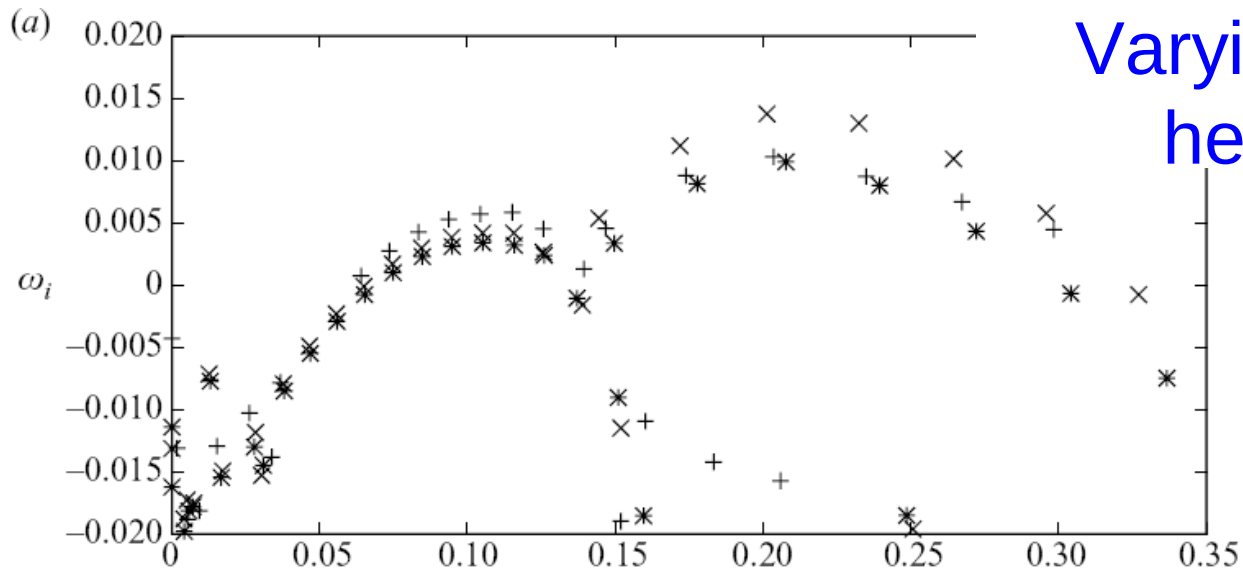


Localized modes

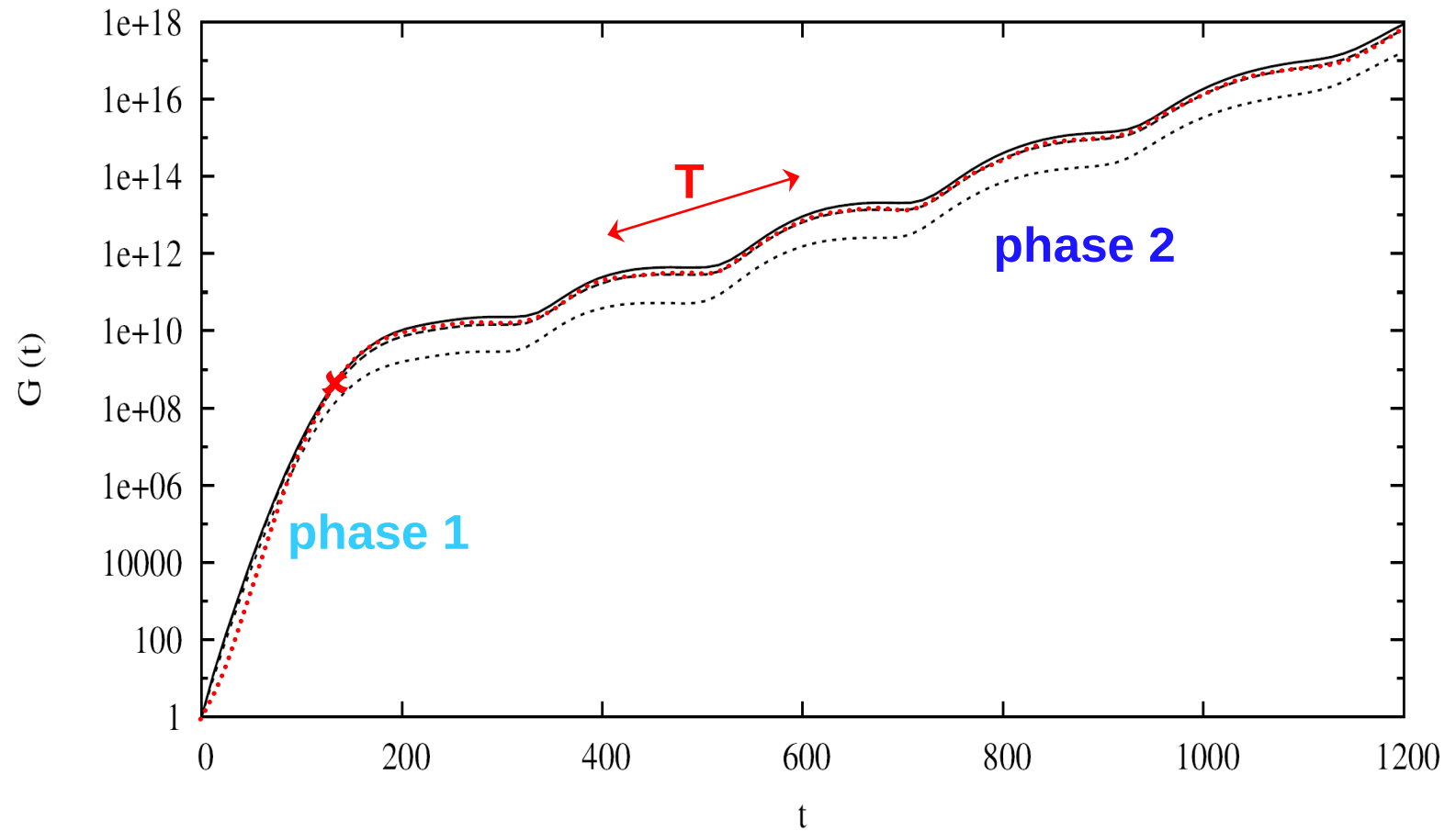


Streamwise velocity components of eigenfunctions

Convergence issues



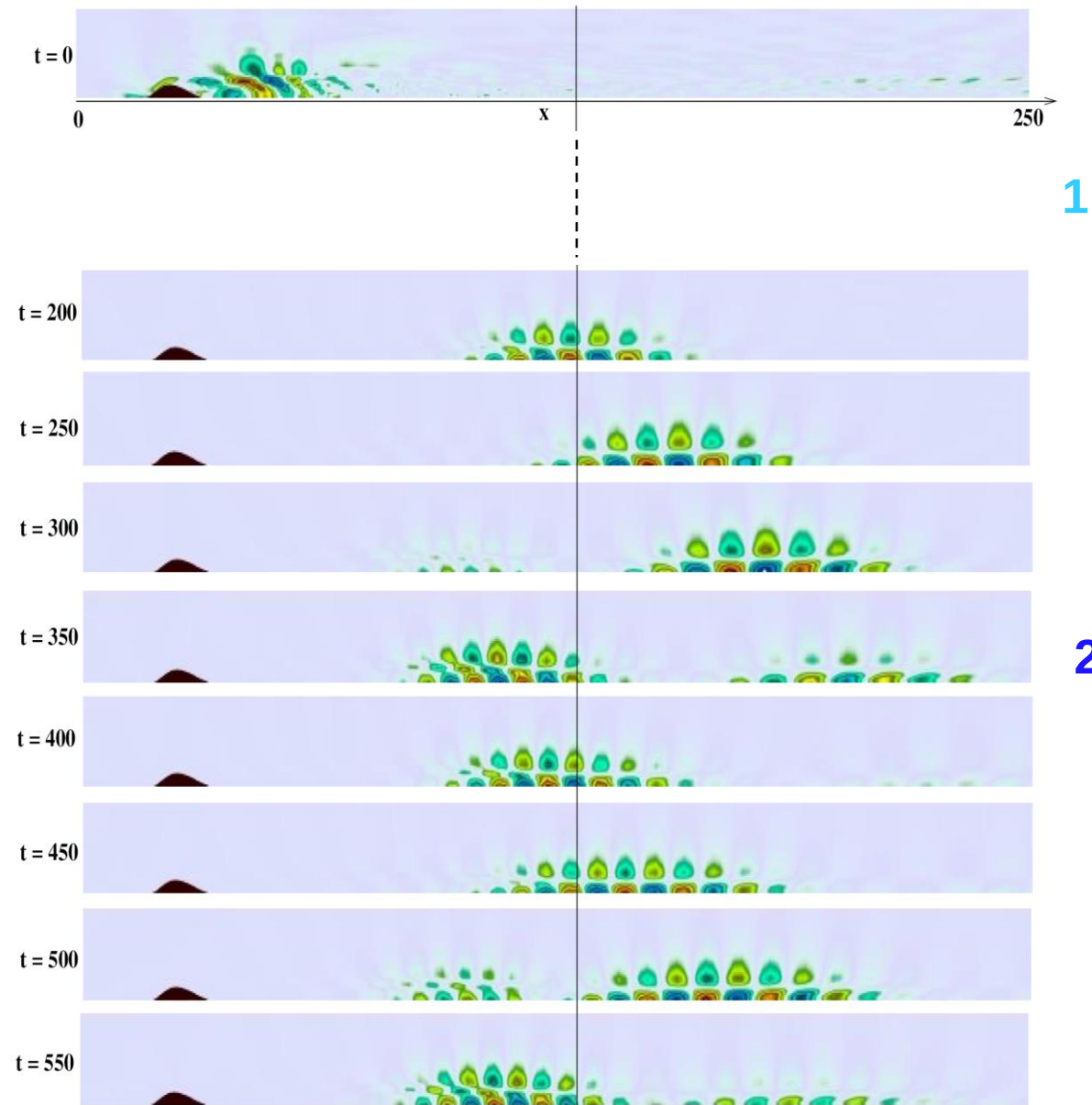
Optimal perturbation



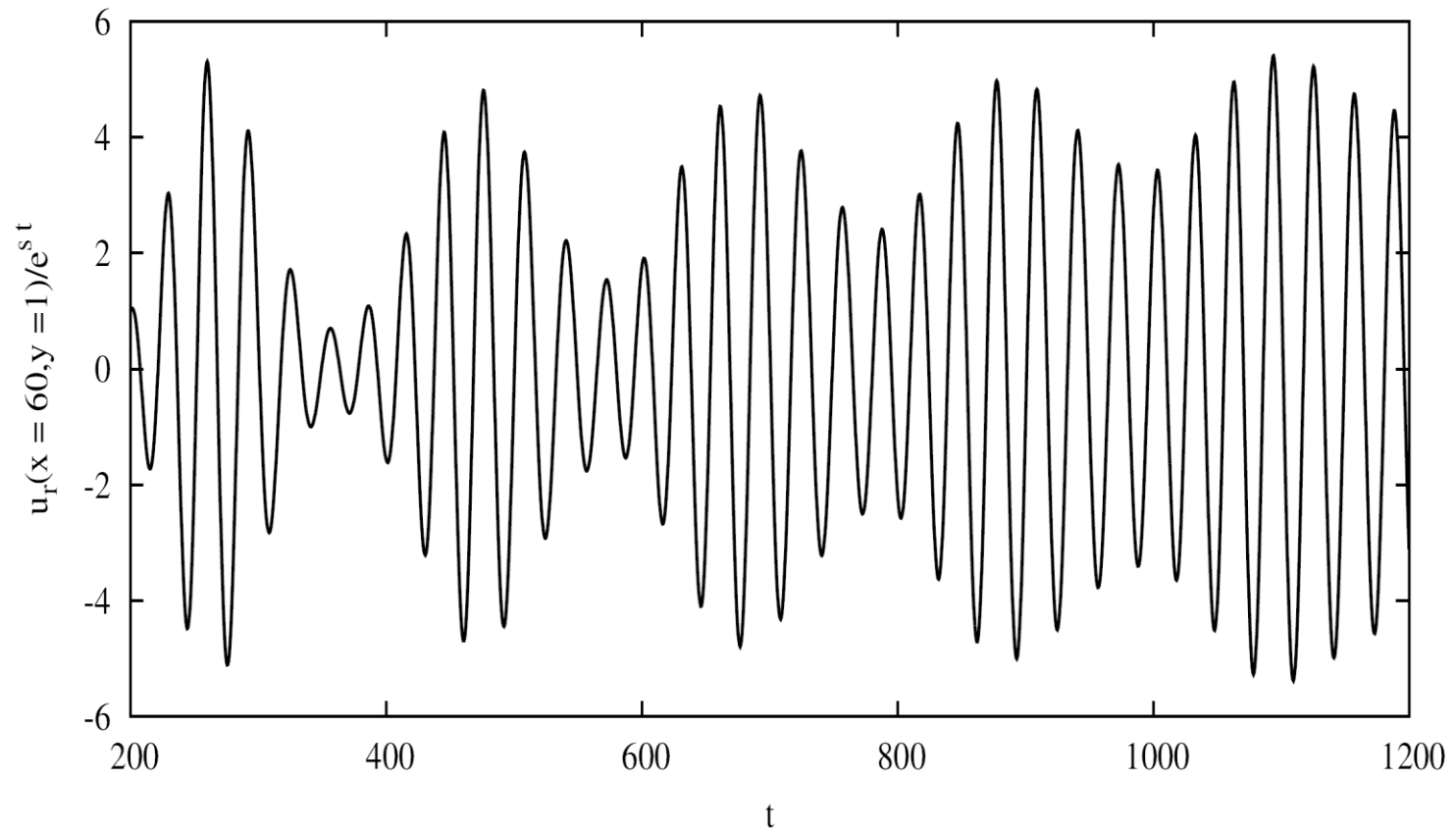
Perturbation evolution



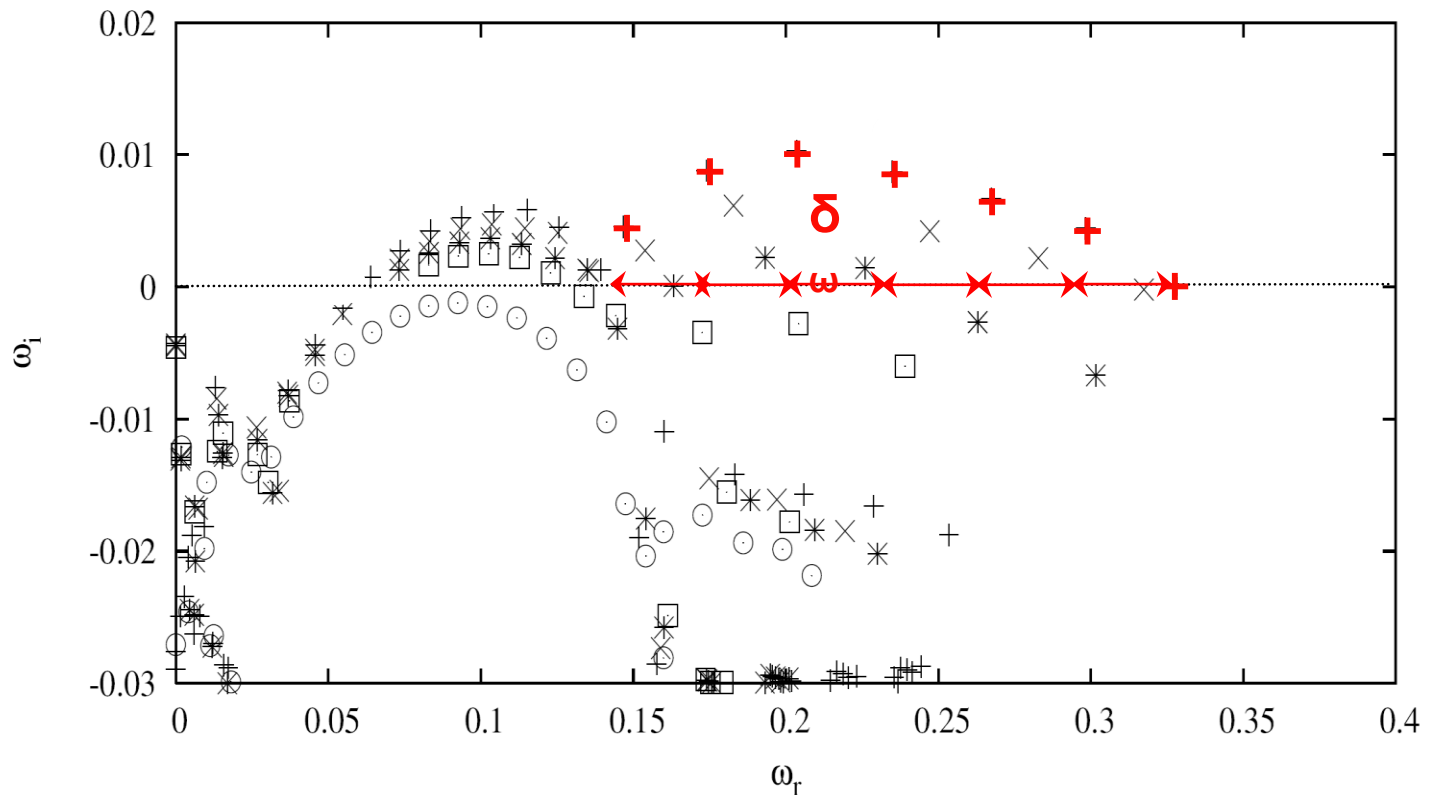
Perturbation evolution



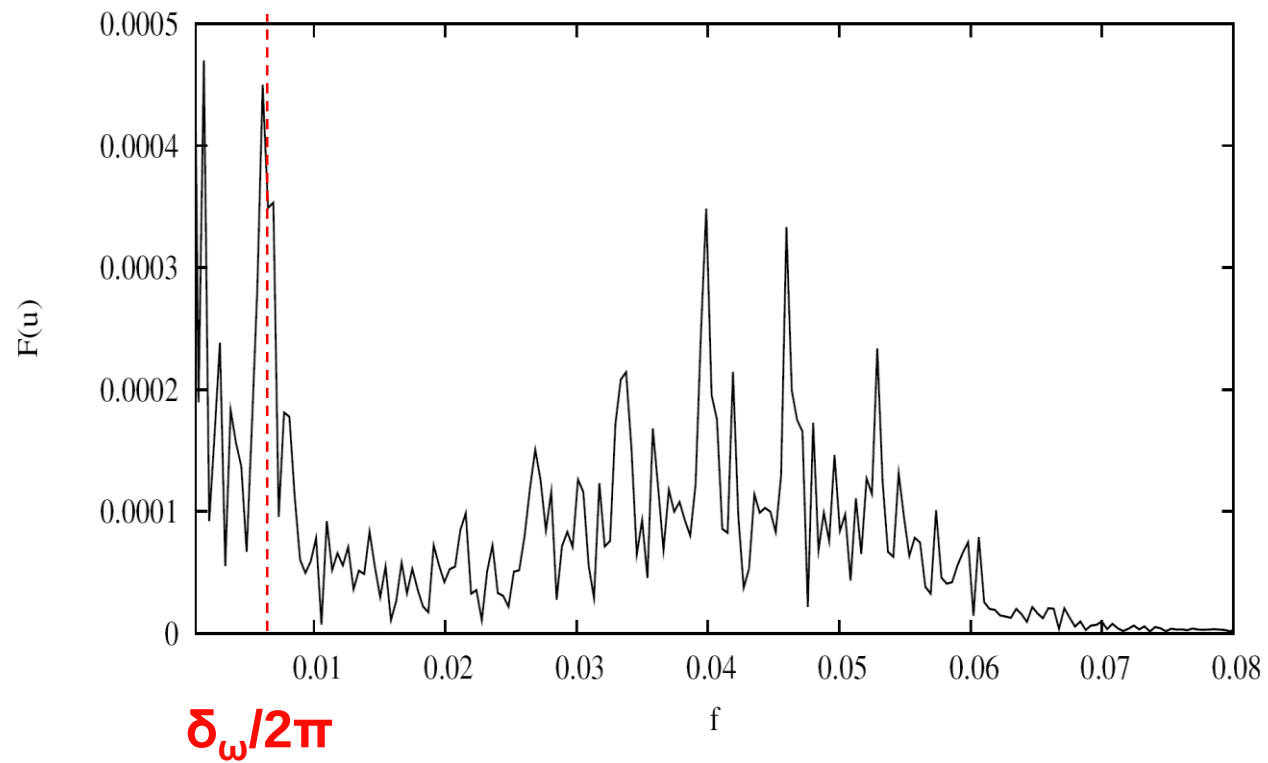
Beating behavior



Similar modes with equidistant frequencies



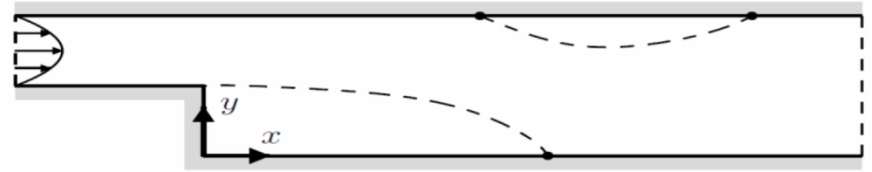
Power spectrum in DNS



Global linear instability of flows in complex geometry

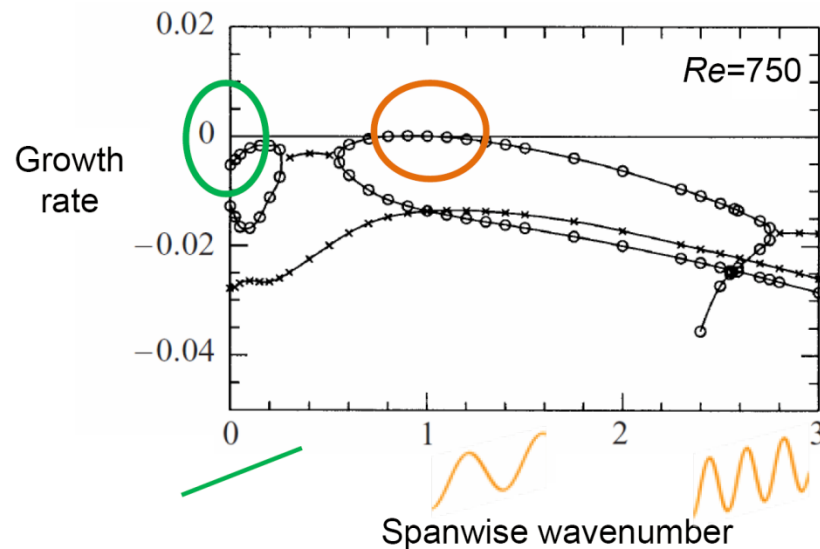
1. Global instability of a classical 2D flow
2. Less classical unstable flows
3. Stable flows

A typical amplifier: the backward-facing step



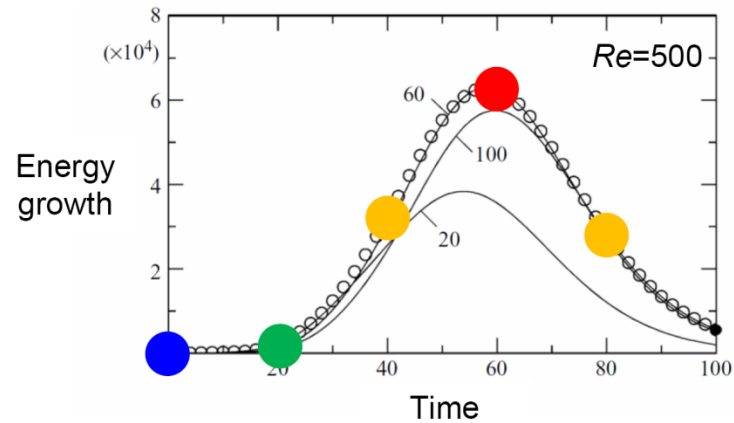
Global linear stability analysis: [Barkley, Gomes & Henderson, 2002; Lanzerstorfer & Kuhlmann, 2012]

- Stable to 2D perturbations for any Re
- Stable to 3D perturbations up to $Re=715-750$

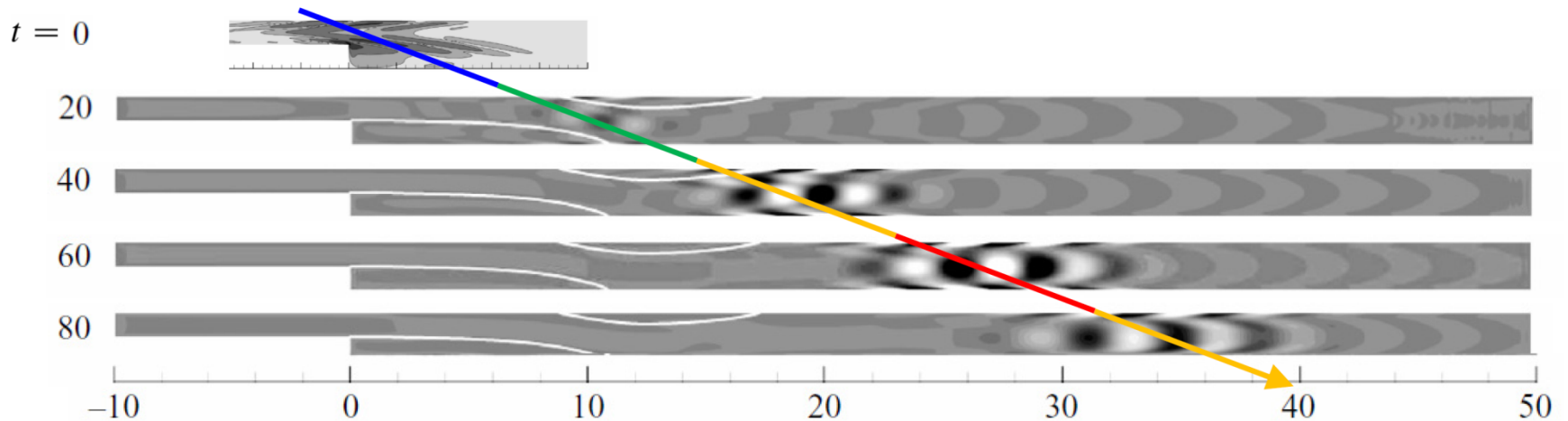


Large transient growth

[Blackburn, Barkley & Sherwin, 2008]

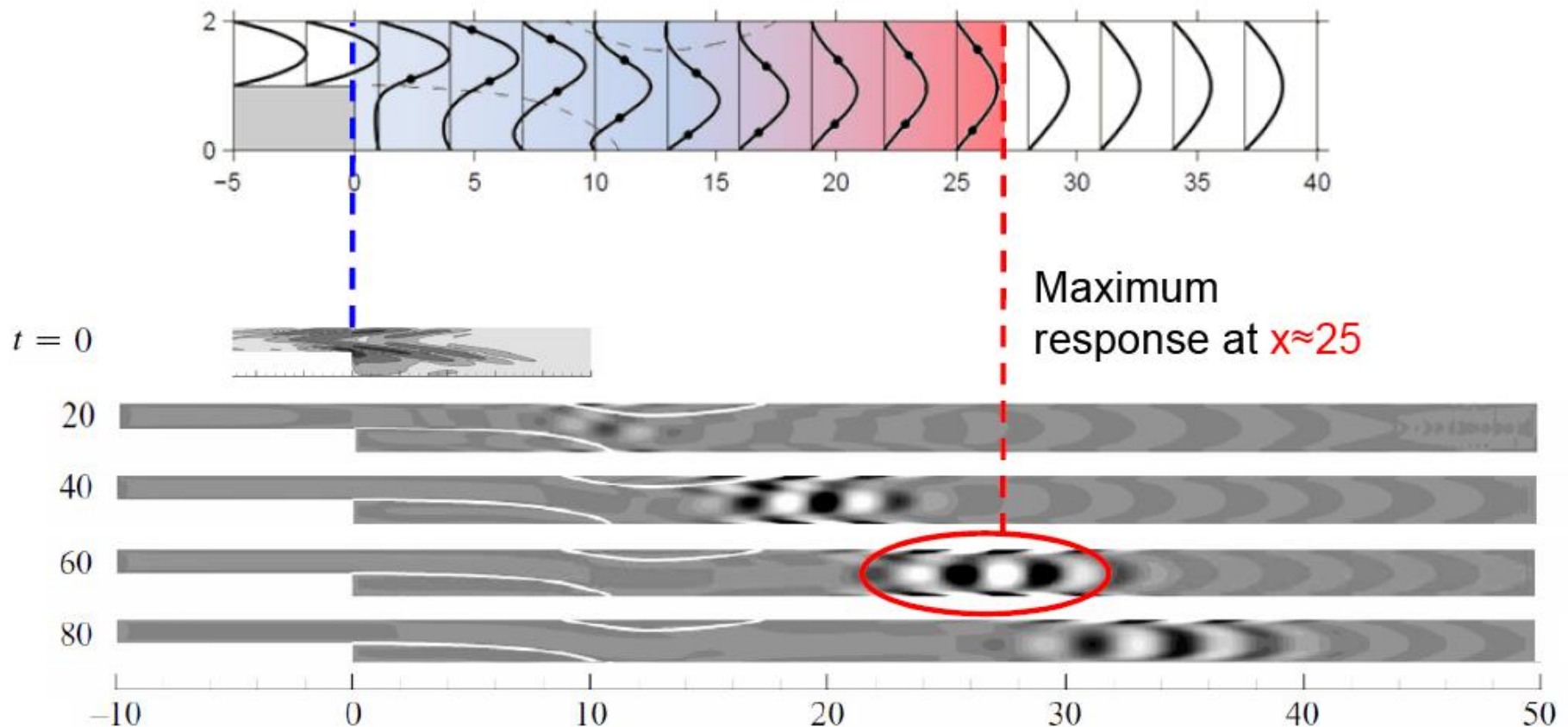


Growth in space & time: optimal perturbations amplified while convected downstream



The global transient growth is due to the local spatial growth

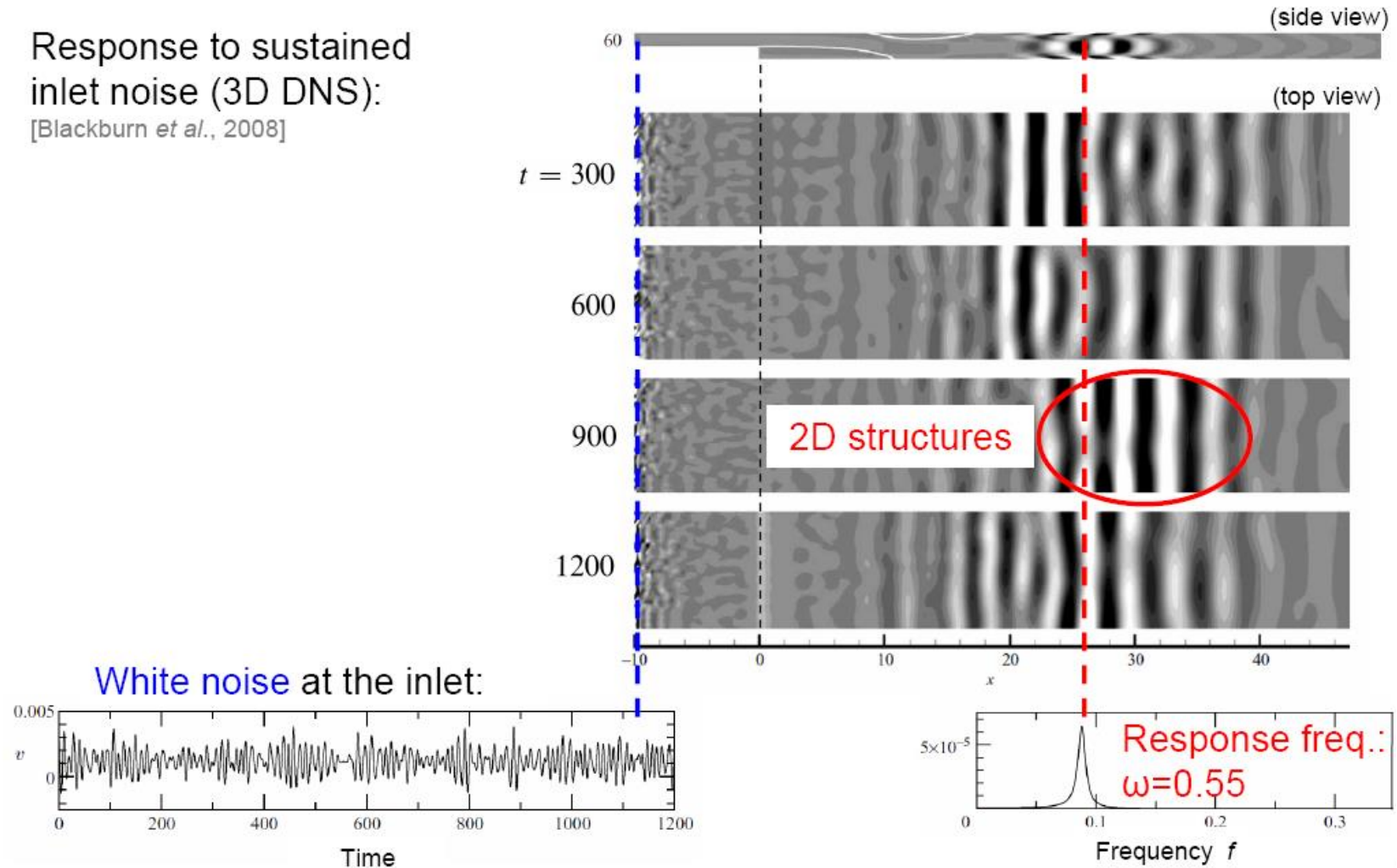
Amplification over the
region of **local instability**



Response to white noise

Response to sustained
inlet noise (3D DNS):

[Blackburn *et al.*, 2008]

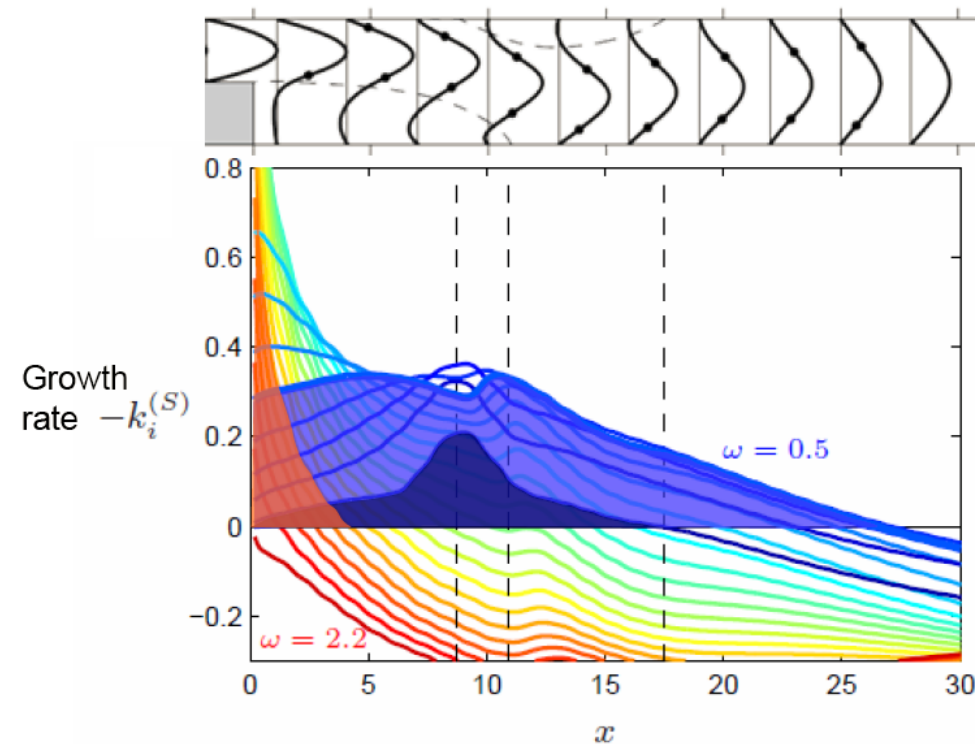


⇒ Very selective amplifier

Method 1: weakly non parallel spatial stability analysis

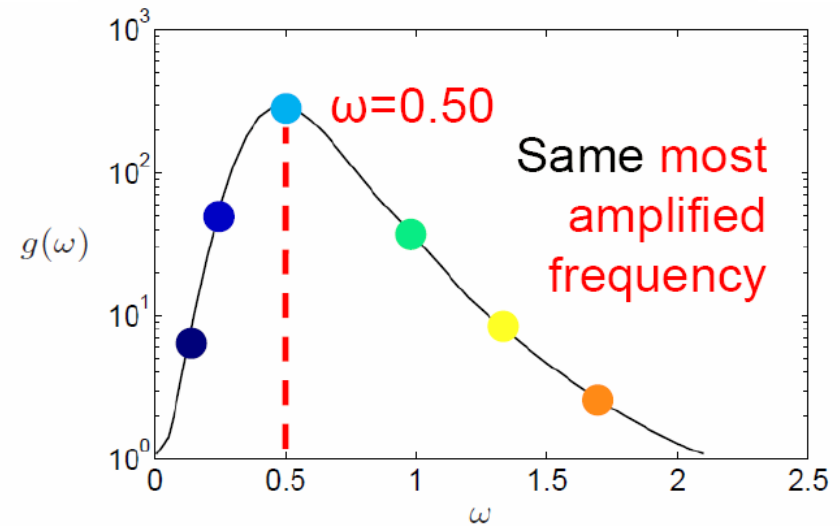
Parallel flow: $\mathbf{u}'(x, y, t) = \mathbf{u}(y) e^{i(kx - \omega t)}$

Spatial analysis $\omega \in \mathbb{R}, k \in \mathbb{C}$



Overall amplification: integral gain

$$g(\omega) = \exp \left(\int -k_i^{(S)}(\omega, x) dx \right)$$



Method 2: transfer function

Nonlinear problem (base flow)

$$\nabla \cdot \mathbf{U}_b = 0,$$

$$\mathbf{U}_b \cdot \nabla \mathbf{U}_b + \nabla P_b - Re^{-1} \nabla^2 \mathbf{U}_b = \mathbf{0},$$

+ linear perturbation

$$\nabla \cdot \mathbf{u}' = 0,$$

$$\partial_t \mathbf{u}' + \nabla \mathbf{u}' \cdot \mathbf{U}_b + \nabla \mathbf{U}_b \cdot \mathbf{u}' + \nabla p' - Re^{-1} \nabla^2 \mathbf{u}' = \mathbf{F}$$

Method 2: transfer function

Nonlinear problem (base flow)

$$\nabla \cdot \mathbf{U}_b = 0,$$

$$\mathbf{U}_b \cdot \nabla \mathbf{U}_b + \nabla P_b - Re^{-1} \nabla^2 \mathbf{U}_b = \mathbf{0},$$

+ linear perturbation

$$\nabla \cdot \mathbf{u}' = 0,$$

$$\partial_t \mathbf{u}' + \nabla \mathbf{u}' \cdot \mathbf{U}_b + \nabla \mathbf{U}_b \cdot \mathbf{u}' + \nabla p' - Re^{-1} \nabla^2 \mathbf{u}' = \mathbf{F}$$

for harmonic forcing $\mathbf{F}(t) = \mathbf{f}e^{i\omega t}$

look for solution $(\mathbf{u}', p')(\mathbf{x}, t) = (\mathbf{u}, p)(\mathbf{x}) e^{i\omega t}$

Method 2: transfer function

harmonic forcing

$$\nabla \cdot \mathbf{u} = 0,$$

$$i\omega \mathbf{u} + \nabla \mathbf{u} \cdot \mathbf{U}_b + \nabla \mathbf{U}_b \cdot \mathbf{u} + \nabla p - Re^{-1} \nabla^2 \mathbf{u} = \mathbf{f}$$

Resolvent operator (transfer function)

$$\mathbf{u} = \mathcal{R}(\omega) \mathbf{f}$$

Method 2: transfer function

harmonic forcing

$$\nabla \cdot \mathbf{u} = 0,$$

$$i\omega \mathbf{u} + \nabla \mathbf{u} \cdot \mathbf{U}_b + \nabla \mathbf{U}_b \cdot \mathbf{u} + \nabla p - Re^{-1} \nabla^2 \mathbf{u} = \mathbf{f}$$

Resolvent operator (transfer function)

$$\mathbf{u} = \mathcal{R}(\omega) \mathbf{f}$$

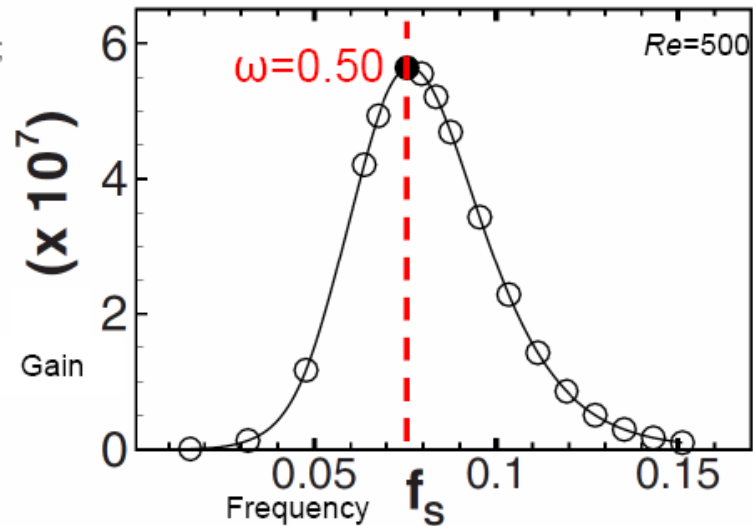
Harmonic gain

$$G^2(\omega) = \frac{||\mathbf{u}||^2}{||\mathbf{f}||^2} = \frac{(\mathcal{R}\mathbf{f} | \mathcal{R}\mathbf{f})}{(\mathbf{f} | \mathbf{f})} = \frac{(\mathcal{R}^\dagger \mathcal{R} \mathbf{f} | \mathbf{f})}{(\mathbf{f} | \mathbf{f})}$$

Method 2: transfer function

Optimal harmonic gain [Marquet & Sipp, 2010;
Marquet *et al.*, 2010, priv. comm.]:

same preferred frequency,
large gain



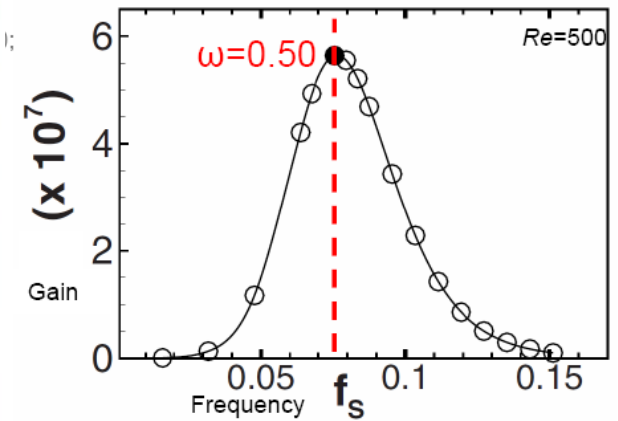
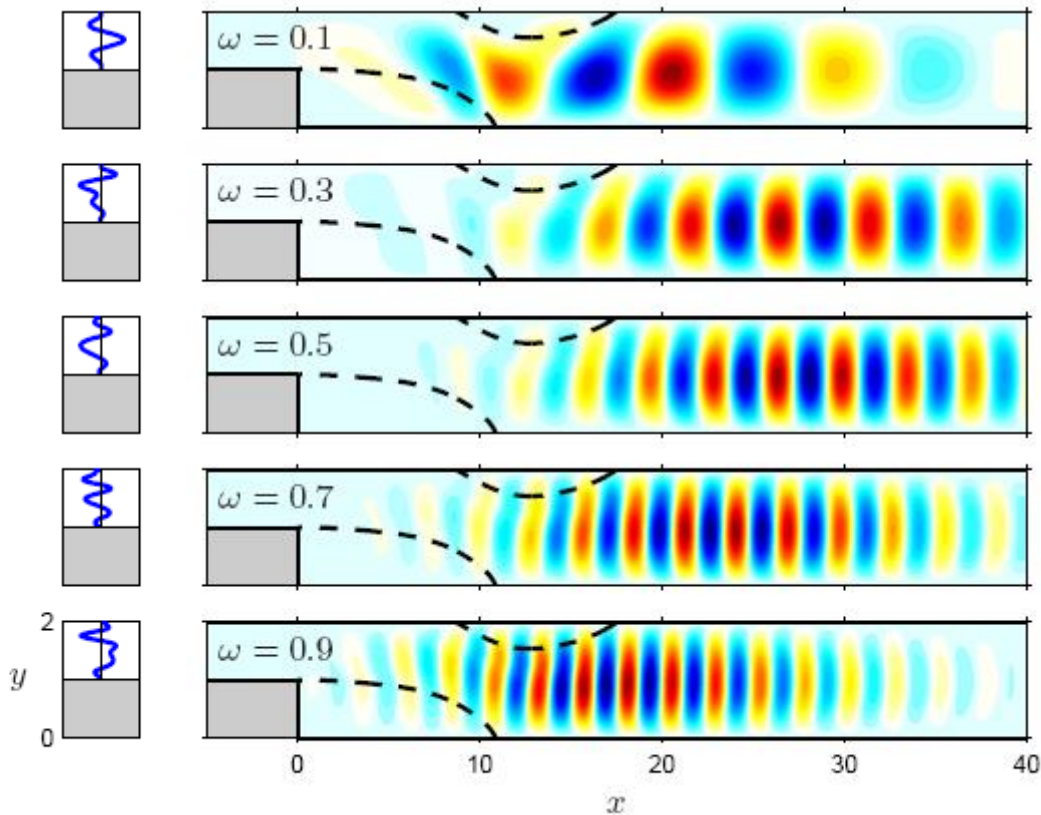
Optimal forcing



and optimal response very similar to transient growth:



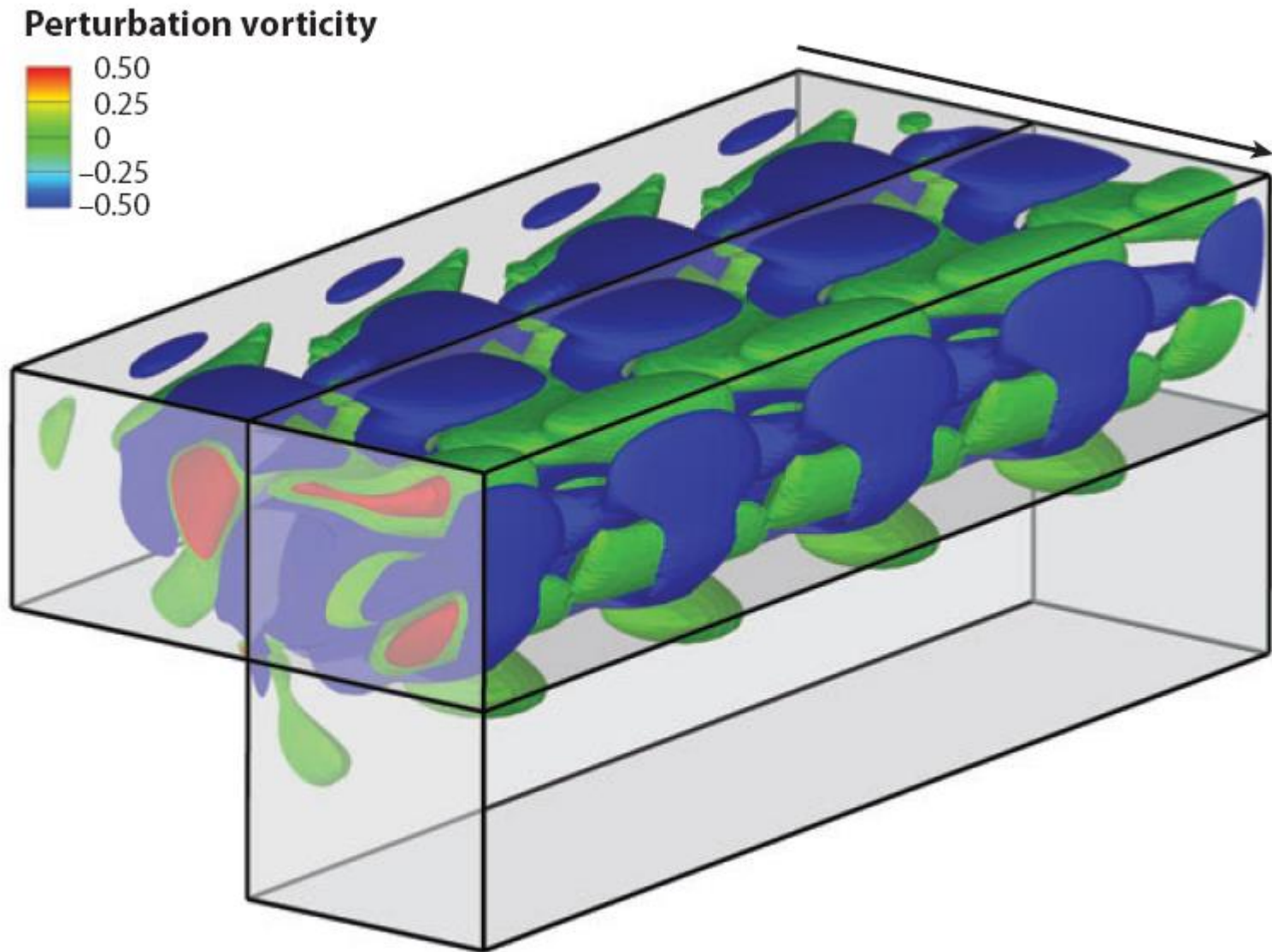
Method 2: transfer function



Global linear instability of flows in complex geometry

1. Global instability of a classical 2D flow
2. Less classical unstable flows
3. Stable flows

Global linear instability of flows in complex geometry



Da Vincente 2010