
Measurement/specification analysis,

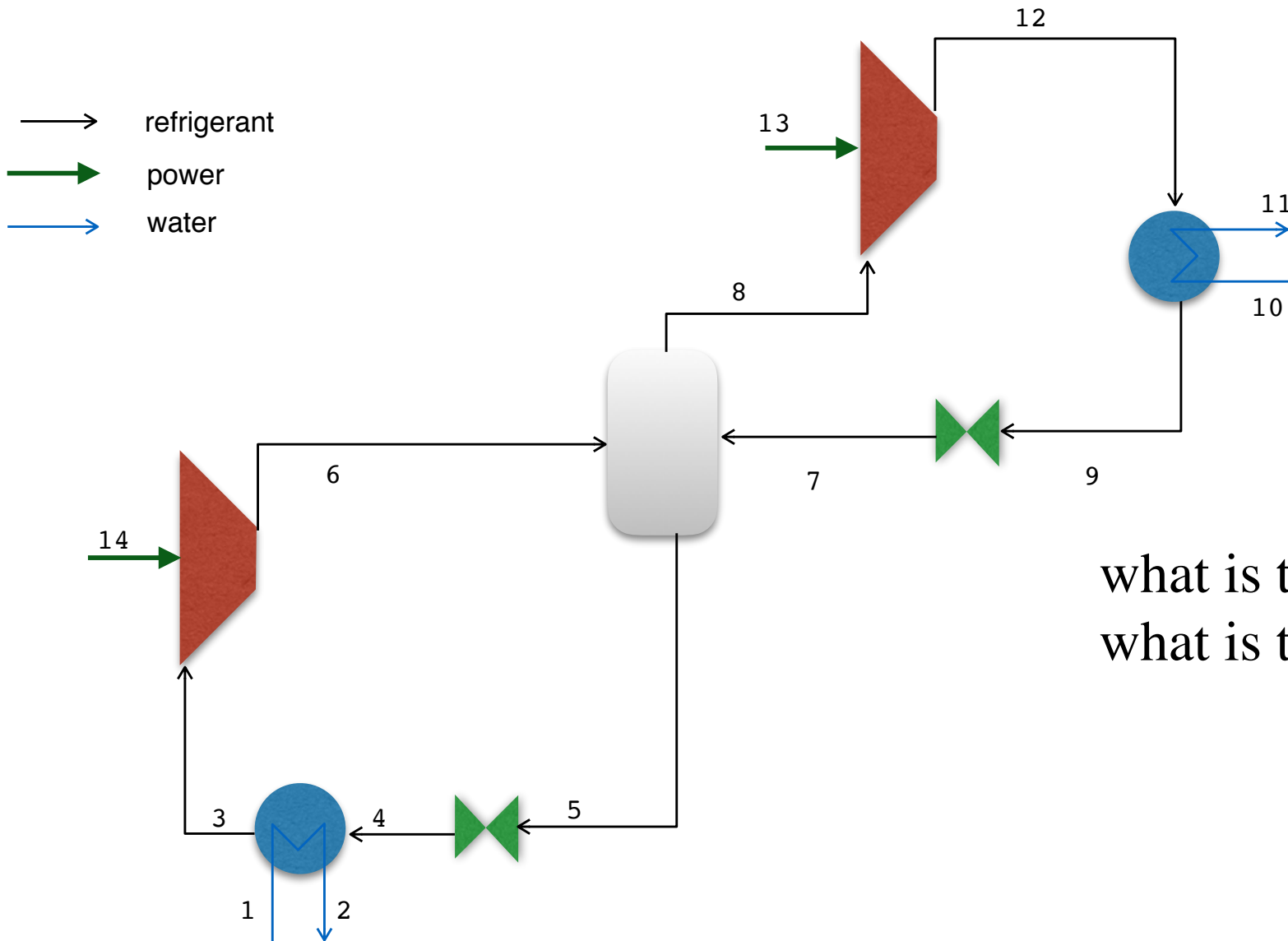
Data reconciliation and
Parameter identification

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IPESE

EPFL-STI-IGM

Two stage heat pump

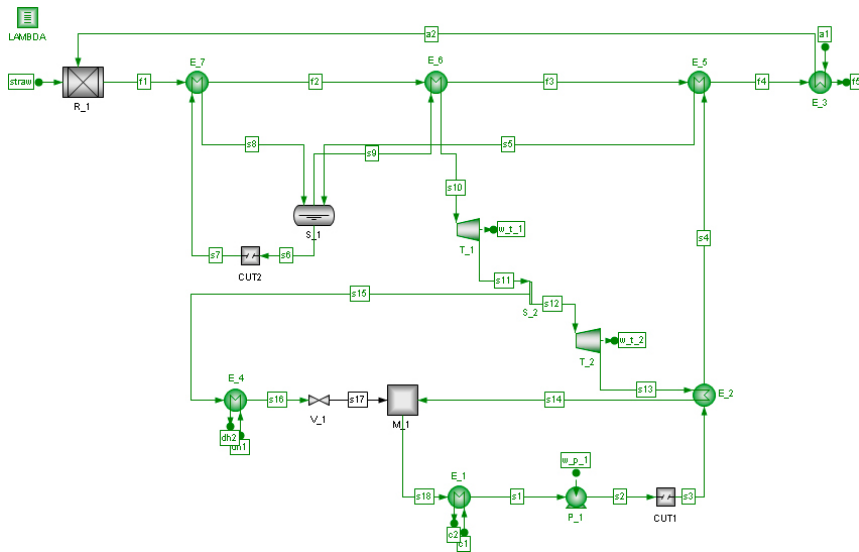
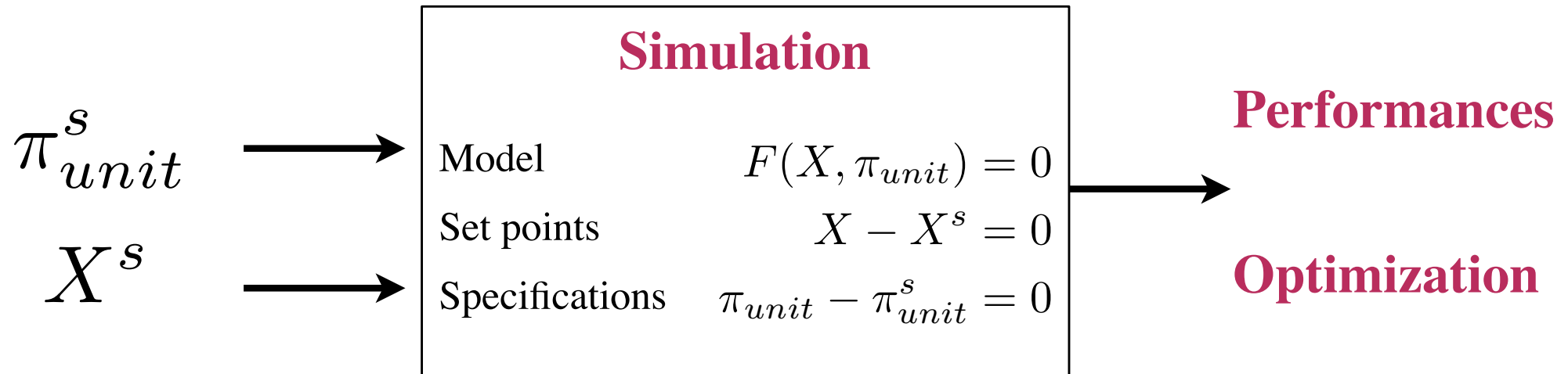


what is the value of U ?
what is the value of eff_{is} ?

Goals of the lecture

- How to calibrate models using measurements
 - Where to place measurements
 - Virtual sensors by process models
 - Data reconciliation
 - correct the values of the measurement
 - Parameter identification

Process models & decision support



Model is defining the level of detail

What are the X we want to know ?

- Streams ?
- Unit parameters ? π_{unit}

-
- The process model and the unit models define the expected level of detail
 - i.e. the data we want to generate with the model
 - Unit models require Parameters with fixed values
 - What are the values of the parameters ?
 - Literature => correlations, experience
 - From experiments
 - sensors => measured values => calculated parameters
 - Calibration on existing equipment

Measurement and parameter identification

1. Measured values

X^m



2. Identification

Model $F(X, \pi_{unit}) = 0$
Measurements $X - X^m = 0$

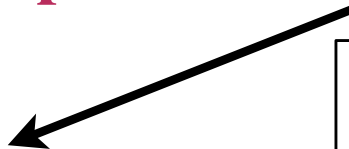
3. Identified parameters

π_{unit}



$$\pi_{unit}^s = \pi_{unit}$$

4. Specified parameters



π_{unit}^s



X^s



5. Simulation

Model $F(X, \pi_{unit}) = 0$
Set points $X - X^s = 0$
Specifications $\pi_{unit} - \pi_{unit}^s = 0$

6. Performances

7. Optimization

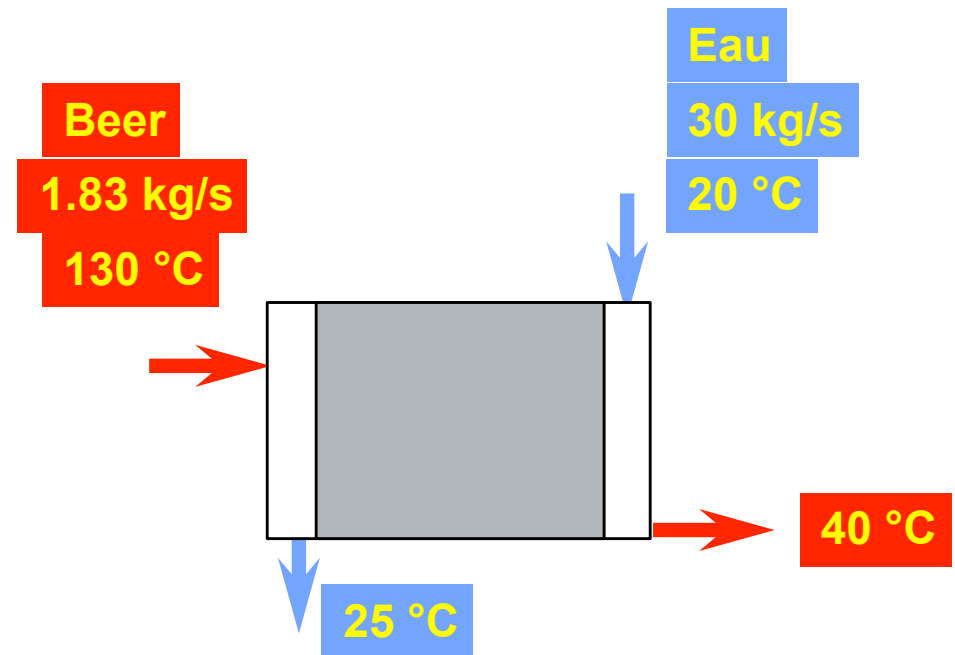


Do we have enough measurement/specifications ?

What is the heat transfer coefficient of the heat exchanger?

Do we have enough measurement ?

- Equations: 3
 - 2 energy balances
 - $Q = UA \Delta T_{lm}$
- State variables: 8
 - 4 temperatures
 - 2 flows
 - 2 parameters Q , U
- Degrees of Freedom : $5 = 8 - 3$
- Measures : 6

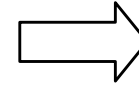


$C_p = \text{water}$

Characterizing an industrial process

Energy conversion system

- Flowsheet (**level of detail**)
- Localisation of **measurement**

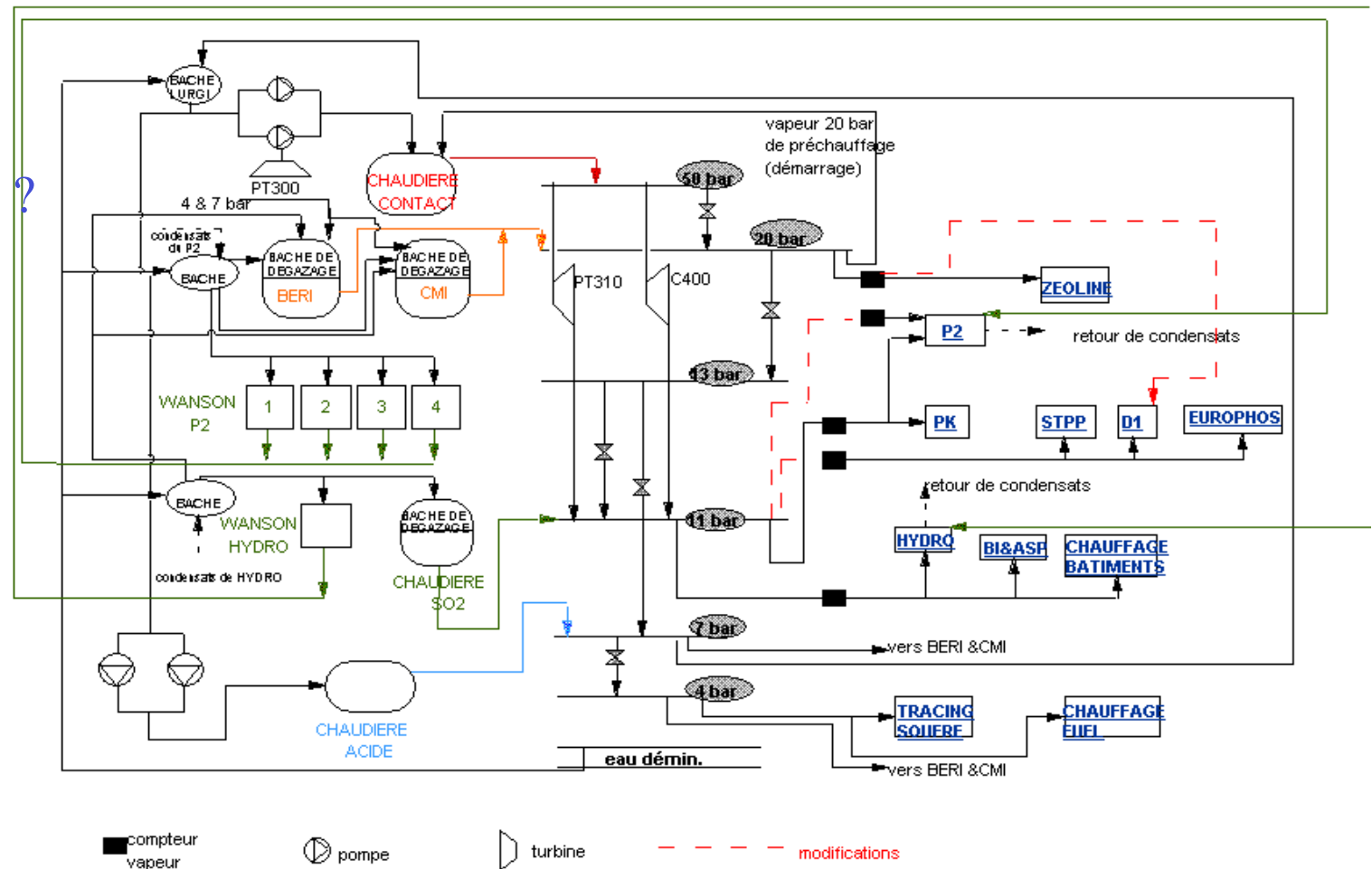


What is the state of the system

Performances ?
Unit parameters?
Maintenance ?
Optimisation ?

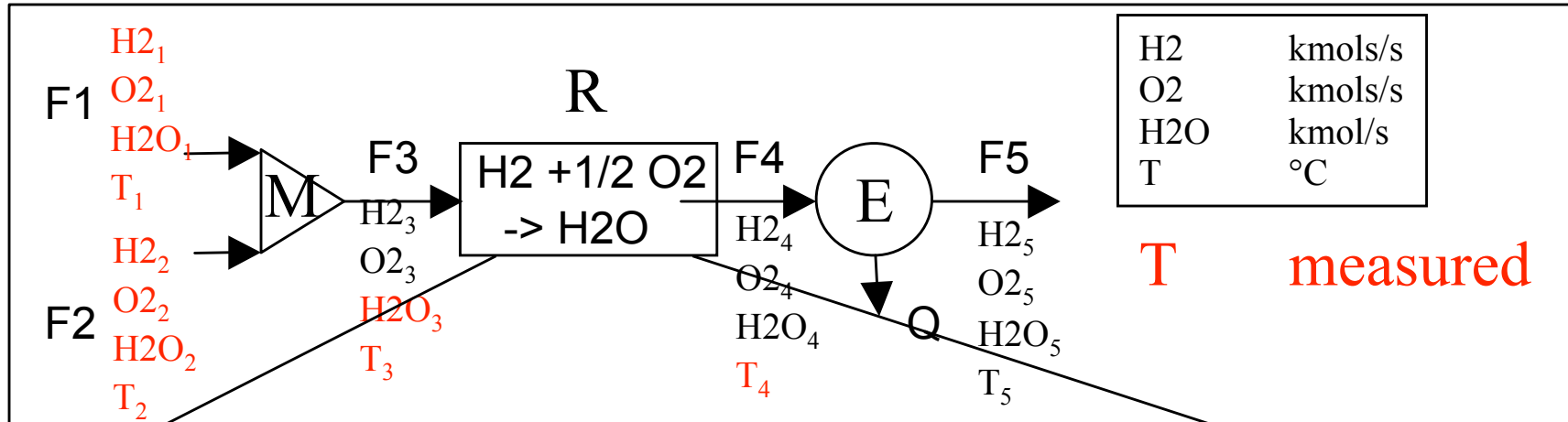
Measurements system ?

Enough ?
Accurate ?
Correction ?
Other needed ?
where ?
how much ?
why ?



Example of a simplified system

Hydrogen combustion with pure oxygen



Unité R

Mass balance:

$$H2_3 - U - H2_4 = 0$$

$$O2_3 - 1/2 U - O2_4 = 0$$

$$H2O_3 + U - H2O_4 = 0$$

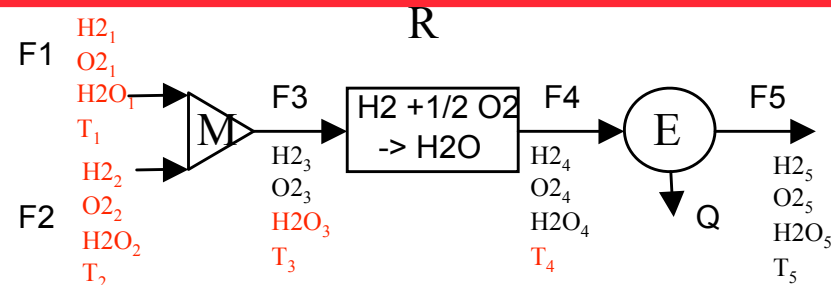
Energy Balance :

$$\sum x_3 * (h^\circ_{x_3} + h_{x_3}(T_3)) - \sum x_4 * (h^\circ_{x_4} + h_{x_4}(T_4)) = 0$$

$$\text{Canonical form : } F(x) = 0 \Rightarrow Ax = c$$

Incidence matrix

Combustion



H2	kmols/s
O2	kmols/s
H2O	kmol/s
T	°C

T **mesures**

Incidence Matrix : $a_{i,j} = 1$ if variable j occurs in equation i

$$A X = c$$

Variables : 22 in which 11 measures $\Delta = 11$

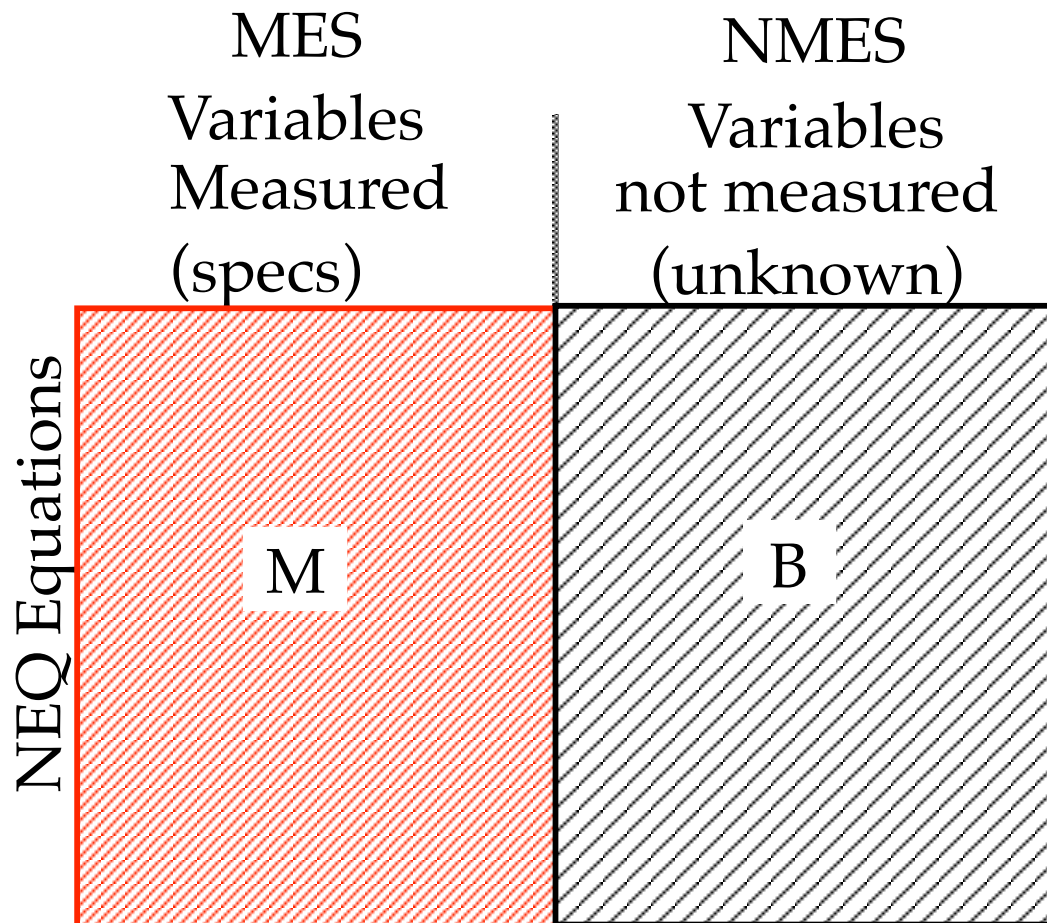
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22
		O2	H2	H2O	T	O2	H2	H2O	T	O2	H2	H2O	T	O2	H2	H2O	T	O2	H2	H2O	T	Q	E
Bilan Matière	M	X	X	X		X	X	X		X	X	X											
Bilan thermique	M	X	X	X	X	X	X	X	X	X	X	X	X										
Bilan Matière	R					X	X			X	X			X	X			X	X				
Bilan Thermique	R					X	X	X	X	X	X	X	X										
Bilan Matière	E									X	X				X			X	X	X			
Bilan thermique	E									X	X	X	X				X	X	X	X	X	X	X

only 10 are needed

Equations 12

Structural analysis : re-arrange the matrix

variables : measured (= specified) or not (to be calculated)



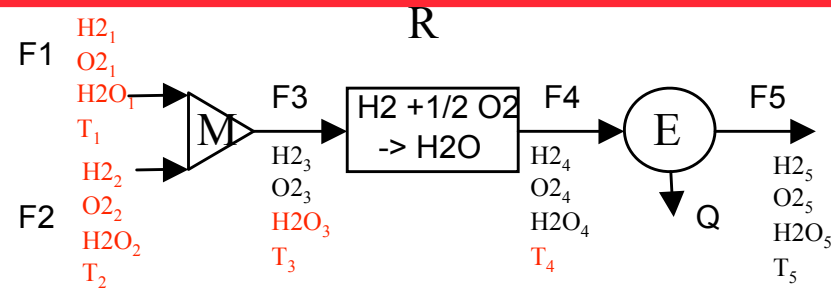
1) **NEQ < NMES** :no solution
(NMES-NEQ) Equations are missing
to calculate unknown variables

2) **NEQ = NMES** : all the unknowns can be
calculated (just calculable system)

3) **NEQ > NMES** : too many equations
(**redundant system**)
in this case some measured values can be
recalculated using the value of the other

Incidence Matrix

Example : combustion



H2	kmols/s
O2	kmols/s
H2O	kmol/s
T	°C

T measured

Measured variables: 11

unknown variables : 11

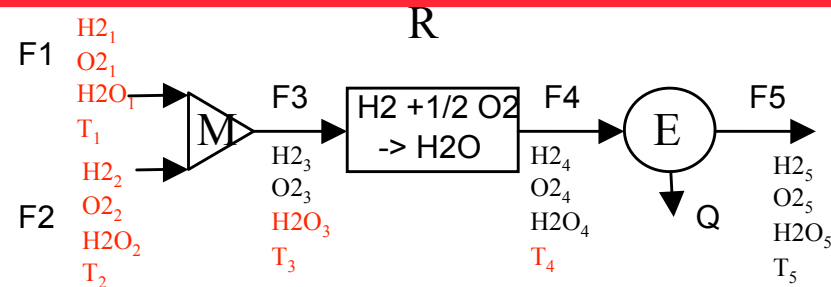
system equations: 12

		Measured variables: 11											unknown variables : 11												
		O2	H2	H2O	T	O2	H2	H2O	T	H2O	T	T	O2	H2	O2	H2	H2O	T	U	R	O2	H2	H2O	Q	E
Bilan Matière	M	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X
Bilan thermique	M	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X	X
Bilan Matière	R																								
Bilan Thermique	R																								
Bilan Matière	E																								
Bilan thermique	E																								

Square system ?

Rearrange the matrix

Exemple : combustion



H2	kmols/s
O2	kmols/s
H2O	kmol/s
T	°C

T mesures

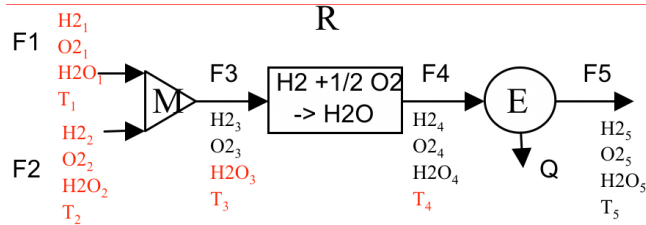
- 1) regroup measured and unknowns (**M+B**)
- 2) Reorganise the B matrix (unknowns) by line and column permutations in order to have :
 - 1 element on each diagonal position
 - regroup in sub-systems (square or rectangles)

measured/specified variables: 11 Non measured : 11

system equations: 12

		measured/specified variables: 11											Non measured : 11										
		3	1	2	1	1	2	2	1	2	3	4	3	3	R	4	4	4	5	5	5	5	E
		H2O	H2O	H2O	O2	H2	O2	H2	T	T	T	T	O2	H2	U	O2	H2	H2O	O2	H2	H2O	T	Q
Bilan Matière	M H2O	X	X	X																			
Bilan Matière	M O2				X	X							X										
Bilan Matière	M H2					X	X						X										
Bilan thermique	M	X	X	X	X	X	X	X	X	X	X	X	X	X									
Bilan Matière	R O2												X		X	X							
Bilan Thermique	R	X											X	X			X	X	X				
Bilan Matière	R H2												X			X							
Bilan Matière	R H2O	X														X		X					
Bilan Matière	E O2															X			X				
Bilan Matière	E H2																X			X			
Bilan Matière	E H2O																	X			X		
Bilan thermique	E											X				X	X	X	X	X	X	X	X

Incidence matrix analysis



			3	1	2	1	1	2	2	1	2	3	4	3	3	R	4	4	4	5	5	5	5	E
			H2O	H2O	H2O	O2	H2	O2	H2	T	T	T	T	O2	H2	U	O2	H2	H2O	O2	H2	H2O	T	Q
Bilan Matière	M	H2O	X	X	X																			
Bilan Matière	M	O2				X		X						X										
Bilan Matière	M	H2					X		X					X										
Bilan thermique	M		X	X	X	X	X	X	X	X	X	X	X	X	X									
Bilan Matière	R	O2												X	X									
Bilan Thermique	R		X											X	X	X								
Bilan Matière	R	H2												X		X								
Bilan Matière	R	H2O	X											X			X							
Bilan Matière	E	O2												X			X							
Bilan Matière	E	H2													X			X						
Bilan Matière	E	H2O														X			X					
Bilan thermique	E													X	X	X	X	X	X	X	X	X	X	X

Redundant = 1 (nb equations - nb unmeasured variables)

Redundant

nbeq > nb var => possibility to correct measures/
eliminate specification

just calculable

NEQ (7) = NMES(7)

T4 can not be corrected/eliminated

not calculable

NEQ (1) < NMES(2)

Add at least 1 measure (2-1)

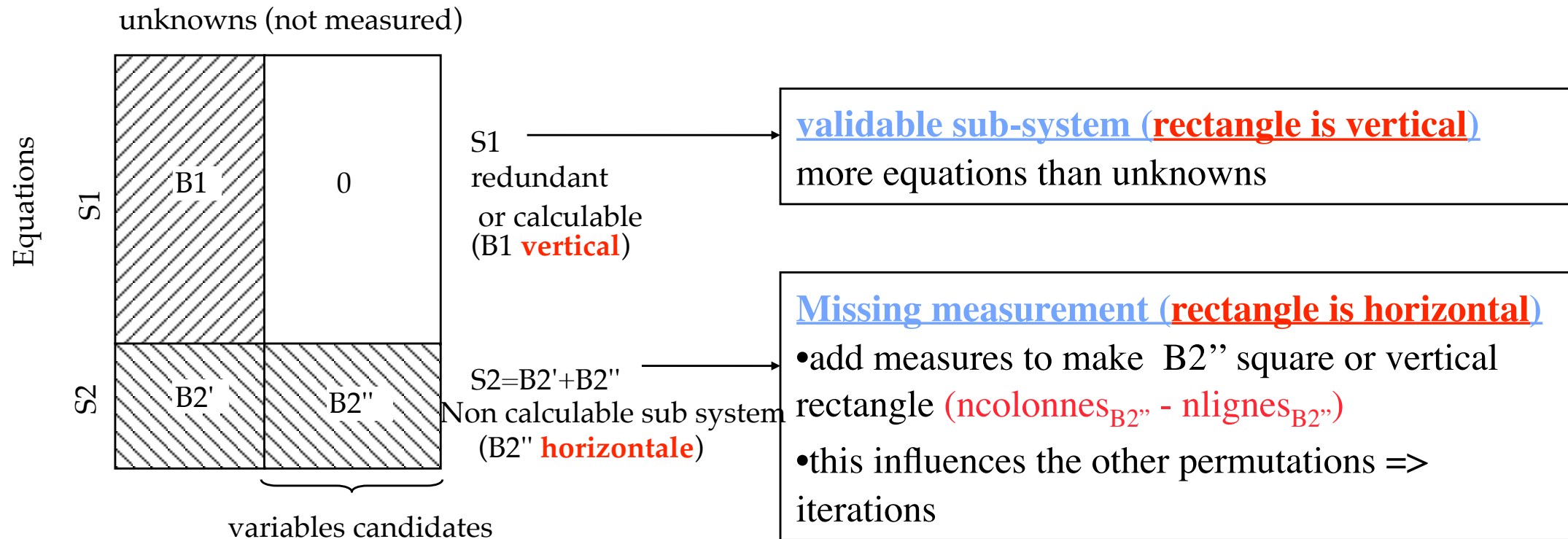
T₅ or Q

Generalisation : In case of complex systems

1) Reorganise the B matrix (unknowns - equations)

Reorganise the B matrix (unknowns) by line and column permutations in order to have:

- 1 element on each diagonal position
- regroup in sub-systems (square or rectangles)



Analogy measurements and DOF analysis

DoF analysis

- Specifications
- Over-specified
 - Spec to be suppressed
- under specified
 - Add specs

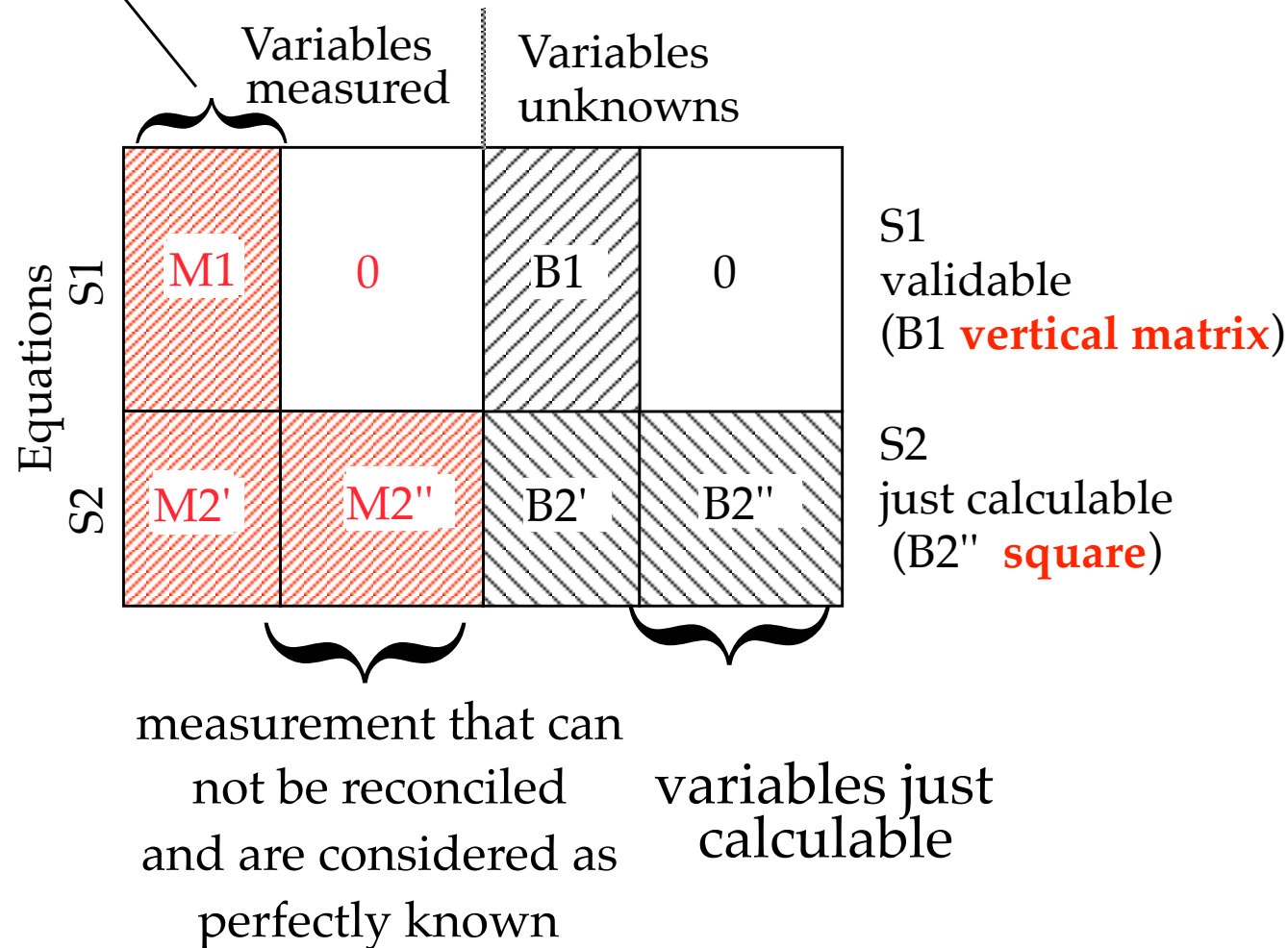
Measurements systems analysis

- Measures
- Redundancy
 - more information available
- Missing measurements
 - add measures

Redundant measurements

Redundant measurement may be reconciled

$$\text{Redundancy number} = n_{\text{lines}}^{B1} - n_{\text{columns}}^{B1}$$



A redundant measurement can be corrected using the values of the other measurements and the model equations

1. Measured values

X^m



2. Identification

Model $F(X, \pi_{unit}) = 0$
Measurements $X - X^m = 0$

3. Identified parameters

π_{unit}



- Do we have enough measurement
 - can the model be solved ?
 - do we need more measurements ?
 - what do we do if we have more measurements ?

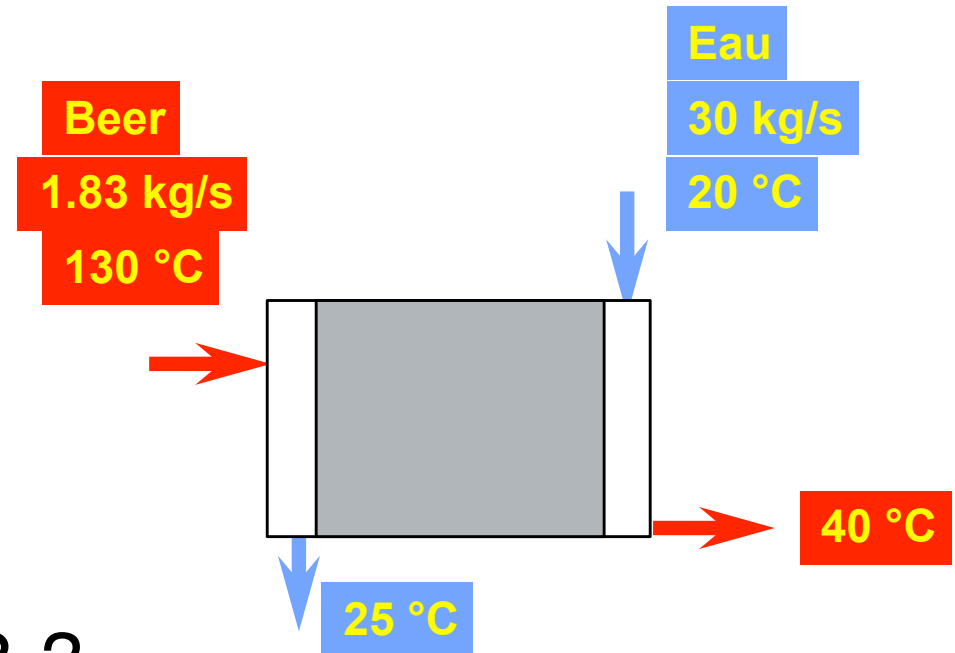
Data reconciliation

What is happening when I have more measures than the minimum number needed ?

What is the heat transfer coefficient of the heat exchanger?

Are the measurements consistent ?

- Equations: 3
 - 2 energy balances
 - $Q = UA \Delta T_{lm}$
- State variables: 8
 - 4 temperatures
 - 2 flows
 - 2 parameters Q , U
- Degrees of Freedom : $5 = 8 - 3$
- Measures : 6
 - do not add losses in as a DOF !



$C_p = \text{water}$

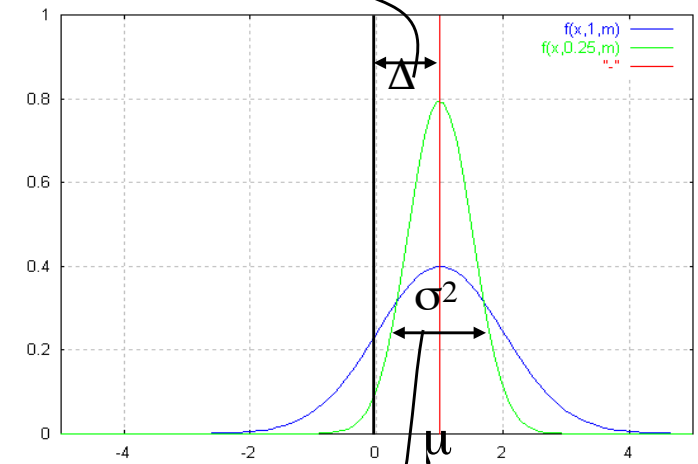
Choosing the good measure

8 variables - 3 equations => 5 measures over 6 have to be fixed

		Measure	1	2	3	4	5	6
Flow 1	kg/s	30.00	32.95	30.00	30.00	30.00	30.00	30.00
T in	°C	20.00	20.00	19.51	20.00	20.00	20.00	20.00
T out	°C	25.00	25.00	25.00	25.49	25.00	25.00	25.00
Q 1	kW	627.	689.	689.	689.	627.	627.	627.
Flow 2	kg/s	1.83	1.83	1.83	1.83	1.67	1.83	1.83
T in	°C	130.	130.	130.	130.	130.	121.9	130.
T out	°C	40.00	40.00	40.00	40.00	40.00	40.00	48.07
Q 2	kW	689.2	689.2	689.2	689.2	627.4	627.4	627.4
ΔT ML	°C	51.3	51.3	51.7	51.1	51.3	48.7	58.3
U	W/m2/K		134	133	135	122	129	108
Measure		corrected	Specified			Calculated		

Measurement system

- Classify variables
 - Measured - non measured
 - Redundant - non redundant
 - Calculable - non calculable
 - Specified
- Measures => sensors
 - Exact (mean value)
 - Precision-Accuracy (standard deviation)
- Redundancy
 - Multiple sensors
 - Mass and energy balances



Data reconciliation problem

State variable value

measured value

$$\min_{X,Y} \sum_{i=1}^{n_{mes}} \left(\frac{y_i - y_i^*}{\sigma_i} \right)^2$$

standard deviation

s.t. $MassBalance(X, Y) = 0$

$EnergyBalance(X, Y) = 0$

$Thermodynamic(X, Y) = 0$

$ConstituteEquations(X, Y) = 0$

$Performance(X, Y, \pi) = 0$

$Inequalities(X, Y) \geq 0$

$F(Y, X) = 0$

Knowledge about the process

Virtual sensors

Problem resolution : constrained NLP Optimisation

$$\underset{x_i, y_i, \lambda_i}{Min} L = \sum_i \left(\frac{y_i - y_i^*}{\sigma_i} \right)^2 + 2 * \sum_j \overset{\text{Lagrange multiplier}}{\lambda_j} * \underbrace{f_j(y_i, x_i)}_{\text{virtual sensor}} \quad \text{Lagrange Formulation}$$

$$\underset{X, Y, \Lambda}{Min} L = (Y - Y^*)^t P (Y - Y^*) + 2 * \Lambda * F(X, Y) \quad \text{Matrix representation}$$

$$\Rightarrow \nabla L = 0 \quad \text{Gradient set to zero}$$

$$\text{soit} \quad \frac{\delta L}{\delta \Lambda} = F(Y, X) = 0$$

$$\frac{\delta L}{\delta X} = 2 * \Lambda * B = 0 \quad \text{avec} \quad b_{i,j} = \frac{\delta f_i(Y, X)}{\delta x_j}$$

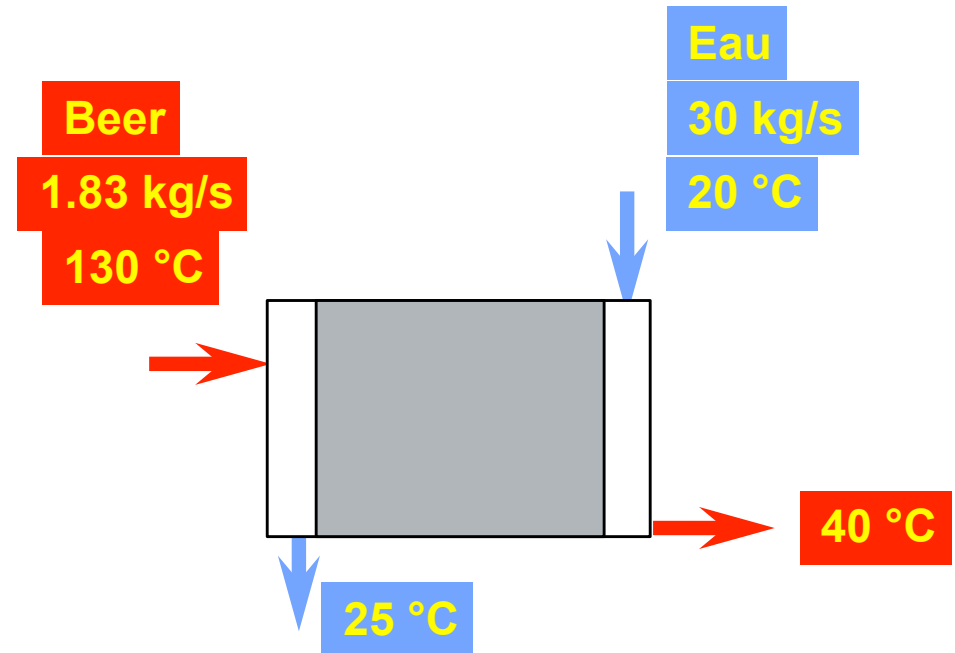
$$\frac{\delta L}{\delta Y} = (Y - Y^*) * P + \Lambda * A = 0 \quad \text{avec} \quad a_{i,j} = \frac{\delta f_i(Y, X)}{\delta y_j}$$

X = non measured, Y = measured

$F(Y, X) = 0$: Set of modeling+ specification equations

What is the heat transfer coefficient of the heat exchanger?

- Equations: 3
 - 2 energy balances
 - $Q = UA \Delta T_{lm}$
- State variables: 8
 - 4 temperatures
 - 2 flows
 - 2 parameters Q , U
- Degrees of Freedom : $5 = 8 - 3$
- Measures : 6



data reconciliation results

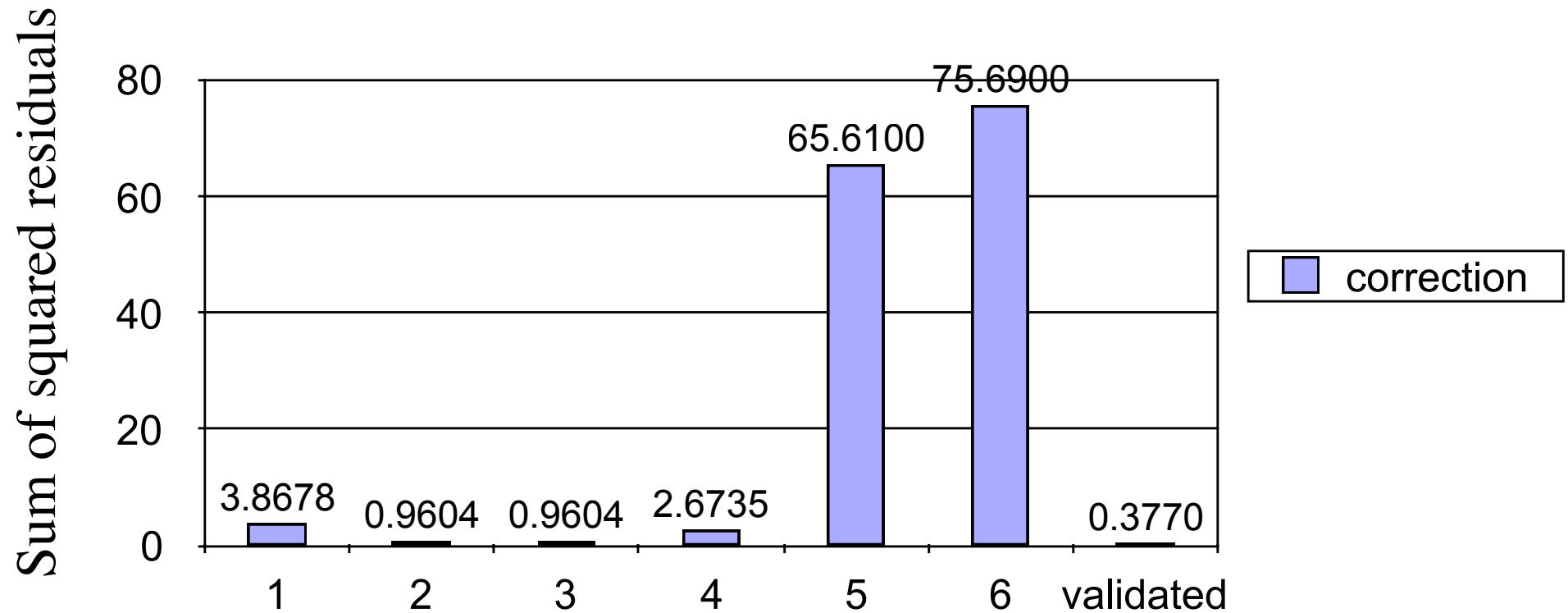
			Mes.	σ	Vali.	(M-V)/ σ
Flow 1	kg/s	M1	30.00	1.50	30.30	-0.197
T in	°C	T1	20.00	0.50	19.81	0.371
T out	°C	T2	25.00	0.50	25.19	-0.371
Q 1	kW		627.4		680.6	
Flow 2	kg/s	M2	1.83	0.10	1.81	0.215
T in	°C	T3	130.00	1.00	129.96	0.044
T out	°C	T4	40.00	1.00	40.04	-0.044
Q 2	kW		689.2		680.6	
			A	m2	100	
			ΔT LM	°C	51.40	
			U	W/m2/K	132	
					SSQ=	0.3643

What are the most probable values of the measured values ?

All measures are considered

		Mesures	1	2	3	4	5	6	
Flow 1	kg/s	30.00	32.95	30.00	30.00	30.00	30.00	30.00	30.30
T in	°C	20.00	20.00	19.51	20.00	20.00	20.00	20.00	19.81
T out	°C	25.00	25.00	25.00	25.49	25.00	25.00	25.00	25.19
Q 1	kW	627.	689.	689.	689.	627.	627.	627.	680.6
Flow 2	kg/s	1.83	1.83	1.83	1.83	1.67	1.83	1.83	1.81
T in	°C	130.	130.	130.	130.	130.	121.9	130.	129.96
T out	°C	40.00	40.00	40.00	40.00	40.00	40.00	48.07	40.04
Q 2	kW	689.2	689.2	689.2	689.2	627.4	627.4	627.4	680.6
ΔT ML	°C	51.3	51.3	51.7	51.1	51.3	48.7	58.3	51.40
U	W/m2/K		134	133	135	122	129	108	132
Measure		Corrected	Specification			Calculated			Validated

Results validity



Results analysis

- How to use the results
 - Sum of square residuals
 - is there a lot of corrections ?
 - Is the model (what we know) valid ?
 - e.g. a leakage is apriori not modeled
 - Are the bounds activated
 - Is the model valid
 - Sensitivity analysis
 - One can calculate the precision of the value of measured and unmeasured values
 - Corrections analysis
 - Failing sensors => Gross errors (if big corrections => remove the sensor)
 - Sensor calibration
 - Importance of the sensors on the results

Sensitivity

When the solution is obtained, we have

$$\nabla L = 0 \quad \equiv \quad \begin{bmatrix} P & 0 & A^T \\ 0 & 0 & B^T \\ A & B & 0 \end{bmatrix} * \begin{bmatrix} Y \\ X \\ \Lambda \end{bmatrix} = \begin{bmatrix} \overset{\text{measure weight}}{\underbrace{P}} Y^* \\ 0 \\ -C \end{bmatrix}$$

Or $MV = D$ D is the set of measured values

And $V = M^{-1}D$ Sensitivity of the calculated variable w.r.t to D

P is the weight of the measures ($\frac{1}{\sigma^2}$)

$$A = \frac{\delta F(X, Y)}{\delta Y} \quad B = \frac{\delta F(X, Y)}{\delta X} \quad F(X, Y) \text{ process model}$$

Sensitivity analysis : Variance of the results

In detail

The variance is calculated as a sensitivity to the variance of the measurement

Measurement
$$Y_i = \sum_{j=1}^{m+n+p} (M^{-1})_{ij} D_j$$

$$= \sum_{j=1}^m (M^{-1})_{ij} P_{jj} y_j^* - \sum_{k=1}^p (M^{-1})_{i \ n+m+k} C_k$$

Calculated
$$X_i = \sum_{j=1}^{m+n+p} (M^{-1})_{n+i \ j} D_j$$

$$= \sum_{j=1}^m (M^{-1})_{n+i \ j} P_{jj} y_j^* - \sum_{k=1}^p (M^{-1})_{n+i \ n+m+k} C_k$$

Variance calculation if
$$Z = \sum_{j=1}^m a_j X_j \quad \text{then} \quad \text{var}(Z) = \sum_{j=1}^m a_j^2 \text{var}(X_j)$$

A posteriori variance

Standard deviation of the calculated variables =f(P,Y*)

$$\text{var}(Y_i) = \sum_{j=1}^m \left\{ (M^{-1})_{ij} P_{jj} \right\}^2 \text{var}(y_j^*)$$

With $\text{var}(y_j^*) = 1/P_{jj}$

$$\text{var}(X_i) = \sum_{j=1}^m \left\{ (M^{-1})_{n_{mes} + i \ j} P_{jj} \right\}^2 \text{var}(y_j^*)$$

$$\text{var}(Y_i) = \sum_{j=1}^m \frac{(M^{-1})_{ij}^2}{\text{var}(y_j^*)}$$

$$\text{var}(X_i) = \sum_{j=1}^m \frac{(M^{-1})_{n_{mes} + i \ j}^2}{\text{var}(y_j^*)}$$

Sensitivity of solutions

to measurement

How much a calculated value is influenced by the value of a measurement

$$M \frac{\delta V}{\delta Y^*} + \frac{\delta M}{\delta Y^*} V - \frac{\delta D}{\delta Y^*} = 0 \Rightarrow \frac{\delta V}{\delta Y^*} = M^{-1} \begin{bmatrix} P \\ 0 \\ 0 \end{bmatrix}$$

Sensitivity of solutions

How much a calculated value is influenced by the accuracy of a measure

to measurement accuracy

$$M \frac{\delta V}{\delta P} + \frac{\delta M}{\delta P} V - \frac{\delta D}{\delta P} = 0$$

$$\Rightarrow \begin{bmatrix} \frac{\delta Y}{\delta P} \\ \frac{\delta X}{\delta P} \\ \frac{\delta \Lambda}{\delta P} \end{bmatrix} = M^{-1} \left[\begin{bmatrix} Y^* \\ 0 \\ 0 \end{bmatrix} - \begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} Y \\ X \\ \Lambda \end{bmatrix}^* \right]$$

Data reconciliation

- Corrects the measurement values (most probable consistent) value
- Consistent with heat and mass balances & thermodynamics
- Considers balances as additional measures (virtual sensors)
- A posteriori precision of each value (measured and non measured)
- Precision of performance indicators
- Sensitivity of measurements on performance indicators
- Quality of sensors

Parameter identification

Parameter identification

Knowing:

- System model $y = y(x, \pi)$
- measurement set (k experiments): $M[1..k] = \{y^i \mid i = 1..k\}$
- Objective function : deviation
$$L(\pi) = \|y - y^M\| = \sum_{i=1}^k \sqrt{(y(i)(x, \pi) - y^M(i))^2}$$

Compute an estimator $\hat{M} = \{y(\pi)\}$ of $M = \{y^i \mid i = 1..k\}$ such that :

$$\min_{\pi} L(\pi)$$

Parameter identification

$$\min_{\Theta} \sum_{i=1}^{n_{\text{exp}}} \frac{\left(y_i - y_i^*(x_i, \Theta)\right)^2}{\sigma_i^2}$$

⇒ When the model is not explicit

$$\min_{\Theta, x_{j,i}} \sum_{j=1}^{n_{\text{var}}} \sum_{i=1}^{n_{\text{exp}}} \frac{\left(x_{i,j} - x_{i,j}^*\right)^2}{\sigma_{i,j}^2}$$

Subject to $h(x_{i,j}, \Theta) = 0$ Model

Not all variables are measured

The problem is a Non linear Programming problem

- Quadratic
- Constrained

Validity of the parameter identification

- Number of parameters (p)
- Number of measurement set (n)
- Regression coefficient

$$R^2 = \frac{\sum (\hat{Y}_i - \bar{Y})^2}{\sum (Y_i - \bar{Y})^2}$$

$$\bar{Y} = \frac{1}{n} \sum_{i=1}^n Y_i$$

- Regression validity : Fischer test

$$F = \frac{(n - p)R^2}{(p - 1)(1 - R^2)}$$

Fisher value

$$> F(p - 1, n - p, 1 - \alpha)$$

α : significativity level