

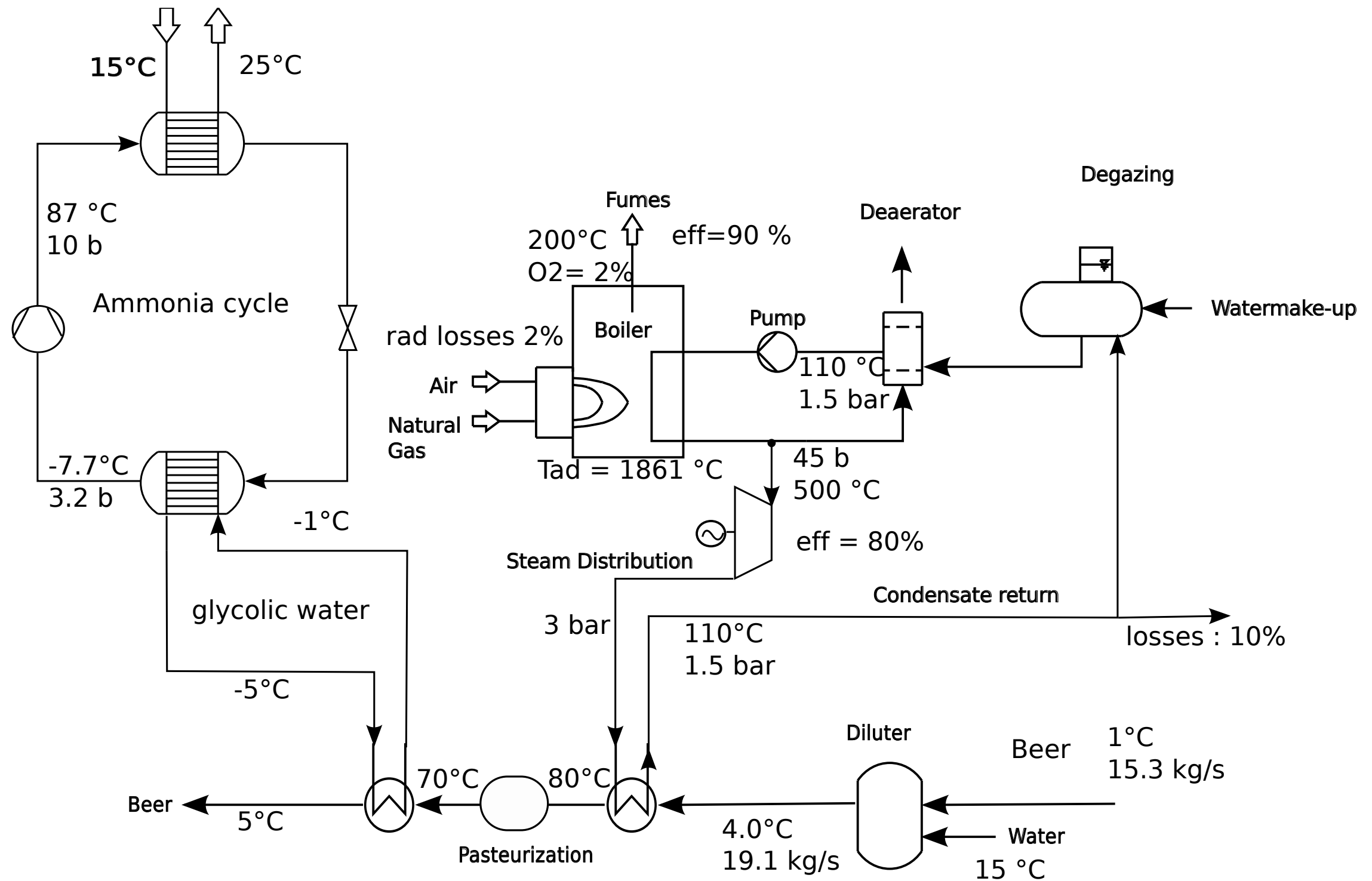


INDUSTRIAL ENERGY SYSTEMS

ENERGY CONVERSION SYSTEM

- How to analyse the energy consumption of an industrial system?
 - close balances: energy, mass, atomic
 - identify and quantify losses
 - calculate energy bill
- How to improve the system's efficiency?
 - locate losses
 - propose improvement options

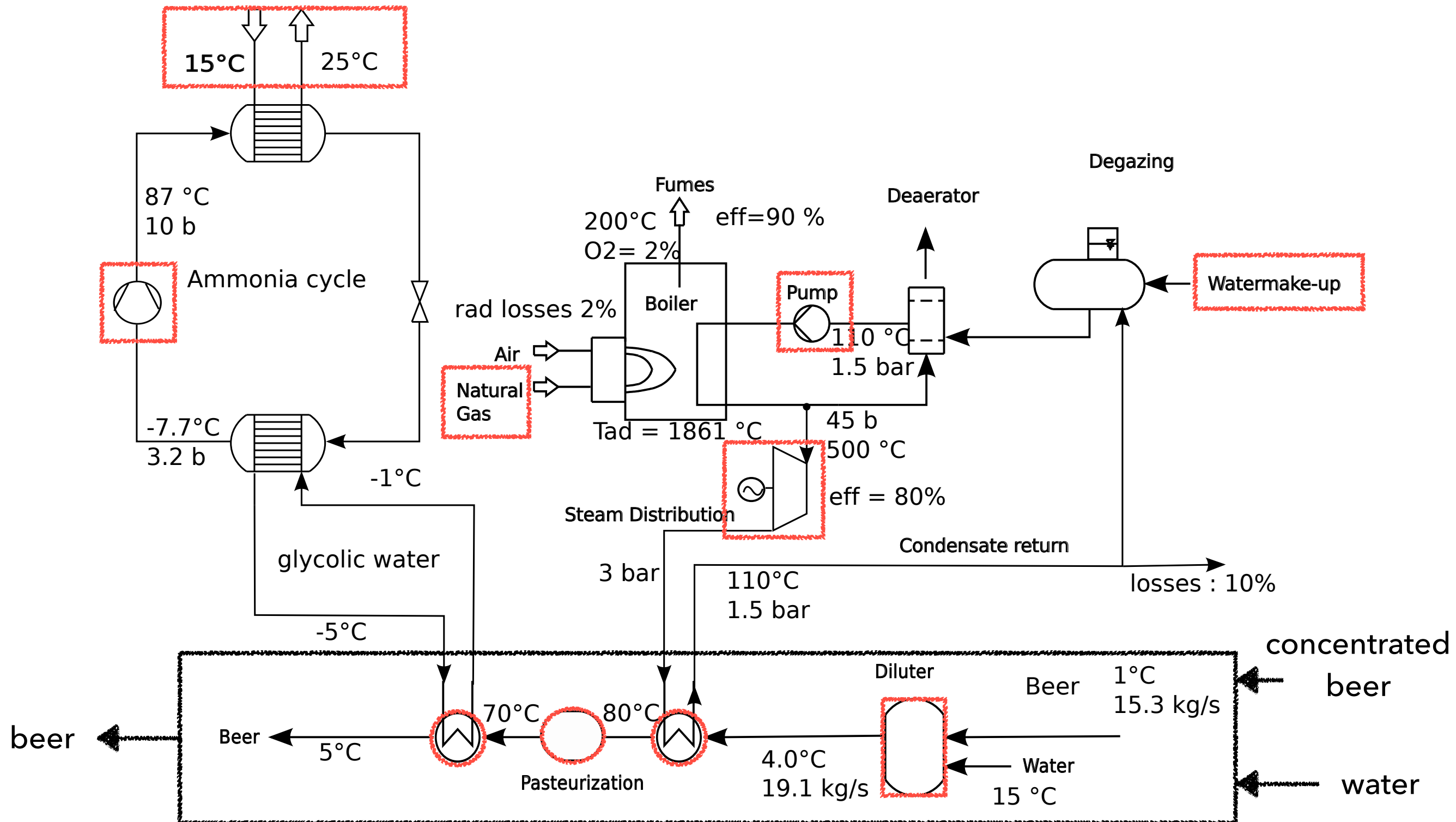
BEER PASTEURISATION



WHERE IS ENERGY ENTERING THE SYSTEM?

4

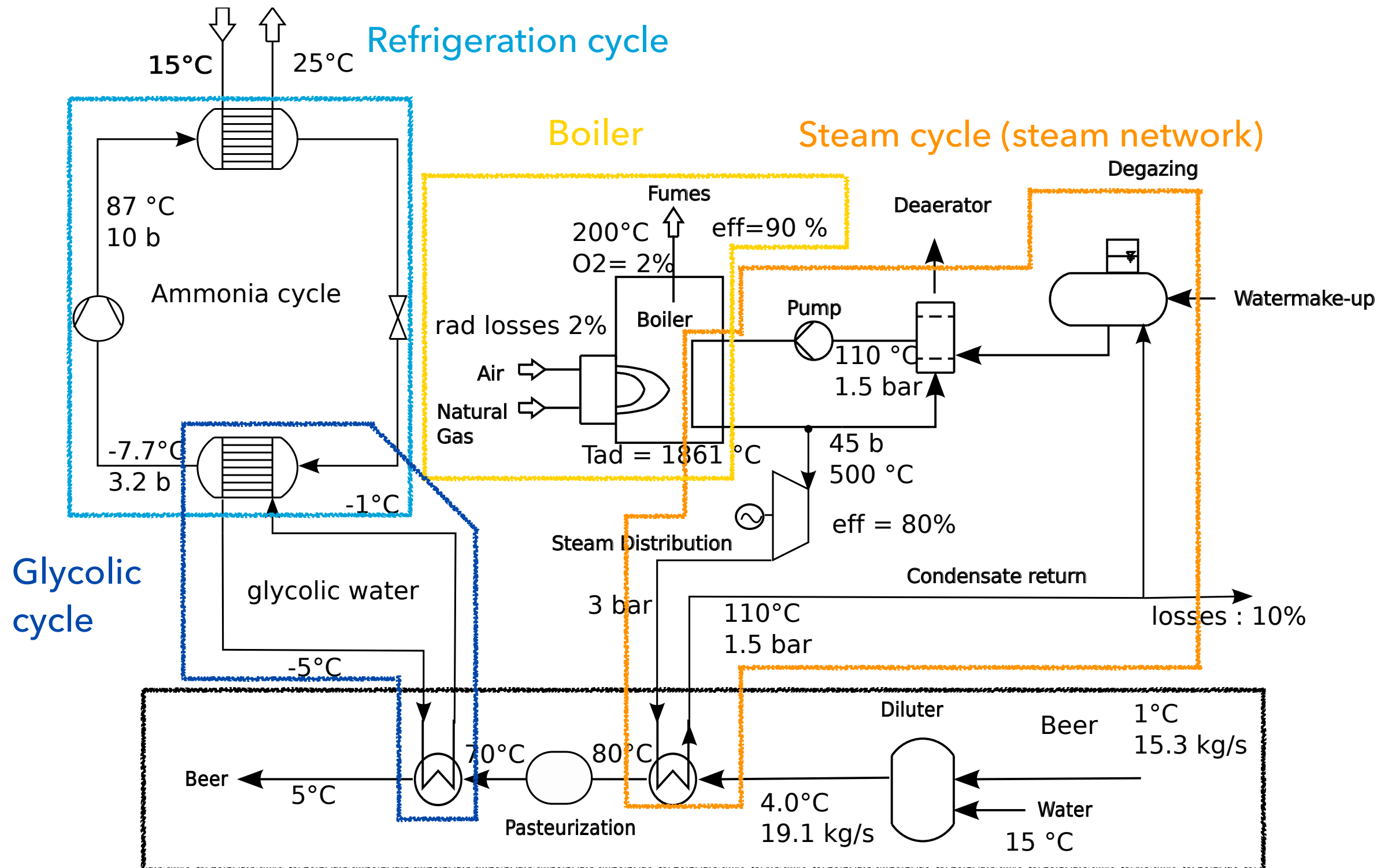
BEER PASTEURISATION



Process unit operation (Beer pasteurisation)

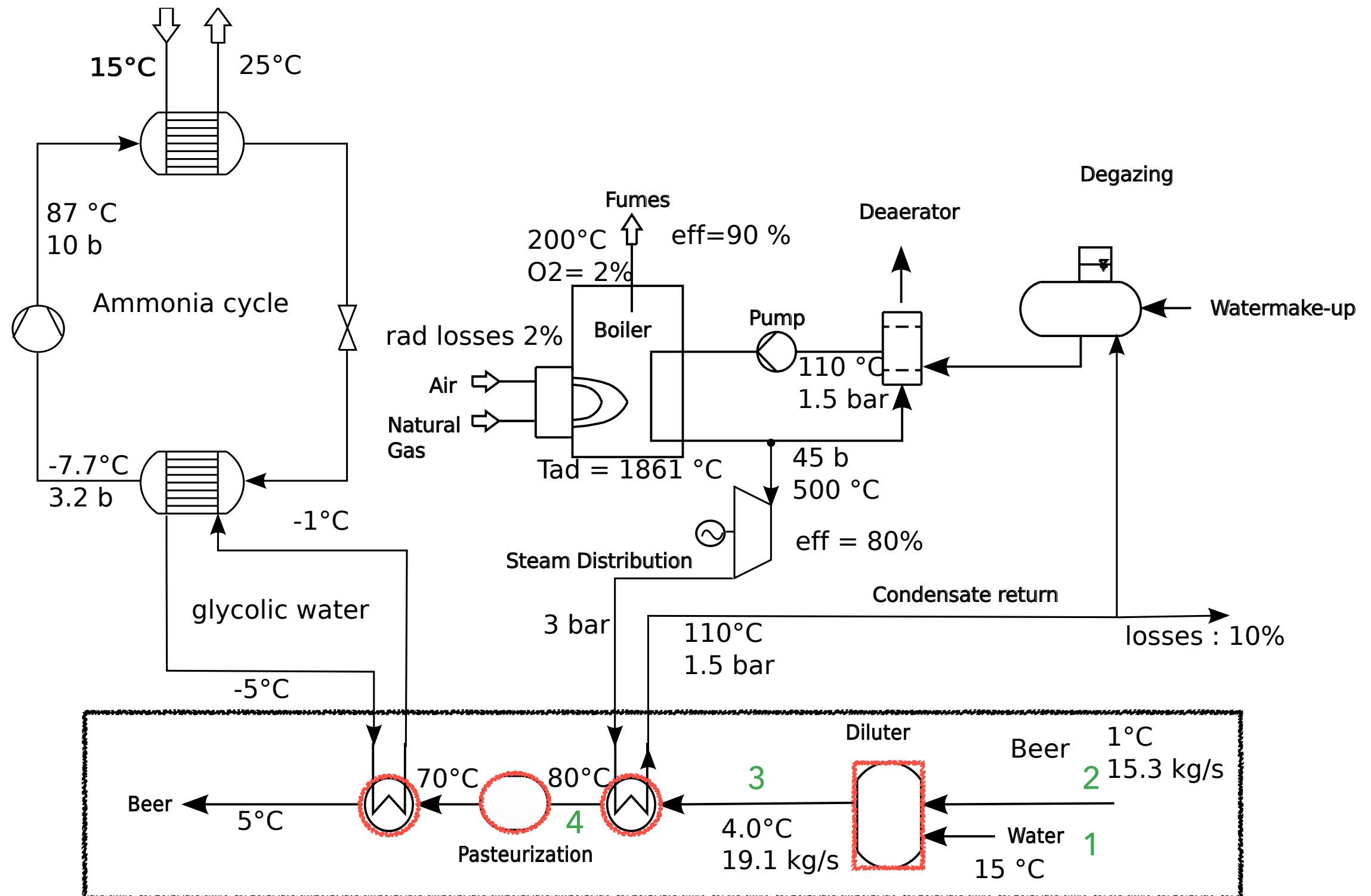
ENERGY CONVERSION

BEER PASTEURISATION



Process unit operation (Beer pasteurisation)

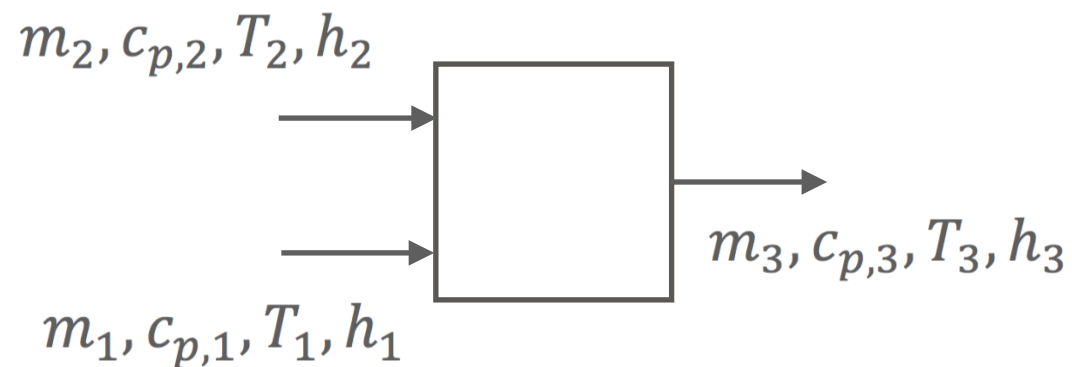
- Resources:
 - natural gas, coal, electricity, waste fuels, cooling water
- Distributed energy: utilities in between the process and the final energy source/sink
 - hot: steam, hot oil, hot water
 - cold: glycolic water, hot water
- energy conversion units: boilers, cogeneration units
- distribution system: networks



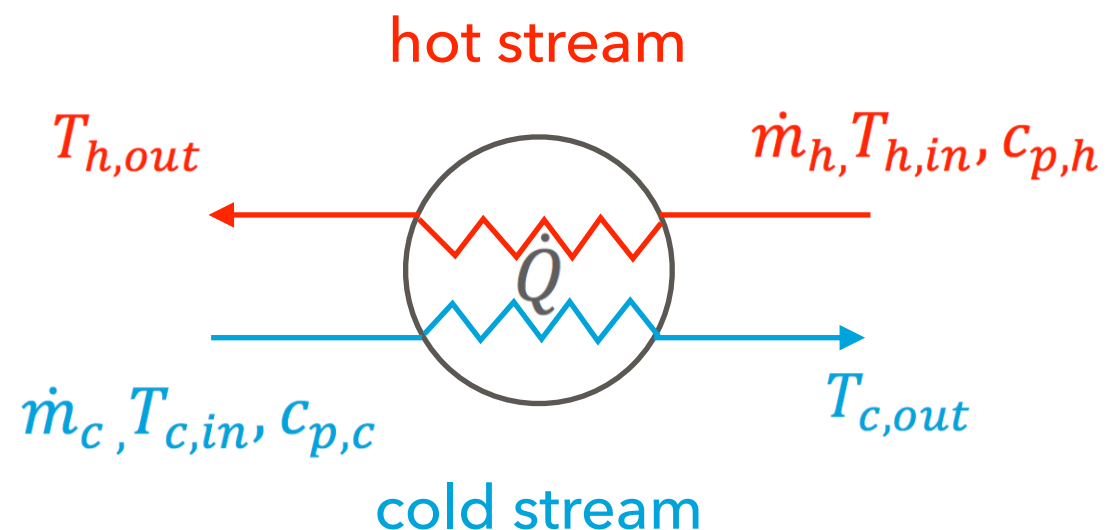
Process unit operation (Beer pasteurisation)

IDENTIFYING ENERGY REQUIREMENTS

- Mixers/splitters



- Heat exchangers



- mass balance:

$$\dot{m}_3 = \dot{m}_1 + \dot{m}_2$$

$$\dot{m}_3 \cdot x_{c,3} = \dot{m}_1 \cdot x_{c,1} + \dot{m}_2 \cdot x_{c,2} \quad \forall c \in n_c$$

- heat balance (non isothermal mixing):

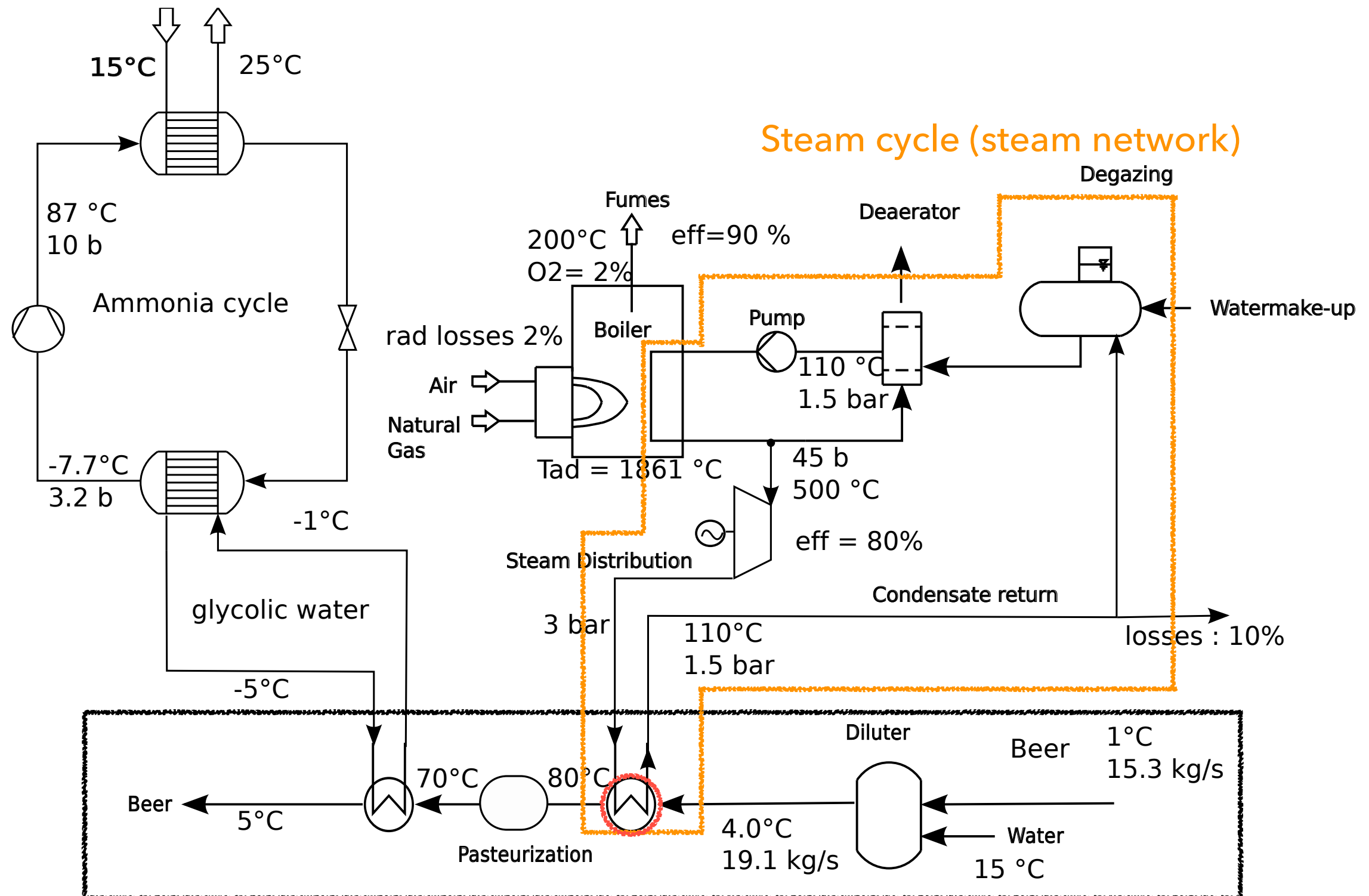
$$c_{p,i} = \sum_{n_{c,i}} x_{c,i} \cdot c_{p,c}$$

$$\dot{m}_3 \cdot h_3^{c=1} = \dot{m}_1 \cdot h_1 + \dot{m}_2 \cdot h_2$$

$$\dot{m}_3 \cdot c_{p,3} \cdot (T_3 - T_{ref}) = \dot{m}_1 \cdot c_{p,1} \cdot (T_1 - T_{ref}) + \dot{m}_2 \cdot c_{p,2} \cdot (T_2 - T_{ref})$$

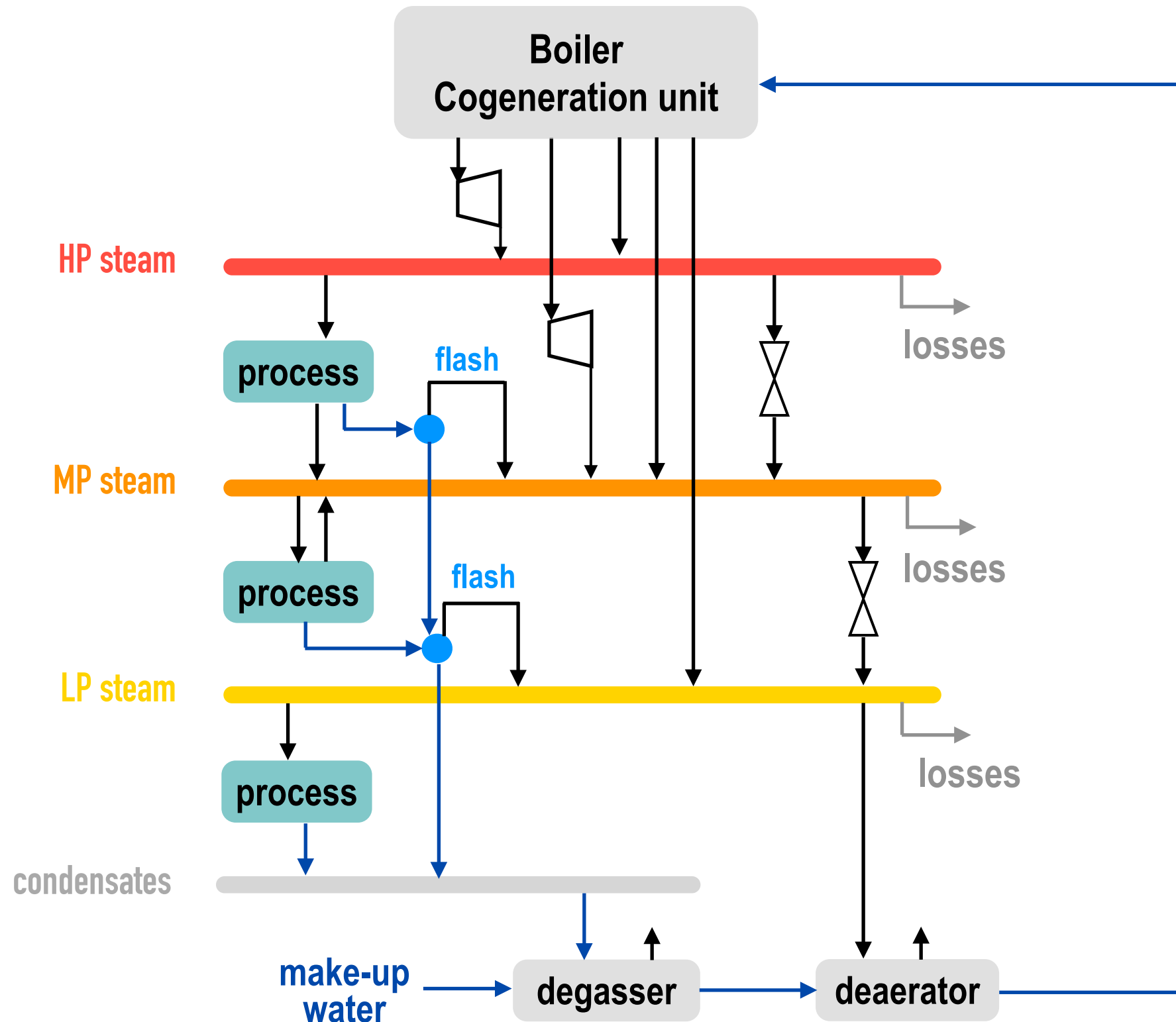
$$\begin{aligned} \dot{Q} &= \dot{m}_c \cdot c_{p,c} \cdot (T_{c,out} - T_{c,in}) \\ &= \dot{m}_h \cdot c_{p,h} \cdot (T_{h,in} - T_{h,out}) \end{aligned}$$

$$\begin{aligned} \dot{Q} &= \dot{m}_c \cdot (h_{out} - h_{in}) \\ &= \dot{m}_h \cdot (h_{in} - h_{out}) \end{aligned}$$



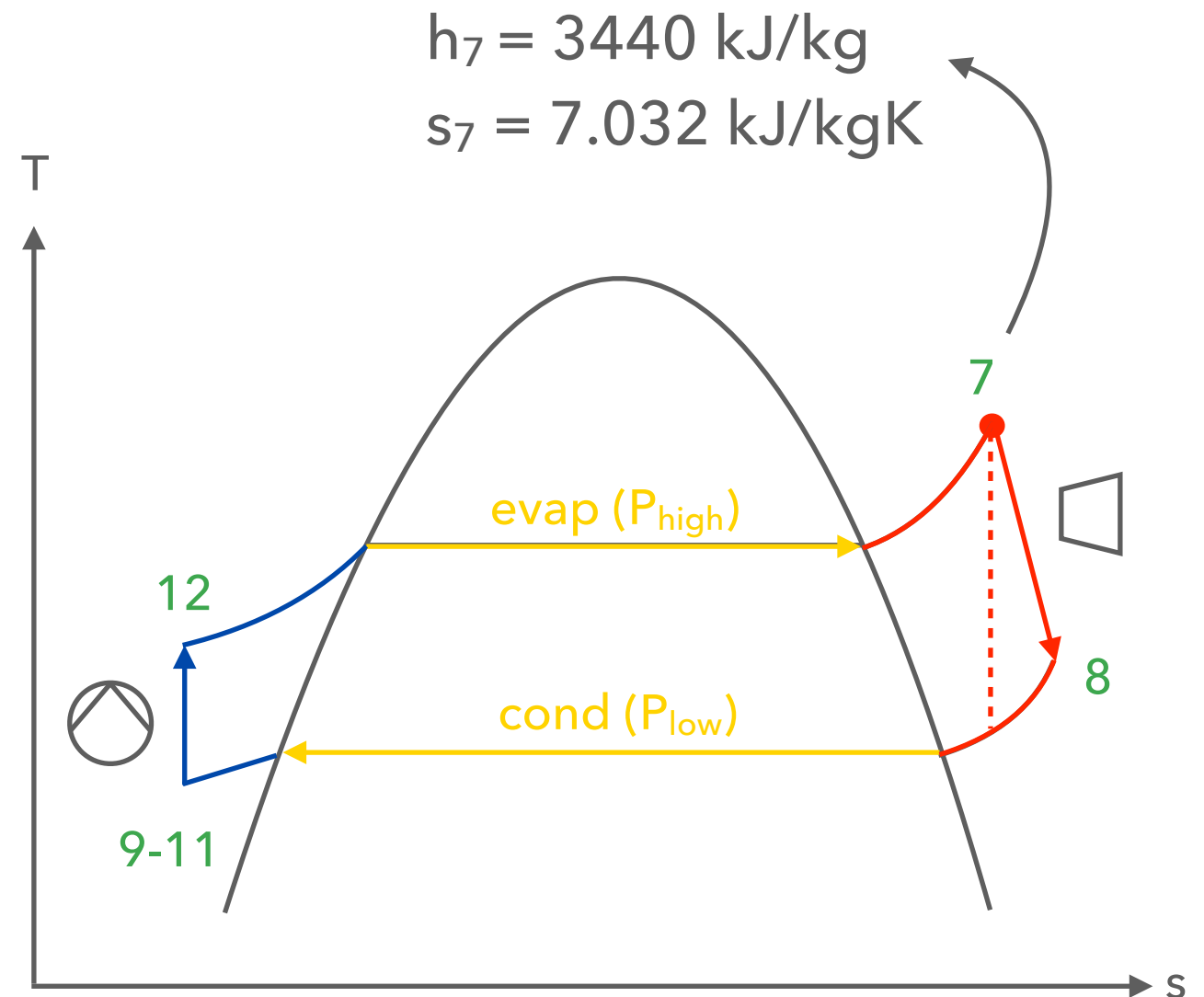
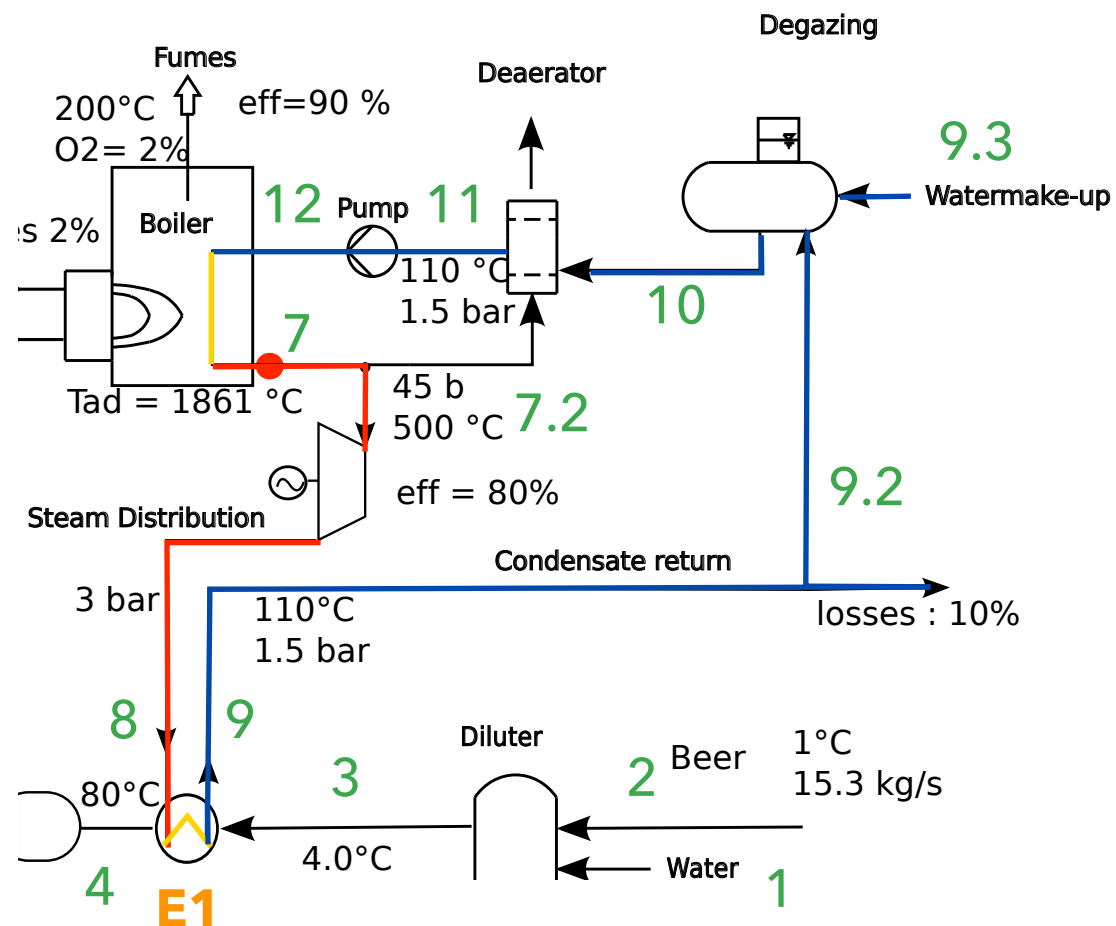
Process unit operation (Beer pasteurisation)

GENERAL ARCHITECTURE



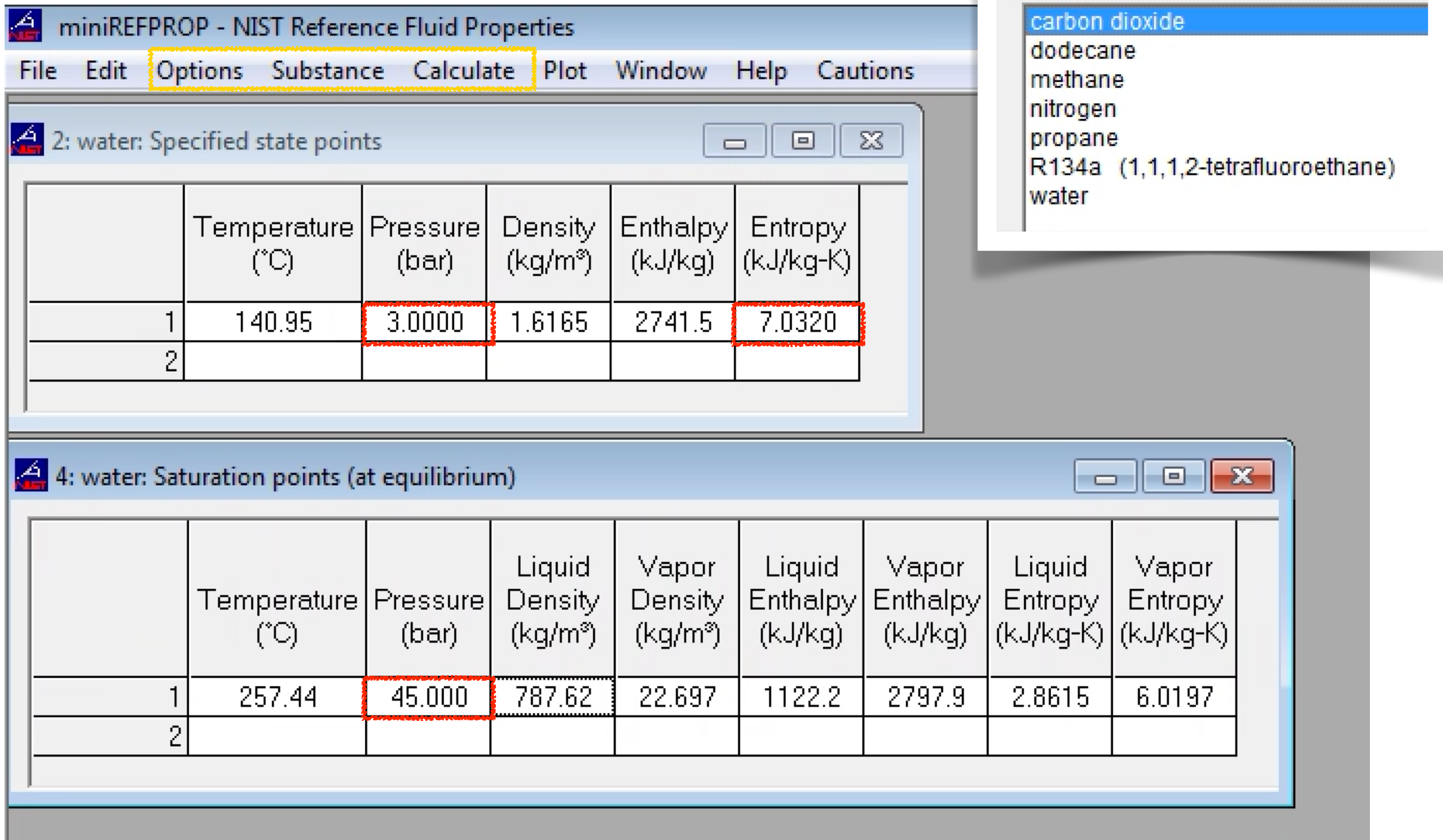
T-S DIAGRAM OF WATER

- MiniRefprop: $h(T,P)$ $s(T,P)$



- turbine isentropic efficiency: $\eta_{is,T} = \frac{h_7 - h_8}{h_7 - h_{8,is}}$
- turbine/pump: $\dot{W}_P = (h_{12} - h_{11})$ $\dot{W}_T = (h_7 - h_8)$

STATE VARIABLES - MINIREFPROP



miniREFPROP - NIST Reference Fluid Properties

File Edit Options Substance Calculate Plot Window Help Cautions

2: water: Specified state points

	Temperature (°C)	Pressure (bar)	Density (kg/m³)	Enthalpy (kJ/kg)	Entropy (kJ/kg-K)
1	140.95	3.0000	1.6165	2741.5	7.0320
2					

4: water: Saturation points (at equilibrium)

	Temperature (°C)	Pressure (bar)	Liquid Density (kg/m³)	Vapor Density (kg/m³)	Liquid Enthalpy (kJ/kg)	Vapor Enthalpy (kJ/kg)	Liquid Entropy (kJ/kg-K)	Vapor Entropy (kJ/kg-K)
1	257.44	45.000	787.62	22.697	1122.2	2797.9	2.8615	6.0197
2								

carbon dioxide
dodecane
methane
nitrogen
propane
R134a (1,1,1,2-tetrafluoroethane)
water

STATE VARIABLES - WEBSITE

http://www.peacesoftware.de/einigewerte/wasser_dampf_e.html

Calculation of thermodynamic properties of **water**

Pressure:

Temperature:

specific enthalpy :	251.55753600597	[kJ / kg]
specific entropy :	0.83096088836028	[kJ / kg K]

Calculation of thermodynamic properties of **overheated steam**
(upper limit: 799 C, 1000 bar)

Pressure:

Temperature:

specific enthalpy :	2776.5918154499	[kJ / kg]
specific entropy :	7.614673430236	[kJ / kg K]

Calculation of thermodynamic properties of **saturated steam**

Pressure:

or

Temperature:

specific enthalpy water :	762.68284433541	[kJ / kg]
specific enthalpy steam :	2777.1195376847	[kJ / kg]
specific entropy water :	2.1384313508991	[kJ / kg K]
specific entropy steam :	6.5849789963522	[kJ / kg K]
boiling temperature : (calculated)	179.88563239147	[Celsius]

STATE VARIABLES - ROSMOSE

```

{python use-coolprop, message=T}
from pyxosmose.state import State

state1 = State(pair='TP',fluid='Water',temperature=298,pressure=101325)
state1.StateCalc()
print(state1.__dict__)

```

specific enthalpy :	251.55753600597	[kJ / kg]
specific entropy :	0.83096088836028	[kJ / kg K]

```

{python use-coolprop, message=T}
from pyxosmose.state import State

state1 = State(pair='TP',fluid='Water',temperature=423,pressure=101325)
state1.StateCalc()
print(state1.__dict__)

```

specific enthalpy :	2776.5918154499	[kJ / kg]
specific entropy :	7.614673430236	[kJ / kg K]

Python 3.8.8 (C:/Users/cterrier/Desktop/documents/ae-project-reporting/venv/Scripts/python.exe)

Reticulate 1.25 REPL -- A Python interpreter in R.

Enter 'exit' or 'quit' to exit the REPL and return to R.

```

{'pair': 'TP', 'fluid': 'Water', 'temperature': 423, 'pressure': 101325,
'density': 0.523449293574313, 'cpmass': 1985.7445133408703, 'cvmass':
1496.585108926608, 'enthalpy': 2776207.7633732506, 'entropy': 7607.795928679631,
'vapfrac': -1.0}

```

```

{python use-coolprop-again, message=F}
from pyxosmose.state import State

state2 = State(pair='PQ',fluid='Water',pressure=1013250, vapfrac=1)
state2.StateCalc()
state2.cpmass
print(state2.__dict__)

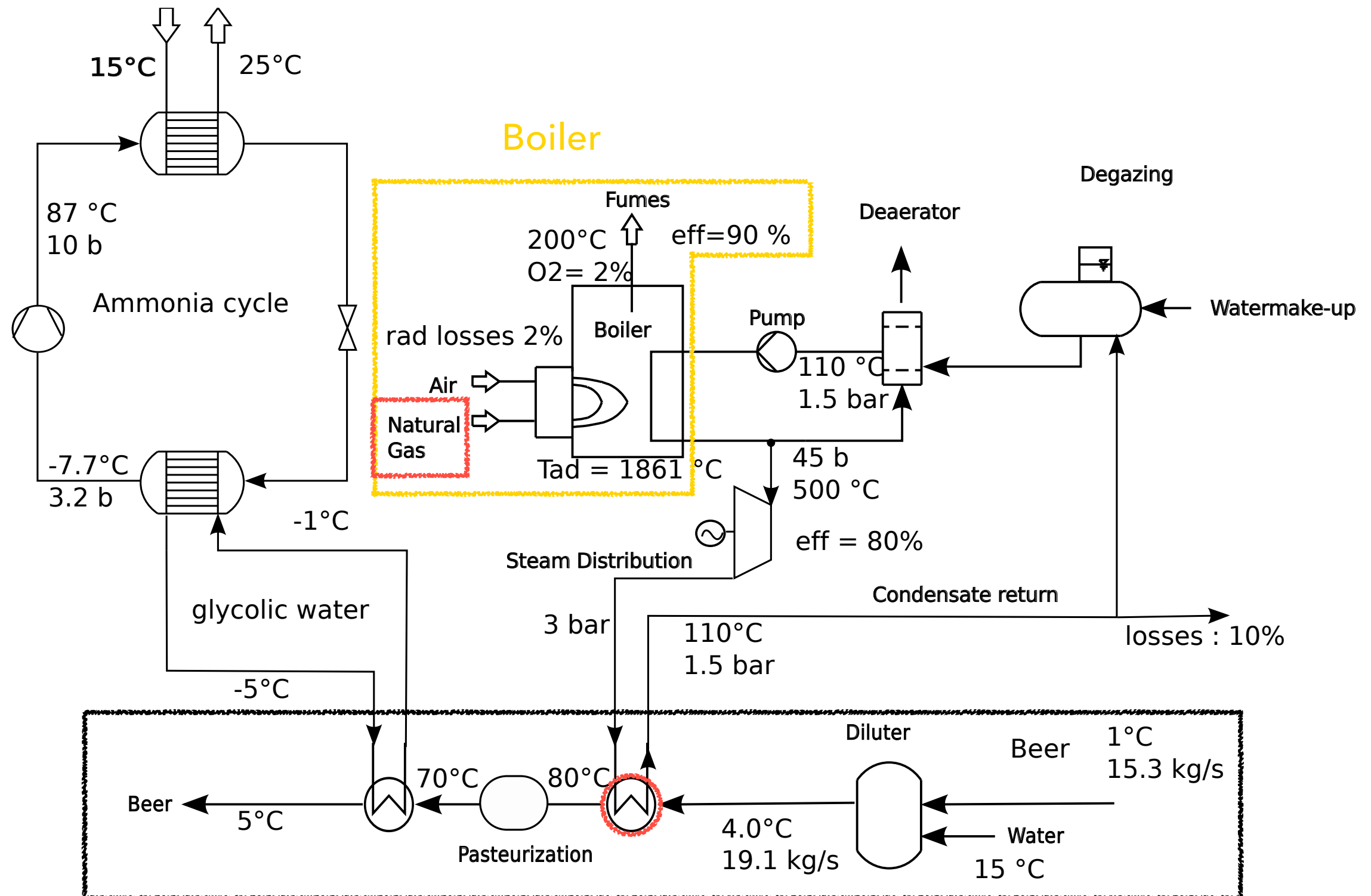
```

specific enthalpy water :	762.68284433541	[kJ / kg]
specific enthalpy steam :	2777.1195376847	[kJ / kg]
specific entropy water :	2.1384313508991	[kJ / kg K]
specific entropy steam :	6.5849789963522	[kJ / kg K]
boiling temperature : (calculated)	179.88563239147	[Celsius]

```

-1.0
{'pair': 'PQ', 'fluid': 'Water', 'temperature': 453.60078378606056
1013250, 'density': 5.210070697253118, 'cpmass': -1.0, 'cvmass': -
2777606.1994804046, 'entropy': 6580.468121095475, 'vapfrac': 1.0}

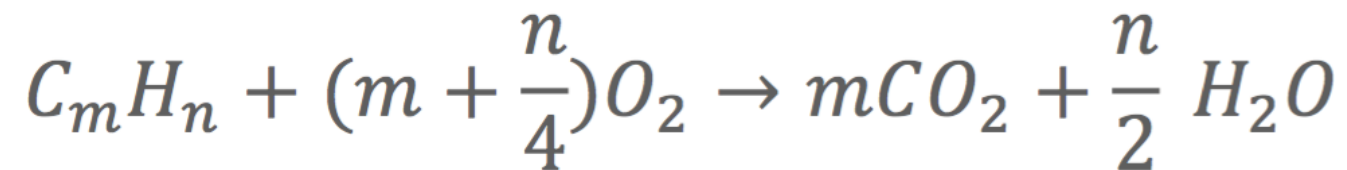
```



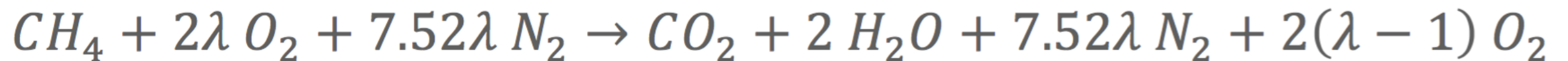
Process unit operation (Beer pasteurisation)

EQUATION

- general equation for HC stoichiometric combustion with O_2 :



- Air: = O_2 21% and N_2 79% (molar%)
- excess O_2 in fumes $\rightarrow$ excess air λ



$$\frac{2(\lambda - 1)}{1 + 2 + 7.52\lambda + 2(\lambda - 1)} = \text{excess } O_2 \text{ (molar\%)}$$

MOLAR QUANTITIES

- specific heat of fumes:

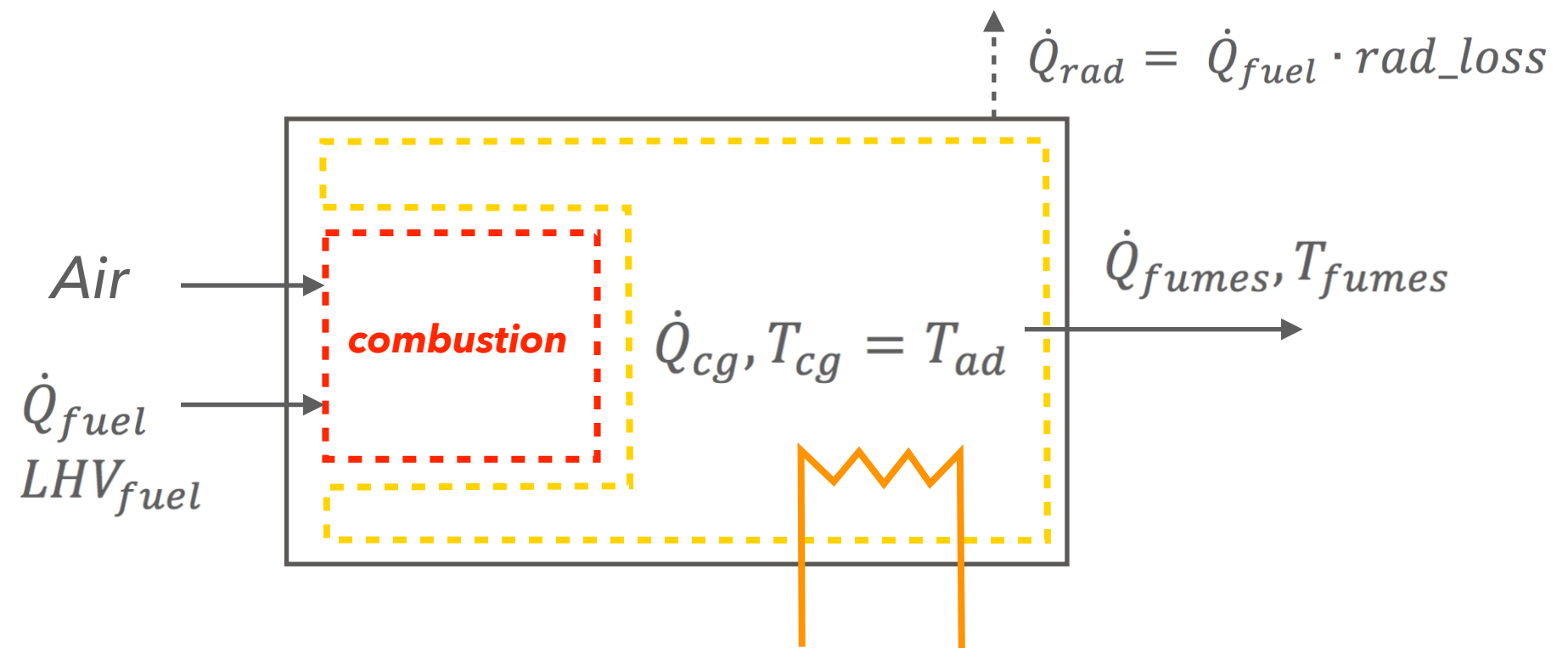
C_p 's to be found in tables

$$C_{p_{fumes}} = w_{CO_2} C_{p,CO_2} + w_{H_2O} C_{p,H_2O} + w_{N_2} C_{p,N_2} + w_{O_2} C_{p,O_2} \quad [kJ \cdot kg^{-1} \cdot K^{-1}]$$

$$w_{CO_2} = \frac{1 \cdot M_{CO_2}}{M_{CO_2} + 2 \cdot M_{H_2O} + 3.76 \cdot 2 \cdot \lambda \cdot M_{N_2} + 2(\lambda - 1) \cdot M_{O_2}} \quad [-]$$

$$w_{N_2} = \frac{7.52 \cdot \lambda \cdot M_{N_2}}{M_{CO_2} + 2 \cdot M_{H_2O} + 7.52 \cdot \lambda \cdot M_{N_2} + 2(\lambda - 1) \cdot M_{O_2}} \quad [-]$$

ENERGY AND MASS BALANCES WITH T_{AD}



$$\dot{Q}_{boiler} = \dot{m}_{fumes} c_{p,fumes} (T_{ad} - T_{fumes})$$

$$\dot{Q}_{fumes} = \dot{m}_{fumes} c_{p,fumes} (T_{fumes} - T_{LHV,ref})$$

$$(\dot{Q}_{boiler} + \dot{Q}_{fumes}) = \eta_{comb,eff} \dot{Q}_{fuel} (1 - rad_{loss})$$

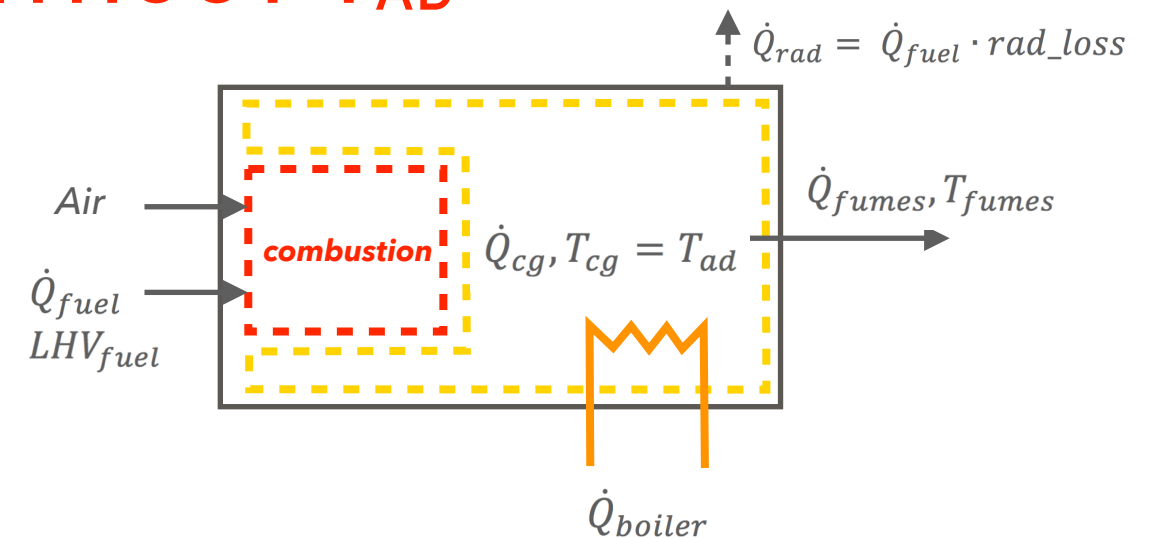
$$\dot{Q}_{fuel} = LHV_{fuel} \dot{m}_{fuel}$$

ENERGE AND MASS BALANCES **WITHOUT** T_{AD}

- Air-Fuel Ratio:

$$r_{air\ to\ fuel} = \frac{2\lambda M_{O_2} + 7.52\lambda M_{N_2}}{M_{CH_4}}$$

$$r_{fumes\ to\ fuel} = r_{air\ to\ fuel} + 1$$



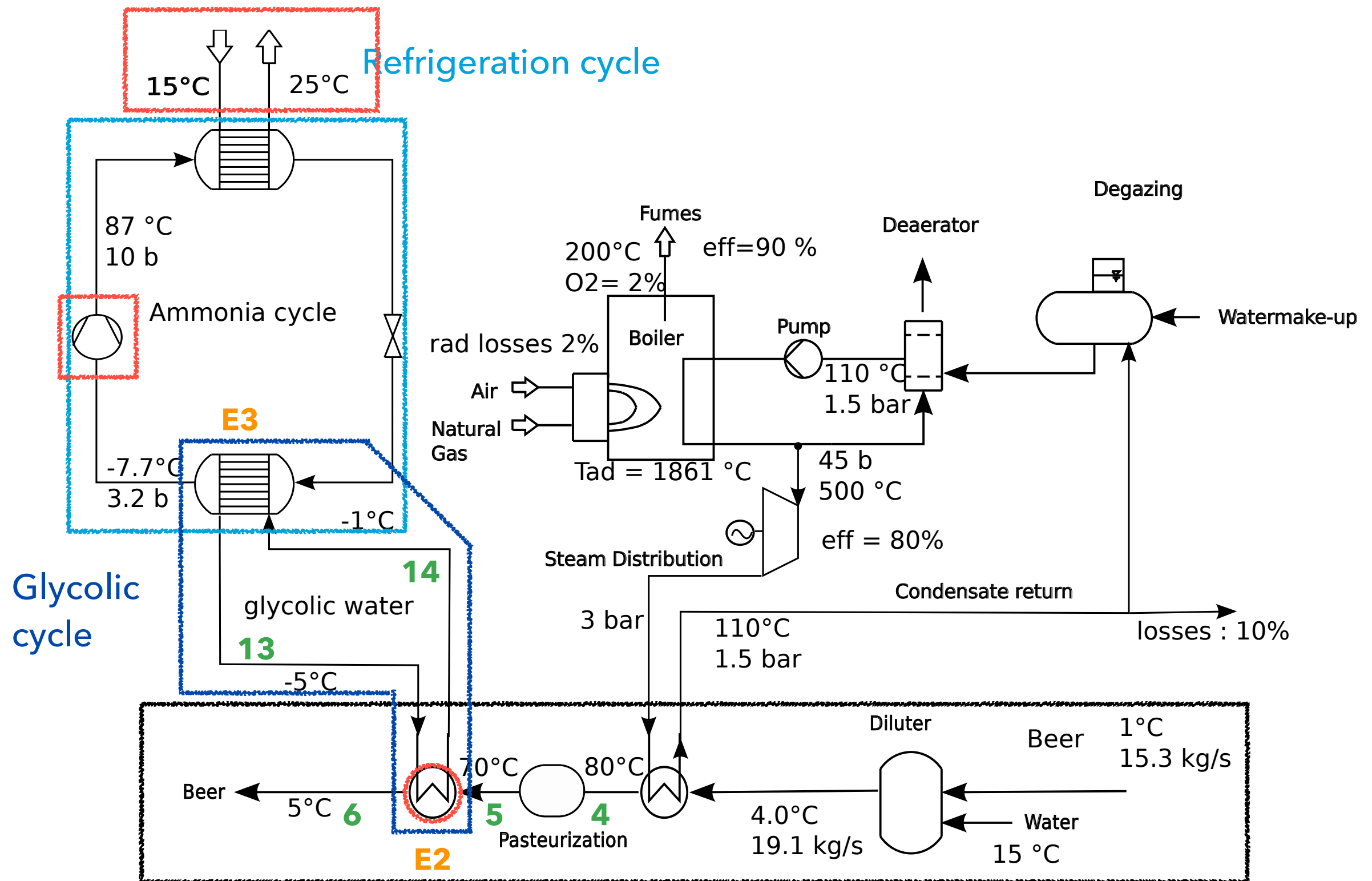
$$\dot{m}_{fumes}^{\text{X}} = r_{fumes\ to\ fuel} \dot{m}_{fuel}^{\text{X}}$$

$$\dot{Q}_{fumes}^{\text{X}} = \dot{m}_{fumes} C_{p,fumes} (T_{fumes} - T_{LHV,ref})$$

$$(\dot{Q}_{boiler} + \dot{Q}_{fumes}^{\text{X}}) = \eta_{comb,eff} \dot{Q}_{fuel}^{\text{X}} (1 - rad_{loss})$$

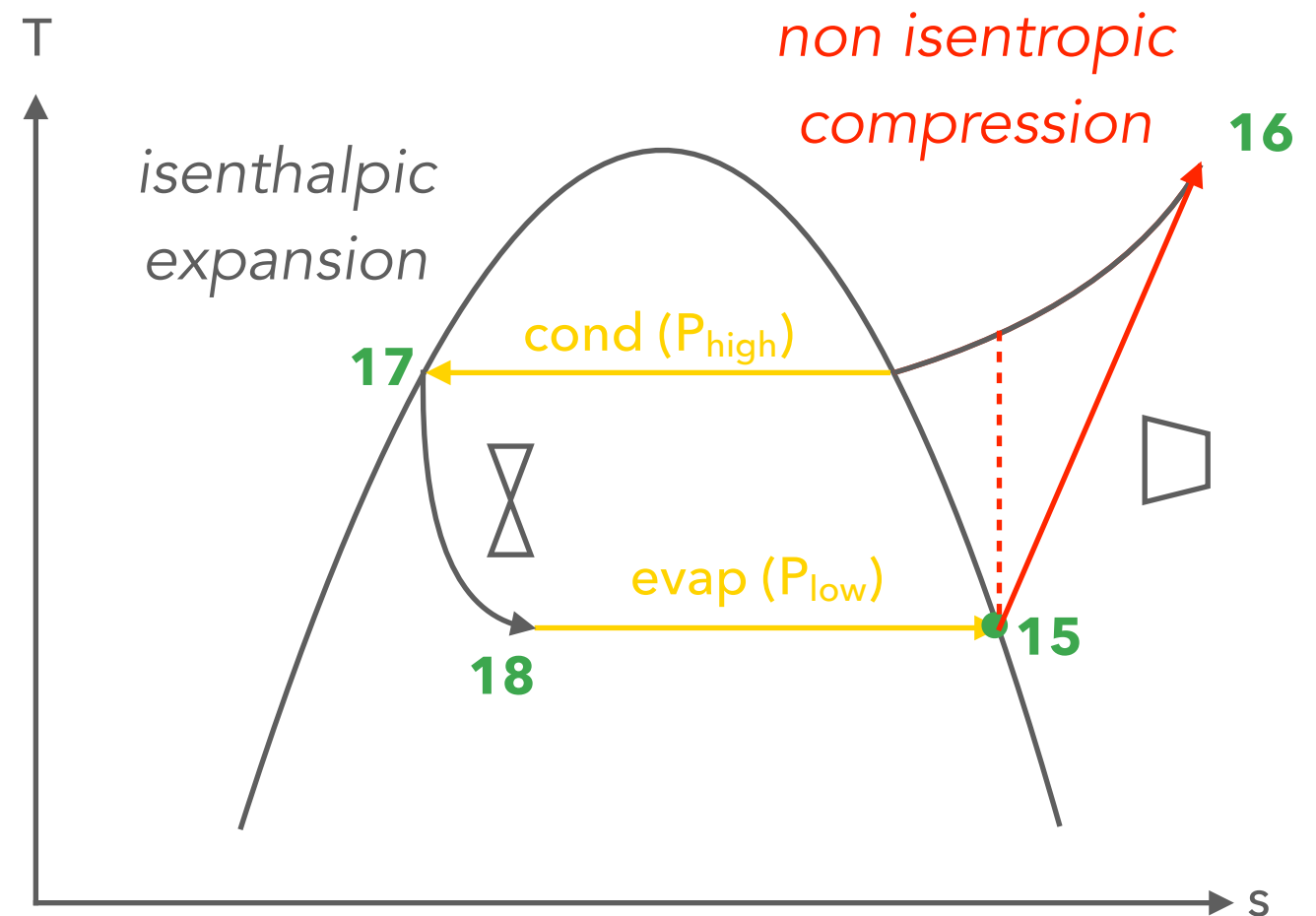
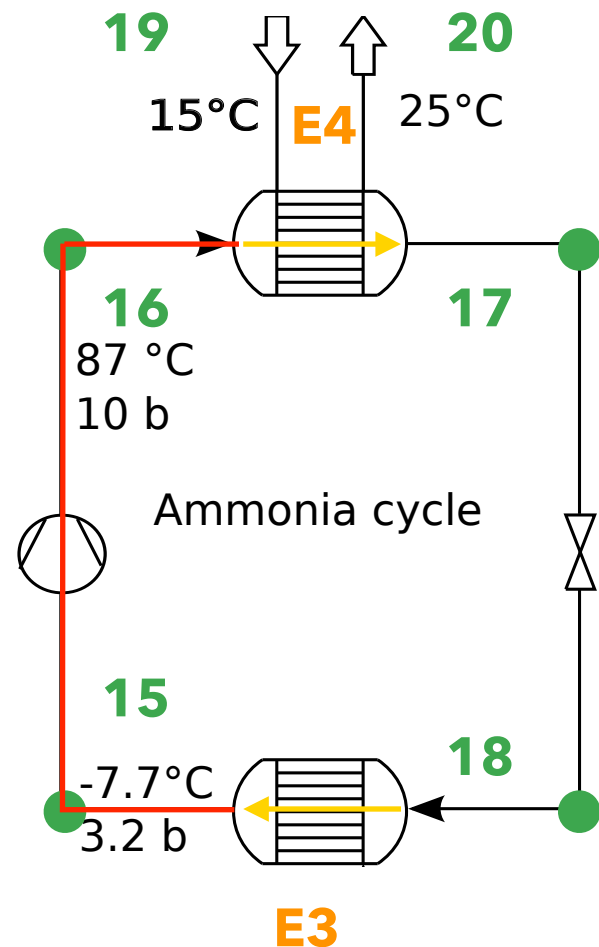
$$\dot{Q}_{fuel}^{\text{X}} = LHV_{fuel} \dot{m}_{fuel}^{\text{X}}$$

- In exercise: 4 equations for **4 unknowns**



Process unit operation (Beer pasteurisation)

- CoolPack: Ammonia = R717



- compressor isentropic efficiency: $\eta_{is,c} = \frac{h_{16,is} - h_{15}}{h_{16} - h_{15}}$
- compressor: $\dot{W}_C = \dot{m}_{amm}(h_{16} - h_{15})$

- Energy costs:

$$OC_{NG}[CHF/y] = \dot{Q}_{fuel}[kW] \cdot op_{time}[h/y] \cdot c_{NG}[CHF/kWh]$$

$$OC_{elec}[CHF/y] = (\dot{W}_{pump} + \dot{W}_{comp})[kW] \cdot op_{time}[h/y] \cdot c_{elec}[CHF/kWh]$$

$$OC_w[CHF/y] = \frac{\dot{m}_w[kg/s]}{\rho_w[kg/m^3]} \cdot op_{time}[s/y] \cdot c_w[CHF/m^3]$$

- Electricity sales income:

$$OI_{elec}[CHF/y] = \dot{W}_{turb}[kW] \cdot op_{time}[h/y] \cdot c_{elec}[CHF/kWh]$$

- Total energy bill:

$$OC_{tot}[CHF/y] = OC_{NG} + OC_{elec} + OC_w - OI_{elec}$$