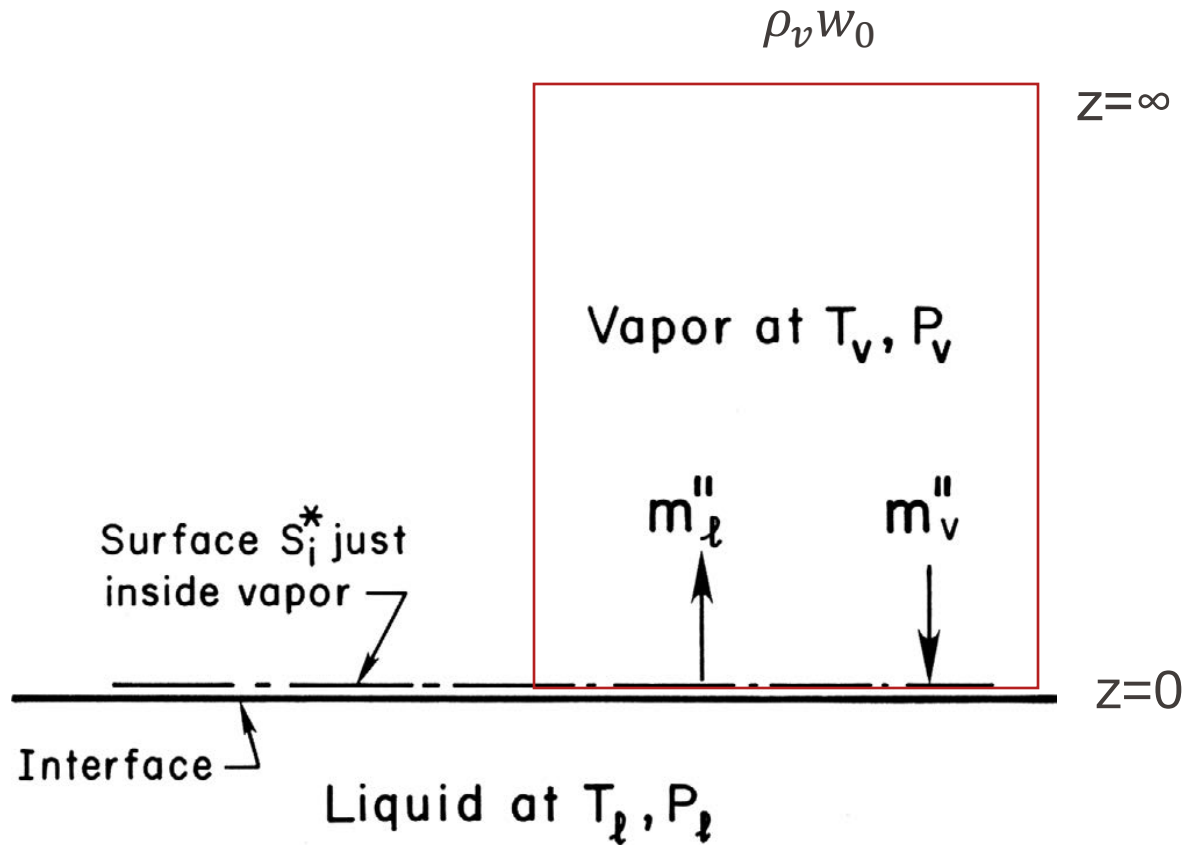


ME-446: Liquid-gas interfacial heat and mass transfer

Boiling I

Zhengmao Lu
Energy Transport Advances
Laboratory
EPFL Mechanical Engineering

- Velocity distribution function
- Relationship between macroscopic properties and velocity distribution
- Evaporation kinetics (Schrage equation)



Mass balance

$$m_l'' - m_v'' = \rho_v w_0$$

$$m_l'' = \hat{\sigma} m_e'' + (1 - \hat{\sigma}) m_v''$$

$$= \hat{\sigma} \frac{P_l}{RT_l} \left(\frac{k_B T_l}{2\pi m} \right)^{\frac{1}{2}} + (1 - \hat{\sigma}) m_v''(w_0)$$

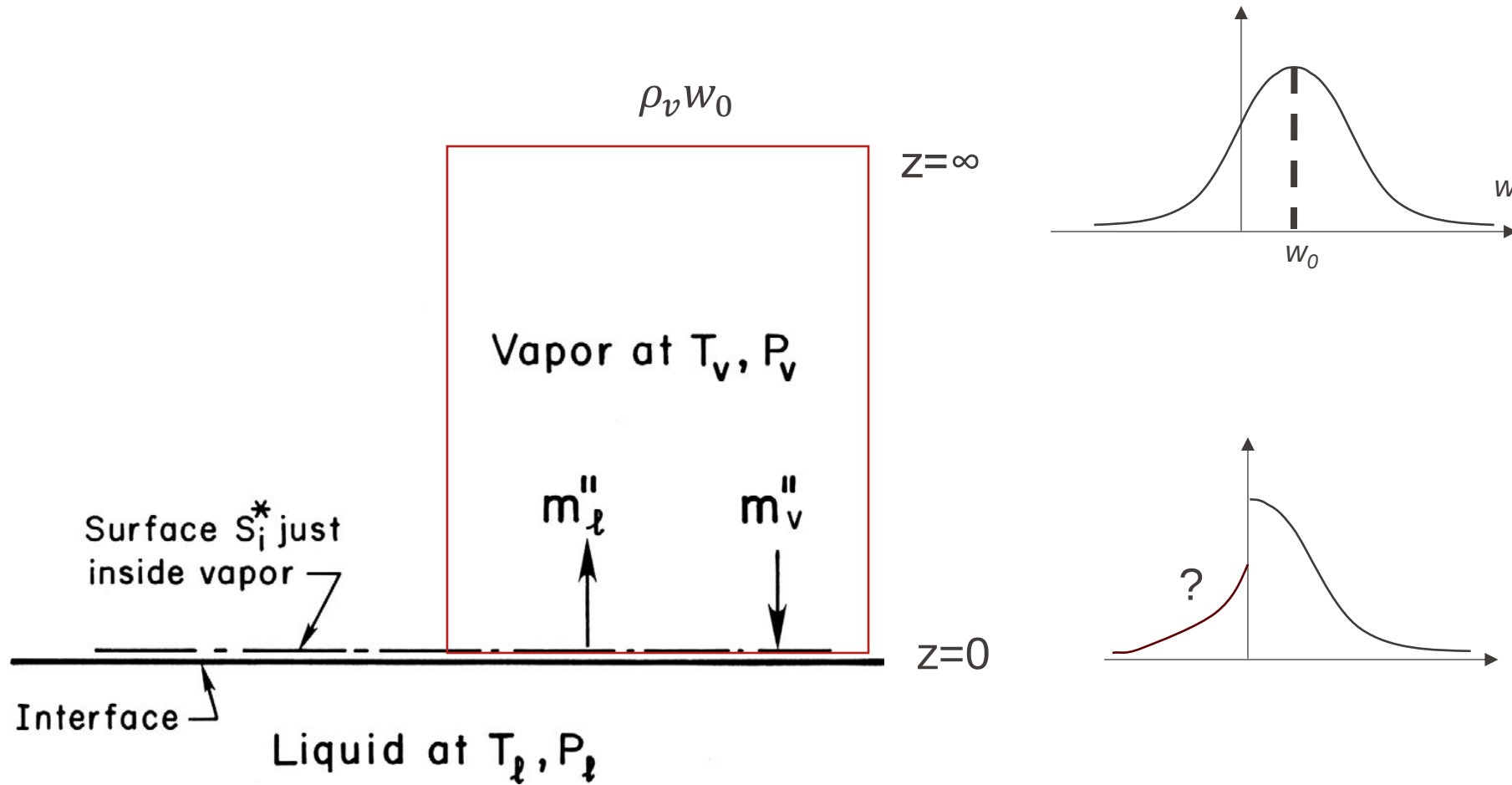
$$\hat{\sigma} \frac{P_l}{RT_l} \left(\frac{k_B T_l}{2\pi m} \right)^{\frac{1}{2}} - \hat{\sigma} m_v''(w_0) = \rho_v w_0$$

$$m_v''(w_0) = \rho_v \int_{-\infty}^0 \left(\frac{m}{2\pi k_B T_v} \right)^{\frac{1}{2}} \exp \left(-\frac{m(w - w_0)^2}{2k_B T_v} \right) w dw$$

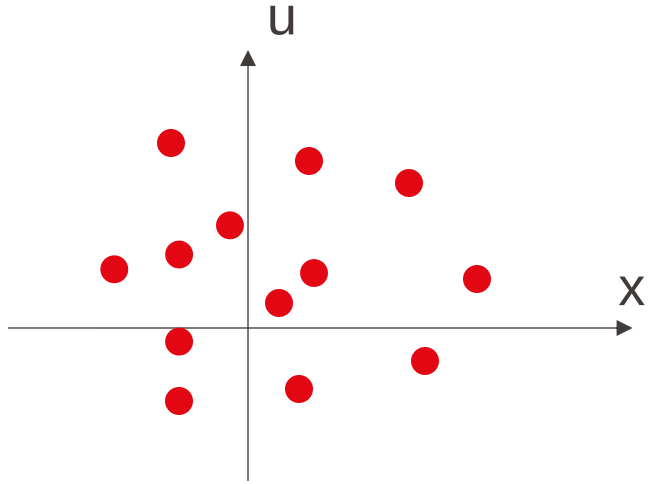
Solve for w_0

$$q_{evap}'' = \rho_v w_0 h_{lv}$$

General Governing Equation



Define $\xi(u, v, w)du dv dw = n f(u, v, w)du dv dw$ which represent the number of molecules one expect to find in the ranges u to $u + du$, v to $v + dv$, w to $w + dw$ in a unit volume



$$\frac{\partial \xi}{\partial t} = \frac{\partial \xi}{\partial x} \cdot \frac{\partial x}{\partial t} + \frac{\partial \xi}{\partial u} \cdot \frac{\partial u}{\partial t} + \Omega(\xi, \xi)$$

$$\frac{\partial \xi}{\partial t} = \frac{\partial \xi}{\partial x} \cdot u + \frac{\partial \xi}{\partial u} \cdot g_x + \Omega(\xi, \xi)$$

Evolution of F caused by streaming of molecules, external forces, and collisions between two molecules

$$\begin{aligned} \frac{\partial \xi}{\partial t} = & \frac{\partial \xi}{\partial x} \cdot u + \frac{\partial \xi}{\partial y} \cdot v + \frac{\partial \xi}{\partial z} \cdot w \\ & + \frac{\partial \xi}{\partial u} \cdot \frac{\partial u}{\partial t} + \frac{\partial \xi}{\partial v} \cdot \frac{\partial v}{\partial t} + \frac{\partial \xi}{\partial w} \cdot \frac{\partial w}{\partial t} + \Omega(\xi, \xi) \end{aligned}$$

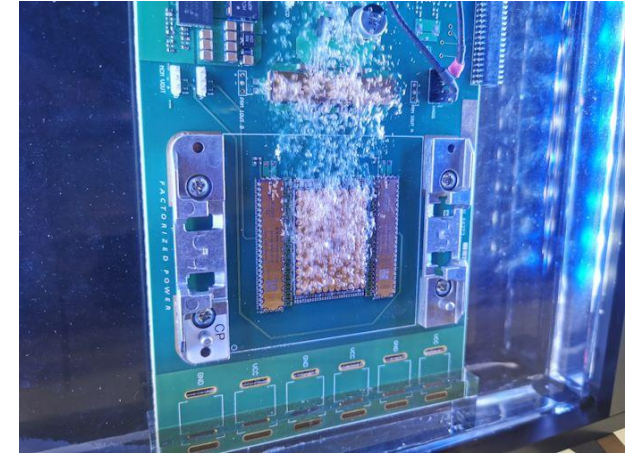
The major complexities are buried in $\Omega(F, F)$



cooking



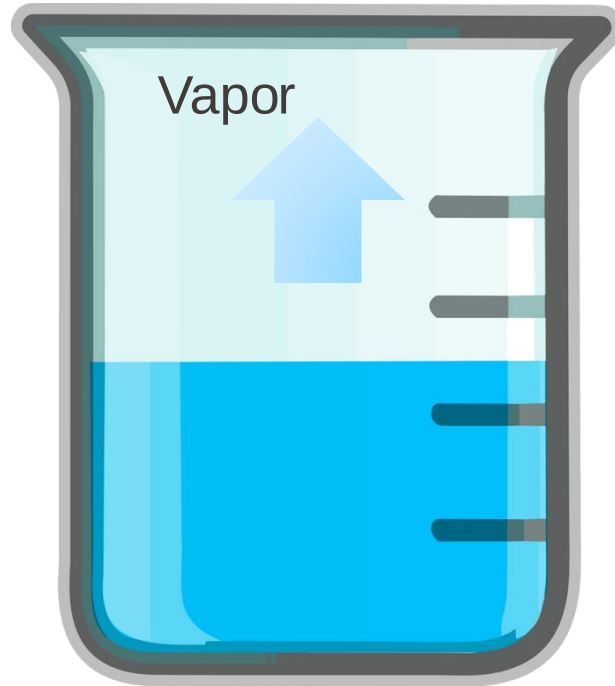
(nuclear) power plant



immersion cooling

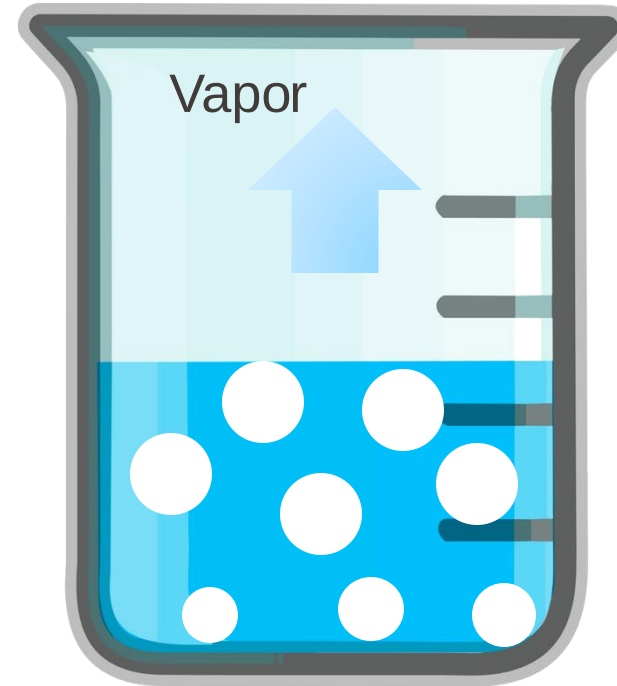
Evaporation vs Boiling

Evaporation



Heat

Boiling



Bubble
nucleation



Heat

Intended Learning Objectives Today

- Analyze the free energy of vapor embryo (Thermodynamics)
- Understand the derivation of bubble growth kinetics at small sizes
- Reading materials: **Carey**, Chapter 5.2, 5.3, 6.1

Formation of a Vapor Embryo (Homogeneous Nucleation)

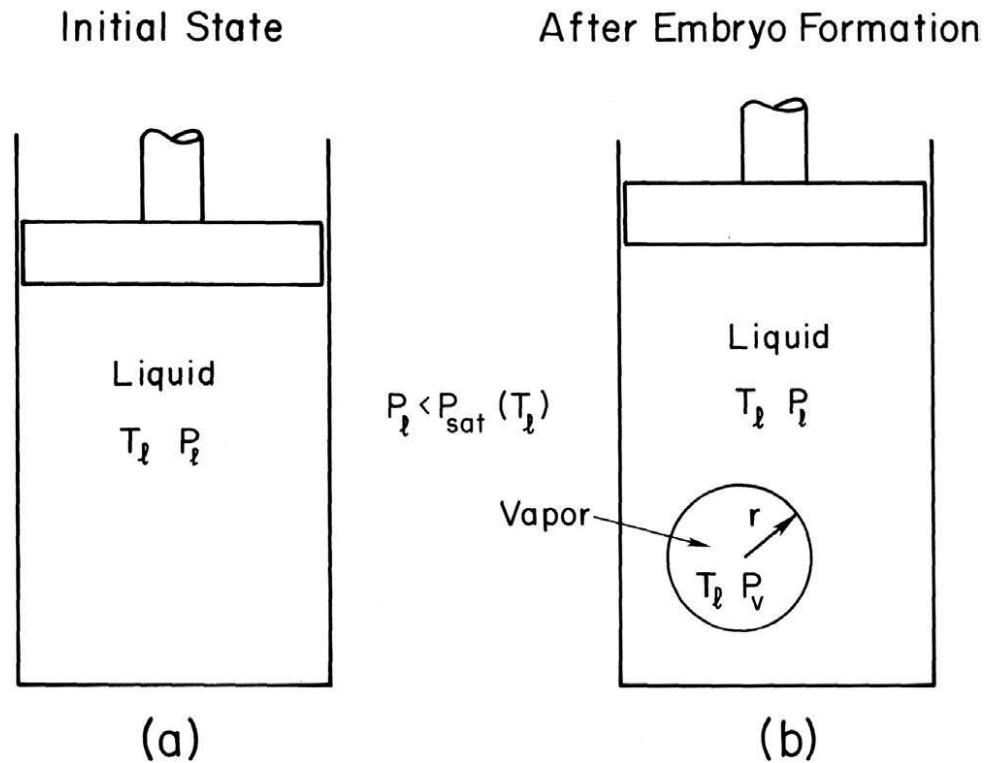


Figure 5.7 in Carey

Vapor bubble in bulk liquid at constant temperature and pressure

Gibbs free energy analysis

$$G = G_l + G_v + G_i$$

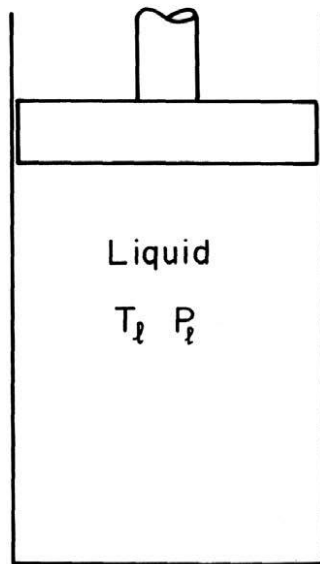
$$(b) - (a)$$

$$\Delta G_l = -\hat{N}_v \hat{g}_l$$

$$\Delta G_v = \hat{N}_v \hat{g}_v(T_l, P_v) + (P_l - P_v)V_v$$

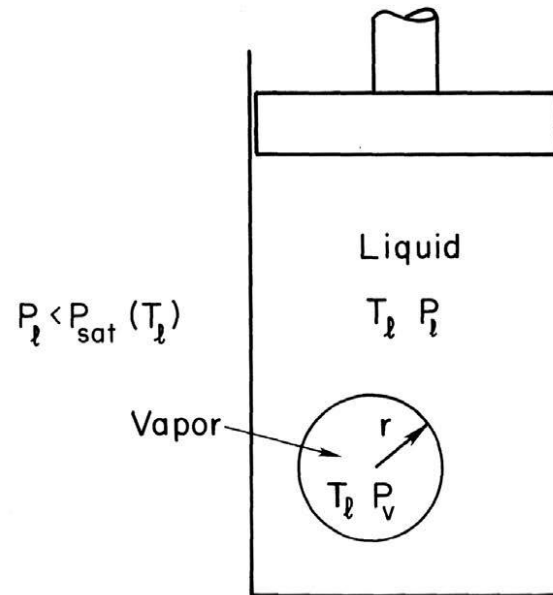
$$\Delta G_i = 4\pi r^2 \sigma_{lv}$$

Initial State



(a)

After Embryo Formation



(b)

$$\Delta G = \hat{N}_v(\hat{g}_v - \hat{g}_l) + (P_l - P_v)V_v + 4\pi r^2 \sigma_{lv}$$

Assuming the system reaches equilibrium when $r = r_e$

$$\hat{g}_v = \hat{g}_l$$

$$P_v - P_l = 2\sigma_{lv}/r_e$$

$$\Delta G_e = \frac{4}{3}\pi r_e^2 \sigma_{lv}$$

Gibbs Free Energy Change

$$\Delta G = \hat{N}_v(\hat{g}_v - \hat{g}_l) + (P_l - P_v)V_v + 4\pi r^2 \sigma_{lv}$$

Considering T_l and P_l as fixed values, assuming mechanical equilibrium is always satisfied

$$P_v = P_l + \frac{2\sigma_{lv}}{r} \text{ is a function of } r$$

With ideal gas law, $\hat{N}_v = P_v V_v / k_B T_l$ is also a function of r

ΔG can be considered as a function of r , to which we can apply Taylor expansion near r_e

$$\begin{aligned} \frac{d\Delta G}{dr} &= \hat{N}_v \left(\frac{\partial \hat{g}_v}{\partial P_v} \right)_{T_l} \frac{dP_v}{dr} + \frac{d\hat{N}_v}{dr} (\hat{g}_v - \hat{g}_l) - \frac{dP_v}{dr} V_v + 4\pi r^2 (P_l - P_v) + 8\pi r \sigma_{lv} \\ &= \cancel{\hat{N}_v \hat{v}_v} \frac{dP_v}{dr} + \frac{d\hat{N}_v}{dr} (\hat{g}_v - \hat{g}_l) - \cancel{\frac{dP_v}{dr} V_v} + 4\pi r^2 \left(\frac{2\sigma_{lv}}{r} + P_l - P_v \right) \end{aligned}$$

$$\text{At } r = r_e, \frac{d\Delta G}{dr} = 0$$

$$\frac{d\Delta G}{dr} = \frac{d\hat{N}_v}{dr} (\hat{g}_v - \hat{g}_l) + 4\pi r^2 \left(\frac{2\sigma_{lv}}{r} + P_l - P_v \right)$$

At $r = r_e$,
$$\frac{d^2\Delta G}{dr^2} = -\frac{8\pi\sigma_{lv}}{3} \left(2 + \frac{1}{1 + \frac{2\sigma_{lv}}{r_e P_l}} \right)$$

Homework

$$\Delta G = \Delta G_e - \frac{8\pi\sigma_{lv}}{3} \left(2 + \frac{1}{1 + \frac{2\sigma_{lv}}{r_e P_l}} \right) (r - r_e)^2 + \dots$$

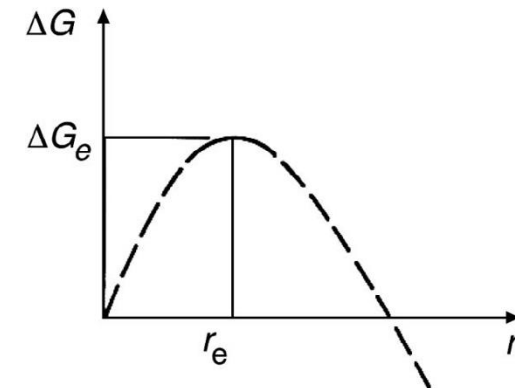


Figure 5.9 in Carey

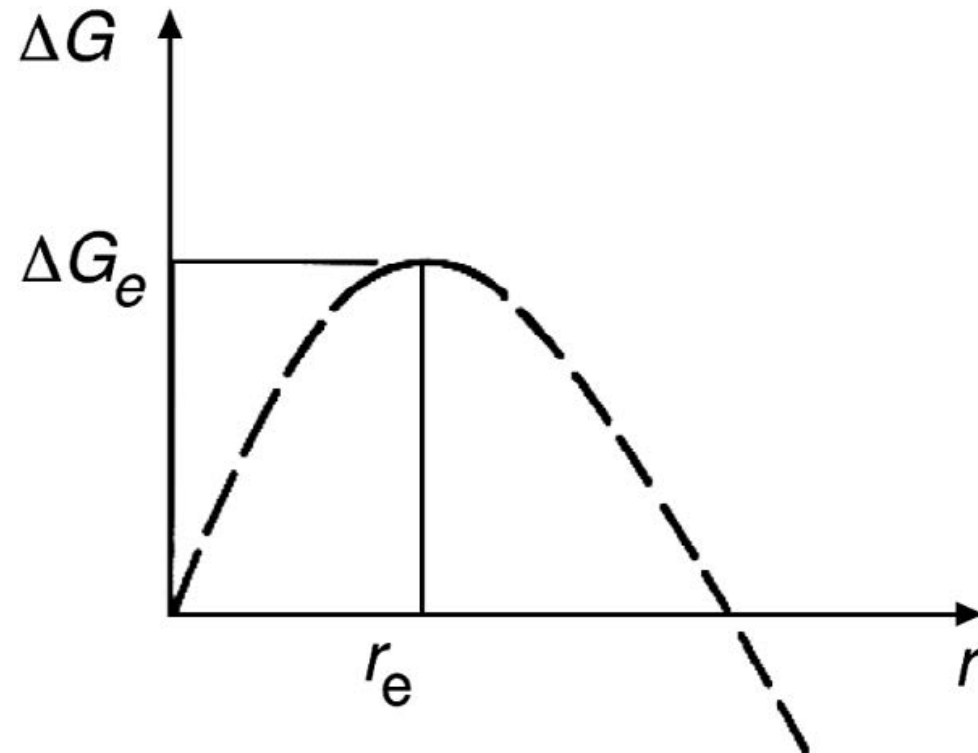


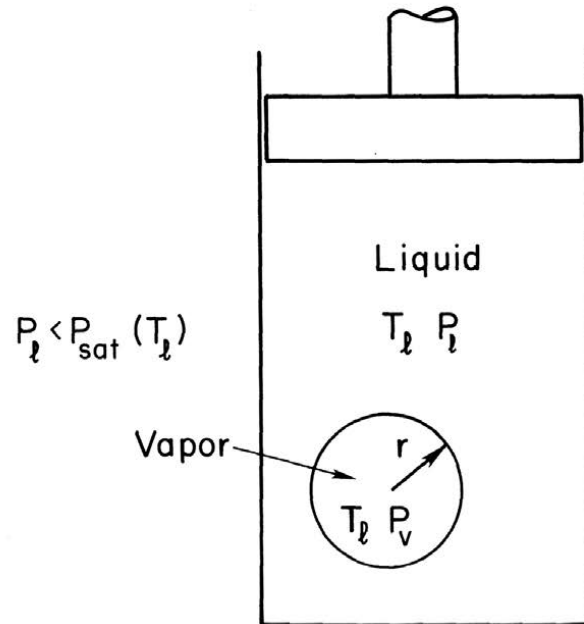
Figure 5.9 in Carey

Density fluctuation in superheated liquid produces bubbles of random r

If $r < r_e$, the bubble collapses
If $r > r_e$, the bubble grows

How do we determine r_e

After Embryo Formation



$$g_{sat,l}(T_l, P_{sat}) = g_{sat,v}(T_l, P_{sat}) = g_{sat}$$

$$dg = v dP - S dT$$

$$g_v - g_{sat} = \int_{P_{sat}}^{P_v} v_v dP = \int_{P_{sat}}^{P_v} \frac{RT_l}{P} dP = RT_l \ln\left(\frac{P_v}{P_{sat}}\right)$$

$$g_l - g_{sat} = \int_{P_{sat}}^{P_l} v_l dP = v_l (P_l - P_{sat})$$

In equilibrium

$$g_v = g_l$$

$$\Rightarrow P_{ve} = P_{sat} \exp\left[\frac{v_l (P_l - P_{sat})}{RT_l}\right]$$

$$r_e = \frac{2\sigma}{P_{ve} - P_l} = \frac{2\sigma}{P_{sat} \exp\left[\frac{v_l (P_l - P_{sat})}{RT_l}\right] - P_l}$$

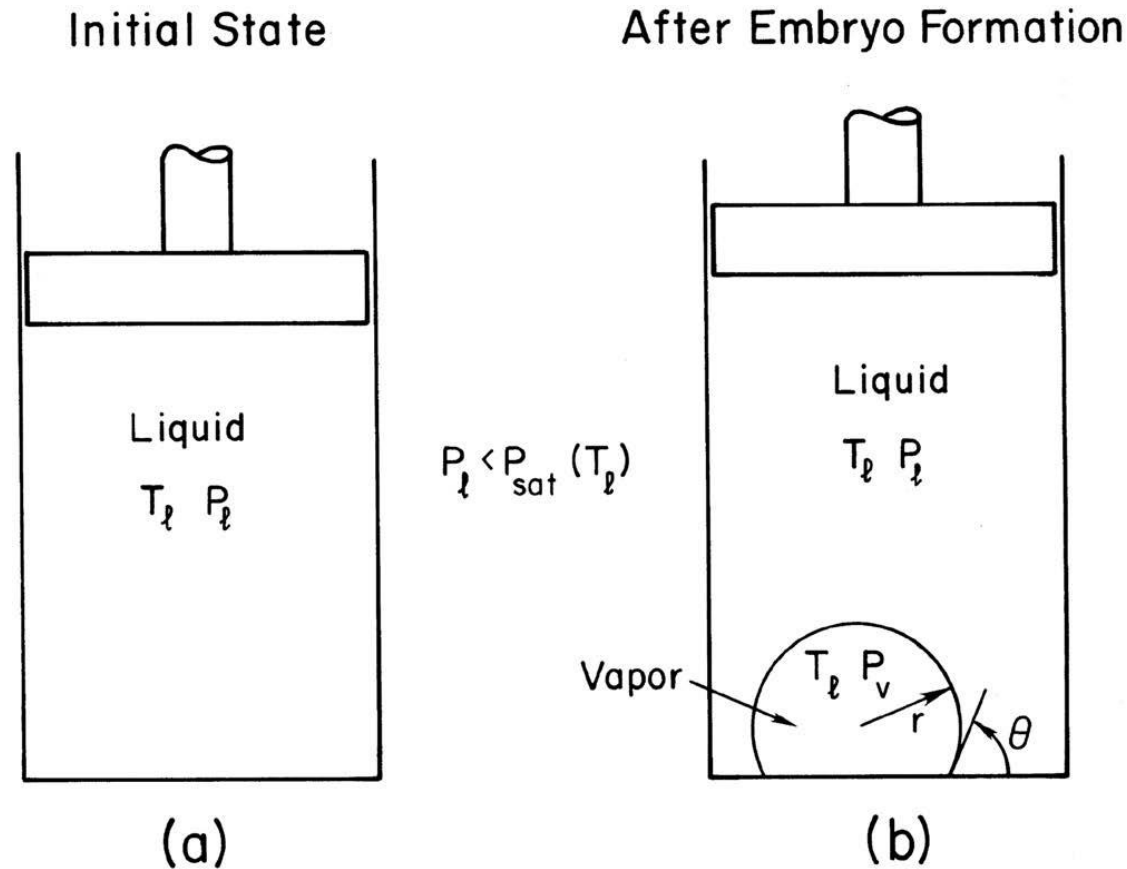


Figure 6.2 in Carey

Constant pressure constant temperature

Gibbs free energy analysis

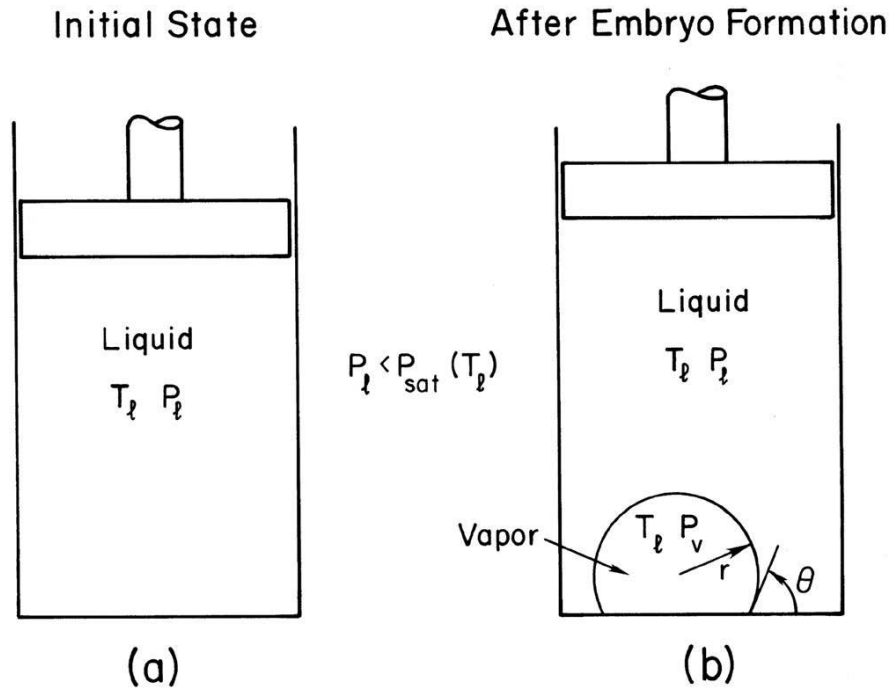
$$G = G_l + G_v + G_i$$

$$(b) - (a)$$

$$\Delta G_l = -\hat{N}_v \hat{g}_l$$

$$\Delta G_v = \hat{N}_v \hat{g}_v + (P_l - P_v)V_v$$

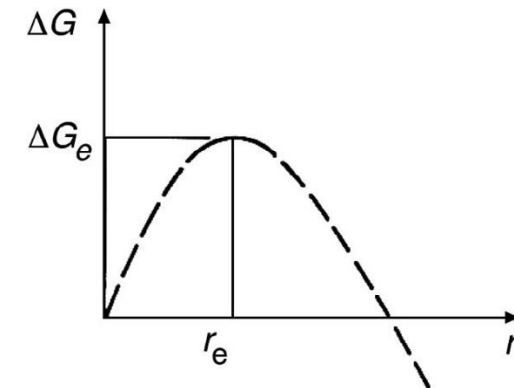
$$\begin{aligned} \Delta G_i &= \sigma_{lv}A_{lv} + \sigma_{sv}A_{sv} - \sigma_{sl}A_{sv} \\ &= \sigma_{lv}A_{lv} + \sigma_{lv} \cos \theta A_{sv} \\ &= \sigma_{lv}(A_{lv} + A_{sv} \cos \theta) \end{aligned}$$



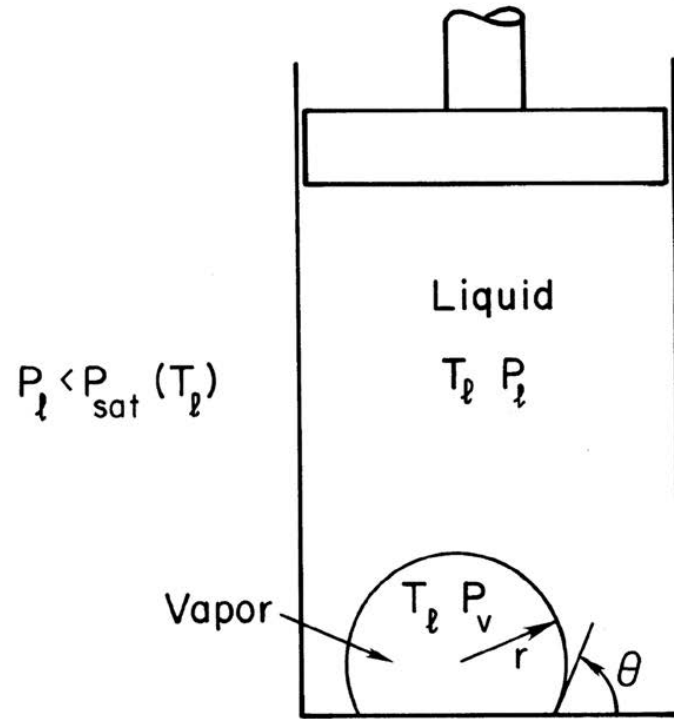
$$\Delta G = \hat{N}_v(\hat{g}_v - \hat{g}_l) + (P_l - P_v)V_v + \sigma_{lv}[2\pi r^2(1 + \cos \theta) + \pi r^2 \cos \theta(1 - \cos^2 \theta)]$$

$$\Delta G_e = \frac{4}{3}\pi r_e^2 \sigma_{lv} \left[\frac{1}{2} + \frac{3}{4} \cos \theta - \frac{1}{4} \cos^3 \theta \right] = \frac{4}{3}\pi r_e^2 \sigma_{lv} F(\theta)$$

$$\Delta G = \Delta G_e - \left(\frac{4\pi\sigma_{lv}F}{3} \right) \left(2 + \frac{P_l}{P_{ve}} \right) (r - r_e)^2 + \dots$$



After Embryo Formation



$$g_{sat,l}(T_l, P_{sat}) = g_{sat,v}(T_l, P_{sat}) = g_{sat}$$

$$dg = v dP - S dT$$

$$g_v - g_{sat} = \int_{P_{sat}}^{P_v} v_v dP = \int_{P_{sat}}^{P_v} \frac{RT_l}{P} dP = RT_l \ln \left(\frac{P_v}{P_{sat}} \right)$$

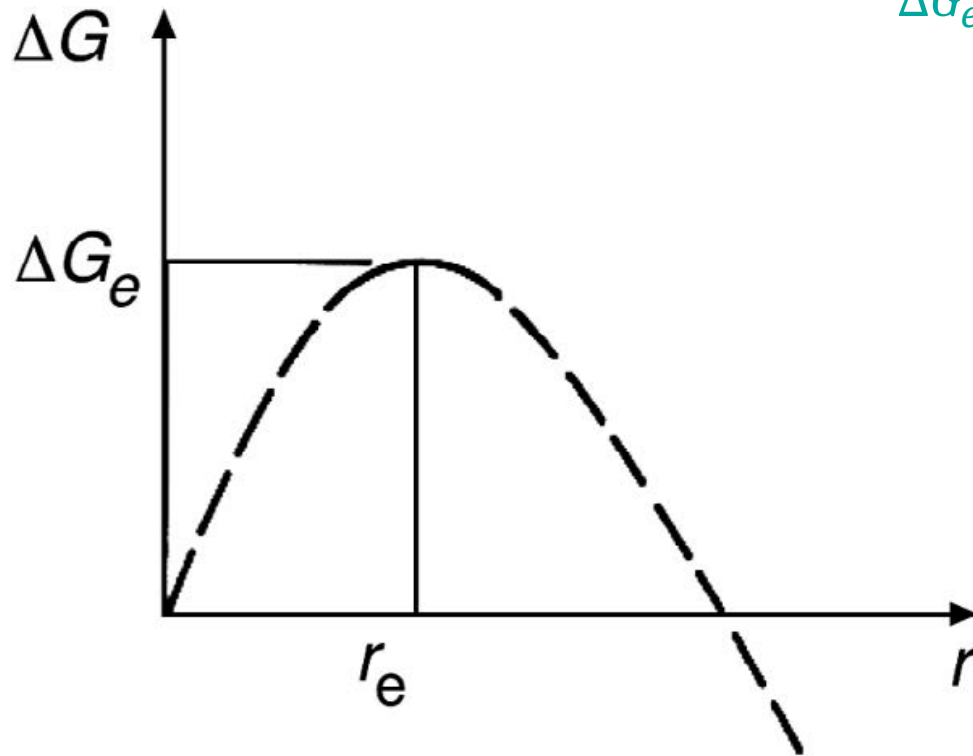
$$g_l - g_{sat} = \int_{P_{sat}}^{P_l} v_l dP = v_l (P_l - P_{sat})$$

In equilibrium

$$g_v = g_l$$

$$\Rightarrow P_{ve} = P_{sat} \exp \left[\frac{v_l (P_l - P_{sat})}{RT_l} \right]$$

$$r_e = \frac{2\sigma}{P_{ve} - P_l} = \frac{2\sigma}{P_{sat} \exp \left[\frac{v_l (P_l - P_{sat})}{RT_l} \right] - P_l}$$



$$\Delta G_e = \frac{4}{3} \pi r_e^2 \sigma_{lv} \left[\frac{1}{2} + \frac{3}{4} \cos \theta - \frac{1}{4} \cos^3 \theta \right] = \frac{4}{3} \pi r_e^2 \sigma_{lv} F(\theta)$$

When $\theta = 180^\circ$, $F(\theta) = 0$

When $\theta = 90^\circ$, $F(\theta) = \frac{1}{2}$

When $\theta = 0^\circ$, $F(\theta) = 1$

Same as homogeneous nucleation

Figure 5.9 in Carey

Let's assume the number of embryos consisting of n molecules per unit volume N_n follows

$$N_n = \rho_{N,l} \exp \left[-\frac{\Delta G(r)}{k_B T_l} \right]$$

$\rho_{N,L}$ can be understood as the number of liquid molecules per unit volume ($\Delta G = 0$ corresponds to the liquid phase)

For an embryo of size n , define j_{ne} as the evaporating molecular flux and j_{nc} as the condensing molecular flux [$\text{m}^{-2}\text{s}^{-1}$]

For equilibrium distribution of N_n $N_n A_n j_{ne} = N_{n+1} A_{n+1} j_{(n+1)c}$

A_n and A_{n+1} are the interfacial areas of n and $n+1$ molecule embryos, respectively

$$N_n A_n j_{ne} = N_{n+1} A_{n+1} j_{(n+1)c}$$

The rate at which n molecule embryos $\rightarrow$ $n+1$ molecule embryos through evaporation is the same as $n+1$ molecule embryos $\rightarrow$ n molecule embryos through condensation
No net exchange between two size groups

In superheated liquid, equilibrium is not necessarily satisfied

Consider the excess rate of n molecule embryos $\rightarrow$ $n+1$ molecule

$$J_n = N_n^* A_n j_{ne} - N_{n+1}^* A_{n+1} j_{(n+1)c}$$

$$J_n = N_n A_n j_{ne} \left(\frac{N_n^*}{N_n} - \frac{N_{n+1}^*}{N_{n+1}} \right) = -N_n A_n j_{ne} \frac{\partial \left(\frac{N^*}{N} \right)}{\partial n}$$

Treating n as a continuous variable