

Fundamentals of Analog & Mixed Signal VLSI Design

Exercise 5 (16.10.2024)

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In this exercise we want to apply the G_m/I_D design methodology using the inversion coefficient IC to the simple common source amplifier shown in Fig. 1 for various specifications. For the design we assume a generic 180 nm CMOS process with the parameters given in Table 1.

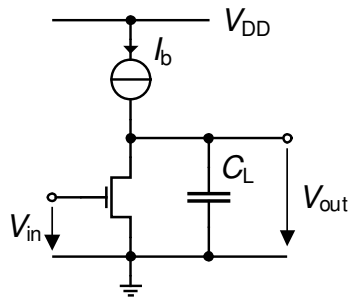


Figure 1: Common source amplifier.

Table 1: Technology parameters of an n-channel transistor for a generic 180-nm CMOS process

Parameter	Value
V_{DD}	1.8 V
C_{ox}	$8.443 \frac{fF}{\mu m^2}$
W_{min}	200 nm
L_{min}	180 nm
ΔW	54 nm
ΔL	-76 nm
V_{T0}	0.455 V
n	1.27
$I_{spec\Box}$	715 nA
L_{sat}	26 nm
λ	$20 \frac{V}{\mu m}$
K_F	$8.1 \times 10^{-24} J$
ρ	$5.794 \times 10^{-2} \frac{V \cdot m^2}{A \cdot s}$
C_J	$1 \frac{fF}{\mu m^2}$
C_{JSW}	$0.2 \frac{fF}{\mu m}$
C_{GS0}	$0.366 \frac{fF}{\mu m}$
C_{GDo}	$0.366 \frac{fF}{\mu m}$
C_{GBo}	$0 \frac{fF}{\mu m}$

Note that the effective channel width and length are defined as follows

$$W_{eff} \triangleq W + \Delta W, \quad (1)$$

$$L_{eff} \triangleq L + \Delta L, \quad (2)$$

where W and L are drawn width and length.

Problem 1 Imposing the gain bandwidth product (unity gain frequency)

Design the CS amplifier shown in Fig. 1, for the following specifications at room temperature ($U_T = 25.9 \text{ mV}$):

$$f_u = 100 \text{ MHz}, \quad C_L = 1 \text{ pF}, \quad IC = 1, \quad L_{long} = 1 \text{ } \mu\text{m}, \quad L_{short} = 180 \text{ nm}.$$

Carry out the design procedure both for long- and short-channel devices in saturation, using the drawn lengths L_{long} and L_{short} respectively. Note that velocity saturation (VS) has to be accounted for in the short-channel case. We assume that the self-loading capacitance at the drain can be neglected (i.e. assume a constant load capacitance equal to C_L).

- Draw the equivalent small-signal schematic ignoring the transistor parasitic capacitances.
- Derive the transfer function $A_v(s) \triangleq \Delta V_{out} / \Delta V_{in}$ and extract the expressions of the dc gain, cut-off frequency and gain-bandwidth product (unity gain frequency) f_u .
- Find the transistor transconductance value G_m .
- Find the normalized source transconductance $g_{ms}(IC) \triangleq G_{ms} / G_{spec} = n G_m / G_{spec} = n U_T G_m / I_{spec}$ from the imposed inversion coefficient IC . Then, deduce the specific current I_{spec} and the bias current I_b . Calculate the power consumption.
- Find the W_{eff} / L_{eff} ratio and the effective width W_{eff} for both the long and short channel case using the given drawn length L . Derive the drawn width W .
- Deduce the output conductance value G_{ds} and then calculate the dc gain value assuming the bias current source is ideal.
- Simulate the circuit using the Smash simulator and compare the theoretical results with the simulations.

Problem 2 Imposing the power consumption

Design the same CS amplifier shown in Fig. 1 for the following specifications at room temperature ($U_T = 25.83 \text{ mV}$):

$$P_{max} = 100 \text{ } \mu\text{W}, \quad C_L = 1 \text{ pF}, \quad IC = 1, \quad L_{long} = 1 \text{ } \mu\text{m}, \quad L_{short} = 180 \text{ nm}.$$

Carry out the design procedure both for long- and short-channel devices in saturation, using the drawn lengths L_{long} and L_{short} respectively. Note that velocity saturation (VS) has to be accounted for in the short-channel case. We assume that the self-loading capacitance at the drain can be neglected (i.e. assume a constant load capacitance C_L).

- Find the bias current I_b for the specified maximum power consumption.
- Find the transconductance value of the transistor for the given inversion coefficient IC by means of the current efficiency.
- Find the unity gain-bandwidth product using the specific current I_{spec} . Calculate the power consumption.
- Find the W_{eff} / L_{eff} ratio and the effective width W_{eff} for both the long and short channel case using the given drawn length L . Derive the drawn width W .
- Deduce the output conductance value G_{ds} and then calculate the dc gain value assuming the bias current source is ideal.
- Simulate the circuit using the Smash simulator and compare the theoretical results with the simulations.

Problem 3 Imposing the gain bandwidth product and the current budget

Design the same CS amplifier shown in Fig. 1 imposing both the gain-bandwidth product and the current budget with the following specifications at room temperature ($U_T = 25.83 \text{ mV}$):

$$f_u = 9 \text{ MHz}, \quad I_b = 400 \text{ nA}, \quad C_L = 1 \text{ pF}, \quad L_{\text{long}} = 1 \text{ } \mu\text{m}.$$

Carry out the design procedure only for the long-channel case with $L = L_{\text{long}}$.

- Find the transistor transconductance value.
- Find the inversion coefficient IC by means of the current efficiency and then the I_{spec} .
- Find the $W_{\text{eff}}/L_{\text{eff}}$ ratio and the effective width W_{eff} for the long channel case only using the given drawn length L . Derive the drawn width W .
- Deduce the output conductance value G_{ds} and then calculate the dc gain value assuming the bias current source is ideal.
- Simulate the circuit using the Smash simulator and compare the theoretical results with the simulations.

Problem 4 Imposing the input-referred noise

In this problem we want to design the CS amplifier shown in Fig. 1 imposing the input-referred noise including both the thermal and flicker noise. The specifications at room temperature ($U_T = 25.83 \text{ mV}$) are given below:

$$f_k = 100 \text{ kHz}, \quad \sqrt{S_{\text{nth}}} = 30 \text{ nV}/\sqrt{\text{Hz}}, \quad C_L = 1 \text{ pF}, \quad IC = 1, \quad \gamma_n = 0.72$$

where f_k is the noise corner frequency and S_{nth} is the input-referred thermal noise power spectral density (PSD).

- Using S_{nth} determine the transconductance G_m .
- Find the normalized transconductance $g_{ms}(IC)$.
- Determine the specific current I_{spec} , the bias current I_b and the $W_{\text{eff}}/L_{\text{eff}}$ ratio.
- Using the noise corner frequency f_k , determine the effective gate area $W_{\text{eff}} \cdot L_{\text{eff}}$.
- Finally, calculate the effective and drawn dimensions of the transistor.
- Simulate the circuit using the Smash simulator and compare the theoretical results with the simulations.

Problem 5 Minimum current for a given gain-bandwidth product accounting for self-loading

In this problem we want to account for the self-loading effect which is particularly important when the transistor is getting wide which typically happens in weak inversion. The specifications at room temperature ($U_T = 25.83 \text{ mV}$) are given below:

$$f_u = 25 \text{ MHz}, \quad C_{L0} = 20 \text{ fF}, \quad C_W = 1.167 \frac{\text{fF}}{\mu\text{m}}, \quad L = 1 \text{ } \mu\text{m}.$$

Follow the procedure illustrated in the lecture notes.

Problem 6 Minimum current for a given gain-bandwidth product accounting for self-loading

In this problem we want to account for the self-loading effect but use the additional degree of freedom, namely the transistor gate length, to set the dc gain. The specifications at room temperature ($U_T = 25.83 \text{ mV}$) are given below:

$$f_u = 25 \text{ MHz}, \quad A_{dc} = 40 \text{ dB}, \quad C_{L0} = 20 \text{ fF}, \quad C_W = 1.167 \frac{\text{fF}}{\mu\text{m}}.$$

Follow the procedure illustrated in the lecture notes.