

Introduction to Chemical Engineering

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Fridays, 14h15 - 17h00

2024-2025

Course Schedule

Date	Subject
13-Sep	1. Fundamentals of Material Balances 1.1. Process definition and classification 1.2. Material balance calculations
20-Sep	1.3. Balances on multiple-unit processes
27-Sep	Review on Mass Balances (non-reactive)
04-Oct	1.4. Chemical reaction stoichiometry 1.5.1 Balances on reactive processes (part 1)
11-Oct	1.5.2 Balances on reactive processes (part 2) 1.6. Balances on multiple unit reactive processes Review on Mass Balances (non-reactive & reactive)
18-Oct	2. Energy and Energy Balances 2.1. Energy balances on closed systems 2.2. Open systems at steady state
01-Nov	3. Balances on Non-Reactive Processes 3.1. Energy balance calculation 3.2. Changes in Pressure, Temperature, Phases 3.3. Mixing and Solution
08-Nov	4. Balances on Non-Reactive Processes Problems: Mass and Energy Balances on non-Reactive Systems
15-Nov	Midterm Exam: Mass & Energy Balances non-Reactive Systems
22-Nov	Review Midterm
29-Nov	5. Balances on Reactive Processes 5.1. Heats of reaction/combustion 5.2. Combustion reactions 5.3. Enthalpy of reaction 5.4. Energy balance calculation
06-Dec	6. Energy balances on mixing processes Review
13-Dec	Review and Study Session

Recommended textbook:
 Elementary Principles of Chemical Processes
 Richard M. Felder & Ronald W. Rousseau

Session V: Friday 18 October 2024

After studying this session you will be able to:

1. Understand the concepts of work and heat (signs!), intrinsic and extensive properties
2. Identify non-reactive **closed** systems & Define an energy balance on them
3. Identify non-reactive **open** systems & Define an energy balance on them

1. Introduction

Introduction to energy balances

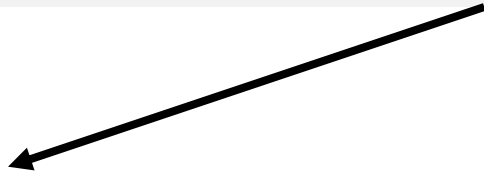
By performing energy balances, we answer questions like:

- How much energy is required for pumping 1000 m³/h?
- What is the rate of energy supply in a distillation column?
- A→B exothermic and 75% conversion @400k, what is the rate of energy removal to achieve the target?
- ...
- Is there a cheaper way of achieving my process specifications? → Energy is expensive!!!

In the design of a process, we must account for:

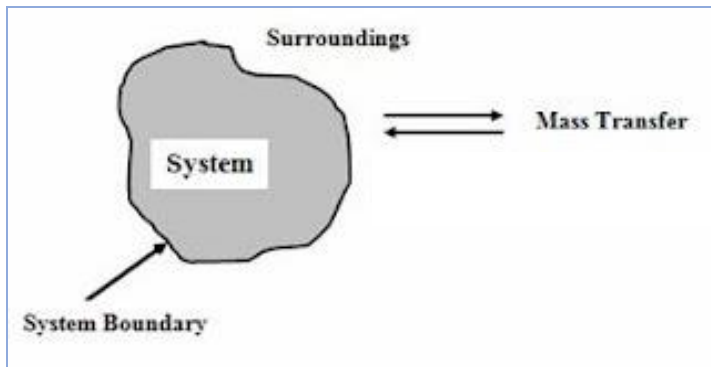
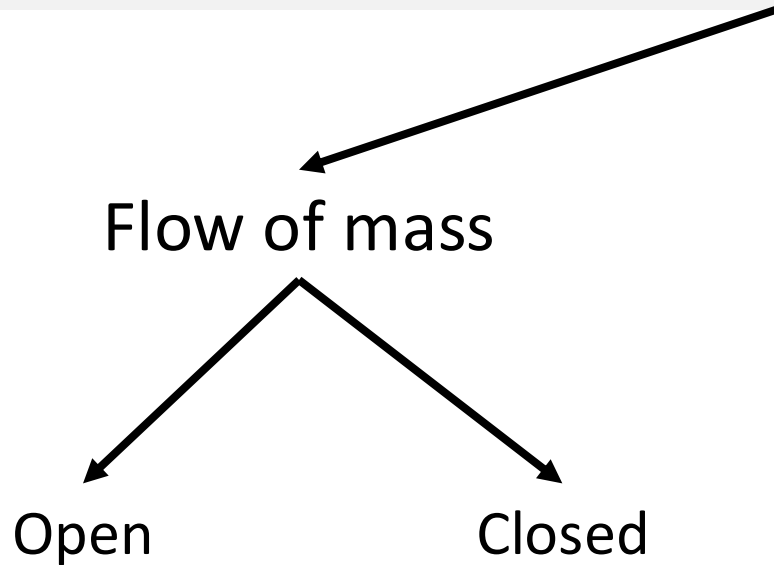
- ✓ the flow of energy into and out of each process unit
- ✓ the overall energy requirement of the process

Recalling the definition of a system

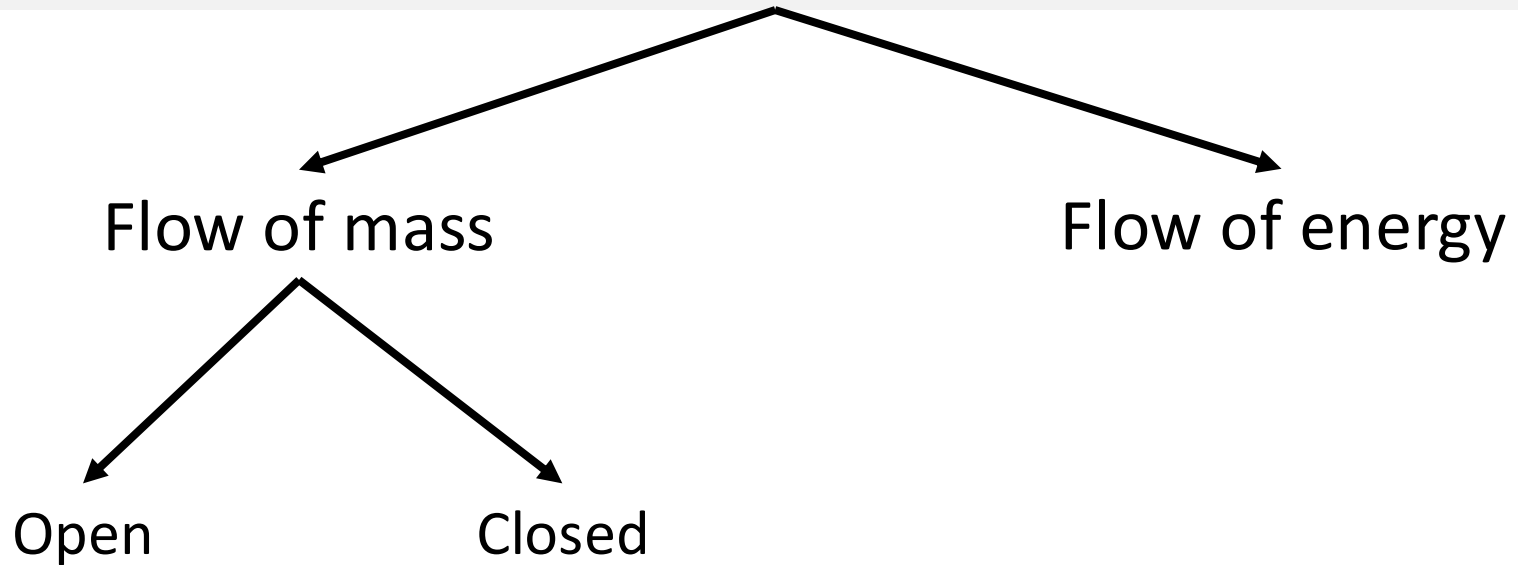


Flow of mass

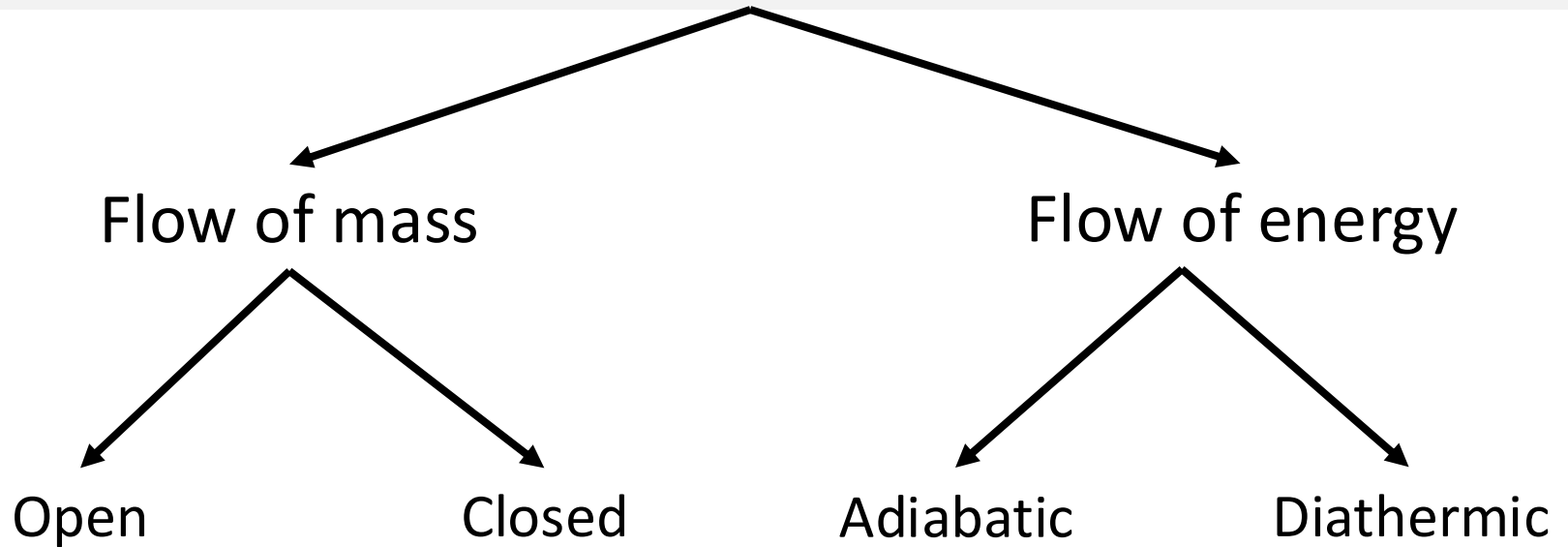
Recalling the definition of a system



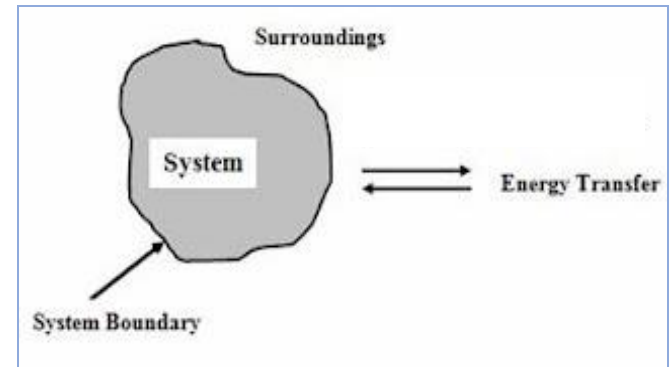
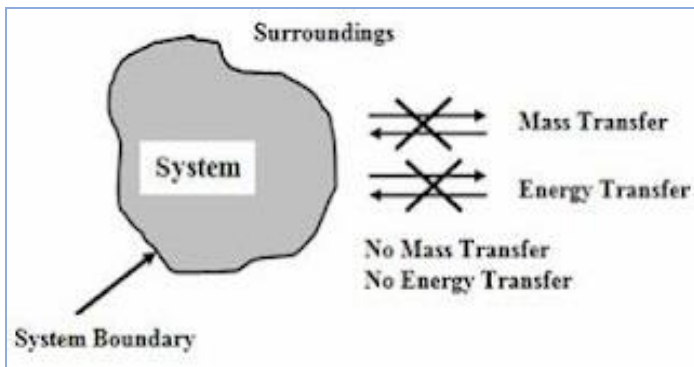
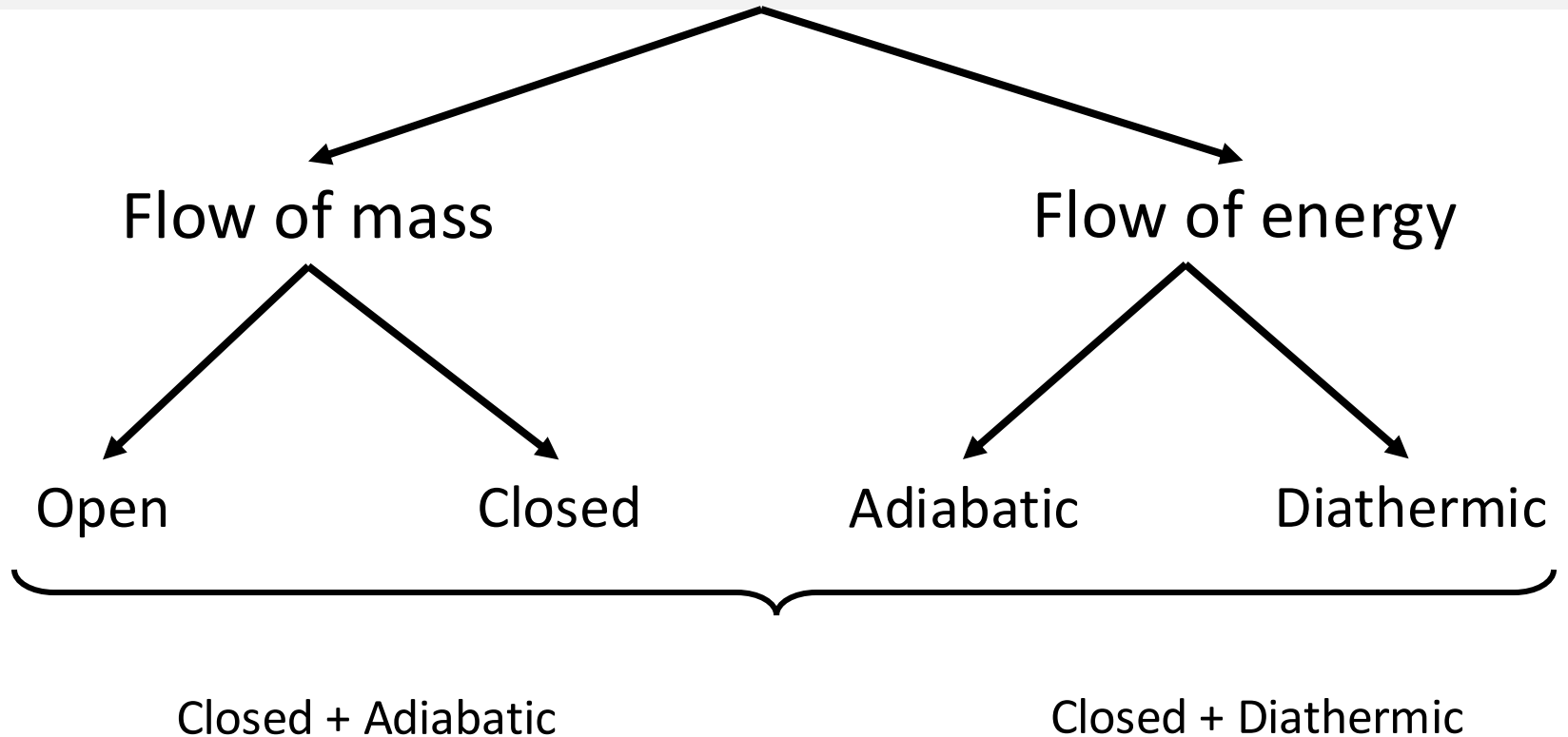
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Recalling the definition of a system



Recalling the definition of a system



Forms and Transfer of energy of a system

The total energy of a system has 3 forms

① Kinetic energy

Energy associated with movement

② Potential energy

Energy in a potential field
Gravitational, electromagnetic, ...

③ Internal energy

“Everything else”
Molecular energy ...

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The energy is transferred from the environment to a process system
(and vice-versa) in 2 ways

A Heat (Q): flow or exchange of energy due to ΔT

- Could enter the system via conduction, convection, or radiation

B Work (W): flow or exchange of energy due to “driving forces” other than temperature (e.g.: voltage, force)

- Could be done on, or by, the system

Clarifications

- Q , W are transferred energies: a system does not possess heat or work
- Signs of Q and W according to this course conventions:

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Heat is positive because the system in effect gains energy when heat enters
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- Signs of Q and W according to this course conventions:
 - $Q > 0$: heat entering the system
Heat is positive because the system in effect gains energy when heat enters
 - $Q < 0$: heat leaving the system
 - $W > 0$: work done BY the system
 - $W < 0$: work done ON the systemThe choice for the sign of work is arbitrary but facilitates the reading of the expression of energy transferred to the system (see next slides):

$$E_{\text{transferred}} = Q - W$$

Types of work

- W_m : mechanical work which is due to movement of the boundary, (e.g., piston)
- W_{el} : electrical work (e.g., electrical generator)
- W_s : shaft work (e.g., mixing, turbine, pump)
- W_{fl} : flow work
 - Work done to push a fluid into system (use example of pistons moving fast)
 - Work done to push fluid out of system

Example 1: Determine the sign of the work transferred to the system in the following cases:

- a piston compress the system
- a generator gives energy to the system
- a pump applies work into a stream (system)
- a turbine acts on a stream (system)
- a fluid (system) flows into a piston

Classification of properties

- Intensive property: is a physical property of a system that does not depend on the system size or the amount of material in the system.

E.g.: density, P, T

- Extensive property: is a property that is directly proportional to the amount of material in the system.

E.g.: mass and volume, internal energy (U)

- Specific property: is a property that depends on, or is calculated based on, another measurable property, and are denoted with a “^”.

E.g.: density is considered 'specific' because it can be calculated from volume and mass

How to calculate an extensive property for the whole system?

- for internal energy of the system: $U(\text{J}) = m(\text{kg}) \hat{U}(\text{J/kg})$
- for the continuous flow: $\dot{U}(\text{J/s}) = \dot{m}(\text{Kg/s}) \hat{U}(\text{J/kg})$

Defining the energy balance on a system

Recall the mother of all equations for conservation of mass:

$$\text{Acc} = \text{In} - \text{Out} + \text{Gen} - \text{Cons}$$

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Law of conservation of energy:

This states that: if E is the entire amount of energy in the system, then:

$$E_{\text{accumulated}} = E_{\text{input}} - E_{\text{output}} + E_{\text{gen}} + E_{\text{transferred}}$$

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$$E_{\text{accumulated}} = E_{\text{input}} - E_{\text{output}} + E_{\text{gen}} + E_{\text{transferred}}$$

$$E_{\text{in}} = \sum_{\text{input streams}} m_j \hat{E}_j \quad , \quad E_{\text{out}} = \sum_{\text{output streams}} m_j \hat{E}_j$$

$$E_{\text{transferred}} = Q - W$$

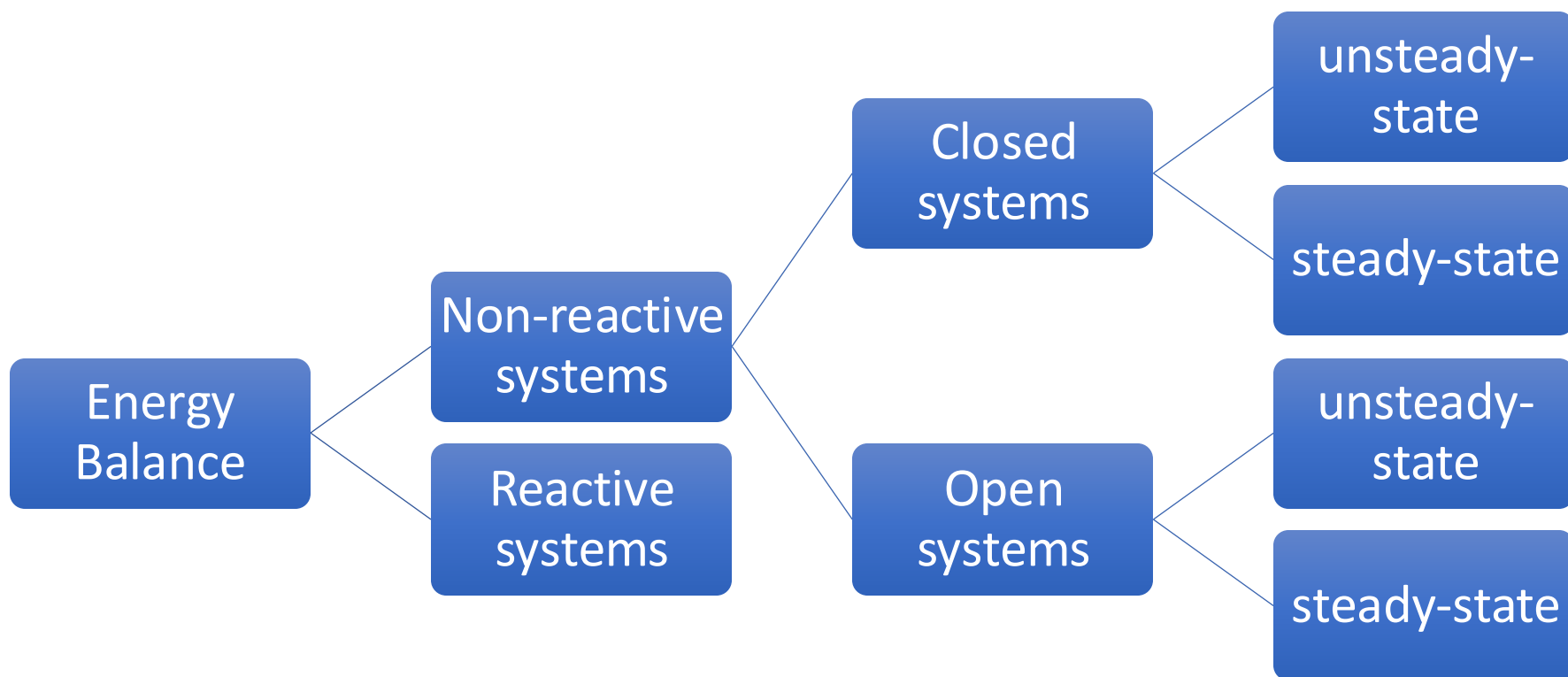
Q : heat transferred to the system from its surrounding (+ sign: gain of energy)

W : work done by system on its surrounding (+ sign so that $-W$ is negative)

Energy balances overview

Depending on the system under study, the energy balance equation will simplify:

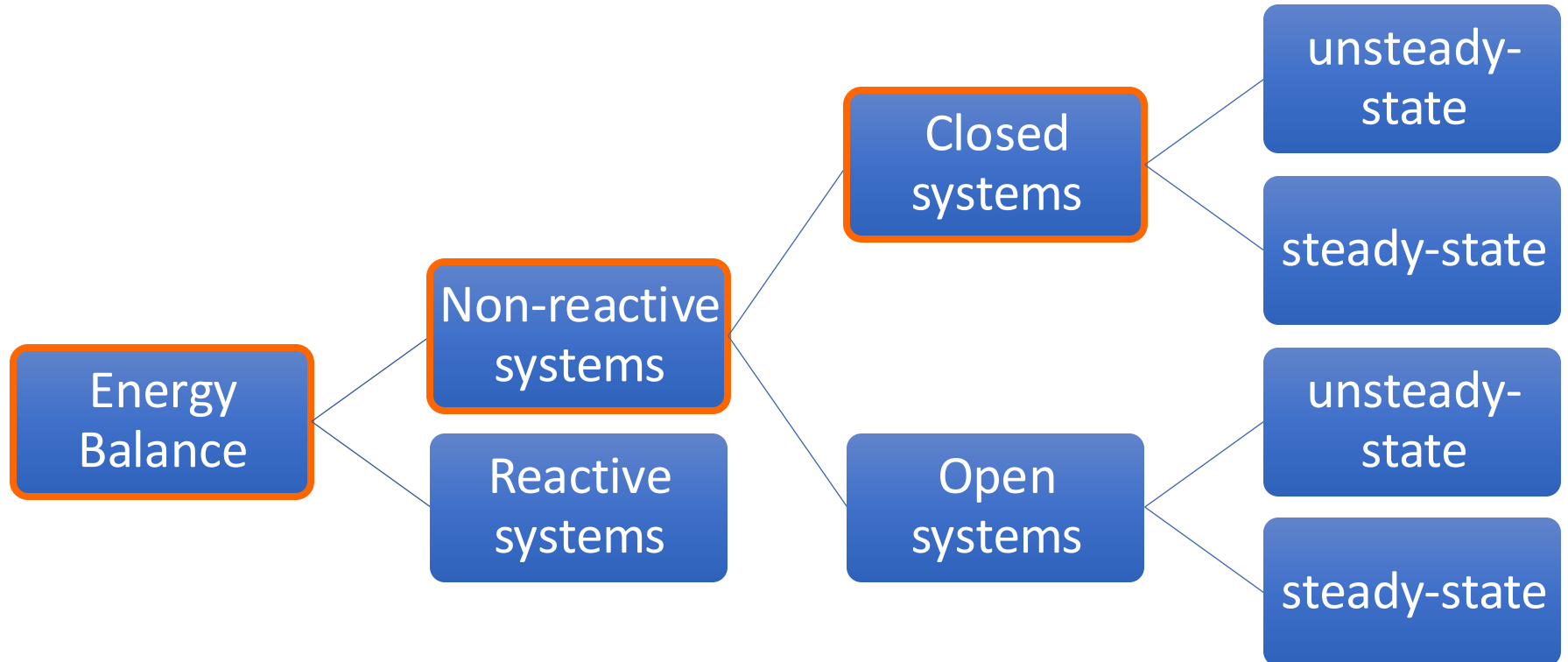
$$E_{\text{accumulated}} = E_{\text{input}} - E_{\text{output}} + E_{\text{gen}} + E_{\text{transferred}}$$



2. Energy balances on closed non-reactive systems

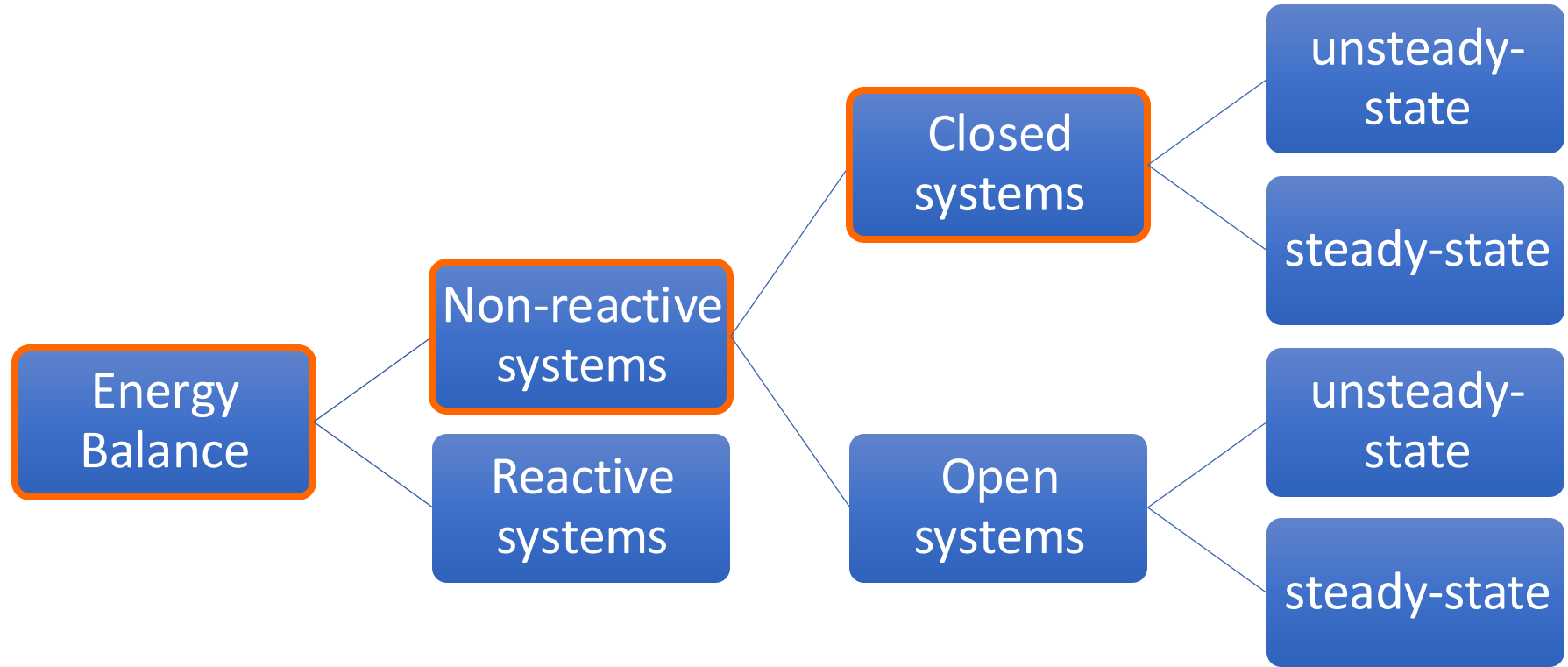
Energy balances on closed non-reactive systems

The simplest case consists in closed systems:



Energy balances on closed non-reactive systems

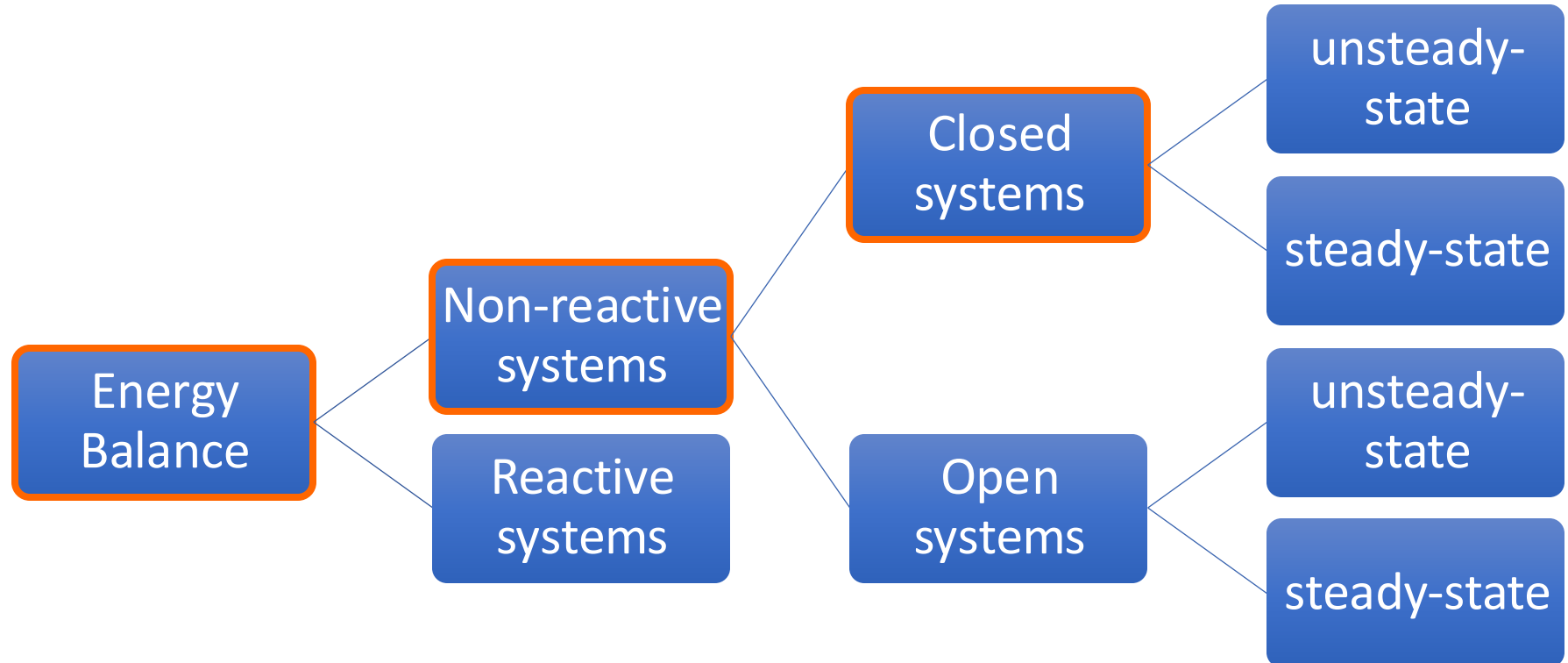
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$$E_{\text{accumulated}} = E_{\text{input}} - E_{\text{output}} + E_{\text{gen}} + E_{\text{transferred}}$$

Energy balances on closed non-reactive systems

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$$E_{\text{accumulated}} = \cancel{E_{\text{input}}} - \cancel{E_{\text{output}}} + \cancel{E_{\text{gen}}} + E_{\text{transferred}}$$

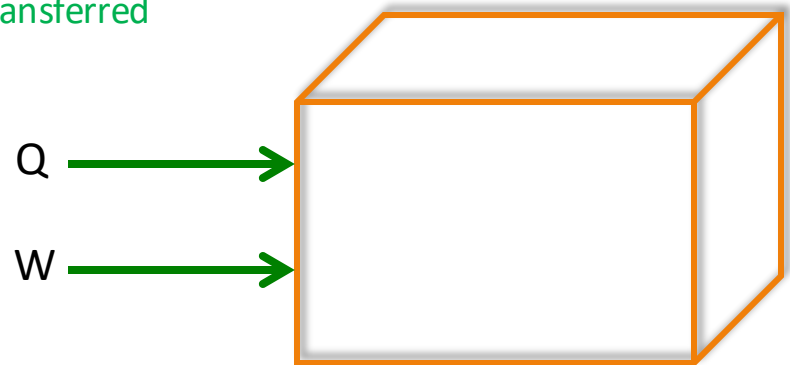
$$E_{\text{accumulated}} = E_{\text{transferred}}$$

Energy Balance on a Closed System

$$E_{\text{accumulated}} = \cancel{E_{\text{input}}} - \cancel{E_{\text{output}}} + \cancel{E_{\text{gen}}} + E_{\text{transferred}}$$

$$E_{\text{accumulated}} = E_{\text{transferred}} = \Delta E$$

$$\Delta E = Q - W$$

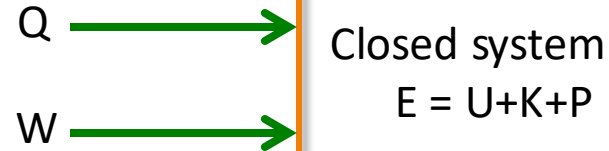


Energy Balance on a Closed System

$$E_{\text{accumulated}} = \cancel{E_{\text{input}}} - \cancel{E_{\text{output}}} + \cancel{E_{\text{gen}}} + E_{\text{transferred}}$$

$$E_{\text{accumulated}} = E_{\text{transferred}} = \Delta E$$

$$\Delta E = Q - W$$



The total energy (E) may be regarded as composed of many forms. Obvious contributions to the total energy arise from the internal, kinetic and potential energies

$$Q - W = \Delta U + \Delta E_k + \Delta E_p$$

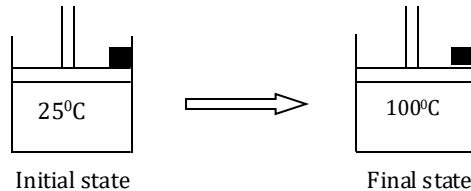
- ΔE_p is change in potential energy
- Q is heat transferred to the system
 - If the system is adiabatic, there is neither gain by the system nor heat loss and Q is zero
- W is work done by the system
 - If there are no moving parts, then W=0

Example: Energy Balance on a Closed System

1 mole of gas contained in a cylinder fitted with movable position:

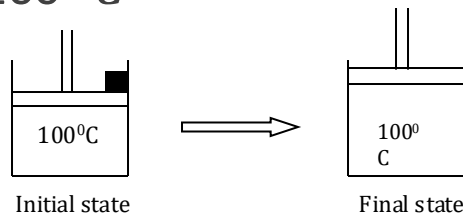
The cylinder is placed in boiling water and

I) Equilibrated: to 100 °C



II) The piston is then released, and the gas does 100 J of work to move the piston to its new equilibrium position.

The final gas temperature is 100 °C



Write and solve energy balances. For two stage with assuming:

- No changes in m , E_k & E_p
- Ideal gas
- $\hat{C}_v = 2 \text{ kcal.mol}^{-1}\text{.K}^{-1}$

Example: Energy Balance on a Closed System (Continued)

I) $E_{\text{accumulated}} = E_{\text{input}} - E_{\text{output}} + E_{\text{gen}} + E_{\text{transferred}}$

$$E_{\text{accumulated}} = E_{\text{transferred}}$$

$$\Delta U + \Delta E_k + \Delta E_p = Q - W$$

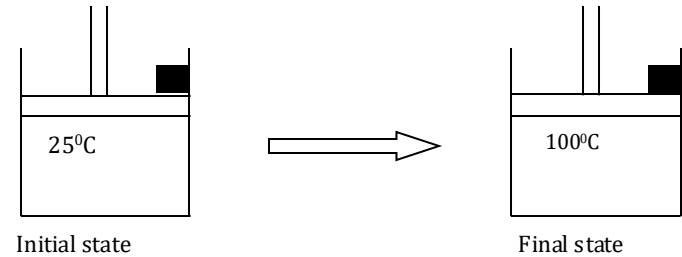
$$m \Delta \hat{U} + m \Delta \hat{E}_k + m \Delta \hat{E}_p = Q - W$$

$$m (\hat{U}_f - \hat{U}_i) + m (\hat{E}_{k, \text{final}} - \hat{E}_{k, \text{initial}}) + m (\hat{E}_{p, \text{final}} - \hat{E}_{p, \text{initial}}) = Q - W$$

$$m (\hat{U}_f - \hat{U}_i) = m \Delta \hat{U} = Q$$

$$\Delta \hat{U} = \hat{C}_v (\Delta T) = 2.75 \text{ k} = 150 \text{ kcal} = 627.6 \text{ kJ}$$

$$\hat{C}_v \text{ for 1 mol of gas} = 2 \text{ kcal} \cdot \text{mol}^{-1} \cdot \text{k}^{-1} \cdot 1 \text{ mol} = 2 \text{ kcal} \cdot \text{k}^{-1}$$



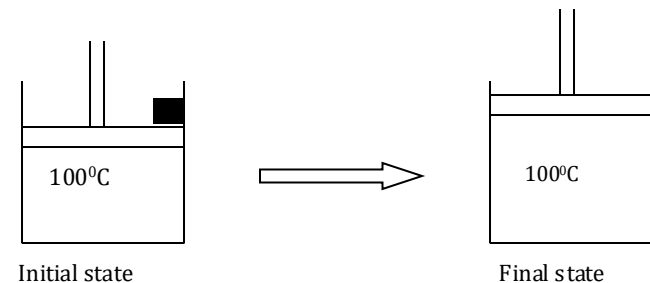
- No changes in m , E_k & E_p
- Ideal gas
- $\hat{C}_v = 2 \text{ kcal} \cdot \text{mol}^{-1} \cdot \text{k}^{-1}$

II) $U_{\text{final}} = U_{\text{initial}}$, because $\Delta T = 0$

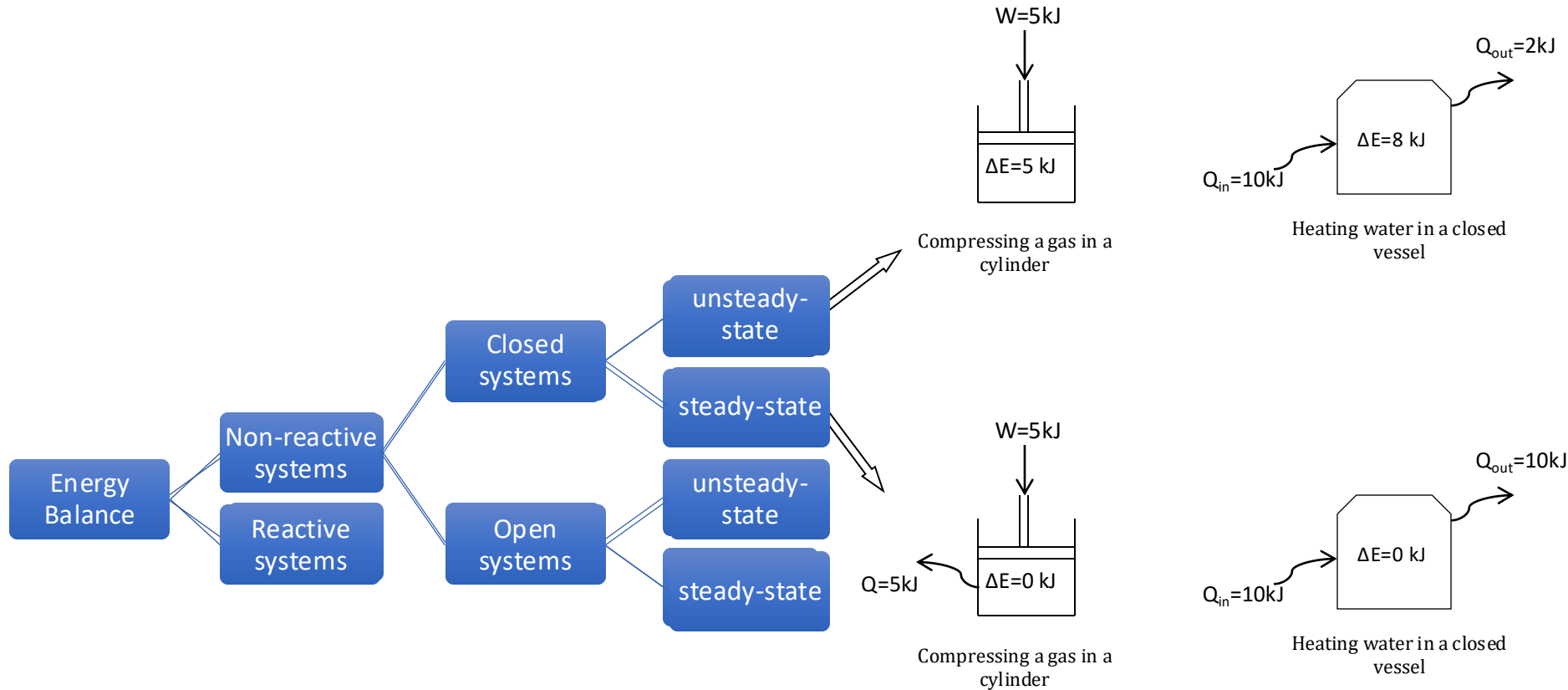
$$\Delta U + \Delta E_k + \Delta E_p = Q - W \quad \text{boundaries move so } W \neq 0!$$

$$\Rightarrow 0 = Q - W \Rightarrow Q = W = 100 \text{ J} > 0$$

What does $Q > 0$ mean? The system further absorbs energy in form of heat to do work

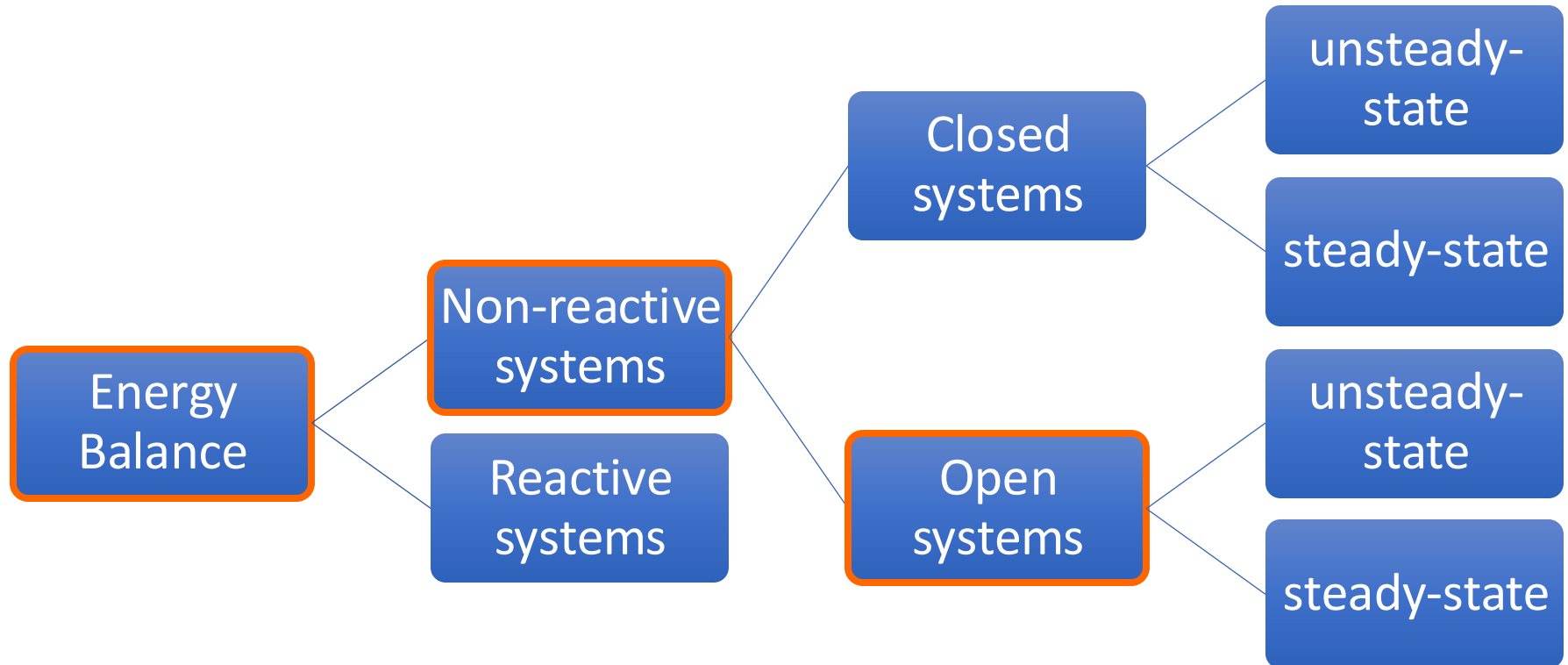


Examples of closed systems



3. Energy balances on open non-reactive systems

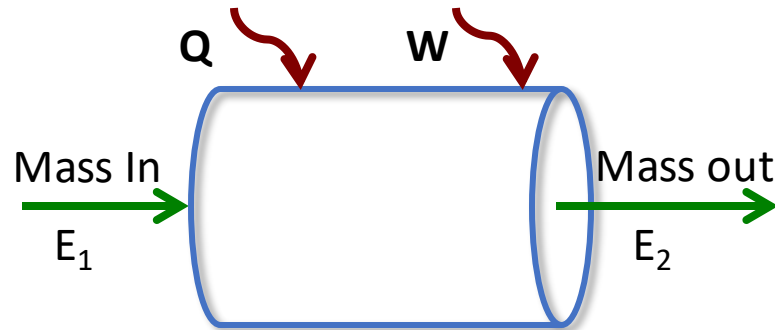
Energy balances on open non-reactive systems



$$E_{\text{accumulated}} = E_{\text{input}} - E_{\text{output}} + E_{\text{gen}} + E_{\text{transferred}}$$

Energy Balance on an Open System

A system is open if mass crosses the system boundary



law of conservation of energy:

$$E_{\text{accumulated}} = E_{\text{input}} - E_{\text{output}} + E_{\text{gen}} + E_{\text{transferred}}$$

$$E_{\text{in}} = \sum_{\text{input streams}} m_j \hat{E}_j \quad , \quad E_{\text{out}} = \sum_{\text{output streams}} m_j \hat{E}_j$$

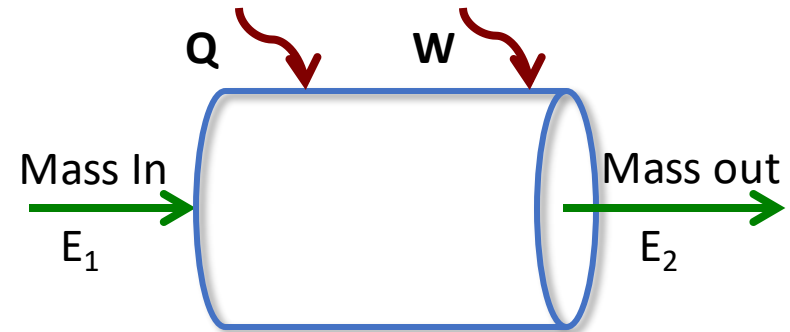
$$E_{\text{transfer}} = Q - W$$

$$\bar{m}_{\text{sys}} \hat{E}_{\text{acc}} = \bar{m}_{\text{in}} \hat{E}_1 - \bar{m}_{\text{out}} \hat{E}_2 + Q - W$$

(hat indicates energy per unit mass)

Energy Balance on an Open System

$$\bar{m}_{sys} \hat{E}_{acc} = \bar{m}_{in} \hat{E}_1 - \bar{m}_{out} \hat{E}_2 + Q - W$$



- For such a system, work must be done on the fluid mass to push it into the system; flow work
- Work could also be done by the fluid mass on moving parts of the system (example: steam driving a turbine); shaft work

$$W = W_s + W_{fl}$$

Accumulation=0



$$\bar{m}_1(\hat{U}_1 + \cancel{\hat{E}k_1} + \cancel{\hat{E}p_1}) - \bar{m}_2(\hat{U}_2 + \cancel{\hat{E}k_2} + \cancel{\hat{E}p_2}) + \dot{Q} - (\cancel{W_s} + W_{fl})$$

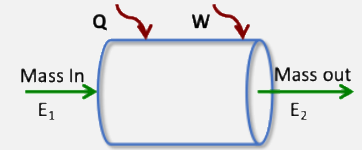
$m_1 = m_2 = m$



if $W_s, E_k, E_p = 0$

$$\dot{m} D\hat{U} + Q - W_{fl} = 0$$

What is W_{fl} ?



Work required to push the mass in = $P_{in} V_{in}$ ($N/m^2 * m^3 = N.m = J$)

Work done by the fluid exiting the system = $P_{out} V_{out}$

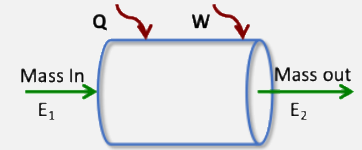
The net rate of work done by the system = $W_{fl} = P_{out} V_{out} - P_{in} V_{in}$

$$\boxed{\dot{m} D\hat{U}} + \boxed{\dot{Q}} - \boxed{W_{fl}} = \boxed{\dot{m}_1 \hat{U}_1 - \dot{m}_2 \hat{U}_2} + \boxed{\dot{Q}} - \boxed{P_{out} V_{out} + P_{in} V_{in}} = 0$$

$P_{out} V_{out} \rightarrow$ Work done by system to push **out**

$P_{in} V_{in} \rightarrow$ Work done on system by pushing **in**

Definition of Enthalpy



$$\dot{m} D\hat{U} + \dot{Q} - W_{fl} = \dot{m}_1 \hat{U}_1 - \dot{m}_2 \hat{U}_2 + \dot{Q} - P_{out} V_{out} + P_{in} V_{in} = 0$$

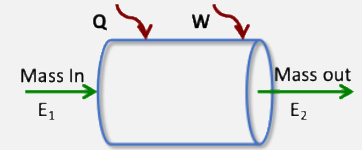
$$\dot{m}_1 \hat{U}_1 - \dot{m}_2 \hat{U}_2 + \dot{Q} - \dot{m}_2 P_2 \hat{V}_2 + \dot{m}_1 P_1 \hat{V}_1 = 0$$

$$\Rightarrow \dot{m}_1 (\hat{U}_1 + P_1 \hat{V}_1) - \dot{m}_2 (\hat{U}_2 + P_2 \hat{V}_2) + \dot{Q} = 0$$

$$\hat{U} + P \hat{V} = ?$$

$$\dot{m}_1 \hat{H}_1 - \dot{m}_2 \hat{H}_2 + \dot{Q} = 0$$

Definition of Enthalpy



$$\hat{U} + P\hat{V} = ? \Rightarrow \hat{U} + P\hat{V} = \hat{H}$$

$$\bar{m}_1 \hat{H}_1 - \bar{m}_2 \hat{H}_2 + \bar{Q} = 0$$

- So, using the enthalpy of streams takes into account the W_{fl} for streams in open systems
- $\hat{U}$ is specific internal energy, P is pressure, and $\hat{V}$ is specific volume
- It is not possible to know or estimate the absolute values of **internal energy and enthalpy**. We need to find only the change in these properties to make an energy balance
- The general energy equation for an open system with flow work, shaft work, kinetic energy changes, potential energy changes and heat transfer becomes:

$$D\bar{H} + D\bar{E}_k + D\bar{E}_p = \bar{Q} - \bar{W}_s$$

Remarks

Closed system : $\Delta U + \Delta E_k + \Delta E_p = Q - W$

Open system: $D\bar{H} = \sum_{out} \dot{n}_i \hat{H}_i - \sum_{in} \dot{n}_i \hat{H}_i$ or $D\bar{H} = \sum_{out} \dot{m}_i \hat{H}_i - \sum_{in} \dot{m}_i \hat{H}_i$

Open system : $D\bar{H} + D\bar{E}_k + D\bar{E}_p = \bar{Q} - \bar{W}_s$

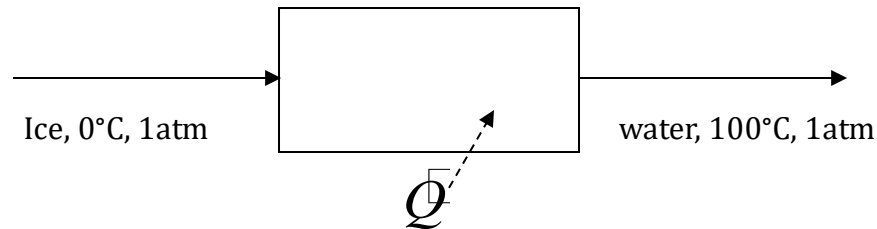
ΔU only depends on the temperature: $\Delta \hat{U} = \int_{T_1}^{T_2} (C_v)_T dT$

so for constant T: $\Delta U = 0 \rightarrow \Delta H = \Delta U + \Delta(PV) = V\Delta P$

For the ideal gas, liquids and solids:

- For the solids and liquids : $C_p = C_v$
- For the gases : $C_p = C_v + R$ (from thermodynamics course!)

Example: Energy balance on an open system



The process is st.st and it reach to a final stable situation

$\dot{Q} = ?$ Kcal / min kg H₂O

$$D\bar{H} + D\bar{E}_k + D\bar{E}_p = \dot{Q} - \dot{W}_s$$

$$\dot{m}_{\text{out}} \hat{H}_{\text{out}} - \dot{m}_{\text{in}} \hat{H}_{\text{in}} = \dot{Q}$$

$$\rightarrow \dot{Q}/\dot{m} = \hat{H}_{\text{out}} - \hat{H}_{\text{in}}$$

For a system with one flux in and one flux out without any accumulation:
the mass in the system $\dot{m}_{\text{in}} = \dot{m}_{\text{out}} = \dot{m}$

$$\bar{Q} / \dot{m} = \hat{H}_{\text{out}} - \hat{H}_{\text{in}}$$

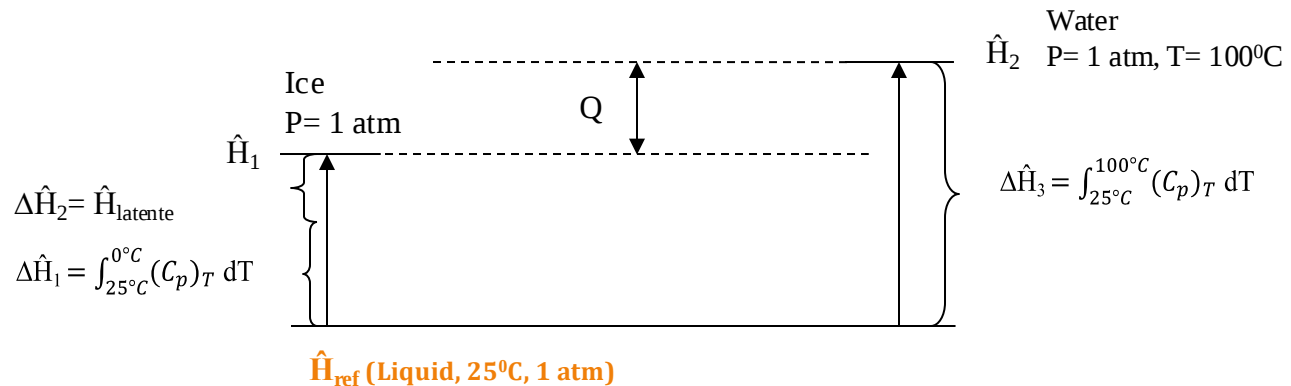
- To get the thermodynamic properties

- using the tables, for a substrate by knowing T and P, we get ($\hat{H}$, $\hat{U}$, V , $\hat{C}_p$, $\hat{C}_v$)
- given information for the reference state (P,T)

Species	$\dot{m}_{\text{in}}$ (mole/h)	$\hat{H}_{\text{in}}$ (KJ/mole)	$\dot{m}_{\text{out}}$ (mole/h)	$\hat{H}_{\text{out}}$ (KJ/mole)
H ₂ O(s)	$\dot{m}_1$	$\hat{H}_{\text{water(s)}} (\hat{H}_1)$	—	—
H ₂ O(l)	—	—	$\dot{m}_2$	$\hat{H}_{\text{water(l)}} (\hat{H}_2)$

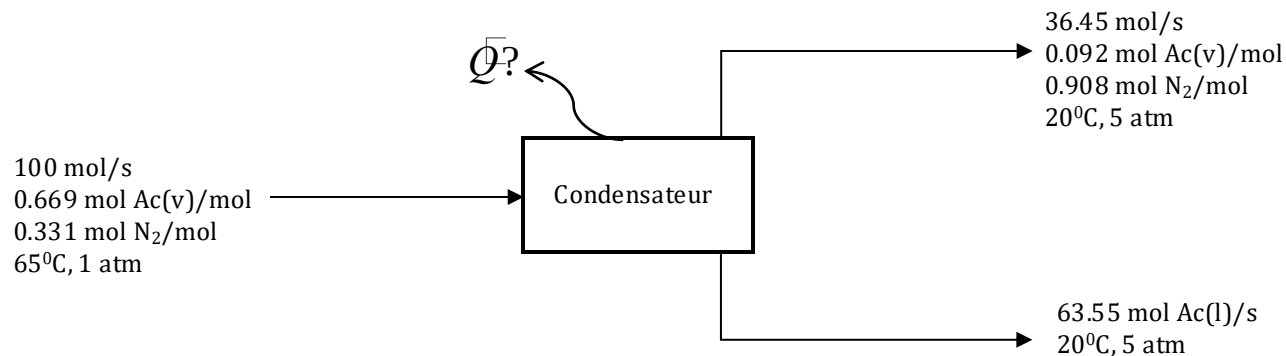
- We need a **reference state** to calculate $\hat{H}$ for the corresponding T and P

- $\hat{H}_1 = \Delta\hat{H}_1 + \Delta\hat{H}_2$
- $\hat{H}_2 = \Delta\hat{H}_3$



Example: Energy balance on a NR Open System

A mixture of Acetone and Nitrogen is entering in a cooling system (condenser) to separate the Acetone. based on the information given on the flowchart, calculate the Q needed to be removed from the system for this separation process.

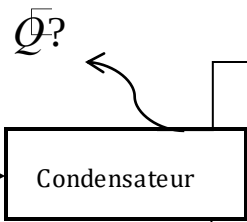


1. Mass balance : already done

2. From the general **energy balance equation** to the **simplified system energy balance equation**

$$\dot{D}H + \dot{D}E_k + \dot{D}E_p = \dot{Q} - \dot{W}_s \xrightarrow{(\Delta E_k = 0, \Delta E_p = 0, \dot{W}_s = 0)} \dot{Q} = \dot{D}H = \sum_{out} n_i \hat{H}_i - \sum_{in} n_i \hat{H}_i$$

In = 100 mol/s
 0.669 mol Ac(v)/mol
 0.331 mol N₂/mol
65°C, 1 atm



Out₁ = 36.45 mol/s
 0.092 mol Ac(v)/mol
 0.908 mol N₂/mol
20°C, 5 atm

Out₂ = 63.55 mol Ac(l)/s
20°C, 5 atm

3. Reference states (for each specie in the system):

Ac (liq, 20°C, 5atm), N₂ (gas, 25°C, 1atm)

4. Open systems → **inlet-outlet enthalpy table**

Species	$\dot{n}_{in}$ (mol/s)	$\hat{H}_{in}$ (kJ/mol)	$\dot{n}_{out}$ (mol/s)	$\hat{H}_{out}$ (kJ/mol)
Ac(v)	66.9	$\hat{H}_1$	3.35	$\hat{H}_3$
Ac(l)	—	—	63.55	0
N₂	33.1	$\hat{H}_2$	33.1	$\hat{H}_4$

All the species in
the system

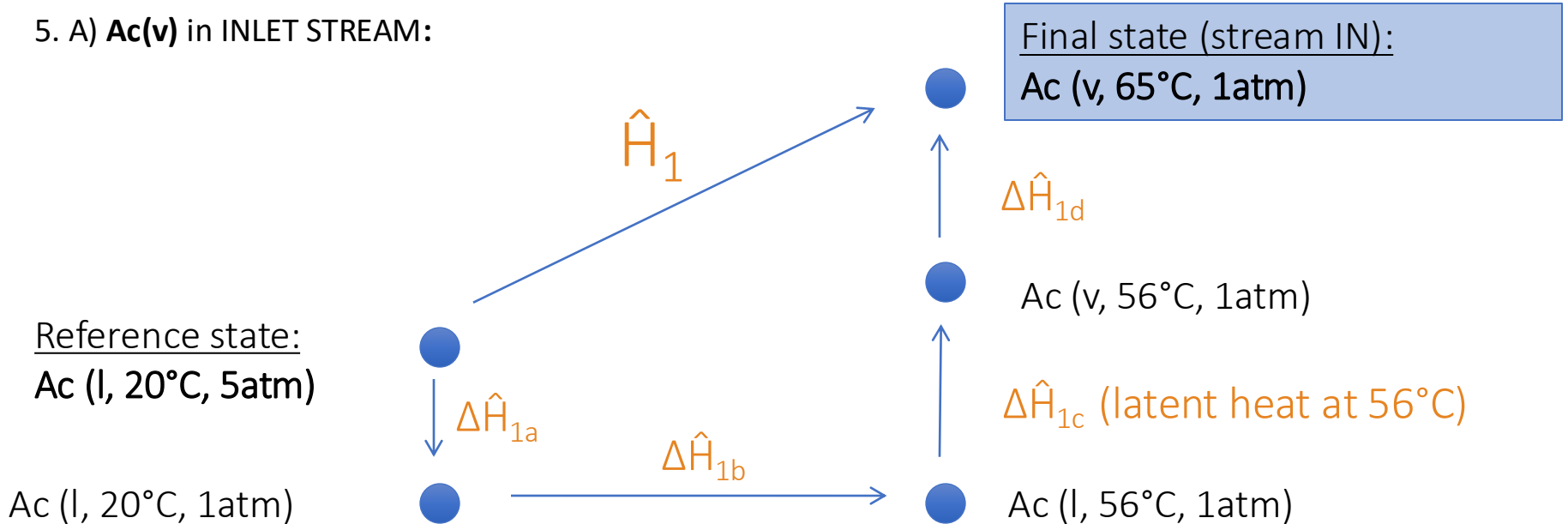
INLET stream(s):
Flowrates and specific
enthalpies*

OUTLET stream(s):
Flowrates and specific
enthalpies*

* $\hat{H}_i$ (specific enthalpy of specie i): should be calculated at the state of that specie in the inlet and outlet streams

5. Construct **process paths**: calculate the **specific enthalpies**

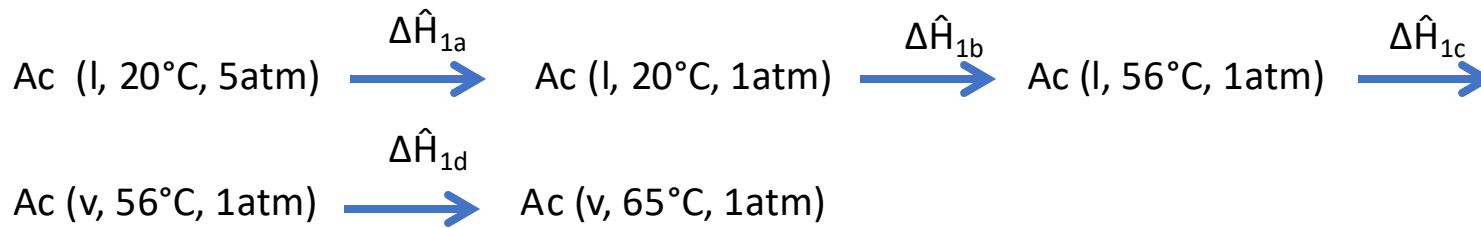
5. A) **Ac(v)** in INLET STREAM:



$$\hat{H}_1 = \Delta \hat{H} \text{ for Ac (l, 20°C, 5atm) } \rightarrow \text{Ac (v, 65°C, 1atm)}$$

$$\hat{H}_1 = \Delta \hat{H}_{1a} + \Delta \hat{H}_{1b} + \Delta \hat{H}_{1c} + \Delta \hat{H}_{1d}$$

Recalling: Enthalpy and internal energy are **state properties**. In other words, the change in enthalpy of a specie depends only on the final and initial states and not on how the final state is reached from the initial state, **they are path independent**



CHANGE IN PRESSURE AT CONSTANT TEMPERATURE (LIQUID PHASE $\rightarrow$ CONSTANT VOLUME):

$$\Delta\hat{H}_{1a} = \hat{V}\Delta P \text{ (the specific gravity of Ac is 0.791 and the MW is 0.058 kg/mol ,}$$

$$\text{so } \hat{V} = 0.0734 \text{ L/mol})$$

$$\Delta\hat{H}_{1a} = \frac{(-4 \times 10^5 \text{ Pa}) \times (0.0734 \times 10^{-3} \text{ m}^3/\text{mol})}{1000} = -0.0297 \text{ kJ/mol}$$

Pay attention to units! to find $\Delta\hat{H}_{1a}$ in KJ/mol, $\hat{V}$ should be in m^3/mol and ΔP in Pa

CHANGE IN TEMPERATURE AT CONSTANT PRESSURE (LIQUID PHASE):

$$\text{from table B.2: Ac (l) : } C_p \text{ (kJ/mol } ^\circ\text{C)} = 0.123 + 18.6 \times 10^{-5} T, \quad \text{for } T \text{ in } ^\circ\text{C}$$

$$\Delta\hat{H}_{1b} = \int_{20^\circ\text{C}}^{56^\circ\text{C}} (C_p)_{\text{Ac(l)}} dT = 4.68 \text{ kJ/mol}$$

CHANGE OF STATE (LATENT HEAT) AT CONSTANT PRESSURE AND TEMPERATURE:

$$\Delta\hat{H}_{1c} = 30.2 \text{ kJ/mol} \quad (\text{latent heat at boiling point, from Table B.1})$$

CHANGE IN TEMPERATURE AT CONSTANT PRESSURE (GAS PHASE):

$$\text{from table B.2: Ac (v) : } C_p \text{ (kJ/mol}^\circ\text{C)} = 0.07196 + 20.10 \times 10^{-5} T - 12.78 \times 10^{-8} T^2 + 34.76 \times 10^{-12} T^3$$

$$\Delta\hat{H}_{1d} = \int_{56^\circ\text{C}}^{65^\circ\text{C}} (C_p)_{\text{Ac(v)}} dT = 0.753 \text{ kJ/mol}$$

$$\hat{H}_1 = (-0.0297 + 4.68 + 30.2 + 0.753) = 35.6 \text{ kJ/mol}$$

5. A) N_2 in INLET STREAM:

$$\hat{H}_2 = \Delta \hat{H} \text{ for } \text{N}_2 (\text{g}, 25^\circ\text{C}, 1\text{atm}) \rightarrow \text{N}_2 (\text{g}, 65^\circ\text{C}, 1\text{atm})$$

CHANGE IN TEMPERATURE AT CONSTANT PRESSURE (GAS PHASE):

From Table B.2: $C_{p,\text{N}_2,\text{g}} = 0.029 + 0.2199 \times 10^{-5}T + 0.5723 \times 10^{-8}T^2 - 2.871 \times 10^{-2}T^3$

$$\hat{H}_2 = \int_{25^\circ\text{C}}^{65^\circ\text{C}} (C_p)_{\text{N}_2(\text{g})} dT = 1.16 \text{ kJ/mol}$$

5. B) $\text{Ac}(\text{v})$ in OUTLET STREAM:

CHANGE OF STATE (LATENT HEAT) AT CONSTANT PRESSURE AND TEMPERATURE:

$$\hat{H}_3 = \Delta \hat{H} \text{ for } \text{Ac} (\text{l}, 20^\circ\text{C}, 5\text{atm}) \rightarrow \text{Ac} (\text{v}, 20^\circ\text{C}, 5\text{atm})$$

$$\hat{H}_3 = 32 \text{ kJ/mol} \quad (\text{creating a path, since we only have the latent heat at the b.p.})$$

5. B) N_2 in OUTLET STREAM:

$$\hat{H}_4 = \Delta \hat{H} \text{ for } \text{N}_2 (\text{g}, 25^\circ\text{C}, 1\text{atm}) \rightarrow \text{N}_2 (\text{g}, 20^\circ\text{C}, 5\text{atm})$$

$$\hat{H}_4 = \text{N}_2 (\text{g}, 25^\circ\text{C}, 1\text{atm}) \rightarrow \text{N}_2 (\text{g}, 20^\circ\text{C}, 1\text{atm}) \rightarrow \text{N}_2 (\text{g}, 20^\circ\text{C}, 5\text{atm})$$

CHANGE IN TEMPERATURE AT CONSTANT PRESSURE (GAS PHASE):

$$\hat{H}_4 = \int_{25^\circ\text{C}}^{20^\circ\text{C}} (C_p)_{\text{N}_2(\text{g})} dT = -0.1 \text{ kJ/mol}$$

CHANGE IN PRESSURE AT CONSTANT TEMPERATURE (GAS PHASE):

For $\text{N}_2 (\text{g}, 20^\circ\text{C}, 1\text{atm}) \rightarrow \text{N}_2 (\text{g}, 20^\circ\text{C}, 5\text{atm})$ there is a very small change of enthalpy that can be neglected

6. Solve the simplified energy balance equation:

$$\dot{Q} = \dot{D}H = \sum_{out} n_i \hat{H}_i - \sum_{in} n_i \hat{H}_i$$

Species	$\dot{n}_{in}$ (mol/s)	$\hat{H}_{in}$ (kJ/mol)	$\dot{n}_{out}$ (mol/s)	$\hat{H}_{out}$ (kJ/mol)
Ac(v)	66.9	$\hat{H}_1 = 35,6$	3.35	$\hat{H}_3 = 32$
Ac(l)	—	—	63.55	0
N ₂	33.1	$\hat{H}_2 = 1,16$	33.1	$\hat{H}_4 = -0,1$

$$\begin{aligned} \Delta \dot{H} = & [(3.35) (32.0) + (63.55) (0) + (33.1) (-0.10)] \text{ kJ/s} + \dots \\ & \dots - [(66.9) (35.6) + (33.1) (1.16)] \text{ kJ/s} = -2320 \text{ kJ/s} \end{aligned}$$

$$\dot{D}H = \dot{Q} = -2320 \text{ kJ/s} = -2320 \text{ kW}$$

Thermodynamics data

- **Enthalpy and internal energy** are state properties. In other words, the change in enthalpy of a species depends only on the final and initial states and not on how the final state is reached from the initial state, **they are path independent**
- Enthalpy and internal energy of species could be tabulated with respect to a **reference state** (temperature, pressure and phase)
- There are “**tables**” at the end of the book that the thermodynamic properties can be looked up from them instead of calculating them every time
- You should get used to knowing how to **read these tables!!**

Procedure for Energy Balance Calculations

1. Make **material balance** calculations and find **flow rates** (or masses) of all streams
2. Write the generalized **energy balance equation** and cancel all the terms that are either zeros or can be neglected
3. Choose **reference states for each specie** involved. By reference state we mean **T, P and the phase** of the species. A proper choice of the reference states enables easy calculation of enthalpies and hence, energy balances
4. For **open systems**: construct an **inlet-outlet enthalpy table** with mass or molar flow rates

For **closed systems**: the table should contain **initial-final amounts of species** and **internal energies**
5. Estimate the specific enthalpies or internal energies and insert the values in the Table constructed in step 4. You need to **construct process paths to determine specific enthalpies and internal energies**
6. **Solve** the simplified **energy balance** equation (from step 2) and calculate the unknowns